

Lesson 22:

I. Inverse Dynamics Control

A. Joint Space IDC (cont'd) (SHV 9.3.1 / 7.2.1)

B. Task Space IDC (SHV 9.3.2 / 7.2.2)

II. Adaptive IDC (SHV 9.3.4 / 7.3.2)

I. Inverse Dynamics Control

A. Joint Space IDC (cont'd)

Recall: Final control for following a trajectory $q^*(t)$

$$u = M(q) a_f + C(q, \dot{q}) \dot{q} + G(q)$$

$$\uparrow$$
$$\ddot{q}^d - K_p \tilde{q} - K_d \dot{\tilde{q}}$$

$$\Rightarrow q(t) \rightarrow q^*(t) \\ t \rightarrow \infty$$

Energy Shaping: Outer loop controller could insert desired dynamics instead of tracking reference trajectory.

$$a_f := \bar{M}(q)^{-1} [v - \bar{C}(q, \dot{q}) \dot{q} - \bar{G}(q)]$$

where $\bar{M} \in \mathbb{R}^{n \times n} \Rightarrow \bar{C} \in \mathbb{R}^{n \times n}$ and $\bar{G} \in \mathbb{R}^n$ are desired dynamics terms, and v is the new input in the "shaped" dynamics

plug into
original dynamics

$$\ddot{q} = a_f \Rightarrow \bar{M} \ddot{q} + \bar{C} \dot{q} + \bar{G} = v$$

This is called "energy shaping" when choosing \bar{M} and \bar{G} to correspond to another physical system with well-defined energy terms:

$$\bar{K} = \frac{1}{2} \dot{q}^T \bar{M}(q) \dot{q}, \quad \bar{P} = \bar{P}(q) \text{ s.t. } \bar{G} = \nabla \bar{P} = \frac{\partial \bar{P}}{\partial q}$$

- Special Case: Potential energy shaping ($\bar{M}=M, \bar{C}=C$)
Results in simpler controller when plugged into inner loop.

Inner loop controller:

$$u = \cancel{M} \underbrace{\cancel{\bar{M}} [v - \cancel{\bar{C}} \dot{q} - \bar{G}]}_{a_q} + \cancel{C} \dot{q} + G$$

$$= v + G - \bar{G}$$

Plug into robot dynamics

$$\Rightarrow M \ddot{q} + C \dot{q} + \cancel{G} = u = v + \cancel{G} - \bar{G}$$

$$\Rightarrow M \ddot{q} + C \dot{q} + \bar{G} = v$$

- Note: Gravity compensation is a special case of PE shaping ($\bar{G}=0$)
- Warning: Underactuated cases are much harder
 - Matching conditions (PDE's) determine what can be shaped.
 - Limitations on achievable dynamics

B. Task-Space IDC

Same inner-loop controller ($\ddot{q} = a_q$) but consider new outer loop.

Goal: Track desired end effector pose trajectory $\Sigma^d(t)$ for some representation of workspace, e.g., $SE(3)$

Recall $\dot{\mathbf{x}} = \mathbf{J}(\mathbf{q}) \dot{\mathbf{q}}$ for manipulator Jacobian $\mathbf{J}(\mathbf{q})$

→ If $\dot{\mathbf{x}} = \mathbf{v}_{st}^b$, then $\mathbf{J}_{st}^b(\mathbf{q}) \in \mathbb{R}^{6 \times n}$

→ If $\dot{\mathbf{x}} = \mathbf{v}_{st}^s$, then $\mathbf{J}_{st}^s(\mathbf{q}) \in \mathbb{R}^{6 \times n}$

Let $n=6$ so that we have a square \mathbf{J} .

$$\dot{\mathbf{x}} = \mathbf{J}(\mathbf{q}) \dot{\mathbf{q}} \Rightarrow \ddot{\mathbf{x}} = \mathbf{J} \ddot{\mathbf{q}} + \dot{\mathbf{J}} \dot{\mathbf{q}}$$

new input, desired task space acceleration.

