

國立臺灣大學理學院應用物理研究所

碩士論文

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College of Science

National Taiwan University

Master Thesis

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張阿茲

A-Z Chang

指導教授：陳 OO 博士

Advisor: O-O Chen, Ph.D.

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國立臺灣大學  
應用物理研究所

碩士論文

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張阿茲  
撰

國立臺灣大學（碩）博士學位論文  
口試委員會審定書

論文中文題目

論文英文題目

本論文係○○○君（○學號○）在國立臺灣大學○○學系、所完成之碩（博）士學位論文，於民國○○年○○月○○日承下列考試委員審查通過及口試及格，特此證明

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# 致謝

這裡將簡單介紹如何利用  $\text{\LaTeX}$  來編輯你的畢業論文，若不知道  $\text{\LaTeX}$  是什麼或是沒有概念的話，建議你可以簡單看過放在此資料夾裡的[李果正-大家來學  \$\text{\LaTeX}\$](#) 前四章內容，在下載適合的  $\text{\LaTeX}$  整合發行套件之後（請看第 III.項），可以嘗試用剛安裝好的  $\text{\LaTeX}$  編輯器來編譯[thesis.tex](#)這份文件，編譯的方法可以看下面第 V.項的介紹，若編譯成功，所編譯出來的 thesis.pdf 文件的應該會跟此 demo.pdf 文件一模一樣，而且沒有任何問號符號，走到這一步的話，就差不多可以開始邊學習  $\text{\LaTeX}$  邊編輯你的畢業論文了！基本上會使用到的指令都包含在論文的各章節裡，怎麼在論文裡寫公式或是放圖之類的就自行看 tex 檔學吧。如果有任何問題或建議可以來信與我討論，我的信箱是[dran31545@gmail.com](mailto:dran31545@gmail.com)，或是到此範本[Google Project](#)裡面的[Issues](#)貼上你的問題與建議，我會盡我所能更新此範本，也歡迎大家自行重製、改良此範本並散布給他人，祝大家順利畢業！

要編輯致謝請打開[acknowledgementsCH.tex](#)

## I. 此範本參考並修改自下列網站的資料：

- [如何用  \$\text{\LaTeX}\$  排版臺灣大學碩士論文](#)  
—台灣大學論文  $\text{\LaTeX}$  樣版原創者[黃子桓](#)的教學網頁
- [\$\text{\LaTeX}\$  常用語法及論文範本](#)  
—[Hitripod](#)所修改的範本，這裡參考了許多他所寫的格式和內容
- [使用  \$\text{\LaTeX}\$  做出精美的論文](#)
- [XeTeX：解決  \$\text{\LaTeX}\$  惱人的中文字型問題](#)
- [台灣大學碩士、博士論文的  \$\text{\LaTeX}\$  模板](#)

## II. 幾個有用的參考資料及網路資源：

- [李果正-大家來學  \$\text{\LaTeX}\$](#) —建議先看完前四章
- [WIKIBOOKS- \$\text{\LaTeX}\$](#) —好用的線上工具書
- [Working with a .bib file using JabRef](#)
- [Using BibDesk - A short tutorial](#)
- [\$\text{\LaTeX}\$  for Physicists](#)

III. 下載 L<sup>A</sup>T<sub>E</sub>X 整合發行套件，可參考 [TeX Collection](#)：

1. [MacTeX](#): For **MacOSX**，下載 [MacTeX.pkg](#)
2. [ProTeXt](#): For **Windows**，下載 [ISO file](#)
3. [TeX Live](#): For **GNU/Linux** and **MacOSX**, and **Windows**，下載 [ISO file](#)
4. [CTAN](#): The Comprehensive TeX Archive Network.

IV. 好用的程式：

- 文獻管理系統：

1. [JabRef](#)

可參考 [Working with a .bib file using JabRef](#) 或是 [Google](#) 及 [YouTube](#)

2. [BibDesk](#) (For Mac)

可參考 [Using BibDesk - A short tutorial](#) 或是 [Google](#) 及 [YouTube](#)

- 方程式編輯器：[Daum Equation Editor](#) (Chrome App，必須使用 Google 瀏覽器)

V. 編譯流程：

1. `xelatex thesis`

對 `thesis.tex` 進行第一次 XeLaTeX 編譯，產生 `thesis.pdf` 以其他檔案

2. `bibtex thesis`

對 `thesis.tex` 進行 BibTeX 編譯，產生 `bbl` 檔以及 `blg` 檔

3. `xelatex thesis`

對 `thesis.tex` 進行第二次 XeLaTeX 編譯，產生目錄、圖表連結及參考文獻

4. `xelatex thesis`

對 `thesis.tex` 進行第三次 XeLaTeX 編譯，產生參考文獻連結，完成編譯

**注意！**此範本使用 `cite` 套件，可依據你利用文獻管理系統所整理好的 [thesisbib.bib](#) 檔在論文最後產生參考文獻頁面，若你的系所規定要在每個章節的後面產生參考文獻，則可以用 `chapterbib` 套件，來對每個有附參考文獻的章節 `tex` 檔進行一次 BibTeX 編譯產生 `bbl` 檔，如範例的 [introduction.tex](#)、[THM.tex](#) 和 [EXP.tex](#)，如果有這需要請把 [thesis.tex](#) 檔裡使用 `cite` 套件的指令利用註解符號 `%` 來取消使用 `cite` 套件，並刪去出現在使用 `chapterbib` 套件指令前面的註解符號 `%` 來啟動使用 `chapterbib` 套件

```
\usepackage{cite}
%\usepackage{chapterbib}
```

改成

```
%\usepackage{cite}  
\usepackage{chapterbib}
```

再來利用註解符號% 取消會把參考文獻放在論文最後的指令

```
\bibliographystyle{unsrt}  
\addcontentsline{toc}{chapter}{\bibname}  
\bibliography{thesisbib}
```

