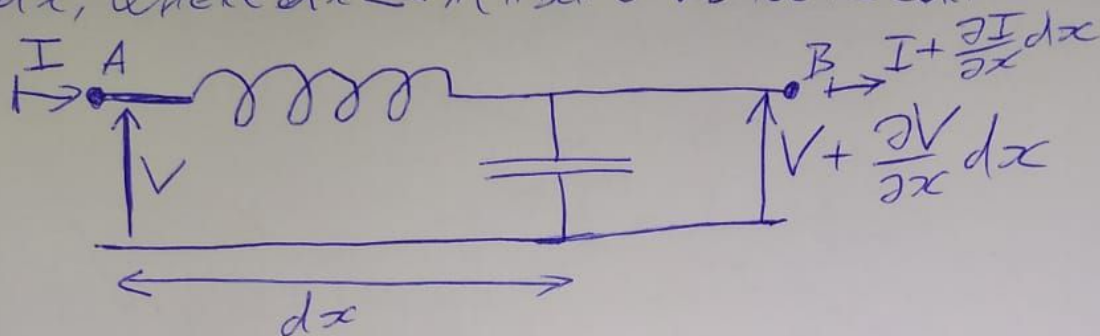


TRANSMISSION LINES

A SHORT ELEMENT OF ZERO RESISTANCE IDEAL TRANSMISSION LINE LENGTH dx , WHERE $dx \ll \lambda$ (λ BEING VOLTAGE OR CURRENT WAVELENGTH.)



POTENTIAL DIFFERENCE BETWEEN POINT A & B =

$$= - \text{THE RATE OF CHANGE OF FLUX OVER TIME} = - \frac{d}{dt} (LI) = - L \frac{\partial I}{\partial t}$$

THIS DIFFERENCE IS ALSO EQUAL TO $\frac{\partial V}{\partial x} dx$, AS SEEN IN THE DRAWING \Rightarrow .

$$\frac{\partial V}{\partial x} dx = - \underbrace{(L_0 dx)}_{\substack{\text{INDUCTANCE} \\ \text{PER UNIT LENGTH} \\ \parallel \\ L}} \frac{\partial I}{\partial t} \Rightarrow \boxed{\frac{\partial V}{\partial x} = - L_0 \frac{\partial I}{\partial t}}$$

THE CURRENT CHARGES UP THE CAPACITOR. POTENTIAL DIFF. BETWEEN CAPACITOR PLATES: $V + \frac{\partial V}{\partial x} dx$

$$\text{CHARGE PILING UP ON PLATES: } q = \underbrace{(C_0 dx)}_{\substack{\text{CAPACITANCE} \\ \text{PER UNIT LENGTH}}} \left(V + \frac{\partial V}{\partial x} dx \right) = C_0 V dx \quad \text{TO FIRST ORDER.}$$

THIS IS WHERE THE CURRENT GOES, SO:

$$\text{CURRENT IN THE BEGINNING} \cdot t = \text{CURRENT IN THE END} \cdot t +$$

$$\begin{aligned} & \Rightarrow I - \left(I + \frac{\partial I}{\partial x} dx \right) \leftarrow + \text{CHARGE ON CAPACITOR} \\ & \text{dH(CURRENT IN THE BEGINNING - CURRENT IN THE END)} = \text{CHARGE ON CAPACITOR.} \end{aligned}$$

$$dt \left(- \frac{\partial I}{\partial x} dx \right) = C_0 V dx$$

$$- \frac{\partial I}{\partial x} dx = \frac{\partial}{\partial t} (C_0 V dx) \Rightarrow \boxed{- \frac{\partial I}{\partial x} = C_0 \frac{\partial V}{\partial t}}$$

