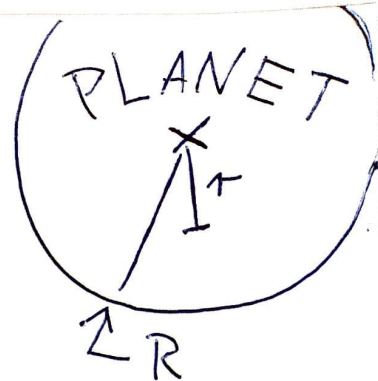


AFDII

1/ HYDROSTATIC EQUILIBRIUM: $\frac{1}{\rho} \nabla p = -\nabla \psi$



$$\nabla \psi(r) = -\frac{GM_{(\text{ENCLOSED})}}{r^2}$$

$$= -G \frac{1}{r^2} \frac{4}{3} r^3 \pi \rho = \frac{4}{3} r (-G \pi \rho)$$

$$\frac{1}{\rho} \nabla p = -\frac{4}{3} G \pi \rho r$$

$$\frac{1}{\rho} \frac{dp}{dr} = -\frac{4}{3} G \pi \rho r$$

$$p = -\frac{2}{3} G \pi \rho^2 r^2 + C$$

WE NEED:

$$p|_{r=R} = 0 \Rightarrow C = \frac{2}{3} G \pi \rho^2 R^2$$

$$\Rightarrow p = \frac{2}{3} G \pi \rho^2 (R^2 - r^2)$$

$$p_{\text{MAX}} = p|_{r=0} = \frac{2}{3} G \pi \rho^2 R^2$$

THIS MUST NOT BE GREATER THAN p_0 .

$$p_0 = \frac{2}{3} G \pi \rho^2 R^2$$

$$R = \sqrt{\frac{3 p_0}{2 G \pi \rho}} \Rightarrow R_{\text{MAX}} = \sqrt{\frac{3 p_0}{2 G \pi \rho}}$$

$$M_{\text{MAX}} = S_{\text{MAX}} V = \frac{4}{3} R^3 \pi \left[\frac{3 p_0}{2 G \pi \rho} \right]$$

$$M_{MAX} = S R_{MAX}^3 \frac{4}{3} \pi$$

$$= \frac{4}{3} \pi \sqrt{\left(\frac{3 \rho_0}{G}\right)^3 \left(\frac{1}{2\pi}\right)^3} \frac{1}{S^2}$$

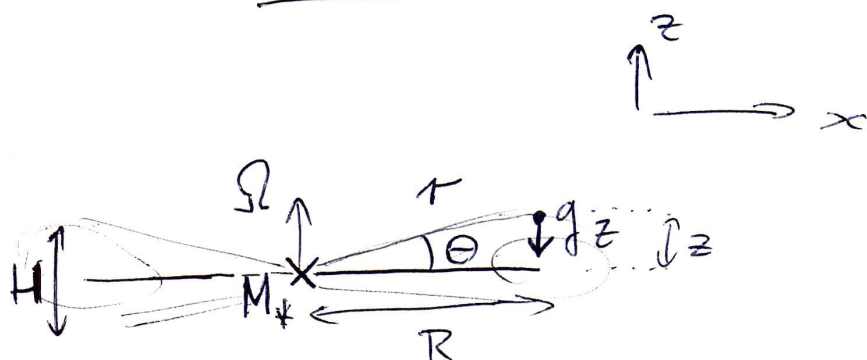
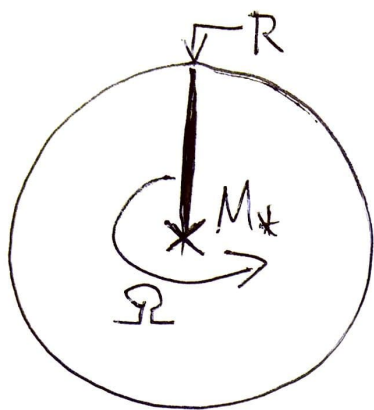
$$= \frac{2}{3S^2} \sqrt{\frac{1}{2\pi} \left(\frac{3 \rho_0}{G}\right)^3}$$

AS REQUIRED.