改成

```
%\bibliographystyle{unsrt}  
%\addcontentsline{toc}{chapter}{\bibname}  
%\bibliography{thesisbib}
```

再把用來輸入章節檔案的\input 指令改成\include 指令

```
\input{introduction}  =>  \include{introduction}  
\input{THM}           =>  \include{THM}  
\input{EXP}           =>  \include{EXP}
```

最後記得在每個有附參考文獻的章節加上產生參考文獻的指令，即在[introduction.tex](#)、[THM.tex](#)和[EXP.tex](#)三個檔案裡最後啟動下面兩行指令

```
%\bibliographystyle{unsrt} => \bibliographystyle{unsrt}  
%\bibliography{thesisbib}  => \bibliography{thesisbib}
```

而編譯時則需要對有附參考文獻的[introduction.tex](#)、[THM.tex](#)和[EXP.tex](#)各做一次 BibTeX 編譯，編譯流程如下

1. xelatex thesis  
對 thesis.tex 進行第一次 XeLaTeX 編譯，產生 thesis.pdf 及其他檔案
2. bibtex introduction  
對 introduction.tex 進行 BibTeX 編譯，產生 bbl 檔以及 blg 檔
3. bibtex THM  
對 THM.tex 進行 BibTeX 編譯，產生 bbl 檔以及 blg 檔
4. bibtex EXP  
對 EXP.tex 進行 BibTeX 編譯，產生 bbl 檔以及 blg 檔
5. xelatex thesis  
對 thesis.tex 進行第二次 XeLaTeX 編譯，產生目錄、圖表連結及參考文獻

## 6. xelatex thesis

對 thesis.tex 進行第三次 XeLaTeX 編譯，產生參考文獻連結，完成編譯

## VI. 補充說明與注意事項：

- 口試委員會審定書：

請到台大圖書館網頁的[電子論文服務](#)下載論文格式範本，並修改成正確的格式，也可到此範本所在資料夾的[cert.doc](#)修改。當然你也可以利用 LaTeX 來編輯，你只要填好[ntuvars.tex](#)檔的資料，並去除在 thesis.tex 裡下面這行的註解符號%

```
%\makecertification
```

編譯完後就可以產生審定書格式。口試通過後，請把已經簽名的審定書掃描成 pdf 檔，再取代原本的[cert.pdf](#)，即可放上已簽名的審定書。處理審定書出現的指令在 thesis.tex 裡

```
%----- generate the certification ...
%\makecertification
%----- includepdf by using package ...
\addcontentsline{toc}{chapter}{口試委員會審定書}
\includepdf[pages={1}]{cert.pdf}
```

- 浮水印：

資料夾已經附上浮水印檔案了，若學校有更改，到請到台大圖書館網頁的[電子論文服務](#)下載pdf 格式的浮水印到此範本所在資料夾。若要開啟關閉浮水印功能，即自行刪去或加上下面位於 thesis.tex 指令的註解符號%

```
%\CenterWallPaper{0.365}{watermark.pdf}
```

- 單面印刷與雙面印刷：

此範本為單面印刷，若論文頁數超過 80 頁，依規定需要用雙面印刷，此時只需把 thesis.tex 裡的

```
\documentclass[a4paper, 12pt, oneside]{book}
```

改成

```
\documentclass[a4paper, 12pt, twoside]{book}
```

- XeTeX：

此範本中文字體使用 XeTeX 轉換，細節請參考[Hitripod](#)寫的[XeTeX：解決 LaTeX 惱人的中文字型問題](#)。

# 中文摘要

請打開並編輯[abstractCH.tex](#)

關鍵字：壹、貳、參、肆、伍、陸、柒



# Abstract

This thesis is constructed by 3 parts. In the first part, I introduce an algorithm to calculate the highest degree of fault tolerance a system can achieve with the control of a safety critical systems. Which can be reduced to solving a game between a malicious environment and a controller. During the game play, the environment tries to break the system through injecting failures while the controller tries to keep the system safe by making correct decisions. I found a new control objective which offers a better balance between complexity and precision for such systems: we seek systems that are  $k$ -resilient. A system is  $k$ -resilient means it is able to rapidly recover from a sequence of small number, up to  $k$ , of local faults infinitely many times if the blocks of up to  $k$  faults are separated by short recovery periods in which no fault occurs.  $k$ -resilience is a simple abstraction from the precise distribution of local faults, but I believe it is much more refined than the traditional objective to maximize the number of local faults. I will provide detail argument of why this is the right level of abstraction for safety critical systems when local faults are few and far between. I have proved, with respect to resilience, the computational complexity of constructing optimal control is low. And a demonstration of the feasibility through an implementation and experimental results will be in following chapters. The second part is to create an logic which can describe the different purposes of each player such as environment, controller, user, and etc in a system. I propose an extension to ATL (alternating-time logic), called BSIL(basic strategy-interaction logic), for the specification of strate-

gies interaction of players in a system. BSIL is able to describe one system strategy that can cooperate with several strategies of the environment for different requirements. Such properties are important in practice and I show that such properties are not expressible in  $ATL^*$ , GL (game logic), and AMC (alternating  $\mu$ -calculus). Specifically, BSIL is more expressive than ATL but incomparable with  $ATL^*$ , GL, and AMC in expressiveness. I show that, for fulfilling a specification in BSIL, a memoryful strategy is necessary. I also show that the model-checking complexity of BSIL is PSPACE-complete and is of lower complexity than those of  $ATL^*$ , GL, AMC, and the general strategy logics. Which may imply that BSIL can be useful in closing the gap between large scale real-world projects and the time consuming game-theoretical results. I then show the feasibility of our techniques by implementation and experiment with our PSPACE model-checking algorithm for BSIL. The final part is an extension to BSIL called temporal cooperation logic(TCL). TCL allows successive definition of strategies for agents and agencies. Like BSIL the expressiveness of TCL is still incomparable with  $ATL^*$ , GL and AMC. However, it can describe deterministic Nash equilibria while BSIL cannot. I prove that the model checking complexity of TCL is EXPTIME-complete. TCL enjoys this relatively cheap complexity by disallowing a too close entanglement between cooperation and competition while allowing such entanglement leads to a non-elementary complexity. I have implemented a model-checker for TCL and shown the feasibility of model checking in the experiment on some benchmarks.

