

燕山大学研究生课程结课论文

《鲁棒控制》

任课教师：赵广磊

班 级： 双控三班

学 号： 202221030205

姓 名： 杨泽坤

具有时滞切换的不确定切换中立系统的鲁棒稳定性

一、介绍

切换系统由有限个连续时间或离散时间子系统和一个指定这些子系统之间切换的切换信号组成。这类系统在过去的几十年中引起了相当大的关注，因为各种实际系统，如化学加工、通信网络、交通控制、制造系统控制、汽车发动机控制和飞机控制等都可以建模为切换系统。在切换系统的稳定性分析和控制综合领域，出现了许多工作。

人们注意到，时滞现象广泛存在于工程和系统中，它可能导致控制系统不稳定或系统性能变差。中立型系统是一类重要的时滞系统，它不仅依赖于状态的时滞，还依赖于状态导数的时滞。中性系统的一些实际例子包括分布式网络、热交换和包括蒸汽在内的过程。近年来，该方向的研究活动日益增多。

另一方面，在实际环境中，执行器可能会发生故障。如果一个控制系统在发生故障时仍能保持某些特性，则称其是可靠的。值得注意的是，通常情况下，固定增益的控制器易于实现，能够满足实际应用的要求。但当故障发生时，常规控制器将变得保守，可能无法满足某些控制性能指标。可靠控制是一种有效的提高系统可靠性的控制方法，其目标是在执行器发生故障的情况下，设计一个结构合适的控制器来保证稳定性和令人满意的性能。自 20 世纪 70 年代 Siljak 提出可靠控制的概念以来，可靠控制问题引起了众多学者的关注。

最近，由于切换中立系统在实际系统中的大量应用，一些研究者开始关注切换中立系统。文献研究了切换中立系统的稳定性分析和控制综合问题。然而，正如文献所指出的，实际运行中不可避免地存在控制器与系统的异步切换，即控制器的切换时刻超过或滞后于系统的切换时刻。在现有研究成果中，已经提出了时滞切换中立系统的镇定问题的一些结果。据我们所知，异步切换下切换中立系统的鲁棒可靠控制问题尚未被研究。采用驻留时间方法进行稳定性分析和控制器设计，为具有时滞切换和执行器故障的切换中立系统设计一个可靠的镇定控制器，使得闭环系统是指数稳定的。

二、问题模型和预备知识

具有执行器故障的不确定中立切换系统

$$\dot{x}(t) - C_{\sigma(t)}\dot{x}(t - \tau_1) = \hat{A}_{\sigma(t)}x(t) + \hat{B}_{\sigma(t)}x(t - \tau_2) + D_{\sigma(t)}u^f(t),$$

$$x(t_0 + \theta) = \varphi(\theta), \quad \theta \in [-\tau, 0],$$

对于执行器故障的控制输入可以被描述为

$$u^f(t) = \Omega_{\sigma(t)}u(t),$$

为了形式简单，我们定义

$$\Omega_{i0} = \text{diag}\{\tilde{\omega}_{i1}, \tilde{\omega}_{i2}, \dots, \tilde{\omega}_{in}\}, \quad \tilde{\omega}_{ik} = \frac{1}{2}(\omega_{lik} + \omega_{uik}),$$

$$\Xi_i^2 = \text{diag}\{\xi_{i1}^2, \xi_{i2}^2, \dots, \xi_{in}^2\}, \quad \xi_{ik}^2 = \frac{\omega_{uik} - \omega_{lik}}{\omega_{lik} + \omega_{uik}},$$

$$\Theta_i = \text{diag}\{\theta_{i1}, \theta_{i2}, \dots, \theta_{in}\}, \quad \theta_{ik} = \frac{\omega_{ik} - \tilde{\omega}_{ik}}{\tilde{\omega}_{ik}}.$$

因此，我们有如下公式

$$\Omega_i = \Omega_{i0}(I + \Theta_i), \quad |\Theta_i| \leq \Xi_i^2 \leq I,$$

然而在实际运行中，不可避免地存在控制器与系统之间的异步切换。不失一般性，我们只考虑控制器的切换时刻相对于系统的切换时刻发生时滞的情况。控制器的切换时刻可以描述为

$$t_1 + \Delta_1, t_2 + \Delta_2, \dots, t_k + \Delta_k, \dots, \quad k \in \mathbb{Z}^+,$$