2/ VIEW FROM

TOP

SIDE



$$g_z = -\frac{GM}{r^2} \sin \theta = -\frac{GM}{r^2} \frac{z}{r} \sim \cancel{\frac{GM}{r^2}}$$

$$\sim -\frac{GM}{R^3} z$$

HYDROSTAT. EQ.:

$$\frac{1}{\rho} \nabla p = -\nabla \psi$$

LET'S MOVE TO ROTATING FRAME SO GAS IS STATIONARY AT $z=0$, AT $z \neq 0$ THE ONLY ACCELERATION IS g_z .

ISOTHERMAL GAS: $p = \frac{R^*}{\mu} \rho T \Rightarrow p = A \rho$ WITH $A = \frac{R^*}{\mu} T$

$$\frac{1}{\rho} \frac{\partial}{\partial z} (A \rho) = -\frac{GM_*}{R^3} z \quad / \text{INTEGRATE}$$

$$A \ln \rho = -\frac{GM_*}{2R^3} z^2 + C$$

$$\rho = \rho_0 \exp\left(-\frac{GM_*}{2AR^3} z^2\right) \quad \text{WHERE } \rho_0 = \rho|_{z=0}$$

NOTING THAT:

$$\frac{GM_*}{R^2} = \Omega^2 R$$

REWRITE:

$$S = S_0 \exp\left(-\frac{\Omega^2 z^2}{2A}\right)$$

SUB FOR A:

$$S = S_0 \exp\left(-\frac{\Omega^2 z^2 \mu}{2R_* T}\right)$$

THIS IS INDEED A GAUSSIAN.

E-FOLDING LENGTH:



$$\sqrt{\frac{2R_* T}{\Omega^2 \mu}}$$

RING IS THIN IF E-FOLDING $\ll R$.

$$\sqrt{\frac{2R_* T}{\Omega^2 \mu}} \ll R$$

$$T \ll \frac{R^2 \Omega^2 \mu}{2R_*}$$

IF $R = 1.5 \cdot 10^{11} \text{ m}$, $\Omega = \frac{2\pi}{365 \cdot 24 \cdot 60^2}$, $\mu = 2$ (FOR H, WHICH IS PROBABLY MOST ABUNDANT)

$$R_* = 8400,$$

THEN:

$$T \ll 10^5 \text{ K}$$

SEEMS A BIT HIGH.

3/ Poisson: $\nabla^2 \psi = 4\pi G S$

IN SPC:

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) = 4\pi G S$$

IN OUR CASE:

$$\frac{\partial \psi}{\partial r} \propto \frac{\partial}{\partial r} \frac{1}{\sqrt{r^2 + b^2}} \propto -\frac{1}{2} (r^2 + b^2)^{-\frac{3}{2}} 2r \propto (r^2 + b^2)^{-\frac{3}{2}} r$$

SUBSTITUTE IN:

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 (r^2 + b^2)^{-\frac{3}{2}} r \right) \propto 4\pi G S$$

$$\frac{\partial}{\partial r} \left(r^3 (r^2 + b^2)^{-\frac{3}{2}} \right) \propto S r^2$$

$$3r^2 (r^2 + b^2)^{-\frac{3}{2}} + r^3 \left(-\frac{3}{2} \right) (r^2 + b^2)^{-\frac{5}{2}} 2r \propto S r^2$$

$$\underbrace{3r^2 (r^2 + b^2)^{-\frac{3}{2}}}_{\propto \psi^3} - \underbrace{3r^4 (r^2 + b^2)^{-\frac{5}{2}}}_{\propto r^2 \psi^5} \propto S r^2$$

$$\psi^3 (1 - r^2 \psi^2) \propto S$$

$$\Rightarrow \underline{S \propto r^2 \psi^5 + O(\psi^3)}$$

IT IS SUSPICIOUS THAT I'VE DONE STH WRONG.