Key words:

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# Chapter 1

## Get started with L<sup>A</sup>T<sub>E</sub>X

Two common font styles in this text:

- **Item1:** *Italic*
- **Item2:** **Bold**

About the advance latex grammer see the next section 1.1.

### 1.1 L<sup>A</sup>T<sub>E</sub>X Adadvanced Features

The following features would be introduced in the coming subsections:

- SubSection 1.1.1: **Figure**
- SubSection 1.1.3: **Verb**
- SubSection 1.1.3: **Verb**
- SubSection 1.1.4: **Enumeration**
- SubSection 1.1.2: **Table**
- SubSection 1.1.5: **Code Display**
- SubSection 1.1.6: **Math**
- SubSection 1.1.7: **Algorithms**

### 1.1.1 Figure



Figure 1.1: A picture of a tiger.

Figure 1.1 is a picture of a tiger.

### 1.1.2 Table

[Table examples on WIKIBOOKS.](#)

Table 1.1: Table Example 1		
Start	End	Character Block Name
3400	4DB5	CJK Unified Ideographs Ex- tension A
4E00	9FFF	CJK Unified Ideographs

Table 1.2: Table Example 2		
Item		
Animal	Description	Price (\$)
Gnat	per gram	13.65
	each	0.01
Gnu	stuffed	92.50
Emu	stuffed	33.33
Armadillo	frozen	8.99



Table 1.3: Table Example 3

Allocation	Allocation, Element, Type, Script
<b>Data Types</b>	Byte2, Byte3, and Byte4 Float2, Float3, Float4 Int2, Int3, Int4 Long2, Long3, Long4 Matrix2f, Matrix3f, Matrix4f Short2, Short3, Short4
<b>Graphics</b>	Mesh ProgramFragment, ProgramRaster ProgramStore, ProgramVertex RSSurfaceView

Table 1.4: Table Example 4

Team sheet		
Goalkeeper	GK	Paul Robinson
Defenders	LB	Lucas Radebe
	DC	Michael Duberry
	DC	Dominic Matteo
	RB	Didier Domi
Midfielders	MC	David Batty
	MC	Eirik Bakke
	MC	Jody Morris
Forward	FW	Jamie McMaster
Strikers	ST	Alan Smith
	ST	Mark Viduka

Table 1.5: Table Example 5

Team	P	W	D	L	F	A	Pts
Manchester United	6	4	0	2	10	5	12
Celtic	6	3	0	3	8	9	9
Benfica	6	2	1	3	7	8	7
FC Copenhagen	6	2	1	2	5	8	7

### 1.1.3 Verb

Let's take a overview on how to type special characters:

<FRAMEWORKS\_BASE>/graphics/java/android/renderscript

<sup>1</sup> You could also go back to the beginning of the chapter by the **hyperref**.

### 1.1.4 Enumeration

1. Enumerated Item1
2. Enumerated Item2
3. Enumerated Item3

### 1.1.5 Code Display

Here is a "Hello, DanDing." example:

```
void main(int argc, char **argv)
{
    printf("  _> ` ");
}
```

Another example with line numbers:

```
1 void main(int argc, char **argv)
2 {
3     printf("  _> ` ");
4 }
```

Matlab example:

```
1 function y = demo(x) % This is a comment.
2     str = 'hello there';
3     y = x + 1;
4 end
```

---

<sup>1</sup>Path of <APP\_intermediates>: <ANDROID\_ROOT>/ out/ target/ common/ obj/ APPS/ APP-NAME\_intermediates/

### 1.1.6 Math

- Inline mode:

The solution to  $\sqrt{x} = 5$  is  $x = 25$ .

- Display mode:

The solution to

$$\sqrt{x} = 5$$

is

$$x = 25.$$

- Numbered mode:

$$2 + 2 = 4 \tag{1.1}$$

- Non-numbered:

$$2 + 2 = 4$$

- Aligning:

$$\begin{aligned} 2x^2 + 3(x-1)(x-2) &= 2x^2 + 3(x^2 - 3x + 2) \\ &= 2x^2 + 3x^2 - 9x + 6 \\ &= 5x^2 - 9x + 6 \end{aligned}$$

- Fractions:

$$\frac{n!}{k!(n-k)!} = \binom{n}{k}$$

- Matrix:

$$A_{m,n} = \begin{pmatrix} a_{1,1} & a_{1,2} & \cdots & a_{1,n} \\ a_{2,1} & a_{2,2} & \cdots & a_{2,n} \\ \vdots & \vdots & \ddots & \vdots \\ a_{m,1} & a_{m,2} & \cdots & a_{m,n} \end{pmatrix}$$

[More examples on WIKIBOOKS.](#)

### 1.1.7 Algorithms

---

**Algorithm 1** Calculate  $y = x^n$

---

**Require:**  $n \geq 0 \vee x \neq 0$

**Ensure:**  $y = x^n$

$y \leftarrow 1$

**if**  $n < 0$  **then**

$X \leftarrow 1/x$

$N \leftarrow -n$

**else**

$X \leftarrow x$

$N \leftarrow n$

**end if**

**while**  $N \neq 0$  **do**

**if**  $N$  is even **then**

$X \leftarrow X \times X$

$N \leftarrow N/2$

**else** [ $N$  is odd]

$y \leftarrow y \times X$

$N \leftarrow N - 1$

**end if**

**end while**

---

[More examples on WIKIBOOKS.](#)

## **Chapter 2**

### **Introduction**

The organization of this thesis is as follows. In chapter 3, the theoretical background and definition of surface plasmon will be included [?]. Chapter 4 contains description of experiment methods such as atomic force microscopy and scanning electron microscopy.