OBTAINED:

$$\frac{\partial V}{\partial x} = -L_0 \frac{\partial I}{\partial t}$$

$$-\frac{\partial I}{\partial x} = C_0 \frac{\partial V}{\partial t}$$

$$\frac{\partial}{\partial t} \rightarrow \frac{\partial^2 V}{\partial x \partial t} = -L_0 \frac{\partial^2 I}{\partial t^2}$$

$$\frac{\partial}{\partial x} \rightarrow \frac{\partial^2 V}{\partial t \partial x} = \frac{1}{C_0} \frac{\partial^2 I}{\partial x^2}$$

$$-L_0 \frac{\partial^2 I}{\partial t^2} = \frac{1}{C_0} \frac{\partial^2 I}{\partial x^2}$$

WAVE EQUATION
FOR CURRENT:

$$\frac{\partial^2 I}{\partial x^2} = L_0 C_0 \frac{\partial^2 I}{\partial t^2}$$

$$\frac{\partial}{\partial x} \rightarrow -\frac{1}{L_0} \frac{\partial^2 V}{\partial x^2} = \frac{\partial^2 I}{\partial x \partial t}$$

$$\frac{\partial}{\partial t} \rightarrow \frac{\partial^2 I}{\partial x \partial t} = -C_0 \frac{\partial^2 V}{\partial t^2}$$

WAVE EQUATION
FOR VOLTAGE:

$$\frac{\partial^2 V}{\partial x^2} = L_0 C_0 \frac{\partial^2 V}{\partial t^2}$$

So, comparing with standard form of wave eq.,
CURRENT & VOLTAGE WAVES HAVE SPEED:

$$v = \pm \frac{1}{\sqrt{L_0 C_0}}$$

SOLUTIONS IN THE FORM:

$$V = V_0 \exp[-j(\beta x - \omega t)] \text{ FOR WAVES TRAVELLING IN THE } \oplus \text{ DIRECTION.}$$

$$I = I_0 \exp[-j(\beta x - \omega t)]$$

SUBSTITUTE THESE INTO $\partial_x V = -L_0 \dot{I}$ & $-\partial_x I = C_0 \dot{V}$

$$\partial_x V = -L_0 \dot{I}$$

$$-\partial_x I = C_0 \dot{V}$$

$$(-j)\beta V = -L_0 (-j)(-\omega) I$$

$$-(-j)\beta I = C_0 (-j)(-\omega) V$$

$$\beta V = L_0 \omega I$$

$$\beta I = C_0 \omega V$$

$$\rightarrow \frac{V}{I} = \frac{L_0 \omega}{\beta} = L_0 C_0 V$$

$$\rightarrow \frac{\omega}{\beta} = \frac{I}{C_0 V}$$

$$\frac{V}{I} = L_0 \frac{I}{C_0 V} \Rightarrow \frac{V^2}{I^2} = \frac{L_0}{C_0} \Rightarrow Z = \frac{V}{I} = \sqrt{\frac{L_0}{C_0}}$$

FOR WAVES TRAVELLING IN THE NEGATIVE DIRECTION:

$$V = V_0 \exp[-j(\beta x + \omega t)]$$

$$I = I_0 \exp[-j(\beta x + \omega t)]$$

$$\partial_x V = -L_0 \dot{I} \quad \leftarrow \quad -\partial_x I = C_0 \dot{V}$$

$$-j\beta V = -L_0(-j)\omega I \quad -j\beta I = C_0(-j)\omega V$$

$$\beta V = -L_0 \omega I$$

$$\beta I = C_0 \omega V$$

$$\frac{V}{I} = -\frac{L_0 \omega}{\beta} = -L_0 \frac{I}{C_0 V} \Rightarrow \frac{V^2}{I^2} = -\frac{L_0}{C_0}$$

