

2016P2Q6(I)

(a) A (CARTESIAN) TENSOR T OF ORDER 2 IS A SET OF COEFFICIENTS $T_{i_1 i_2}$ DEFINED WITH RESPECT TO A SET OF ORTHONORMAL BASIS VECTORS \underline{e}_i , SUCH THAT THE COEFFICIENTS WITH RESPECT TO ANOTHER ORTHONORMAL BASIS $\underline{e}'_i = L_{ij} \underline{e}_j$ ARE GIVEN BY THE TRANSFORMATION LAW:

$$T'_{i_1 i_2} = L_{i_1 j_1} L_{i_2 j_2} T_{j_1 j_2}$$

WHERE L IS GIVEN BY:

$$L_{ij} = \underline{e}'_i \cdot \underline{e}_j \quad \checkmark$$

[FROM NOTES]

(b) IN AN UNPRIMED BASIS:

$$\begin{aligned} \uparrow \quad T &= C_{ij} A_{ij} = C_{\ell\ell} A_{\ell\ell} \\ \text{IN ANOTHER, PRIMED BASIS:} \\ \ominus \quad T &= C'_{ij} A'_{ij} = C'_{ij} \underbrace{L_{il} L_{jk}}_{\text{REWRITE}} A_{\ell\ell} \end{aligned}$$

$$(C'_{ij} L_{il} L_{jk} - C_{\ell\ell}) A_{\ell\ell} = 0$$

$$A_{\ell\ell} \neq 0 \quad \checkmark$$

$$\Rightarrow C'_{ij} L_{il} L_{jk} = C_{\ell\ell}$$

LEAVE
EINSTEIN
NOTATION

REARRANGE

USING ORTHOGONALITY
OF L

$$L_{jk} C'_{ij} L_{il} = C_{\ell\ell}$$

$$L^T C' L = C$$

$$L \cdot L^T \rightarrow C' = L C L^T$$

undo
indices
by
symmetric
convention

$$C_{i_1 i_2} = L_{i_1 j_1} C_{j_1 j_2} L_{i_2 j_2}$$

SO BY THE DEF. GIVEN ABOVE,
 C_{ij} IS AN ORDER 2 TENSOR.

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ROTATION MATRIX AROUND x_3 AXIS BY θ ANGLE:

$$R_{x_3}(\theta) = \begin{pmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} C & -S & 0 \\ S & C & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

ROTATION MATRIX OF $\frac{\pi}{2}$ ABOUT x_3 AXIS IS THEN:

$$R = \begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \checkmark$$

$$T' = R^T T R = \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} T_{11} & T_{12} & T_{13} \\ T_{21} & T_{22} & T_{23} \\ T_{31} & T_{32} & T_{33} \end{pmatrix} \begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} T_{12} & -T_{11} & T_{13} \\ T_{22} & -T_{21} & T_{23} \\ T_{32} & -T_{31} & T_{33} \end{pmatrix} =$$

$$= \begin{pmatrix} T_{22} & -T_{21} & T_{23} \\ -T_{12} & T_{11} & -T_{13} \\ T_{32} & -T_{31} & T_{33} \end{pmatrix}$$

~~$T_{12} = -T_{21}$~~

$$T' = T \Rightarrow \begin{cases} T_{11} = T_{22} \\ T_{12} = -T_{21} \\ T_{21} = -T_{12} \end{cases}$$

T IS IN THE FORM:

$$T = \begin{pmatrix} \alpha & \omega & 0 \\ -\omega & \alpha & 0 \\ 0 & 0 & \beta \end{pmatrix} \checkmark$$

$$\begin{cases} T_{13} = T_{23} \\ T_{13} = T_{23} \end{cases} \rightarrow T_{13} = T_{23} = 0$$

$$\begin{cases} T_{32} = T_{31} \\ -T_{31} = T_{32} \end{cases} \rightarrow T_{31} = T_{32} = 0$$