## Chapter 3

# Theory of surface plasmon polaritons in metallic nano-structures

### 3.1 Definition of plasmon

Plasmon is collective oscillation of conduction electron gas, a quasi-particle resulting from the quantization of plasma oscillations just like phonons are quantizations of mechanical vibrations. The simplest case is the volume plasmon as shown in Figure 3.1. We

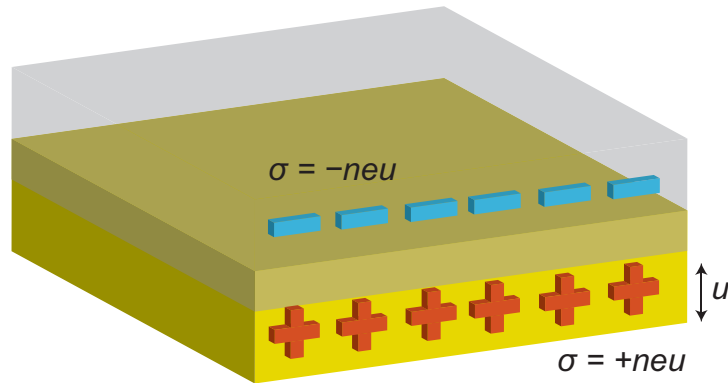


Figure 3.1: Longitudinal collective oscillations of the conduction electrons of a metal (Volume plasmons)

can derive plasma frequency  $\omega_p$  from the simple harmonics oscillation model, a collective displacement of the electron cloud by a distance  $u$  leads to a surface charge density  $\sigma = \pm neu$  at the slab boundaries. This establishes a homogeneous electric field  $\mathbf{E} = \frac{neu}{\epsilon_0}$  inside the slab. Thus, the displaced electrons experience a restoring force, and their move-

ment can be described by the equation of motion  $nm\ddot{u} = -ne\mathbf{E}$ . Inserting the expression for the electric field, this leads to

$$nm\ddot{u} = -\frac{n^2e^2u}{\varepsilon_0} \quad (3.1a)$$

$$\ddot{u} + \omega_p^2 u = 0. \quad (3.1b)$$

The plasma frequency  $\omega_p = \sqrt{\frac{ne^2}{\varepsilon_0 m}}$  can thus be recognized as the natural frequency of a free oscillation of the electron sea. The quanta of these charge oscillations are called plasmons. Due to the longitudinal nature of the excitation, volume plasmons do not couple to transverse electromagnetic waves, and can only be excited by particle impact. We can derive the dispersion relation of the generalization of volume plasmons, traveling plasma waves, from curl electric field equations (Equations 3.2a)

$$\nabla \times \nabla \times \mathbf{E} = -\mu_0 \frac{\partial^2 \mathbf{D}}{\partial t^2} \quad (3.2a)$$

$$\mathbf{K}(\mathbf{K} \cdot \mathbf{E} - K^2 \mathbf{E}) = -\varepsilon(\mathbf{K}, \omega) \frac{\omega^2}{c^2} \mathbf{E} \quad (3.2b)$$

and plasma model, and a simple equation of motion for an electron of the plasma subjected to an external electric field  $\mathbf{E}$

$$m\ddot{\mathbf{x}} + m\gamma\dot{\mathbf{x}} = -e\mathbf{E}. \quad (3.3)$$

Assuming a harmonic time dependence  $\mathbf{E}(t) = \mathbf{E}_0 e^{-i\omega t}$  of the driving field, a particular solution of this equation describing the oscillation of the electron is  $\mathbf{x}(t) = \mathbf{x}_0 e^{-i\omega t}$ . The complex amplitude  $\mathbf{x}_0$  incorporates any phase shifts between driving field and response via

$$\mathbf{x}(t) = \frac{e}{m(\omega^2 + i\gamma\omega)} \mathbf{E}(t). \quad (3.4)$$

The displaced electrons contribute to the macroscopic polarization

$$\mathbf{P} = -\frac{ne^2}{m(\omega^2 + i\gamma\omega)} \mathbf{E}(t). \quad (3.5)$$

Inserting  $\mathbf{P}$  into dielectric displacement field equation  $\mathbf{D} = \varepsilon_0 \mathbf{E} + \mathbf{P}$  yields

$$\mathbf{D} = \varepsilon_0 \left(1 - \frac{\omega_p^2}{\omega^2 + i\gamma\omega}\right) \mathbf{E}, \quad (3.6)$$

where  $\omega_p^2 = \frac{ne^2}{\varepsilon_0 m}$ . Therefore, the dielectric function of the free electron gas

$$\varepsilon(\omega) = 1 - \frac{\omega_p^2}{\omega^2 + i\gamma\omega}. \quad (3.7)$$

We arrive at the desired result by using equation 3.7 and the generic dispersion relation  $K^2 = \varepsilon(\mathbf{K}, \omega) \frac{\omega^2}{c^2}$ , the dispersion relation of traveling waves becomes

$$\omega^2 = \omega_p^2 + \mathbf{K}^2 c^2. \quad (3.8)$$

From this relation, we can figure out the oscillation properties in any frequency of external field. Note that this branch can not confine the electromagnetic waves, it would radiate out the energy, so this mode is also called radiative surface plasmon.