CONTINUE WITH: $S \propto \psi^5$

$$\frac{1}{S} \nabla \eta = -\nabla \psi$$

$$\frac{d\eta}{d\tau} = -S \frac{d\psi}{d\tau} \Rightarrow \frac{d\eta}{d\psi} = -S$$

$$\Rightarrow \frac{d\eta}{d\psi} \propto \psi^5 \Rightarrow \eta \propto \psi^6 \Rightarrow \eta \propto S^{\frac{6}{5}} = S^{1+\frac{1}{5}}$$

\Rightarrow POLYTROPIC EOS w/ $n=5$.

REST: PROBABLY UNDOABLE
WITHOUT GETTING
FIRST PART RIGHT.



$$\text{As } z \rightarrow 0, S \rightarrow S_0$$

$$\text{As } z \rightarrow \infty, S \rightarrow 0$$

$$S = \frac{S_0}{\cosh^2 \left(\sqrt{\frac{2\pi G S_0}{A}} z \right)} \quad \text{w/ } A = \frac{R^* T}{N}$$

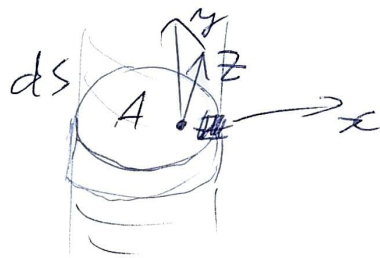
(FROM NOTES)

POISSON: $\nabla^2 \psi = 4\pi G S$

FROM UNIT AREA OF SLAB LOOKING FROM ABOVE:

$$\int \nabla \cdot \nabla \psi dV = 4\pi G \int S dV$$

$$\int \nabla \psi \cdot dS = 4\pi G \int S dV$$



WHEN AT z , ACCELERATION:

\ddot{z} = ACCELERATION FROM MASS ABOVE z — ACCELERATION FROM MASS BELOW z

GRAV. FIELD LINES ARE PARALLEL TO z , SO:


$$\int \nabla \psi \cdot dS = \nabla \psi \cdot A = -g A$$

ACCELERATION FROM MASS ABOVE z = $-\frac{1}{A} 4\pi G \int S dV$

$$= -\frac{1}{A} 4\pi G \int_z^\infty S A dz'$$

$$= -4\pi G \int_z^\infty S dz'$$

$$\begin{aligned}
&= -4\pi G \int_{-\infty}^{\infty} \frac{S_0}{z \cosh^2\left(\sqrt{\frac{2\pi G S_0}{A}} z'\right)} dz' \\
&= -4\pi G S_0 \tanh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right) \left[\frac{A}{2\pi G S_0} \right]_{-\infty}^{\infty} \\
&= -\sqrt{8\pi G A S_0} \left[1 - \tanh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right) \right]
\end{aligned}$$

ACCELERATION FROM
MASS BELOW $z =$  $-4\pi G \int_{-\infty}^z S dz'$

$$= -4\pi G \int_{-\infty}^z \frac{S_0}{\cosh^2\left(\sqrt{\frac{2\pi G S_0}{A}} z'\right)} dz'$$

$$\begin{aligned}
&= -\sqrt{8\pi G A S_0} \tanh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right) \left[\frac{A}{2\pi G S_0} \right]_{-\infty}^z \\
&= -\sqrt{8\pi G A S_0} \left[\tanh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right) + 1 \right]
\end{aligned}$$

TOTAL
ACCELERATION = ACCELERATION FROM MASS ABOVE z - ACCELERATION FROM MASS BELOW z
(IN $\oplus z$ DIR)

$$= 2 \sqrt{8\pi G A S_0} \tanh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right)$$

VERTICAL
VELOCITY = $\int \ddot{z} dz = 2 \sqrt{8\pi G A S_0} \ln\left(\cosh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right)\right) \cdot \left[\frac{A}{2\pi G S_0} \right] + C$

$$= 4A \ln\left[\cosh\left(\sqrt{\frac{2\pi G S_0}{A}} z\right)\right] + C$$

STAR IS AT REST AT z_0 , ~~IE~~ $\dot{z}=0$, SO:

$$C = -4A \ln \left[\cosh \left(\sqrt{\frac{2\pi G S_0}{A}} z_0 \right) \right]$$

$$\text{LET } a = \sqrt{\frac{2\pi G S_0}{A}}$$

WE HAVE:

$$\dot{z} = 4A \ln \cosh(az) - 4A \ln \cosh(az_0)$$

$$= 4 \frac{R_* T}{\mu} \ln \frac{\cosh(az)}{\cosh(az_0)}$$

WHICH IS NOT WHAT WE WANT,
BUT ~~VERY CLOSE~~ SEEMS TO BE CLOSE TO IT.

