Design of a Magnetic Levitation Control System - Complex Engineering Problem

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Abstract—A non-linear and unstable system is made linear and stable using linearization and phase lead compensator using MATLAB.

I. INTRODUCTION

The objective of this complex engineering problem is to design a controller for a magnetic levitation system as a classroom demonstration device. The objective of a controller is to either stabilize a system if the system is unstable or to meet specific characteristic requirements that we require by our system.

Given to us was a non-linear and unstable system - magnetic levitation system - and we had to make it stable. In order to make a system linear and stable, we have to first linearize it and then ensure that the **closed loop poles** are in the **left half plane** of the *S-plane*.

The initial equations of the system are:

$$f = C(\frac{i}{r})^2 \tag{1}$$

$$e = Ri + L\frac{di}{dt} \tag{2}$$

$$m\frac{d^2x}{dt^2} = mg - f \tag{3}$$

Where

- f electromagnetic force
- i coil current
- x distance between electromagnet and ball bearing
- C constant
- e voltage across the coil
- R coil resistance
- L coil resistance
- \bullet m mass of ball bearing
- q gravitational acceleration

As described in the reference paper given to us [1], the system is initially non-linear and linear controls theory can not be applied on non-linear systems, hence we first make it linear. The linearized equations describing the variations from the operating point are obtained by using only the linear terms from the Taylor series expansion. The linearlized equations are:

$$f_1 = 2C(\frac{i_0}{x_0^2}i_1 - \frac{i^2_0}{x_0^3}x_1) \tag{4}$$

$$e_1 = Ri_1 + L\frac{di_1}{dt} \tag{5}$$

$$m\frac{d^2x}{dt^2} = mg - f_1 \tag{6}$$

Once we obtain the linear equations and taking their Laplace, we can obtain the characteristic equation of the system, which is:

$$Q(S) = x_0 LmS^3 + x_0 RmS^2 - ki_0 LS - ki_0 R + G_{\mathbb{C}}(S)kx_0 B = 0$$
(7)

where,

$$k = 2C \frac{i_0}{x_0^2} \tag{8}$$

The sign changes in the characteristic equation indicates that the system is unstable.

Rearranging the above equation and putting in the values from the reference paper [1], we get:

$$Q(s) = 1 + \frac{60990G_{\rm C}(S)}{(S+49.5)(S-49.5)(S+58)} = 0$$
 (9)

From the above equation, we know that the:

- 1) Open loop poles are at: + 49.5, -49.5, +58
- 2) There are no Open Loop Zeros.
- 3) Value of gain is 60990

The block diagram of the system is:

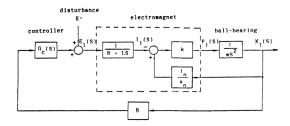


Fig. 1. Block Diagram of system

II. PROPORTIONAL CONTROLLER

Proportional controller is basically a gain K_p being multiplied with the error signal. This means:

$$G_{\mathcal{C}}(S) = \mathbf{K}_{\mathbf{p}} \tag{10}$$

where,

- $G_{\mathbb{C}}(S)$ is the proportional controller
- K_p is the proportional gain

This signal is then cascaded with the system (G(s)). A proportional controller is responsible for changes in the rise time of the system. As our system is unstable, meaning it has a pole in the right half plane and the closed loop poles also lie in right half plane, it can not be made stable by just adding a proportional controller. We tested this out on MATLAB. The code is as bellow:

```
1  G = zpk([],[-49.5,49.5,-58],60990);
2  G2 = zpk([],[-49.5,49.5,-58],60990*10);
3  G3 = zpk([],[-49.5,49.5,-58],60990*100);
4  G0 = zpk([],[-49.5,49.5,-58],1);
5  rlocus(G0,G,G2,G3)
```

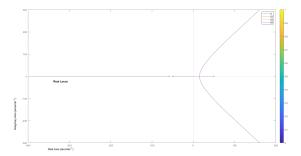


Fig. 2. Output of Proportional controllers with various K_p

In the above code, we gave different values of gain to the system and made their root locus. As seen in the output, the system is still unstable and the root loci of each system is at the same location no matter what the gain is given. (We can see overlapping of all the root loci)

III. LEAD COMPENSATOR

To make the system stable, we have to add a lead compensator. In lead compensation, we add a zero and a distant pole on the real axis. This means:

$$G_{\mathcal{C}}(S) = \frac{K(S+z)}{S+p} \tag{11}$$

where,

- K is the gain
- z is the compensator's zero

• p is the compensator's pole

In our case, we can make the system stable by adding a zero between the origin and -49.5, while the distant pole of the compensator is placed about 10 times from the zero's position [1]

Since we just have to make the system stable and not meet any other requirements, this means that we have infinite places to place our zero and pole. Each pair will reshape the root loci differently.