## 3.2 Surface plasmon polaritons at interface between dielectric and metal

Surface plasmon polaritons (SPPs) are eigenmodes of transverse magnetic (TM) waves, which coupling the electromagnetic fields to oscillations of the conductor's electron plasma, propagate at a interface between dielectric and metal, and are confined in perpendicular direction. Providing a flat interface between dielectric and metal half-spaces with dielectric constants  $\varepsilon_d$  and  $\varepsilon_m$ , respectively, and assuming the interface normal to  $z$  direction and the SPPs propagate along the  $x$  direction, the SPP wave vector  $\beta$  is related to the frequency  $\omega$  through the dispersion relation

$$\beta = k_0 \sqrt{\frac{\varepsilon_d \varepsilon_m}{\varepsilon_d + \varepsilon_m}}, \quad (3.9)$$



where  $k_0 = \omega/c$  is the free-space wave vector. We take  $\omega$  to be real and allow  $\beta$  to be complex.

The optical response of metals is often described by the Drude model for a free-electron gas [?],

$$\varepsilon_{Drude}(\omega) = 1 - \frac{\omega_p^2}{\omega^2 + i\Gamma\omega}, \quad (3.10)$$

in which  $\Gamma$  is a damping rate due to electron-electron and electron-phonon scattering. Figure 3.2 shows the dispersion curve 3.9 with Drude metal in the absence of losses ( $\Gamma = 0$ ) for air ( $\varepsilon_d = 1$ ) and fused silica ( $\varepsilon_d = 2.25$ ) interface. For small wave vectors SPPs

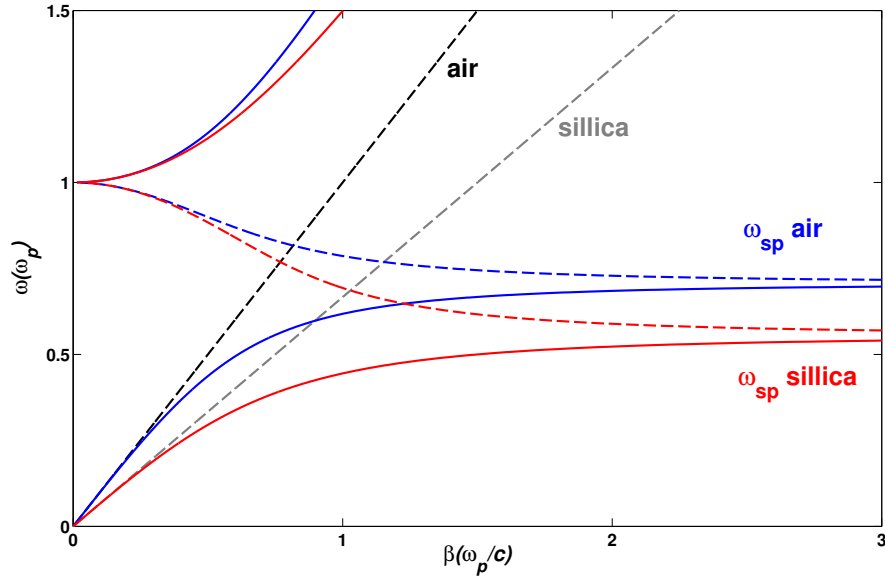


Figure 3.2: Dispersion relation of SPPs at the interface between a Drude metal with negligible collision frequency and air (blue curves) and silica (red curves).

propagation constant  $\beta$  is close to  $k_0$  at the light line, in the opposite regime of the frequency close to surface plasmon frequency  $\omega_p$ . It also shows that the SPPs line lying to the right of the respective light lines of air and silica, so that SPPs are directed by light due to phase mismatching. The wave vector mismatch between SPPs and radiation modes needs to be overcome in order to excite or detect SPPs. This can be achieved by multiple methods [?]. In the Otto configuration, light in a prism that is brought in close vicinity to a metal surface can excite SPPs through coupling to the evanescent field. Because light in the prism has a larger wave vector than that in air, it can be phase-matched to the SPPs. In the related Kretschmann-Raether geometry, coupling to SPPs occurs through a metal film

that is deposited on a prism. In the grating coupling configuration, metal surface with a shallow grating of grooves or holes with lattice constant  $a$ . For the simple 1D grating of grooves depicted in Figure 3.3, phase-matching takes place when the condition is fulfilled

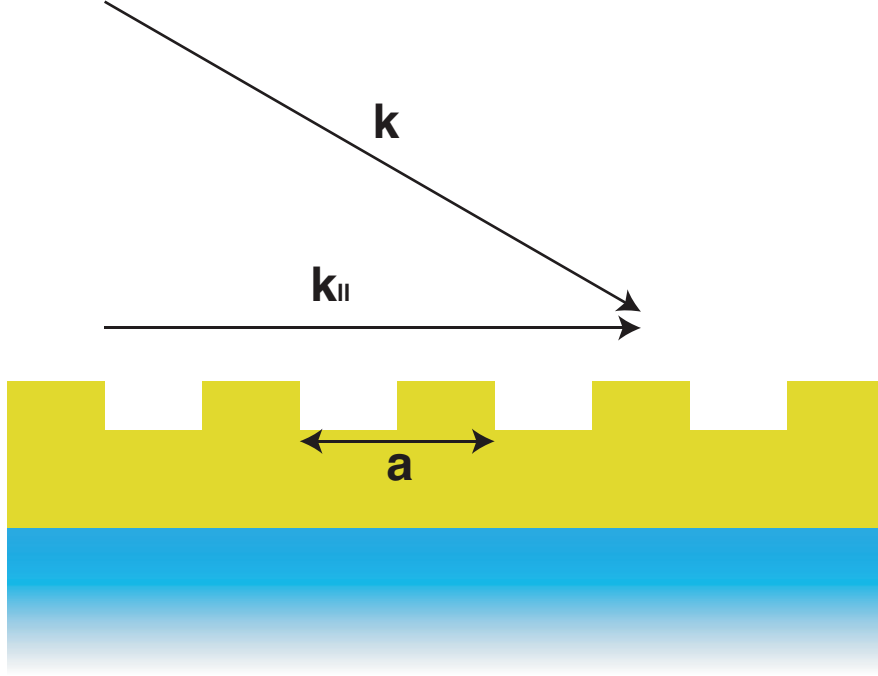


Figure 3.3: Phase-matching of light to SPPs the grating coupling configuration.