$$\frac{\omega}{\beta} = \frac{I}{C_0 V}$$

WHY NOT: $\frac{V}{I} = \sqrt{-\frac{L_0}{C_0}}$

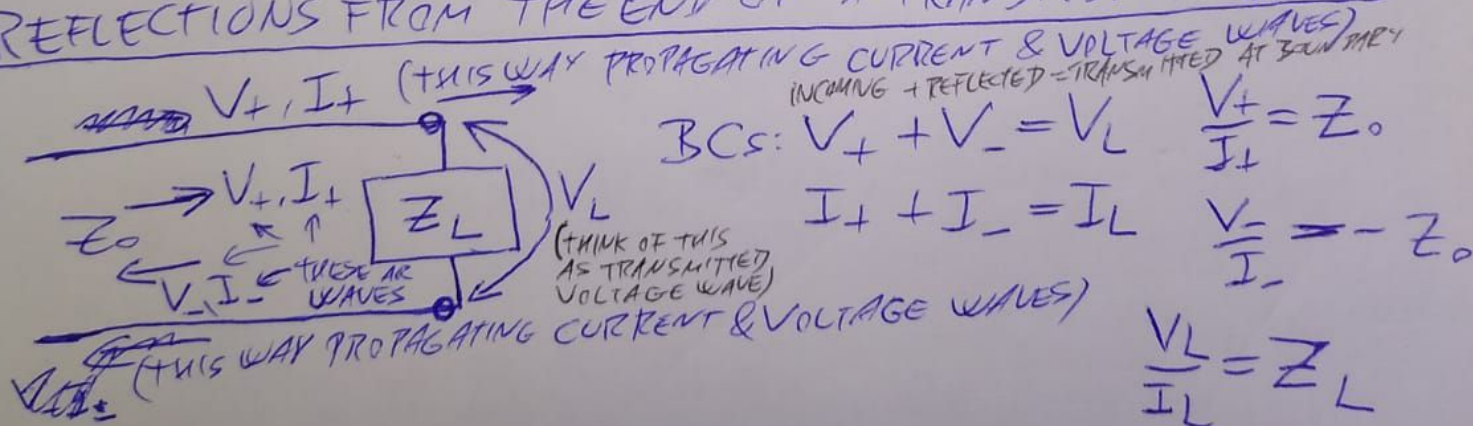
$$Z = \frac{V}{I} = i \sqrt{\frac{L_0}{C_0}}$$

$$-Z = -\frac{V}{I} = \sqrt{\frac{L_0}{C_0}}$$

$$Z = -\sqrt{\frac{L_0}{C_0}}$$

DIMENSION OF CHARACTERISTIC IMPEDANCE IS PURE RESISTANCE.

REFLECTIONS FROM THE END OF A TRANSMISSION LINE



$$Z_L = \frac{V_L}{I_L} = \frac{V_+ + V_-}{I_+ + I_-} = \frac{V_+ + V_-}{\frac{V_+}{Z_0} + \frac{V_-}{-Z_0}} = \frac{Z_0 V_+ + Z_0 V_-}{V_+ - V_-}$$

IMPEDANCE OF BACKWARD PROPAGATING WAVE.

$$Z_L = \frac{Z_0 V_+ + Z_0 V_-}{V_+ + V_-}$$

$$Z_L (V_+ + V_-) = Z_0 V_+ + Z_0 V_-$$

$$V_+ (Z_L - Z_0) = (Z_0 + Z_L) V_-$$

$$\frac{Z_L - Z_0}{Z_L + Z_0} = \frac{V_-}{V_+}$$

$$\frac{V_-}{V_+} = \frac{Z_L - Z_0}{Z_L + Z_0} = \Gamma$$

(VOLTAGE AMPLITUDE REFLECTION COEFFICIENT)

$$Z_L = \frac{Z_0 V_+ + Z_0 V_-}{V_+ + V_-} = \frac{Z_0 (\underbrace{V_+}_{Z_0 I_+} + \underbrace{V_-}_{Z_0 I_-})}{Z_0 I_+ + Z_0 I_-} = \frac{Z_0 I_+ + Z_0 I_-}{I_+ + I_-}$$

