

Combined Control Law & Estimator

- **Separation principle**
- **What is $D(z)$?**
- **Example**

Combined Control Law & Estimator

When all states are measured, the control law design is:

$$\begin{aligned} \mathbf{x}(k+1) &= \Phi \mathbf{x}(k) + \Gamma u(k) \\ y(k) &= \mathbf{H} \mathbf{x}(k) + J u(k) \end{aligned} \quad \Longrightarrow \quad u(k) = -\mathbf{K} \mathbf{x}(k)$$

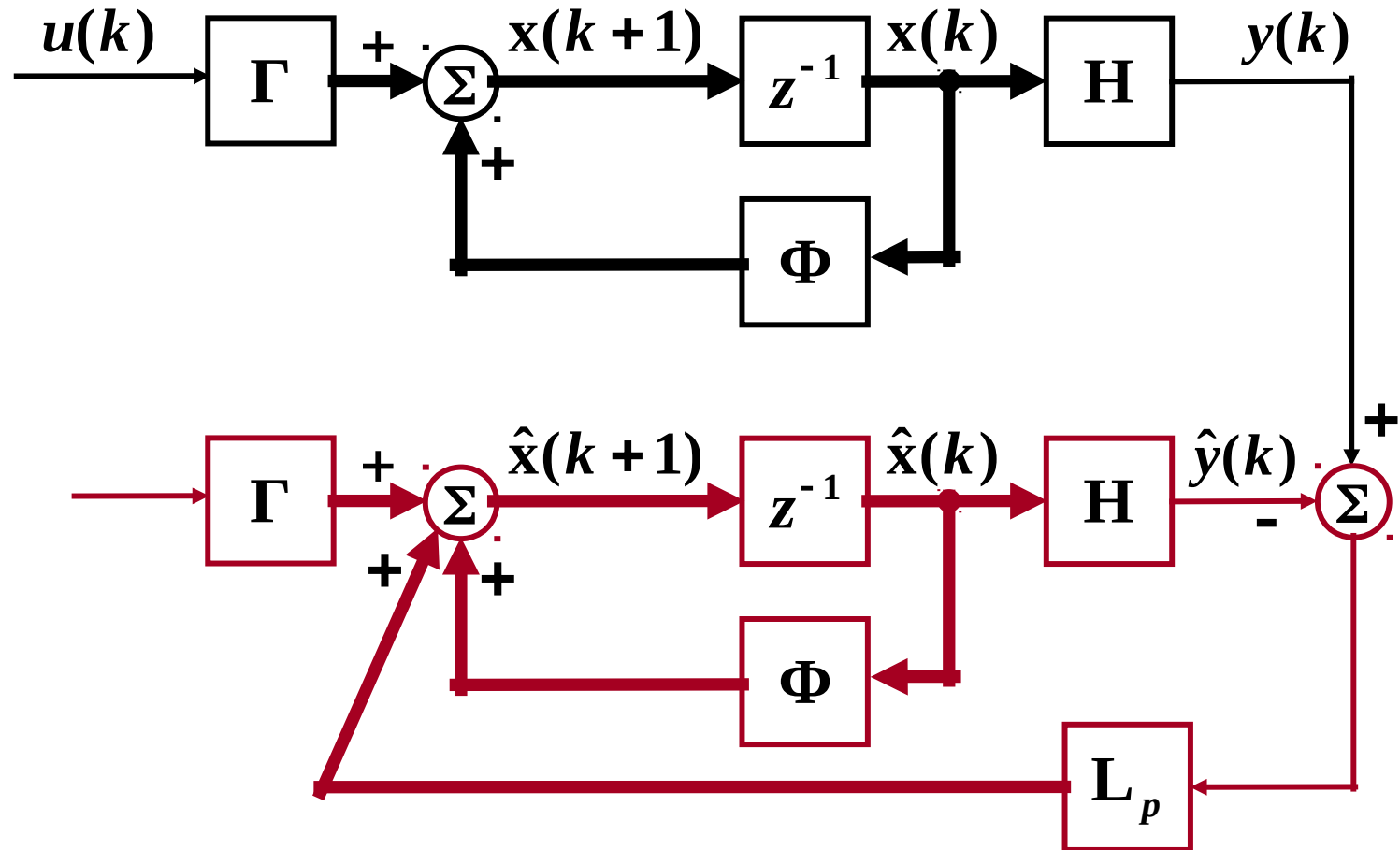
But if not all states are measured, or measurements are noisy, design a state estimator with desired estimator error dynamics:

$$\tilde{\mathbf{x}}(k+1) = (\Phi - \mathbf{L}_p \mathbf{H}) \tilde{\mathbf{x}}(k)$$

and then use: $u(k) = -\mathbf{K} \hat{\mathbf{x}}(k)$

- But state feedback was designed assuming \mathbf{x} is feedback, not $\hat{\mathbf{x}}$.
- Is it really okay to feedback $\hat{\mathbf{x}}$
- Or do we need to completely redesign \mathbf{K} , taking into account now that we are feeding back \mathbf{x} and not $\hat{\mathbf{x}}$?

