Chapter 1: Feedback Linearisation Control

Chapter 1.1 Lie Derivative

% Input the extra parameters

```
% The plant is considered bellow
      close all;
      figure(1)
      imshow(imread("plant_siso_system.png"));
               the following state of the control o
      syms x1 x2 u % symbolic presentation
      fx=[x2;-sin(x1)];
      g=[0;1];
      x=[x1 x2];
      h=x1;
      LH=LieDerivative(h,x)
      LH = (1 \ 0)
      [lhf lhg]=solvelieder(LH,fx,g)
      1hf = \chi_2
      lhg = 0
Chapter 1.2 Feedback Linearisation Controller Examples
      clear all;clc
      disp('-----
      disp('The Nonlinear systems should ');
      The Nonlinear systems should
      disp('be written in the following form ');
      be written in the following form
      disp('State space equations x=f(x)+g(x)u');
      State space equations x=f(x)+g(x)u
      disp('----');
      % The your system contains
```

```
par=input('Parameters ','s');
eval(sprintf('syms %s',par));
parameters=sprintf('%s',par)

parameters =
```

parameters =

1×0 empty char array

```
%% Declare how many states and inputs
n=input('Number of states:=');
nin=input('Number of inputs:=');
x=sym(zeros(1,n));
u=sym(zeros(1,nin));
for j=1:n
    eval(sprintf('syms x%d',j))
    x(:,j)=sprintf('x%d',j);
end
for k=1:nin
    eval(sprintf('syms u%d',k));
    u(:,k)=sprintf('u%d',k);
end
% Enter the functions from the keyboard
f=input('The vector f(x):=','s');
g=input('The vector g(x):=','s');
Hc=input('The output variables:=','s');
%Represent all the functions
%f(x), g(x) and h(x) on a symbolic format
fx=str2sym(f);
g=str2sym(g);
Hc=str2sym(Hc); %
% Use the inoutfeedbacklinearization.m
% programm to generate the desired functions
[Lhf Lhg]=inoutfeedbacklinearization(fx,g,Hc,x)
```

Chapter 1.3 Illustrative examples

1.3.1 Aircraft altitude dynamics

```
% The plant is considered bellow
close all;
```

```
figure(1)
imshow(imread("aircraft_motion_equations.png"));
  Let us obtain the matrix of install contains of a small by the matrix one of a_{ij} , in Eq. ( ), the equations of that a_{ij}
       garley ex ex
  Were Explorage server along the sample of server goods for a set and other hands of server the first behavior of the
clear all;clc
disp('-----
   _____
disp('The Nonlinear systems should ');
The Nonlinear systems should
disp('be written in the following form ');
be written in the following form
disp('State space equations x=f(x)+g(x)u');
State space equations x=f(x)+g(x)u
disp('----');
% The your system contains
% Input the extra parameters
par=input('Parameters ','s');
eval(sprintf('syms %s',par));
parameters=sprintf('%s',par)
parameters =
  1×0 empty char array
%% Declare how many states and inputs
n=input('Number of states:=');
nin=input('Number of inputs:=');
x=sym(zeros(1,n));
u=sym(zeros(1,nin));
for j=1:n
     eval(sprintf('syms x%d',j))
     x(:,j)=sprintf('x%d',j);
end
for k=1:nin
     eval(sprintf('syms u%d',k));
     u(:,k)=sprintf('u%d',k);
end
% Enter the functions from the keyboard
f=input('The vector f(x):=','s');
```

```
g=input('The vector g(x):=','s');
 Hc=input('The output variables:=','s');
 %Represent all the functions
 %f(x), g(x) and h(x) on a symbolic format
 fx=str2sym(f);
 g=str2sym(g);
 Hc=str2sym(Hc); %
 % Use the inoutfeedbacklinearization.m
 % programm to generate the desired functions
 [Lhf Lhg]=inoutfeedbacklinearization(fx,g,Hc,x)
 The relative degree of h1
 equal:=2
 Lhf = 6x_1
 Lhg = -1
1.3.2 Asynchronous motor speed control
 % The plant is considered bellow
 close all;
 figure(1)
 imshow(imread("asynchronous_motor_dynamical_model.png"));
 clear all;clc
 disp('-----
```

```
disp('The Nonlinear systems should ');
```

The Nonlinear systems should

```
disp('be written in the following form ');
```

be written in the following form

```
disp('State space equations x=f(x)+g(x)u');
```