$$\Rightarrow Z_L (I_+ - I_-) = Z_0 (I_+ + I_-)$$

$$(Z_L - Z_0) I_+ = (Z_0 + Z_L) I_-$$

$$\frac{I_-}{I_+} = \frac{Z_L - Z_0}{Z_L + Z_0} = \Gamma$$

(CURRENT AMPLITUDE REFLECTION COEFFICIENT)

$$Z_L = \frac{Z_0 (V_+ + V_-)}{V_+ + V_-} = \frac{Z_0 V_L}{V_+ - (V_- - V_+)} = \frac{Z_0 V_L}{2V_+ - V_L} \Rightarrow (2V_+ - V_L) Z_L = Z_0 V_L$$

$$\Rightarrow 2V_+ Z_L = (Z_0 + Z_L) V_L \Rightarrow \frac{V_L}{V_+} = \frac{2Z_L}{Z_L + Z_0} = \tau_V$$

$$\frac{I_L}{I_+} = \frac{\frac{V_L}{Z_L}}{\frac{V_+}{Z_0}} = \frac{V_L Z_0}{V_+ Z_L} = \frac{2Z_0}{Z_L + Z_0} = \tau_I$$

VOLTAGE AMPLITUDE TRANSMISSION COEFFICIENT

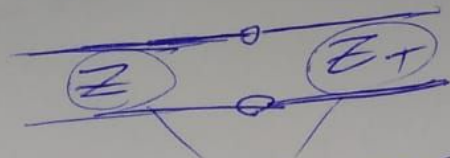
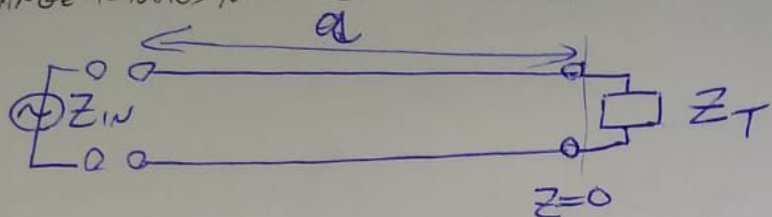
CURRENT AMPLITUDE TRANSMISSION COEFFICIENT

INPUT IMPEDANCE

[CHANGE TO NOTES NOTATION]

⊖ DIRECTION ⊕

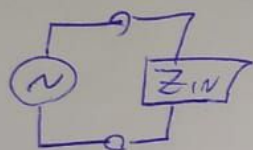
OR IMAGINE IT LIKE THIS:



CHARACTERISTIC IMPEDANCE.

(IF Z_T IS REAL SINCE CHARACTERISTIC IMPEDANCE IS ALWAYS REAL, (RESISTIVE))

Z_{IN} IS WHAT THE POWER SUPPLY "SEES".



$$V_i = V_1 \exp(-j(\beta z - \omega t))$$

$$V_r = \tau V_1 \exp(-j(\beta z - \omega t))$$

IE THE REFLECTED WAVE HAS AMPLITUDE τ TIMES THE INCOMING WAVE & TRAVELS IN THE \ominus DIR. THAT'S WHY THE EXTRA MINUS SIGN.

$$I_i = \frac{V_i}{Z} \quad I_r = -\frac{V_r}{Z}$$

$$Z_{IN} = \frac{V_i + V_r}{I_i + I_r} \bigg|_{z=0} = \frac{V_1 e^{-j\beta z} e^{j\omega t} + \tau V_1 e^{j\beta z} e^{j\omega t}}{\frac{V_1}{Z} e^{-j\beta z} e^{j\omega t} - \frac{V_1}{Z} \tau e^{j\beta z} e^{j\omega t}} \bigg|_{z=0}$$

$$= \frac{e^{j\beta a} + \tau e^{-j\beta a}}{e^{j\beta a} - \tau e^{-j\beta a}} Z$$