Block Diagram of Combined Control & Estimator System



Analysis of the Combined Control & Estimator System with $\hat{\mathbf{x}}$ Feedback

$$\mathbf{x}(k+1) = \Phi \mathbf{x}(k) + \Gamma u(k) = \Phi \mathbf{x}(k) - \Gamma K \hat{\mathbf{x}}(k)$$

$$\mathbf{x}(k+1) = \Phi \mathbf{x}(k) - \Gamma K (\mathbf{x}(k) - \tilde{\mathbf{x}}(k))$$

along with estimator error dynamics equation:

$$\tilde{\mathbf{x}}(k+1) = (\Phi - L_p H) \tilde{\mathbf{x}}(k)$$

yields the overall system dynamics (control and estimator):

$$\begin{bmatrix} \mathbf{x}(k+1) \\ \tilde{\mathbf{x}}(k+1) \end{bmatrix} = \begin{bmatrix} \Phi - \Gamma K & \Gamma K \\ 0 & \Phi - L_p H \end{bmatrix} \begin{bmatrix} \mathbf{x}(k) \\ \tilde{\mathbf{x}}(k) \end{bmatrix}$$

Overall Closed-Loop Characteristic Equation

$$\det(zI - F) = 0$$

$$\det \begin{bmatrix} zI - \Phi + \Gamma K & -\Gamma K \\ 0 & zI - \Phi + L_p H \end{bmatrix} = 0$$

$$\det(zI - \Phi + \Gamma K) \det(zI - \Phi + L_p H) = 0$$

Poles of the overall closed-loop system:

desired control poles + desired estimator poles

Separation Principle

Controller design and estimator design can be carried out independently.

What is $D(z)$?

$$\hat{\mathbf{x}}(k+1) = \Phi \hat{\mathbf{x}}(k) + \Gamma u(k) + \mathbf{L}_p (y(k) - \hat{y}(k))$$

$$\begin{aligned} \hat{\mathbf{x}}(k+1) &= (\Phi - \Gamma \mathbf{K} - \mathbf{L}_p \mathbf{H}) \hat{\mathbf{x}}(k) + \mathbf{L}_p y(k) \\ u(k) &= -\mathbf{K} \hat{\mathbf{x}}(k) \end{aligned}$$

Compare with standard state-space equation:

$$\begin{aligned} \mathbf{x}(k+1) &= \Phi \mathbf{x}(k) + \Gamma u(k) \\ y(k) &= \mathbf{H} \mathbf{x}(k) + J u(k) \end{aligned}$$

$$G(z) = \frac{b(z)}{a(z)} = \mathbf{H} (z\mathbf{I} - \Phi)^{-1} \Gamma + J$$

Compensator transfer function is then:

$$D(z) = \frac{U(z)}{Y(z)} = -\mathbf{K} (z\mathbf{I} - \Phi + \Gamma \mathbf{K} + \mathbf{L}_p \mathbf{H})^{-1} \mathbf{L}_p$$

Comments

- Poles and zeros of $D(z)$ are never specified in the state-space compensator (controller & estimator) design.
- The compensator $D(z)$ itself may in fact be unstable!
 - Overall closed-loop system of plant and compensator is stable for stable controller and estimator designs, but the compensator itself may have unstable poles.
- The transfer function $D(z)$ from the state-space controller/estimator design has similarities with compensators designed using Root Locus or Frequency Response/Bode methods.

Example

$$G(s) = \frac{1}{s(s+1)} = \frac{Y(s)}{U(s)} \xrightarrow{T=2\text{sec}} G(z) = 1.135 \frac{z + 0.523}{(z - 1)(z - 0.135)}$$

$$\Phi = \begin{bmatrix} 1 & 1 - e^{-T} \\ 0 & e^{-T} \end{bmatrix} = \begin{bmatrix} 1 & 0.865 \\ 0 & 0.135 \end{bmatrix},$$

$$\Gamma = \begin{bmatrix} T + e^{-T} - 1 \\ 1 - e^{-T} \end{bmatrix} = \begin{bmatrix} 1.135 \\ 0.865 \end{bmatrix},$$

$$H = \begin{bmatrix} 1 & 0 \end{bmatrix}, \quad J = 0$$

State feedback: $\zeta = 0.3, \quad \omega_n = 1 \text{ rad/sec}$
 $\Rightarrow K = \begin{bmatrix} 0.9623 & 0.4693 \end{bmatrix}$

Estimator: $\zeta = 0.5, \quad \omega_n = 1.5 \text{ rad/sec} \Rightarrow L_p = \begin{bmatrix} 1.5173 \\ 0.1385 \end{bmatrix}$

What is the compensator transfer function $D(z)$?

$$D(z) = \frac{-1.53z + 0.147}{z^2 + 1.88z + 0.76} = \frac{-1.53(z - 0.096)}{(z + 1.296)(z + 0.585)}$$