Given $\ddot{\mathbf{q}} = \mathbf{a}_q$, choose $\mathbf{a}_q := \mathbf{J}^{-1}(\mathbf{a}_x - \dot{\mathbf{J}} \dot{\mathbf{q}})$
(first outer-loop controller)

$$\Rightarrow \ddot{\mathbf{q}} = \mathbf{J}^{-1}(\mathbf{a}_x - \dot{\mathbf{J}} \dot{\mathbf{q}}) \Rightarrow \mathbf{J} \ddot{\mathbf{q}} + \dot{\mathbf{J}} \dot{\mathbf{q}} = \mathbf{a}_x$$

$$\Rightarrow \ddot{\mathbf{x}} = \mathbf{a}_x \leftarrow \text{new input for end-effector accel.}$$

Define 2nd outer-loop control law to insert linear dynamics:

$$\mathbf{a}_x := \ddot{\mathbf{x}}^d - \underbrace{K_p(\mathbf{x} - \mathbf{x}^d)}_{\tilde{\mathbf{x}}} - \underbrace{K_d(\dot{\mathbf{x}} - \dot{\mathbf{x}}^d)}_{\dot{\tilde{\mathbf{x}}}}$$

$$\Rightarrow \ddot{\tilde{\mathbf{x}}} + K_d \dot{\tilde{\mathbf{x}}} + K_p \tilde{\mathbf{x}} = 0 \quad (\text{closed-loop task error dynamics})$$

Choose $K_p, K_d > 0$ then $(\tilde{\mathbf{x}}, \dot{\tilde{\mathbf{x}}}) \xrightarrow[\text{fast}]{\text{exp}} (0, 0)$

exponentially stable $\Rightarrow \mathbf{x} \rightarrow \mathbf{x}^d(t)$

Benefit: No need for inverse kinematics in real-time.

Limitations:

- Must avoid singularities to maintain invertibility of J in a a_g control law.
- We considered square $J \in \mathbb{R}^{n \times n}$
 - 6-DOF robot for $WCSE(3)$
 - 3-DOF " " $WCSE(2)$
 - 3-DOF " " $WCSE(3)$
- For non-square J , can use pseudo-inverse in some cases.

II. Adaptive Control

Problem: Model uncertainty (e.g., parametric uncertainty)
Unmodeled dynamics (e.g., actuator)

Recall IDC input: $u = \hat{M}(q) a_g + \hat{C}(q, \dot{q}) \dot{q} + \hat{G}(q)$

where $\hat{(\cdot)}$ is a model estimate and

$\tilde{(\cdot)} = \hat{(\cdot)} - (\cdot)$ is model error

Two classical ways of dealing with model uncertainty

- Robust Control: enables bounded tracking by defining certain bounds on model error.
 - Requires many parameters to be identified for these bounds.
 - Covered in SHV 9.3.3 / 7.3.1

- Adaptive Inverse Dynamics Control:

Deals with parametric uncertainty

Recall "linearity in the parameters"

$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = Y(q, \dot{q}, \ddot{q}) \Theta$$

regressor matrix parameter vector

We will vary parameters in $\hat{M}, \hat{C}, \hat{G}$ over time (adapt)

We want to find $\hat{\Theta}$ st. $Y(q, \dot{q}, \ddot{q}) \hat{\Theta} = Y(q, \dot{q}, \ddot{q}) \Theta$

↑
(parameter estimate)

$$M\ddot{q} + C\dot{q} + G = u := \hat{M}a_q + \hat{C}\dot{q} + \hat{G} \quad \text{--- } (*)$$

$$\Rightarrow \ddot{q} = M^{-1}(\hat{M}a_q + \tilde{C}\dot{q} + \tilde{G}) \quad \text{recall } \hat{M} = \tilde{M} + M$$

$$= a_q + M^{-1}(\tilde{M}a_q + \tilde{C}\dot{q} + \tilde{G})$$

Plug in $a_q = \ddot{q}^d(t) - K_d\dot{\tilde{q}} - K_p\tilde{q}$, where $\tilde{q} = q - q^d$

Simplify (ex. 9-11 in SHV)

\Rightarrow closed-loop

$$\ddot{\tilde{q}} + K_d\dot{\tilde{q}} + K_p\tilde{q} = \hat{M}^{-1} Y(q, \dot{q}, \ddot{q}) \tilde{\Theta}$$

where $\tilde{\Theta} = \hat{\Theta} - \Theta$ is parametric error vector.

Let $e = \begin{bmatrix} \tilde{q} \\ \dot{\tilde{q}} \end{bmatrix}$ be tracking error state vector

$$A = \begin{bmatrix} 0 & I \\ -K_p & -K_d \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ I \end{bmatrix}$$

designed Hurwitz by choice of $K_p, K_d > 0$

(all e-values are in LHS of complex plane,
i.e. all e-values have negative real part)

$$\begin{aligned} \Rightarrow \dot{e} &= A e + B \hat{M}^{-1} \Upsilon(q, \dot{q}, \ddot{q}) \tilde{\Theta} \\ &= A e + B \Phi \tilde{\Theta} \quad \text{where} \quad \Phi := \hat{M}^{-1} \Upsilon(q, \dot{q}, \ddot{q}) \end{aligned}$$

To be continued!...