INVARIANCE UNDER GENERAL ROTATION:

$$T' = R^T T R = \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \alpha & \omega & 0 \\ -\omega & \alpha & 0 \\ 0 & 0 & \beta \end{pmatrix} \begin{pmatrix} C & S & 0 \\ -S & C & 0 \\ 0 & 0 & 1 \end{pmatrix} =$$

$$= \begin{pmatrix} C S & 0 & 0 \\ -S C & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} C\alpha + S\omega & -S\alpha + C\omega & 0 \\ -C\omega + S\alpha & S\omega + C\alpha & 0 \\ 0 & 0 & \beta \end{pmatrix} =$$

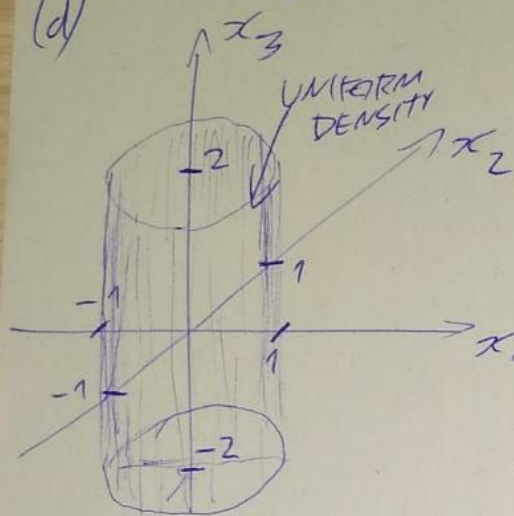
There is an easier way to do this.

$$= \begin{pmatrix} C(C\alpha + S\omega) + S(-C\omega + S\alpha) & C(-S\alpha + C\omega) + S(S\omega + C\alpha) & 0 \\ -S(C\alpha + S\omega) + C(-C\omega + S\alpha) & -S(-S\alpha + C\omega) + C(S\omega + C\alpha) & 0 \\ 0 & 0 & \beta \end{pmatrix} =$$

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$$= \begin{pmatrix} C^2\alpha + S^2\alpha & C^2\omega + S^2\omega & 0 \\ -S^2\omega - C^2\omega & S^2\alpha + C^2\alpha & 0 \\ 0 & 0 & \beta \end{pmatrix} = \begin{pmatrix} \alpha & \omega & 0 \\ -\omega & \alpha & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

(d) SO T_{ij} IS INVARIANT UNDER A GENERAL ROTATION ABOUT THE x_3 -AXIS. ✓



THIS CYLINDER IS INVARIANT UNDER ROTATION ABOUT THE x_3 AXIS, SO ITS MOMENT OF INERTIA TENSOR MUST BE INVARIANT AS WELL.

SO, USING THE EARLIER FINDINGS WE CONCLUDE THAT I_{ij} HAS THE FORM:

$$I = \begin{pmatrix} \alpha & \omega & 0 \\ -\omega & \alpha & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

$$I_{12} = \int_V \rho ((x_1^2 + x_2^2 + x_3^2) \cdot \frac{1}{2} \frac{\partial^2}{\partial x_1 \partial x_2} - x_1 x_2) dV =$$

$$= \int_V \rho x_1 x_2 dV = 0$$

THIS MUST BE ZERO BECAUSE FOR EVERY VOLUME ELEMENT FOR WHICH $- \int x_1 x_2$ IS POSITIVE, THERE IS A VOLUME ELEMENT WITH $- \int x_1 x_2$ HAVING THE SAME ABS. VALUE BUT OPPOSITE SIGN.