State space equations x=f(x)+g(x)u

```
disp('-----');
```

```
% The your system contains
% Input the extra parameters
par=input('Parameters ','s');
eval(sprintf('syms %s',par));
parameters=sprintf('%s',par)
```

parameters =
'T1 gamma K Tr p fm Jm Lr M Ls sigma'

```
%% Declare how many states and inputs
n=input('Number of states:=');
nin=input('Number of inputs:=');
x=sym(zeros(1,n));
u=sym(zeros(1,nin));
for j=1:n
    eval(sprintf('syms x%d',j))
    x(:,j)=sprintf('x%d',j);
end
for k=1:nin
    eval(sprintf('syms u%d',k));
    u(:,k)=sprintf('u%d',k);
end
% Enter the functions from the keyboard
f=input('The vector f(x):=','s');
g=input('The vector g(x):=','s');
Hc=input('The output variables:=','s');
%Represent all the functions
%f(x), g(x) and h(x) on a symbolic format
fx=str2sym(f);
g=str2sym(g);
Hc=str2sym(Hc); %
% Use the inoutfeedbacklinearization.m
% programm to generate the desired functions
[Lhf Lhg]=inoutfeedbacklinearization(fx,g,Hc,x)
```

The relative degree of h1 equal:=2 The relative degree of h2 equal:=2 Lhf =

$$\left(\frac{4 x_3}{\text{Tr}} - \frac{2 M x_1}{\text{Tr}}\right) \sigma_4 - \left(\frac{4 x_4}{\text{Tr}} - \frac{2 M x_2}{\text{Tr}}\right) \sigma_3 + \frac{2 M x_3 \sigma_2}{\text{Tr}} - \frac{2 M x_4 \sigma_1}{\text{Tr}}$$

$$\frac{\text{fm} \left(\frac{T_1}{\text{Jm}} + \frac{\text{fm } x_5}{\text{Jm}} + \frac{M p (x_1 x_4 - x_2 x_3)}{\text{Jm Lr}}\right)}{\text{Jm Lr}} - \frac{M p x_3 \sigma_1}{\text{Jm Lr}} - \frac{M p x_4 \sigma_2}{\text{Jm Lr}} - \frac{M p x_1 \sigma_3}{\text{Jm Lr}} - \frac{M p x_2 \sigma_4}{\text{Jm Lr}}\right)$$

where

$$\sigma_1 = \gamma x_2 - \frac{K x_4}{\text{Tr}} + K p x_3 x_5$$

$$\sigma_2 = \frac{K x_3}{\text{Tr}} - \gamma x_1 + K p x_4 x_5$$

$$\sigma_3 = p x_3 x_5 - \frac{x_4}{\text{Tr}} + \frac{M x_2}{\text{Tr}}$$

$$\sigma_4 = \frac{x_3}{\text{Tr}} + p \, x_4 \, x_5 - \frac{M \, x_1}{\text{Tr}}$$

Lhg =

$$\begin{pmatrix}
\frac{2 M x_3}{\text{Ls Tr }\sigma} & \frac{2 M x_4}{\text{Ls Tr }\sigma} \\
-\frac{M p x_4}{\text{Jm Lr Ls }\sigma} & \frac{M p x_3}{\text{Jm Lr Ls }\sigma}
\end{pmatrix}$$

Chapter 2 Sliding Mode Control

2.1 Sliding mode control examples for SISO Systems

2.1.1 Van der Pol system

```
% The plant is considered bellow
close all;
figure(1)
imshow(imread("van_der_pol_dynamical_equations.png"));
```

Observe the Vin day following depends on $\frac{b_1-c_2}{b_1-c_2} = c_1-c_2^2 - a_1^2c_2+c_2^2 - a_2^2$

```
clear all;clc
disp('----');
```

disp('The Nonlinear systems should be written in the following form');

```
disp('--Sliding Mode Controller for a class of Nonlinear systems--');
```

--Sliding Mode Controller for a class of Nonlinear systems--

```
disp(' State space equations x=f(x)+gu ');
```