CHECK DIMENSIONS:

$$[R_*] = J/K$$

$$\left[\frac{R_* T}{\mu} \right] = \frac{J/K \cdot K}{Jg} = \frac{Jg \frac{m^2}{Jg}}{Jg} = \frac{m^2}{Jg^2} \Rightarrow \text{THE ABOVE RESULT MUST BE WRONG.}$$

5 / [EVEN IF THIS IS CORRECT (I HAVE DOUBTS)
I AM UNSURE WHAT I AM DOING]

ADIABATIC CASE $\Rightarrow \gamma = 1 + 1/n$

$$\Rightarrow \delta Q = 0$$

FIRST LAW:

$$\delta Q = dE + p dV \quad -dW$$

BECOMES:

$$dE = -p dV$$

LAGRANGIAN VIEW:

$$\frac{DE}{Dt} = \frac{DW}{Dt} + \frac{\delta Q}{dt}$$

(OMG, WHY IS IT THIS
LAST TERM $\delta Q/Dt$,
RATHER THAN $\delta Q/dt$)

$$\frac{DW}{Dt} = \frac{D}{Dt}(-pV) \Big|_p = -p \frac{D}{Dt} V = -p \frac{D}{Dt} \frac{1}{\rho} = \frac{1}{\rho^2} \frac{D\rho}{Dt}$$

$$\delta Q = 0 \Rightarrow \delta Q/dt = 0$$

$$\Rightarrow \frac{DE}{Dt} = \frac{DW}{Dt} \Rightarrow E = W + C$$

IF I STRETCH WHAT OUR NOTATION CAN BEAR:

$$DE = DW$$

$$= \frac{DW}{Dt} Dt = \frac{1}{\rho^2} D\rho \Rightarrow E = \int DE = \int_0^S \frac{1}{\rho^2} D\rho$$

ALL
LEVELS

$$= \int_0^s \frac{r}{s'^2} ds' \quad (?)$$

G/

$$\left. \begin{aligned} \mu &= K S^{1+1/n} \\ \mu &= \frac{R_*}{\rho} S T \end{aligned} \right\} \Rightarrow T_c = \frac{\mu K}{R_*} S_c^{1/n}$$

$$T \text{ const} \Rightarrow K \propto S_c^{-1/n}$$

$$M = \int_0^{r_{\text{MAX}}} 4\pi r^2 S dr \quad d\tau = \sqrt{\frac{K(1+n)}{4\pi G S_c^{1-1/n}}} d\xi$$

$$r^2 = \frac{K(1+n)}{4\pi G S_c^{1-1/n}}$$

~~$4\pi S_c$~~

$$= 4\pi \int_{\xi|_{r=0}}^{\xi|_{r_{\text{MAX}}}} \left(\frac{K(1+n)}{4\pi G S_c^{1-1/n}} \right)^{\frac{3}{2}} S_c \xi^2 d\xi$$

$$\Rightarrow M \propto S_c \left(S_c^{-1+1/n} \right)^{\frac{3}{2}} K^{\frac{3}{2}} \propto S_c^{\frac{1}{2}(\frac{3}{n}-1)} K^{\frac{3}{2}}$$

SUB IN FOR K:

$$\Rightarrow M \propto S_c^{\frac{1}{2}(\frac{3}{n}-1)} \left(S_c^{-\frac{1}{n}} \right)^{\frac{3}{2}} \propto S_c^{-1/2}$$

WE NOTE SOMEWHAT SURPRISEDLY THAT n DEPENDENCE HAS BEEN LOST.