三、主要结果

1. 稳定性分析

首先我们分析无切换的中立系统稳定性

引理 1

考虑以下中立系统

$$\dot{x}(t) - C\dot{x}(t - \tau_1) = Ax(t) + Bx(t - \tau_2),$$

$$x(t_0 + \theta) = \varphi(\theta), \quad \theta \in [-\tau, 0],$$

如果存在合适维数常量矩阵 A, B, C, 对于给定常数 α 如果存在正定系统矩阵 P, R 满足

$$\begin{bmatrix} A^T P^{-1} + P^{-1} A + \alpha P^{-1} + R_1^{-1} & P^{-1} B & P^{-1} C & A^T \\ * & -e^{-\alpha \tau_2} R_1^{-1} & 0 & B^T \\ * & * & -e^{-\alpha \tau_1} R_2^{-1} & C^T \\ * & * & * & -R_2 \end{bmatrix} < 0,$$

那么有沿着系统轨迹以下不等式成立

$$V(x(t)) < e^{-\alpha(t-t_0)} V(x(t_0)).$$

引理 2

对于给定的正常数 β , 如果存在具有适当的维数的正定对称矩 P, R 满足

$$\begin{bmatrix} A^T P^{-1} + P^{-1} A - \beta P^{-1} + R_1^{-1} & P^{-1} B & P^{-1} C & A^T \\ * & -e^{\beta \tau_2} R_1^{-1} & 0 & B^T \\ * & * & -e^{\beta \tau_1} R_2^{-1} & C^T \\ * & * & * & -R_2 \end{bmatrix} < 0.$$

那么有沿着系统轨迹以下不等式成立

$$V(x(t)) < e^{\beta(t-t_0)} V(x(t_0)).$$

注释

引理 1, 2 给出了候选 Lyapunov 泛函的评估方法, 并将其用于异步切换中立系统的控制器设计。

2. 鲁棒稳定性控制器设计

考虑上述系统在异步切换控制器 $u^f(t) = \Omega_{\sigma'(t)} K_{\sigma'(t)} x(t)$, 相对应的闭环系统可以写为

$$\begin{aligned} \dot{x}(t) - C_{\sigma(t)} \dot{x}(t - \tau_1) &= (\hat{A}_{\sigma(t)} + D_{\sigma(t)} \Omega_{\sigma'(t)} K_{\sigma'(t)}) x(t) + \hat{B}_{\sigma(t)} x(t - \tau_2), \\ x(t_0 + \theta) &= \varphi(\theta), \quad \theta \in [-\tau, 0]. \end{aligned}$$

假设第 i 个子系统在切换时刻 t_k 被激活, 第 j 个子系统在切换时刻 $t_k + 1$ 被激活, 相应的切换控制器分别在切换时刻 $t_k + \Delta_k$, $t_{k+1} + \Delta_{k+1}$ 被激活。

定理 1

考虑系统 (1) 和 (2), 对于给定的正常数 α, β , 如果存在正定对称矩阵 P, R 适当维数的矩阵 W 和正标量 ε, δ 使得对 i, j , 下列不等式成立。

$$\begin{aligned} & \begin{bmatrix} \Pi_{11i} & B_i R_{1i} & C_i R_{2i} & \Pi_{14i} & P_i & W_i^T \Xi_i & P_i E_{1i}^T \\ * & -e^{-\alpha \tau_2} R_{1i} & 0 & R_{1i} B_i^T & 0 & 0 & R_{1i} E_{2i}^T \\ * & * & -e^{-\alpha \tau_1} R_{2i} & R_{2i} C_i^T & 0 & 0 & 0 \\ * & * & * & \Pi_{44i} & 0 & 0 & 0 \\ * & * & * & * & -R_{1i} & 0 & 0 \\ * & * & * & * & * & -\varepsilon_i I & 0 \\ * & * & * & * & * & * & -\delta_i I \end{bmatrix} < 0, \\ & \begin{bmatrix} \Pi_{11ij} & B_j R_{1ij} & C_j R_{2ij} & \Pi_{14ij} & P_{ij} & P_{ij} K_i^T \Xi_i & P_{ij} E_{1ij}^T \\ * & -e^{\beta \tau_2} R_{1ij} & 0 & R_{1ij} B_j^T & 0 & 0 & R_{1ij} E_{2ij}^T \\ * & * & -e^{\beta \tau_1} R_{2ij} & R_{2ij} C_j^T & 0 & 0 & 0 \\ * & * & * & \Pi_{44ij} & 0 & 0 & 0 \\ * & * & * & * & -R_{1ij} & 0 & 0 \\ * & * & * & * & * & -\varepsilon_{ij} I & 0 \\ * & * & * & * & * & * & -\delta_{ij} I \end{bmatrix} < 0. \end{aligned}$$