$$\beta = k_0 \sin \theta \pm \nu g, \quad (3.11)$$

where  $g = \frac{2\pi}{a}$  is the reciprocal vector of the grating, and  $\nu = (1, 2, 3 \dots)$ . As with prism coupling, excitation of SPPs is detected as a minimum in the reflected light. The reverse process can also take place, SPPs propagating along a surface modulated with a grating can couple to light and thus radiate.

# Chapter 4

## Experiment

### 4.1 Atomic force microscopy

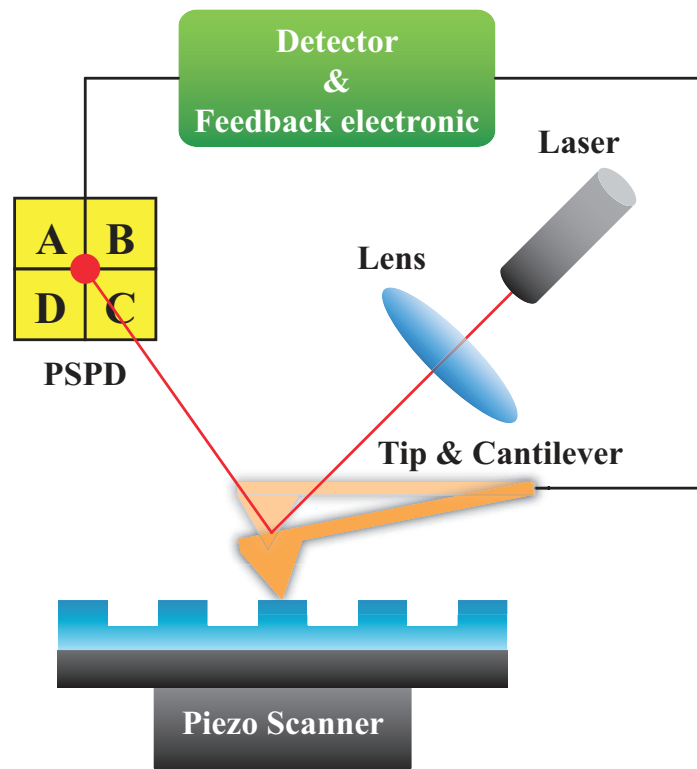


Figure 4.1: Schematic of atomic force microscopy.

Atomic force microscope (AFM) is a type of scanning probe microscopes (SPM) [?]. The schematic of AFM is shown in Figure 4.1. AFM operates by measuring force between a probe and the specimen surfaces. In general, the probe is a sharp tip at a cantilever's end. The cantilever can be deflected by atomic forces to sufficiently large amount, then AFM

can measure the vertical and lateral deflections of the cantilever by using the optical system. A laser beam is transmitted to cantilever, and the reflected laser beam is detected with a position-sensitive photo detector (PSPD). PSPD is four-sectional that allows measuring not only vertical but lateral bending too(Figure 4.2). The output of the PSPD is provided to a computer for processing of the data for providing a topographical image of the surface with atomic resolution, and controlling the height between probe and specimen surfaces by applying voltage on piezoelectric scanner.

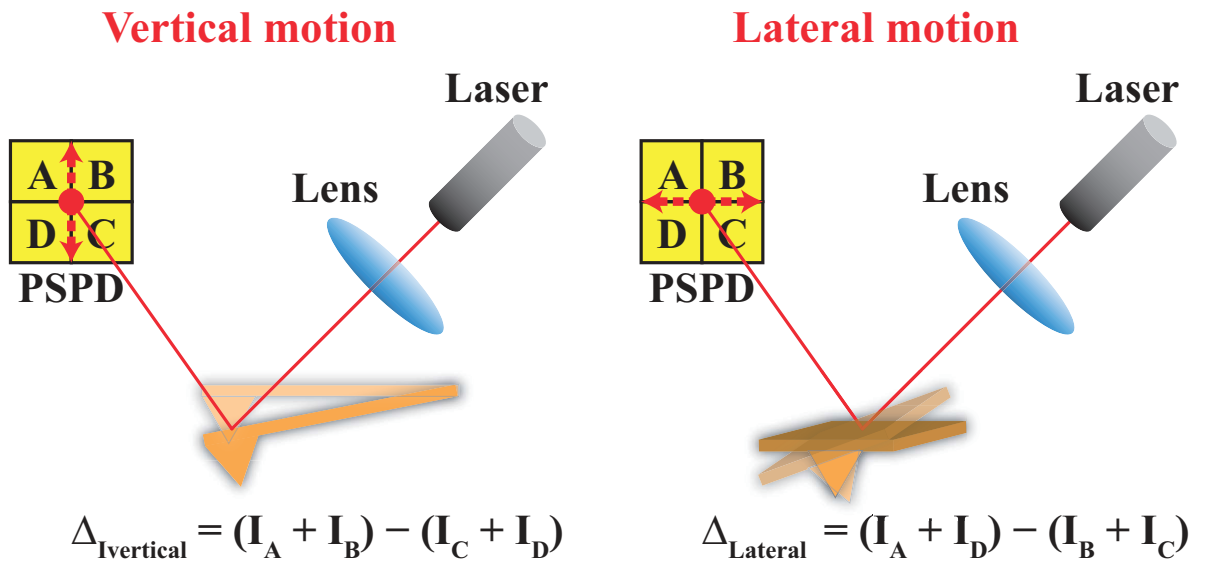


Figure 4.2: Schematic of optical system for cantilever deflections detection.