We choose different points to place our zero and then we plotted its root locus. The MATLAB code is:

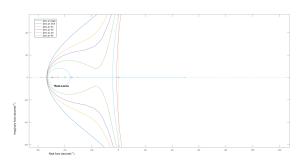


Fig. 3. Root Locus of various lead compensator systems

From the above code, we get the root locus of all the systems with compensated zeros and poles. After analyzing the different root loci, we choose to move forward with the system where we are placing a zero at -35 and a pole at -350. It is near to the existing pole at -49.5 of the uncompensated system and gives a clean root loci.

The next step is to find a suitable gain for the compensator. The gain depends on the place of closed loop poles of the system. Since we are not given any specifications such as overshoot or settling time, this means we have, again, an infinite gains to choose from. However, not each gain will give us a stable output. First we find the range of gains that will give us a stable output.

Value of gain can be found out easily by seeing where the

root loci intersects with a line drawn at the angle that is achieved by the cosine of our zeta. So in short, the value of gain depends upon the the Zeta we choose.

This was achieved by this code on MATLAB:

```
1 G_C_35 = zpk([-35],[-49.5,49.5,-58,-350],60990);
2 rlocus(G_C_35)
3 Zeta = cosd(theta); %varying theta from 0 to ...
89 degrees with an increment of 5 degree.
4 sgrid(Zeta,0)
5 [k, p] = rlocfind(G_C_35)
6 To = feedback(k*G_C_35,1);
7 step(To)
```

From this code, we found out that we get use able values of gain from about 65 degrees. All that was left is choose the right angle value from which we will obtain zeta's value. After analyzing the step response that we got from various values of theta, we choose to go with 75 degrees. This value of theta yields a value of 0.2588 for Zeta.

When we run the above code for theta = 75, we get the outputs displayed in figure 4 (the root loci of our system) and figure 5 (step response of our system):

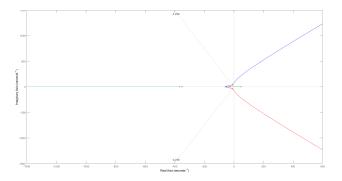


Fig. 4. Root Loci of our compensated system

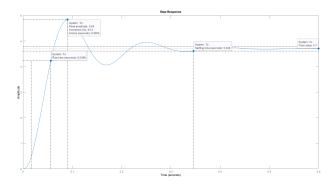


Fig. 5. Step response of our compensated system

The value of gain K comes out to 29.6 which yields an overshoot of 24.3%, settling time of 0.346 seconds and rise time of 0.0398 seconds as seen in the step response of our system. In our opinion, these are satisfactory characteristics

of the system and these are also very close to the ones in the given reference paper [1].

Now that we have made a lead compensator i.e. $G_{\rm C}(S)$ which is cascaded with our system, the overall equation of the system becomes:

$$Q(s) = 1 + \frac{K'(S+35)}{(S+49.5)(S-49.5)(S+58(s+350))} = 0$$
(12)

Where,

• K' = 60990K, K : amplifiergain(29.6)

IV. CONCLUSION

In this project we had to stabilize an unstable system. First we tried to stabilize it using a proportional controller but no matter what value of gain we kept, the system stayed unstable and the root locus stayed at the same location. Next, we made a lead compensator, with a zero at -35 and a pole at -350 on the real axis, which reshaped the root loci and moved the closed loop poles in the left half plane of the S-plane. With a zeta of value 0.25 and gain K of value 29.6. In the step response, the overshoot for these values of zeta and gain is 24.3% and a settling time of 0.34 seconds.

These values are almost identical to the reference paper [1] we were given.

REFERENCES

- T. H. Wong, "Design of a Magnetic Levitation Control System An Undergraduate Project," in IEEE Transactions on Education, vol. E-29, no. 4, pp. 196-200, Nov. 1986, doi: 10.1109/TE.1986.5570565.
- [2] J. J. D'azzo and C. H. Houpis. Linear Control System Analysis and Design, Conventional and Modern. New York: McGraw-Hill, 1975.