那么在异步切换控制器 $u^f(t) = \Omega_{\sigma'(t)} K_{\sigma'(t)} x(t)$ 安定平均驻留时间满足

$$\inf_{t > t_0} \frac{T^-(t_0, t)}{T^+(t_0, t)} \geq \frac{\lambda^+ + \lambda^*}{\lambda^- - \lambda^*}, \quad \tau_a > \tau_a^* = \frac{\ln(\mu_1 \mu_2)}{\lambda^*},$$

时, 对应的闭环系统是渐近稳定的, 其中

$$\begin{aligned} \Pi_{11i} &= A_i P_i + P_i A_i^T + \alpha P_i + D_i \Omega_{i0} W_i + W_i^T \Omega_{i0}^T D_i^T + \varepsilon_i D_i \Omega_{i0} \Xi_i^2 \Omega_{i0}^T D_i^T + \delta_i H_i H_i^T, \\ \Pi_{14i} &= P_i A_i^T + W_i^T \Omega_{i0}^T D_i^T + \varepsilon_i D_i \Omega_{i0} \Xi_i^2 \Omega_{i0}^T D_i^T + \delta_i H_i H_i^T, \\ \Pi_{44i} &= -R_{2i} + \varepsilon_i D_i \Omega_{i0} \Xi_i^2 \Omega_{i0}^T D_i^T + \delta_i H_i H_i^T, \\ \Pi_{11ij} &= A_j P_{ij} + P_{ij} A_j^T - \beta P_{ij} + D_j \Omega_{j0} K_i P_{ij} + P_{ij} K_i^T \Omega_{j0}^T D_j^T + \varepsilon_{ij} D_j \Omega_{j0} \Xi_i^2 \Omega_{j0}^T D_j^T + \delta_{ij} H_j H_j^T, \\ \Pi_{14ij} &= P_{ij} A_j^T + P_{ij} K_i^T \Omega_{j0}^T D_j^T + \varepsilon_{ij} D_j \Omega_{j0} \Xi_i^2 \Omega_{j0}^T D_j^T + \delta_{ij} H_j H_j^T, \\ \Pi_{44ij} &= -R_{2ij} + \varepsilon_{ij} D_j \Omega_{j0} \Xi_i^2 \Omega_{j0}^T D_j^T + \delta_{ij} H_j H_j^T, \\ \lambda^+ &= \beta, \lambda^- = \alpha, 0 < \lambda^* < \lambda^-, \mu_1, \mu_2 > 1 \text{ satisfying} \\ P_i^{-1} &< \mu_1 P_{ij}^{-1}, \quad P_{ij}^{-1} < \mu_2 P_i^{-1}, R_{1i}^{-1} < \mu_1 R_{1ij}^{-1}, \quad R_{1ij}^{-1} < \mu_2 R_{1i}^{-1}, \quad R_{2i}^{-1} < \mu_1 R_{2ij}^{-1}, \quad R_{2ij}^{-1} < \mu_2 R_{2i}^{-1}. \end{aligned}$$

四、仿真

在这一部分我们给出一个例子来说明所提出方法的有效性。考虑上述系统, 给出参数如下:

$$\begin{aligned} A_1 &= \begin{bmatrix} 1 & -2 \\ 1 & -1 \end{bmatrix}, \quad B_1 = \begin{bmatrix} -1 & 0 \\ -1 & -1 \end{bmatrix}, \quad C_1 = \begin{bmatrix} -0.2 & 0 \\ 0.5 & -0.1 \end{bmatrix}, \quad D_1 = \begin{bmatrix} -4 & -1 \\ 2 & 1 \end{bmatrix}, \\ E_{11} &= \begin{bmatrix} 0.1 & 0.2 \\ 0.3 & 0 \end{bmatrix}, \quad E_{21} = \begin{bmatrix} 0.1 & 0 \\ 0.1 & 0.2 \end{bmatrix}, \quad H_1 = \begin{bmatrix} 0.8 & 0.6 \\ 0.4 & 1 \end{bmatrix}, \\ A_2 &= \begin{bmatrix} 2 & 3 \\ -4 & -5 \end{bmatrix}, \quad B_2 = \begin{bmatrix} -1 & -2 \\ 0 & -1 \end{bmatrix}, \quad C_2 = \begin{bmatrix} -0.1 & 0 \\ -0.5 & -0.2 \end{bmatrix}, \quad D_2 = \begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix}, \\ E_{12} &= \begin{bmatrix} 0.1 & 0.2 \\ 0.2 & 0.1 \end{bmatrix}, \quad E_{22} = \begin{bmatrix} 0.2 & 0 \\ 0.3 & 0.2 \end{bmatrix}, \quad H_2 = \begin{bmatrix} 0.6 & 0.3 \\ 0.4 & 0.4 \end{bmatrix}, \\ F_1 &= \begin{bmatrix} \sin t & 0 \\ 0 & \sin t \end{bmatrix}, \quad F_2 = \begin{bmatrix} \cos t & 0 \\ 0 & \cos t \end{bmatrix}. \end{aligned}$$

故障矩阵为 $\Omega_i = \text{diag}\{\omega_{i1}, \omega_{i2}\}$, $i = 1, 2$, 其中

$$0.6 \leq \omega_{11} \leq 0.7, \quad 0.2 \leq \omega_{12} \leq 0.7, \quad 0.3 \leq \omega_{21} \leq 0.6, \quad 0.2 \leq \omega_{22} \leq 0.8.$$

在定理 1 中的各个参数取为

$$\begin{aligned} K_1 &= \begin{bmatrix} 18.8234 & 7.5050 \\ -11.6482 & -5.7466 \end{bmatrix}, \quad K_2 = \begin{bmatrix} 32.3175 & 1.1808 \\ -5.0367 & -2.3803 \end{bmatrix}, \\ P_1 &= \begin{bmatrix} 2.1232 & -4.0345 \\ -4.0345 & 8.5620 \end{bmatrix}, \quad R_{11} = \begin{bmatrix} 2.4296 & -4.0505 \\ -4.0505 & 8.0769 \end{bmatrix}, \quad R_{12} = \begin{bmatrix} 14.9833 & -7.9728 \\ -7.9728 & 40.6105 \end{bmatrix}, \end{aligned}$$

$$P_{12} = \begin{bmatrix} 0.0539 & -0.0504 \\ -0.0504 & 0.1719 \end{bmatrix}, \quad R_{112} = \begin{bmatrix} 0.7954 & -0.2026 \\ -0.2026 & 0.3864 \end{bmatrix}, \quad R_{212} = \begin{bmatrix} 1.1159 & 0.4358 \\ 0.4358 & 0.8462 \end{bmatrix},$$

$$P_2 = \begin{bmatrix} 0.3947 & 0.3143 \\ 0.3143 & 2.3980 \end{bmatrix}, \quad R_{21} = \begin{bmatrix} 3.3264 & -1.2587 \\ -1.2587 & 1.2138 \end{bmatrix}, \quad R_{22} = \begin{bmatrix} 14.0713 & 5.9282 \\ 5.9282 & 28.6057 \end{bmatrix},$$

$$P_{21} = \begin{bmatrix} 0.0134 & -0.0148 \\ -0.0148 & 0.2576 \end{bmatrix}, \quad R_{121} = \begin{bmatrix} 0.4821 & -0.1346 \\ -0.1346 & 0.6508 \end{bmatrix}, \quad R_{221} = \begin{bmatrix} 0.9277 & -0.0454 \\ -0.0454 & 0.7785 \end{bmatrix}.$$