$$\rho \propto S_c^{\frac{1}{2}(1-1/n)} K^{-\frac{1}{2}} \propto S_c^{\frac{1}{2}(1-1/n)} \left(S_c^{-\frac{1}{n}} \right)^{-\frac{1}{2}} \propto S_c^{\frac{1}{2}}$$

$$\left. \rho \right|_{r_{\text{MAX}}} = \text{CONSTANT} \Rightarrow r \propto S_c^{-\frac{1}{2}}$$

NOTING THAT: $M \propto S_c^{-1/2}$ & $r_{\text{MAX}} = r \propto S_c^{-1/2} \Rightarrow M \propto R$

7/ FLUID EQUATIONS:

$$\frac{\partial S}{\partial t} + \nabla \cdot (S \underline{u}) = 0$$

I (CONTINUITY)

$$\frac{\partial \underline{u}}{\partial t} + (\underline{u} \cdot \nabla) \underline{u} = -\frac{1}{\rho} \nabla p$$

II (MOMENTUM)

CONSIDER SMALL PERTURBATIONS:

$$S = S_0 + \Delta S \text{ WHERE } \Delta S = \Delta S_0 e^{i(kx - \omega t)} \quad \begin{matrix} A \\ B \end{matrix}$$

$$u = u_0 + \Delta u \text{ WHERE } \Delta u = \Delta u_0 e^{i(kx - \omega t)}$$

[I HAVE CONCEPTUAL DIFFICULTIES WITH WHAT Δu IS EXACTLY IN THE LAGRANGIAN VIEW; I THINK I CAN VISUALIZE EULERIAN Δu]

SUBSTITUTE A&B TO I:

$$\begin{aligned} & \frac{\partial}{\partial t} (S_0 + \Delta S) + \cancel{\frac{\partial}{\partial x} (S_0 + \Delta S)} \frac{\partial}{\partial x} ([S_0 + \Delta S][u_0 + \Delta u]) = \\ & = \frac{\partial \Delta S}{\partial t} + \frac{\partial}{\partial x} (S_0 \Delta u) + \frac{\partial}{\partial x} (u_0 \Delta S) + \frac{\partial}{\partial x} (\Delta S \Delta u) \\ & = \frac{\partial \Delta S}{\partial t} + S_0 \frac{\partial}{\partial x} \Delta u + u_0 \frac{\partial \Delta S}{\partial x} + \text{HIGHER ORDER TERM} \end{aligned}$$

NOTING THAT WE CAN SET $u_0 = 0$ BECAUSE
LET'S HAVE THE WAVE IN A FLUID
WHICH IS PREVIOUSLY ~~IN EQUILIBRIUM~~
AT REST.

OR u_0 IS 0 BECAUSE I AM TAKING LAGRANGIAN VIEW? SLIGHTLY CONFUSED.

$$\frac{\partial \Delta S}{\partial t} + S_0 \frac{\partial}{\partial x} \Delta u = 0 \quad (1)$$

SUBSTITUTE TO MOMENTUM EQ.:

$$\begin{aligned} & \frac{\partial}{\partial t} (u_0 + \Delta u) + (u_0 + \Delta u) \frac{\partial}{\partial x} (u_0 + \Delta u) \\ &= \frac{\partial \Delta u}{\partial t} + u_0 \frac{\partial}{\partial x} \Delta u + \text{HIGHER ORDER TERM} = 0 \\ & \quad \quad \quad \rightarrow 0 = -\frac{1}{S_0 + \Delta S} \frac{\partial}{\partial x} (\underbrace{u_0 + \Delta u}_p) \end{aligned}$$

EXPAND:

$$\frac{1}{S_0 + \Delta S} = \frac{1}{S_0} \frac{1}{1 + \frac{\Delta S}{S_0}} = S_0^{-1} \left(1 + \frac{\Delta S}{S_0} \right)^{-1} \approx S_0^{-1} \left(1 - \frac{\Delta S}{S_0} \right) \approx S_0^{-1}$$