The physical principle of the AFM operation is based on interaction between the probe tip and the specimen surface(Figure 4.3). When the cantilever approaches the specimen surface, Van der Waals forces start acting upon it . They are sufficiently far-ranging and are felt at the distance of a few tens of angstroms. Then at the distance of several angstroms repulsive force starts acting. In humid air a water layer is present on the specimen surface. The capillary force arises that holds the tip in contact with the surface and increases the minimum achievable interaction force. Electrostatic interaction between the probe and the sample may appear rather often. This can be both attraction and repulsion. Van der Waals attraction forces, capillary, electrostatic and repulsion forces at the point where the tip touches the sample and forces acting upon the tip from the deformed cantilever compensate each other in equilibrium. Based on the type and degree of this interaction

the AFM modes can be broken down into contact and semi-contact(Figure 4.3 ), which is a transition mode between the contact and non-contact modes.

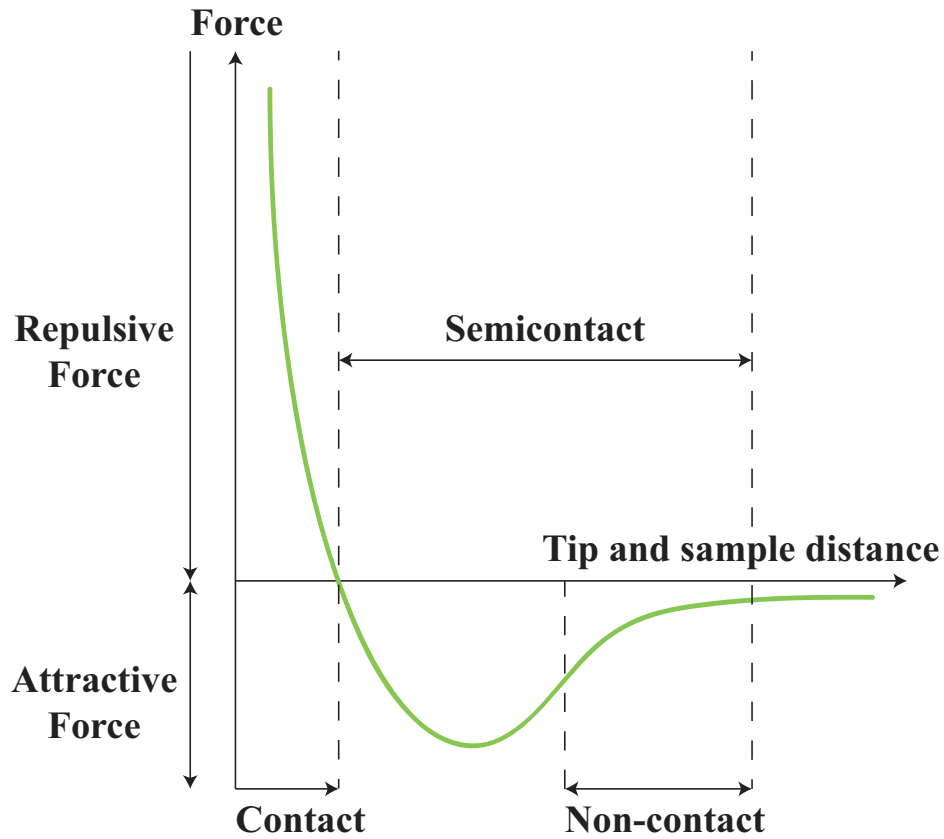


Figure 4.3: Sketch of tip-sample forces.

**Contact mode** In contact mode of operation the cantilever deflection under scanning reflects repulsive force acting upon the tip. Repulsion force  $F$  acting upon the tip is related to the cantilever deflection value  $x$  under Hooke's law:  $F = -K \cdot x$ , where  $K$  is cantilever spring constant. The spring constant values for different cantilevers usually vary from 0.01 to several N/m.

In our units the vertical cantilever deflection value is measured by means of the optical registration system and converted into electrical signal DFL (difference signal between the upper and lower halves of the PSPD) . In contact mode the DFL signal is used as a parameter characterizing the interaction force between the tip and the surface. There is a linear relationship between the DFL value and the force. In constant force mode of operation the deflection of the cantilever is maintained by the feedback circuitry on the

preset value. So vertical displacement of the scanner under scanning reflects topography of sample under investigation.

Contact force microscopy is surface topography measurement in the contact mode. The microscope operation in the mode of maintaining constant interaction force between the tip and the surface sample, and is the base for measuring surface topography as well as for measuring local rigidity, local viscosity and local friction force. Constant force mode has some advantages and disadvantages. Main advantage of constant force mode is possible to measure with high resolution simultaneously with topography and some other characteristics, such as friction forces, spreading resistance etc. Constant force mode has also some disadvantages. Speed of scanning is restricted by the response time of feedback system. When exploring soft samples they can be destroyed by the scratching because the probe scanning tip is in direct contact with the surface. Therefore, under scanning soft unhomogeneous samples the local flexure of sample surface varies. As a result acquired topography of the sample can be proved distorted. Possible existence of substantial capillary forces imposed by a liquid adsorption layer can decrease the resolution.

**Semi-contact mode** The semi-contact mode can be characterized by some advantages in comparison with contact mode. First of all, in this mode the force of pressure of the cantilever onto the surface is less, that allows to work with softer materials such as polymers and bio-organics. The semi contact mode is also more sensitive to the interaction with the surface that gives a possibility to investigate some characteristics of the surface distribution of magnetic and electric domains, elasticity and viscosity of the surface.