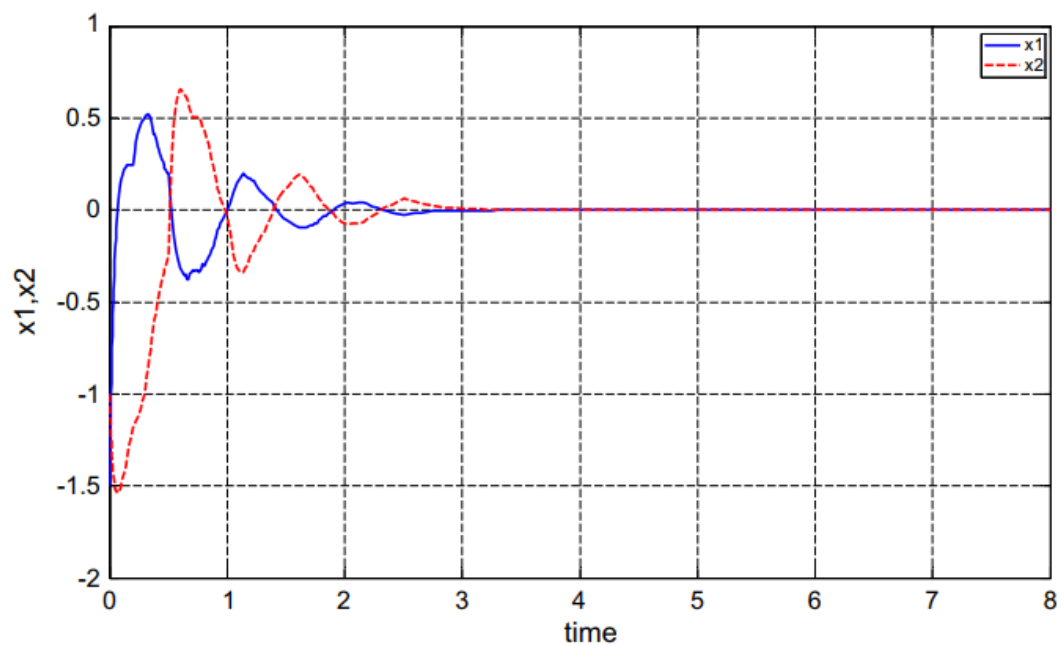


图 1 闭环系统状态轨迹

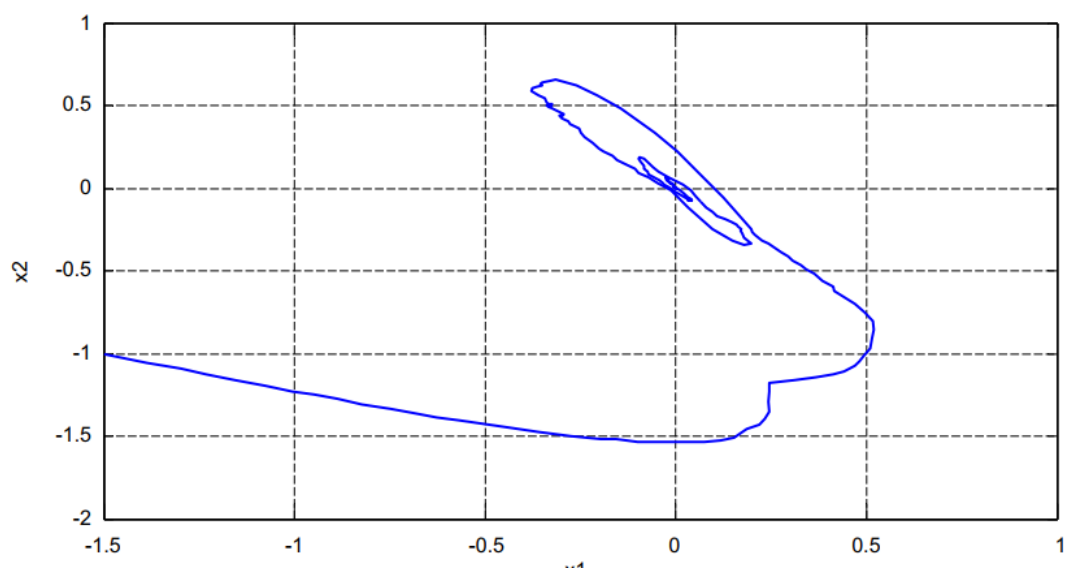


图 2 闭环系统的相轨迹图

从图 1 和 2 中, 可以观察到可靠控制器可以保证闭环系统的渐近稳定性和可靠性。这证明了所提方法的有效性。

四、总结

本文主要针对一类具有时滞切换和执行器故障的不确定切换中立系统设计鲁棒可靠控制器。提出了一种可靠的控制器设计方法, 并采用驻留时间方法进行稳定性分析。以线性矩阵不等式的形式给出了此类控制器存在的充分条件。还给出了一个例子来说明所提方法的适用性。

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