WE GET:

$$\frac{\partial \Delta u}{\partial t} = -\frac{1}{S_0} \frac{\partial}{\partial x} \Delta p \quad (2)$$

$\frac{\partial}{\partial t}$ OF (1):

$$\frac{\partial^2 \Delta S}{\partial t^2} + S_0 \frac{\partial}{\partial t} \frac{\partial}{\partial x} \Delta u = 0$$

$$\frac{\partial^2 \Delta S}{\partial t^2} = -S_0 \frac{\partial}{\partial x} \frac{\partial}{\partial t} \Delta u$$

USING (2):

$$\frac{\partial^2 \Delta S}{\partial t^2} = -S_0 \left(-\frac{1}{S_0} \right) \frac{\partial^2}{\partial x^2} \Delta p$$

IF WE HAVE:

$$\Delta \eta = \left. \frac{d\eta}{dS} \right|_{S=S_0} \Delta S$$

CAN REWRITE:

$$\frac{\partial^2 \Delta S}{\partial t^2} = \left. \frac{d\eta}{dS} \right|_{S=S_0} \frac{\partial^2 \Delta S}{\partial x^2}$$

THIS HAS SOLUTIONS IN THE FORM:

$$\Delta S = \Delta S_0 e^{i(kx - \omega t)}$$

~~LET~~ LET: $\Delta u = \Delta u_0 e^{i(kx - \omega t)}$

~~(HMM, I HAVEN'T DERIVED WHY EXACTLY THIS FORM IS JUSTIFIED FOR Δu)~~

SUBSTITUTE THIS TO (1), ~~ALONG WITH $\Delta S = \Delta S_0 + \Delta u$~~

GET:

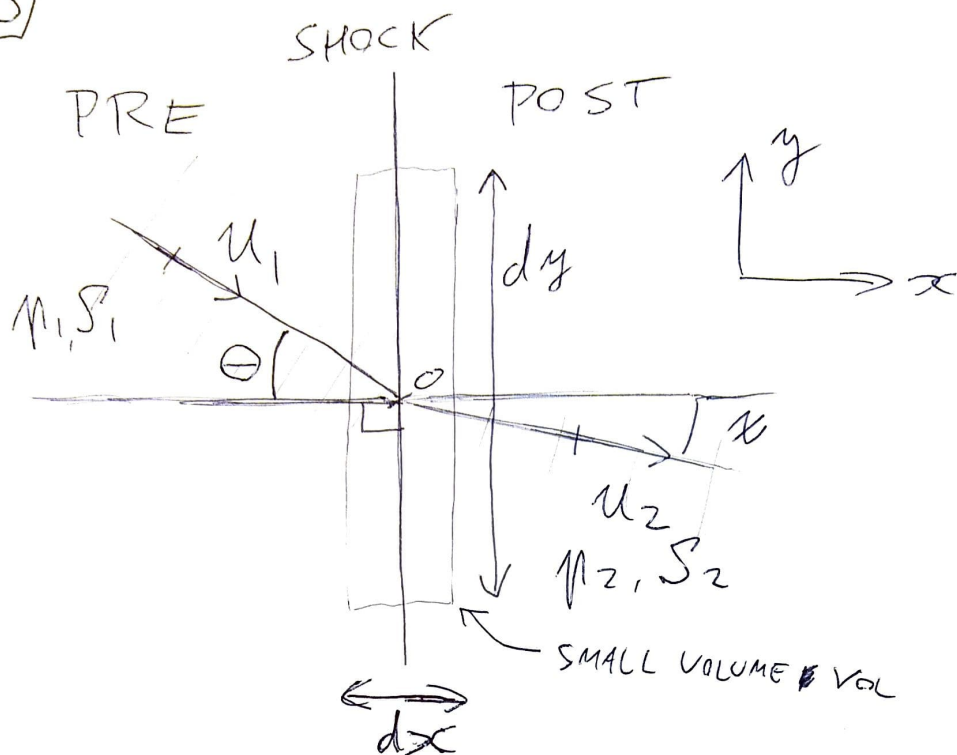
$$-i\omega \Delta S + S_0 i k \Delta u = 0$$

$$\Rightarrow \Delta u = \frac{\omega}{k} \frac{\Delta S}{S_0} = c_\Delta \frac{\Delta S}{S_0}$$

$$\text{if } \frac{\Delta S}{S_0} \ll 1 \Rightarrow \underline{\underline{c_\Delta \gg \Delta u}}$$