State space equations x=f(x)+gu

```
disp('-----');
```

```
n=input('Number of states:=');
nin=input('Number of inputs:=');
x=sym(zeros(1,n));
u=sym(zeros(1,nin));
par=input('Parameters ','s');
eval(sprintf('syms %s',par));
parameters=sprintf('%s',par)
```

```
parameters =
'e'
```

```
for j=1:n
    eval(sprintf('syms x%d',j))
    x(:,j)=sprintf('x%d',j);
end
for k=1:nin
    eval(sprintf('syms u%d',k));
    u(:,k)=sprintf('u%d',k);
end
syms u1
f=input('The vector f(x):=','s');
g=input('The vector g(x):=','s');
Hc=input('The output variables:=','s');
f=str2sym(f);Hc=str2sym(Hc);g=str2sym(g);
[Lhf,Lhg,dh,L,u,r]=NonContSidFed(f,g,Hc,x,u1);
[Surf,dSurf,dd,K,Uc]=SlidingModeTerms(Hc,L,r,Lhg);
```

```
The sliding mode control law for SISO systems=: Uc = d3yr + x_1 + kp \, sgnS + k_1 \, (d2yr - x_2) + e \, x_2 \, \left(x_1^2 - 1\right) The Sliding mode surface:= Surf = d2yr - x_2 + k_1 \, (d1yr - x_1) The derivative of Sliding mode surface:= dsurf = d3yr + x_1 + k_1 \, (d2yr - x_2) + e \, x_2 \, \left(x_1^2 - 1\right)
```

2.1.1 DC motor angular position control

```
% The plant is considered bellow
close all;
```

```
figure(1)
imshow(imread("DC_motor_mathematical_model.png"));
clear all;clc
disp('-----
disp('The Nonlinear systems should be written in the following form');
The Nonlinear systems should be written in the following form
disp('--Sliding Mode Controller for a class of Nonlinear systems--');
--Sliding Mode Controller for a class of Nonlinear systems--
disp(' State space equations x=f(x)+gu ');
State space equations x=f(x)+gu
disp('----
                                                ----');
n=input('Number of states:=');
nin=input('Number of inputs:=');
x=sym(zeros(1,n));
u=sym(zeros(1,nin));
par=input('Parameters ','s');
eval(sprintf('syms %s',par));
parameters=sprintf('%s',par)
parameters =
'b J km ke L R'
for j=1:n
    eval(sprintf('syms x%d',j))
    x(:,j)=sprintf('x%d',j);
end
for k=1:nin
    eval(sprintf('syms u%d',k));
    u(:,k)=sprintf('u%d',k);
end
syms u1
f=input('The vector f(x):=','s');
g=input('The vector g(x):=','s');
Hc=input('The output variables:=','s');
f=str2sym(f);Hc=str2sym(Hc);g=str2sym(g);
[Lhf,Lhg,dh,L,u,r]=NonContSidFed(f,g,Hc,x,u1);
```

[Surf,dSurf,dd,K,Uc]=SlidingModeTerms(Hc,L,r,Lhg);

The sliding mode control law for SISO systems=: Uc =

$$d4yr + kp sgnS + k_1 \left(d3yr + \frac{b x_2}{J} - \frac{km x_3}{J} \right) + k_2 (d2yr - x_2) + \frac{km \left(\frac{R x_3}{L} + \frac{ke x_2}{L} \right)}{J} - \frac{b \left(\frac{b x_2}{J} - \frac{km x_3}{J} \right)}{J}$$

The Sliding mode surface:=
Surf =

$$d3yr + k_2 (d1yr - x_1) + k_1 (d2yr - x_2) + \frac{b x_2}{J} - \frac{km x_3}{J}$$

The derivative of Sliding mode surface:=
dSurf =

$$d4yr + k_1 \left(d3yr + \frac{b x_2}{J} - \frac{km x_3}{J} \right) + k_2 \left(d2yr - x_2 \right) + \frac{km \left(\frac{R x_3}{L} + \frac{ke x_2}{L} \right)}{J} - \frac{b \left(\frac{b x_2}{J} - \frac{km x_3}{J} \right)}{J}$$

2.2 Sliding mode control examples for MIMO Systems

2.2.1 Permanent magnet synchronous motor speed control

```
% The plant is considered bellow
close all;
figure(1)
imshow(imread("PMSM_dynamical_model.png"));
```

The dynamical model of PMSM [15] describing the electrical and mechanical part is given by:

$$\begin{split} \dot{x}_1 &= -\frac{R}{L_d} x_1 + p \frac{L_q}{L_d} x_2 x_3 + \frac{1}{L_d} u_d \\ \dot{x}_2 &= -\frac{R}{L_q} x_2 - p \frac{L_q}{L_d} x_1 x_3 - p \frac{\Phi}{L_q} + \frac{1}{L_q} u_q \\ \dot{x}_3 &= p \frac{\Phi_f}{J} x_2 - p \frac{L_q - L_d}{J} x_1 x_2 - \frac{f}{J} x_3 - \frac{1}{J} \tau \end{split}$$

Where x_1 and x_2 are the d and q axis stator currents respectively; x_3 is the mechanical speed of the motor; u_d and u_q are the d axis and q axis stator voltages respectively; R and $L_d = L_d$ are the winding resistance and inductance on the d and q axis. J is mechanical inertia of the motor; τ is the electrical torque.

