

Lesson 14:

- I. Manipulator Jacobians (cont'd) (MLS 3.4)
 - II. Singularities (MLS 3.4.3)
 - III. Manipulability (MLS 3.4.4)
 - IV. Wrenches & Joint torques (MLS 3.4.2)
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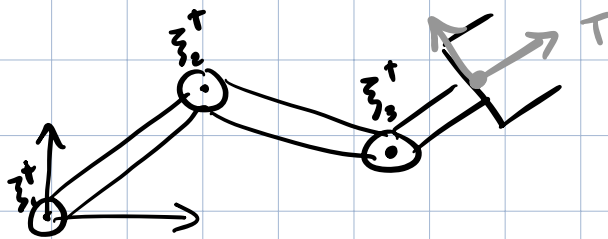
I. Manipulator Jacobians (cont'd)

Recall: Body manipulator Jacobian J_{st}^b satisfies

$$V_{st}^b = J_{st}^b(\theta) \dot{\theta}, \text{ where } J_{st}^b(\theta) = [\xi_1^+, \xi_2^+, \dots, \xi_n^+]$$

$$\xi_i^+ = \text{Ad}_{(e^1 \dots e^n g_{st}(\theta))}^{-1} \xi_i$$

- Columns ξ_i^+ correspond to joint twist coords w.r.t. current config of the tool frame.



- Derived in similar manner to the spatial case from

$$\hat{V}_{st}^b = g_{st}^{-1}(\theta) \dot{g}_{st}(\theta)$$

- Can relate body & spatial Jacobians by

$$J_{st}^s(\theta) = \text{Ad}_{g_{st}(\theta)} J_{st}^b(\theta)$$

- Can use the body or spatial Jacobian to compute the inst. velocity of a point, specifically attached to end effector

$$\bar{V}_q^b = \hat{V}_{st}^b \bar{q}_b = (J_{st}^b(\theta) \dot{\theta})^\wedge \bar{q}_b \quad (\text{in body/tool coords})$$

$$\bar{V}_q^s = \hat{V}_{st}^s \bar{q}_s = (J_{st}^s(\theta) \dot{\theta})^\wedge \bar{q}_s \quad (\text{in spatial coords})$$

Control implications:

- Can use the manipulator Jacobian to move a robot from one end-effector config. to another without calculating inv. kinematics explicitly.

- If J_{st} is square (e.g. 6-DOF in $WC \subset SE(3)$) and invertible, then

$$\dot{\theta}(t) = (J_{st}^s(\theta(t)))^{-1} V_{st}^s(t) \quad \leftarrow \text{desired velocity profile}$$

$$= (J_{st}^b(\theta(t)))^{-1} V_{st}^b(t) \quad \leftarrow \text{note: or body coords by reverse order}$$

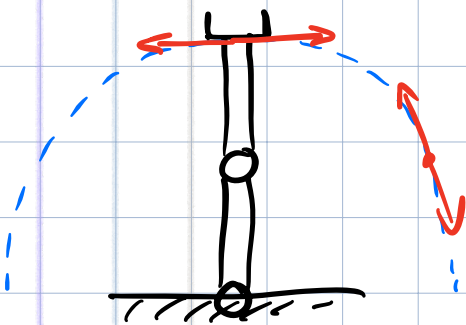
- Calculate $\hat{V}_{st}^s(t) = \dot{g}_{st}(t) g_{st}^{-1}(t)$ from a desired workspace path $g_{st}(t)$ from $g_{st}(0)$ to $g_{st}(T)$
- Robot controls desired $\dot{\theta}(t)$

II. Singularities

Def: A singular config. is a robot config. at which the manipulator Jacobian J_{st} drops rank.

- For square J_{st} , $\det(J_{st}) = 0$ at rank drop.
- Singularity means the robot is unable to achieve inst. motion in at least one direction of the workspace.
 - When approaching singular config. increasingly faster joint velocities are required for increasingly smaller end effector velocities.
 - Avoid singularities when controlling via end effector velocity.

Ex: For planar 2-DoF arm where $W \subset \mathbb{R}^2$



the boundary of the workspace is a set of singular configs.

Ex: Honda ASIMO

What happens when J_{st} is not square?