HOW DO I KNOW THAT ΔS & Δu HAS THE SAME FORM? MAYBE FROM THE NOTION THAT CHANGES IN DENSITY MUST BE DIRECTLY LINKED TO FLUID MOTION? CAN DO THE MATH BUT PHYSICAL UNDERSTANDING IS WEAK.

8



CONTINUITY EQUATION FOR VOL:

$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x}(S u_x) + \frac{\partial}{\partial y}(S u_y) = 0$$

$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x}(S u_x) + \frac{\partial}{\partial y}(S u_y) = 0$$

$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x}(S \cos \theta u_1) + \frac{\partial}{\partial y}(S \sin \theta u_1) = 0$$

INTEGRATE UP:

$$\int_{-\frac{dx}{2}}^{\frac{dx}{2}} \left[S dx + S u_x \right]_{x=-\frac{dx}{2}}^{x=\frac{dx}{2}} + S u_y = 0$$

$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x}(S u_x) + \frac{\partial}{\partial y}(S u_y) = 0$$

INTEGRATE UP:

$$\int \int \dot{S} dx dy + \underbrace{\int \int \frac{\partial}{\partial x} (S u_x) dx dy}_{\text{first term}} + \underbrace{\int \int \frac{\partial}{\partial y} (S u_y) dx dy}_{\text{second term}} = 0$$

IN STEADY
STATE
(NO PILING UP)

$$\begin{aligned} &= \int_{-\frac{dy}{2}}^{\frac{dy}{2}} \left[S u_x \right]_{x=-\frac{dx}{2}}^{x=\frac{dx}{2}} dy + S u_y \Big|_{-\frac{dy}{2}}^{\frac{dy}{2}} dx \\ &= \left[S u_x \right]_{-\frac{dx}{2}}^{\frac{dx}{2}} dy + S u_y \Big|_{-\frac{dy}{2}}^{\frac{dy}{2}} dx \end{aligned}$$

REWRITE:

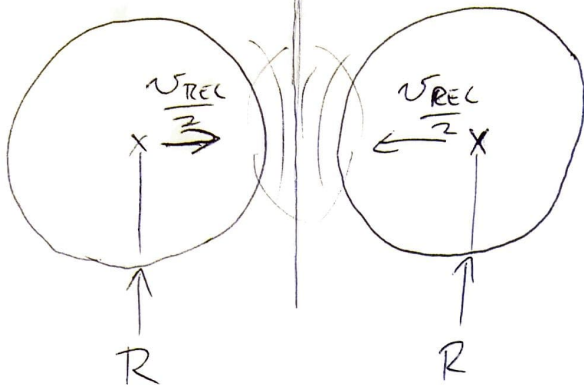
$$\left[S u_x \right]_{-\frac{dx}{2}}^{\frac{dx}{2}} dy + \left[S u_y \right]_{-\frac{dy}{2}}^{\frac{dy}{2}} dx = 0$$

I THINK I HAVE IMPLICITLY ASSUMED THAT
 $S = S(x)$ & NOT $S(x, y)$.

WHERE DO I EVALUATE THIS S THEN?

9

ZMF: ~~FRAGILE~~



$$t_{coll} = \frac{2R}{\frac{v_{REL}}{2}} = \frac{2 \cdot 3 \cdot 10^{16}}{4000} = \frac{3}{10^3} \cdot 10^{13} \text{ SEC} \approx \text{500} \text{ } \text{10.5 MYR}$$

~ 1 MYR

$$Q^- = 10^{-4} \frac{J}{22 \text{ kg}} \sim 3000 \frac{J}{\text{yr kg}}$$

↑
COMPARE THESE TWO:
ISOTHERMAL