Widely used semi-contact mode has some disadvantage concerned with the usage of the feedback circuit. The scanning speed in semi-contact mode is restricted by the feedback circuit reaction time. This disadvantage can be overcome by the fact that under scanning new value of cantilever oscillation amplitude (and error signal) usually is achieved faster than preset value of the cantilever oscillation amplitude can be reached by the feedback system. Time of the reaching new value of the oscillation amplitude is determined by the oscillation period and Q-quality of the cantilever. The feedback error signal, emerging when scanning in the semi-contact mode, contains some additional information about the

topography. It can be utilized for achieving a more precise recovery of the relief.

Additionally, similarly to the contact error mode, which can be considered as intermediate between the constant force mode and constant height mode, the feedback gain factor (i.e. the feedback processing speed) can be adjusted for the system to be able to trace subtle changes of the relief and to be too slow to trace the steep changes. Then, when the probe travels over minor irregularities, scanning will be carried out with an almost constant piezo scanner length. As a result, the slow changes of the relief will hardly show up on the images, and the steep changes will appear in high contrast. This may be helpful in finding minor irregularities on large areas against major sloping relief features. It must be noted that height of the minor irregularities must be less than amplitude of cantilever oscillation.

## **4.2 Scanning electron microscopy**

The scanning electron microscope (SEM) is used for the observation of specimen surfaces [?]. When the specimen is irradiated with a fine electron beam, secondary electrons are emitted from the specimen surface. Topography of the surface can be observed by two-dimensional scanning of the electron probe over the surface and acquisition of an image from the detected secondary electrons. The concept schematic of commercial SEM (JEOL, JSM-6500F) is shown in Figure 4.4. The basic unit is composed of an electron optical system, a specimen stage, a secondary-electron detector, an image display unit, and an operation system. The electron optical system consists of an electron gun, a condenser lens and an objective lens to produce an electron probe, a scanning coil to scan the electron probe, and other components. The system inside of the microscope column are kept at vacuum.

The JSM-6500F utilizes a Schottky type field-emission (T-FE) gun for the electron source. The T-FE gun can constantly supply the surface of the cathode with zirconium oxide by heating the surface of cathode to 1800 K. For this reason, it can easily obtain stable and high probe current (range from several pA to 100 nA) compared with the traditional thermal emission electron gun and cold field-emission gun.

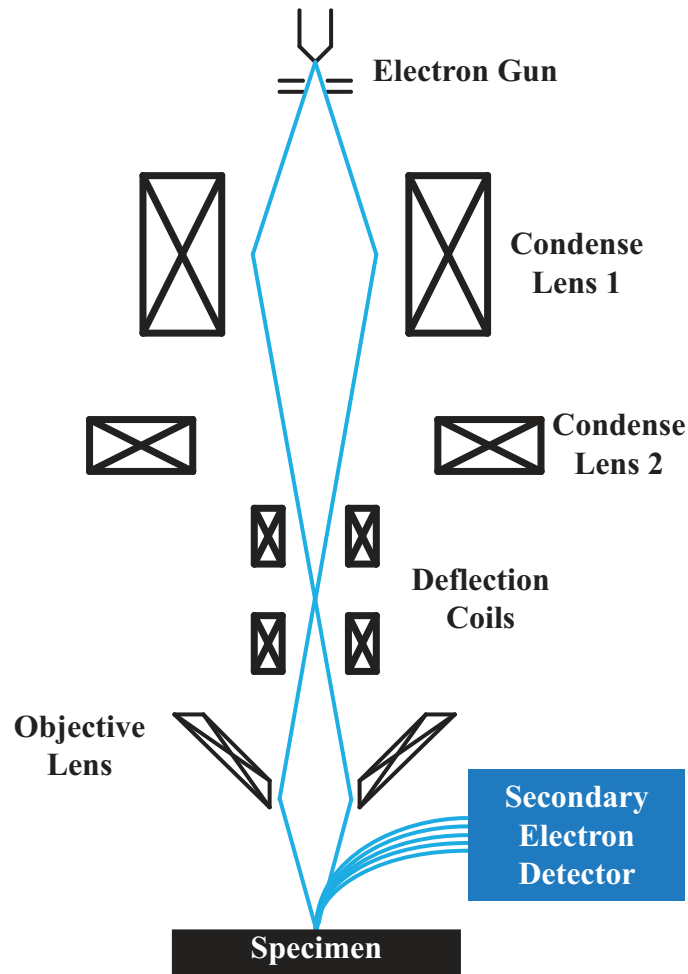


Figure 4.4: Basic construction of a scanning electron microscopy.

The magnetic condenser and objective lens system act to control the diameter of the beam as well as to focus the beam on the specimen due to a rotationally-symmetric magnetic field is formed when we pass a direct electric current through a coilwound electric wire in the magnetic lens. A pair of deflector coils, which between the condenser and objective lens, controlled by the scan generator, which are responsible for rastering that focused beam across the specimen surface. The size of the rastering pattern is under magnification control. The beam is rastered from left to right and top to bottom. There is a one-to-one correspondence between the rastering pattern on the specimen and the rastering pattern used to produce the image on the monitor. The resolution we choose to image at will obviously affect the number of pixels per row as well as the number of rows that constitute the scanned area.

The signal is generated from the specimen, and collected by the detector and subse-



quently processed to generate the image. That processing takes the intensity of the signal coming from a pixel on the specimen and converts it to a grayscale value of the corresponding monitor pixel. The monitor image is a two dimensional rastered pattern of grayscale values.

With the beam focused on the specimen surface, all we need to do to change magnification is to change the size of the rastered area on the specimen. The size of the monitor raster pattern is constant. Magnification will increase if we reduce the size of the area scanned on the specimen.