For n -DOF robot, $J_{st} \in \mathbb{R}^{\dim W \times n}$, where $\dim W \leq 6$,
if $n \neq \dim W$ then J_{st} is not square!

Case 1: ($n < \dim W$)

The end effector starts with fewer DOFs than workspace, and loses workspace DOFs at singular configurations.

\Rightarrow Cannot invert Jacobian for full workspace
(can work w/ a lower-dimensional workspace)

Case 2: ($n > \dim W$)

This is a redundant manipulator.

Has "internal" DOFs to avoid $\text{rank}(J_{st})$ dropping.

How do you "invert" J_{st} in this case?

Use pseudo-inverse to calculate (non-unique) joint velocities for a desired V_{st} :

$$\dot{\Theta} = J_{st}^T \left(\underbrace{J_{st} J_{st}^T}_{\dim W \times \dim W} \right)^{-1} V_{st}$$

$\dim W \times \dim W \rightarrow$ Invertibility requires $\text{rank}(J_{st}) = \dim W$

or

$$\dot{\Theta} = A J_{st}^T (J_{st} A J_{st}^T)^{-1} V_{st}, \text{ for weighting matrix } A \in \mathbb{R}^{n \times n} \\ A > 0$$

III. Manipulability

Recall workspace $W = \{g_{st}(\theta) \mid \theta \in Q\} \subset SE(3)$

note: "reachable workspace" and "dexterous workspace"
(just positions) (all positions where you can freely orient the end effector)

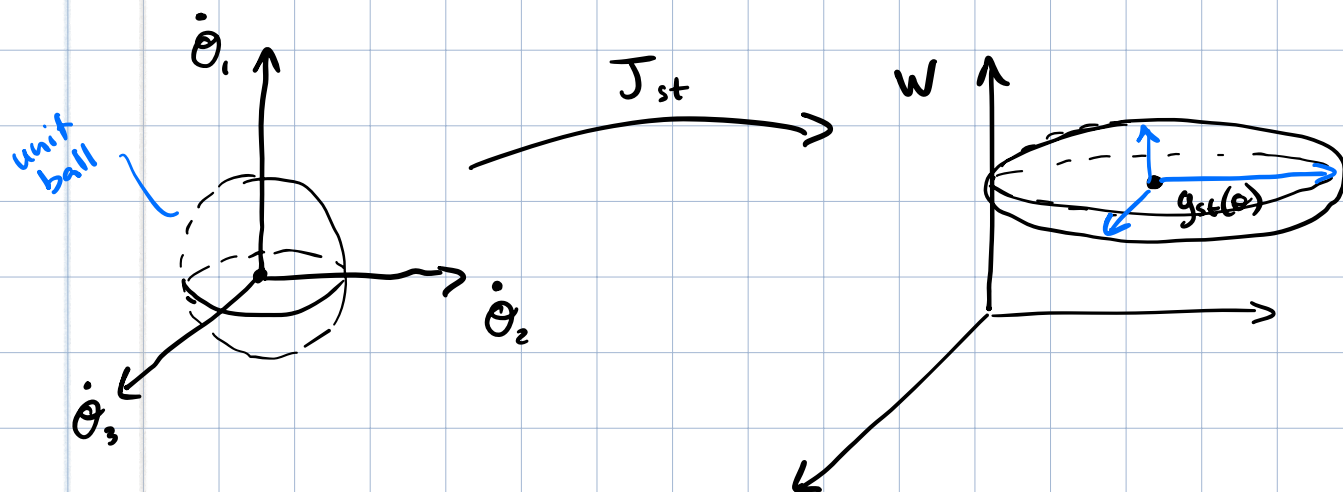
Manipulability describes robot's ability to move freely in all directions of the workspace.

- Local property characterized by the manipulator Jacobian, relating inf. joint motions to inf. workspace motions.
- Manipulability determined by singular values of J_{st}
 - For square J_{st} , can define as

$$\mu(\theta) := \det(J_{st}(\theta)) = \prod_{i=1}^n \lambda_i(J_{st}(\theta))$$

← product of

- Measures the volume of velocity ellipsoid in workspace generated by unit joint velocity vectors:



- Principal axes of ellipsoid correspond to eigenvectors of J_{st}
- Magnitude of principal axes correspond to eigenvalues of J_{st}