The objective is to control the mechanical velocity x_3 and the x_1 current.

$$h(x) = \left[\begin{array}{c} h_1 \\ h_2 \end{array} \right] = \left[\begin{array}{c} x_1 \\ x_3 \end{array} \right]$$

```
clear all;clc
disp('----
disp('The Nonlinear systems should be written in the following form');
The Nonlinear systems should be written in the following form
disp('--Sliding Mode Controller for MIMO Nonlinear systems--');
--Sliding Mode Controller for MIMO Nonlinear systems--
disp(' State space equations x=f(x)+gu');
State space equations x=f(x)+gu
disp('----
                                                            -');
n=input('Number of states:=');
nin=input('Number of inputs:=');
x=sym(zeros(1,n));
u=sym(zeros(1,nin));
par=input('Parameters ','s');
eval(sprintf('syms %s',par));
parameters=sprintf('%s',par);
for j=1:n
eval(sprintf('syms x%d',j))
x(:,j)=sprintf('x%d',j);
end
for k=1:nin
eval(sprintf('syms u%d',k));
u(:,k)=sprintf('u%d',k);
end
f=input('The vector f(x):=','s');
g=input('The vector g(x):=','s');
h=input('The output variables:=','s');
f=str2sym(f);h=str2sym(h);g=str2sym(g);
[Lhf Lhg L r]=MIMOSlidingModeLieDer(f,g,h,x);
The relative degree of h1
equal:=1
The relative degree of h2
equal:=2
[e,der,Surf,dSurf,Uc]=MIMOSlidingModeController(h,L,r,Lhg);
The sliding mode control law for MIMO systems
-----Is given by Uc=:inv(Lhg)*(S)-----
-----The function S:=-----
```

$$d2yr_1 + kp_1 sgnS_1 + \frac{Rx_1}{Ld} - \sigma_2$$

$$d2yr_2 + kp_2 sgnS_2 + \frac{T_1}{J} + k_1 \left(d3yr_2 + \left(\frac{p\phi}{J} + \frac{px_1 (Ld - Lq)}{J} \right) \left(\frac{Rx_2}{Lq} + \frac{p\phi}{Ld} + \frac{Lq px_1x_3}{Ld} \right) - \frac{f \left(\frac{T_1}{J} + \frac{J}{J} \right)}{J} \right)$$

where

$$\sigma_1 = \frac{p \, x_1 \, x_2 \, (\text{Ld - Lq})}{J}$$

$$\sigma_2 = \frac{\text{Ld } p \, x_2 \, x_3}{\text{Lq}}$$

$$\sigma_3 = \frac{p \phi x_2}{J}$$

-----The Matrix Lhg:=-----

Lhg =

$$\begin{pmatrix}
\frac{1}{Ld} & 0 \\
\frac{p x_2 (Ld - Lq)}{J Ld} & \frac{p \phi}{J} + \frac{p x_1 (Ld - Lq)}{J} \\
\frac{Lq}{Lq}
\end{pmatrix}$$

The sliding mode control law for MIMO systems=: Uc =

$$\left(\frac{\int \operatorname{Lq} \left(d2 \operatorname{yr}_{2} + \operatorname{kp}_{2} \operatorname{sgn} \operatorname{S}_{2} + \frac{T_{1}}{J} + k_{1} \left(d3 \operatorname{yr}_{2} + \left(\frac{p \phi}{J} + \frac{p x_{1} (\operatorname{Ld} - \operatorname{Lq})}{J}\right) \left(\frac{R x_{2}}{\operatorname{Lq}} + \frac{p \phi}{\operatorname{Ld}} + \frac{\operatorname{Lq} p x_{1} x_{3}}{\operatorname{Ld}}\right) - \frac{f}{m}\right)}{p \phi + \operatorname{Ld} p x_{1} - \operatorname{Lq} p x_{1}}\right)$$

where

$$\sigma_1 = \frac{p \, x_1 \, x_2 \, (\text{Ld} - \text{Lq})}{J}$$

$$\sigma_2 = \frac{p \phi x_2}{J}$$

$$\sigma_3 = d2yr_1 + kp_1 sgnS_1 + \frac{R x_1}{Ld} - \sigma_4$$

$$\sigma_4 = \frac{\text{Ld } p \, x_2 \, x_3}{\text{Lq}}$$