(SEE SKETCH). ✓

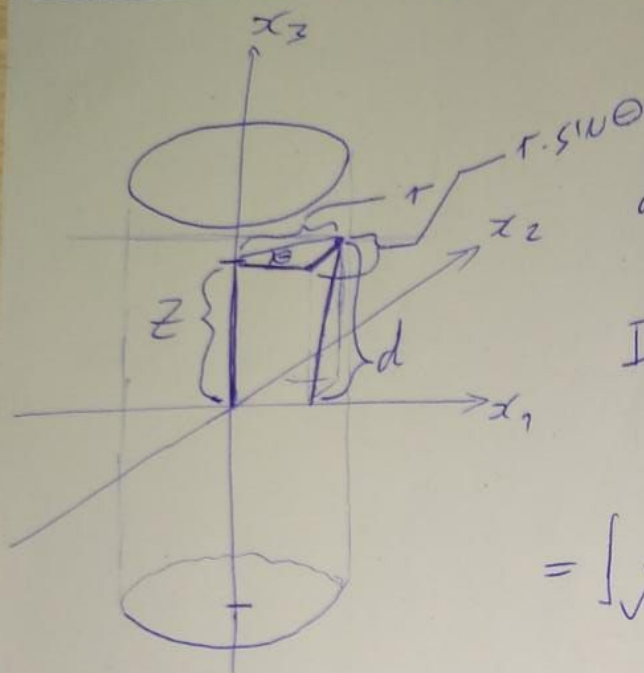
IN SHORT: BY SYMMETRY CONSIDERATIONS

SO NOW WE HAVE:

$$I = \begin{pmatrix} \alpha & 0 & 0 \\ 0 & \alpha & 0 \\ 0 & 0 & \beta \end{pmatrix} \quad \checkmark$$

2016P2QG(IV)

LET'S CALCULATE α :



$$d^2 = r^2 \sin^2 \theta + z^2$$

$$I_{11} = \int_V \rho (x_1 x_1 + x_2 x_2 + x_3 x_3 - x_1 x_1) dV =$$

$$= \int_V \rho (x_2^2 + x_3^2) dV = \int_V \rho d^2 dV =$$

$$= \int_V \rho (r^2 \sin^2 \theta + z^2) dV = \rho \int_{z=-2}^2 \int_{r=0}^1 \int_{\theta=0}^{2\pi} (r^2 \sin^2 \theta + z^2) r d\theta dr dz =$$

$$= \rho \int_{z=-2}^2 \int_{r=0}^1 \left(\cancel{r^2 \sin^2 \theta + z^2} \right) r (r^2 \pi + 2\pi z^2) dr dz =$$

$$= \rho \int_{z=-2}^2 \pi \left(\left[\frac{r^4}{4} \right]_0^1 + 2z^2 \left[\frac{r^2}{2} \right]_0^1 \right) dz = \rho \int_{z=-2}^2 \pi \left(\frac{1}{4} + z^2 \right) dz =$$

$$= \rho \pi \left(\left[\frac{1}{4} z \right]_{-2}^2 + \left[\frac{z^3}{3} \right]_{-2}^2 \right) = \rho \pi \left(1 + \frac{16}{3} \right) = \alpha$$

WE NEED ρ
NOW.

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$$\begin{aligned}
 B = I_{zz} &= \int_V (x_1^2 + x_2^2) dV = \\
 &= \int_{z=-2}^2 \int_{\theta=0}^{2\pi} \int_{r=0}^1 \underbrace{\left(\underbrace{r^2}_{\substack{\text{from } x_1^2 + x_2^2}} \right)}_{\substack{\text{from } dV}} r dr d\theta dz = \int_{z=-2}^2 \int_0^{2\pi} \left[\frac{r^4}{4} \right]_0^1 d\theta dz =
 \end{aligned}$$

$$= \int_{z=-2}^2 \frac{1}{4} \cdot 2\pi dz = \int_{z=-2}^2 2\pi dz$$

SO WE END UP WITH:

$$I = \begin{pmatrix} 5\pi(1 + \frac{16}{3}) & 0 & 0 \\ 0 & 5\pi(1 + \frac{16}{3}) & 0 \\ 0 & 0 & 32\pi \end{pmatrix}$$

$\frac{19}{3}$

this is not printed

$\frac{1}{2} m a^2$
or $\frac{1}{2} p a^2$

$$4\pi p = M$$