RECALL: $\tau = \frac{Z_T - Z}{Z_T + Z}$

$$\frac{Z_{IN}}{Z} = \frac{e^{j\beta a} + \frac{Z_T - Z}{Z_T + Z} e^{-j\beta a}}{e^{j\beta a} - \frac{Z_T - Z}{Z_T + Z} e^{-j\beta a}} = \frac{(Z_T + Z) e^{j\beta a} + (Z_T - Z) e^{-j\beta a}}{(Z_T + Z) e^{j\beta a} - (Z_T - Z) e^{-j\beta a}}$$

$$= \frac{Z \cos(\beta a) + j Z_T \sin(\beta a)}{Z \cos(\beta a) + j Z_T \sin(\beta a)} = \frac{Z_T \cos(\beta a) + j Z \sin(\beta a)}{Z \cos(\beta a) + j Z_T \sin(\beta a)}$$

SHORT-CIRCUITED LINE

$$Z_t \rightarrow 0 \Rightarrow \frac{Z_{in}}{Z} = \frac{j Z \sin(\beta a)}{Z \cos(\beta a)} = j \tan \beta a$$

OPEN-CIRCUITED LINE

$$Z_t \rightarrow \infty \Rightarrow \frac{Z_{in}}{Z} \rightarrow \frac{Z \cos(\beta a)}{j Z \sin(\beta a)} = -j \cot(\beta a)$$

QUARTER-WAVELENGTH LINE

length of transmission line = $\frac{\lambda}{4}$

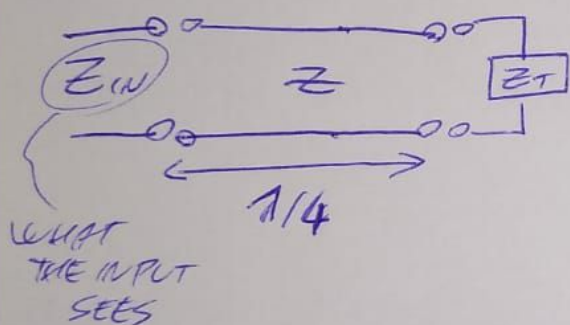
$$a = \frac{\lambda}{4} \quad \beta = \frac{2\pi}{\lambda} \rightarrow \beta a = \frac{2\pi}{4}$$

$$\beta a = \frac{2\pi}{4} = \frac{\pi}{2} \Rightarrow \beta a = \frac{\pi}{2}$$

$$\cos \beta a = \cos \frac{\pi}{2} = 0$$

$$\Rightarrow \frac{Z_{in}}{Z} = \frac{j Z \sin(\frac{\pi}{2})}{j Z_t \sin(\frac{\pi}{2})} = \frac{Z}{Z_t}$$

$$\Rightarrow \boxed{Z_{in} Z_t = Z^2}$$



$$\text{IF } \boxed{Z = Z_t}, \text{ THEN, SINCE } Z_{in} = \left. \frac{Z^2}{Z_t} \right|_{Z=Z_t} = Z$$

IMPEDANCE OF THE LOAD IS THE SAME IMPEDANCE THE INPUT SEES, SO THERE ARE NO REFLECTIONS.

Another way of looking at this:

[NOTATION CHANGE] $Z = Z_0, Z_t = Z_L$

recall:

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$\text{IF } Z_L - Z_0 = 0 \Rightarrow \boxed{Z_L = Z_0}, \Gamma = 0$$

CHARACTERISTIC IMPEDANCE

IMPEDANCE OF LOAD. [BEWARE MIXED NOTATION]

No reflection when $Z = Z_{in}$, $\frac{Z_{in}}{Z} = \frac{Z}{Z_t}$ IF $a = \frac{\lambda}{4}$ (SEE ABOVE)

↳ at load-transmission line boundary

boundary

NO REFLECTION AT ALL.

if $\frac{Z}{Z_t} = 1$, there won't be reflection on the transmission line - load boundary.