

# Bode Design and Lead, Lag, & PID Compensators

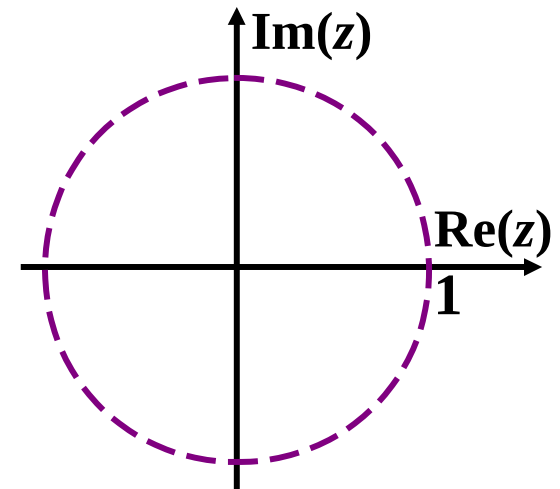
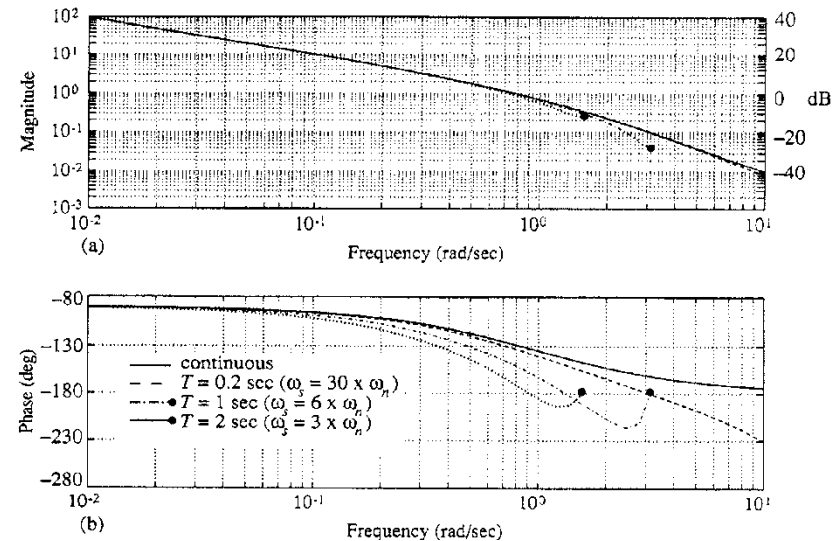
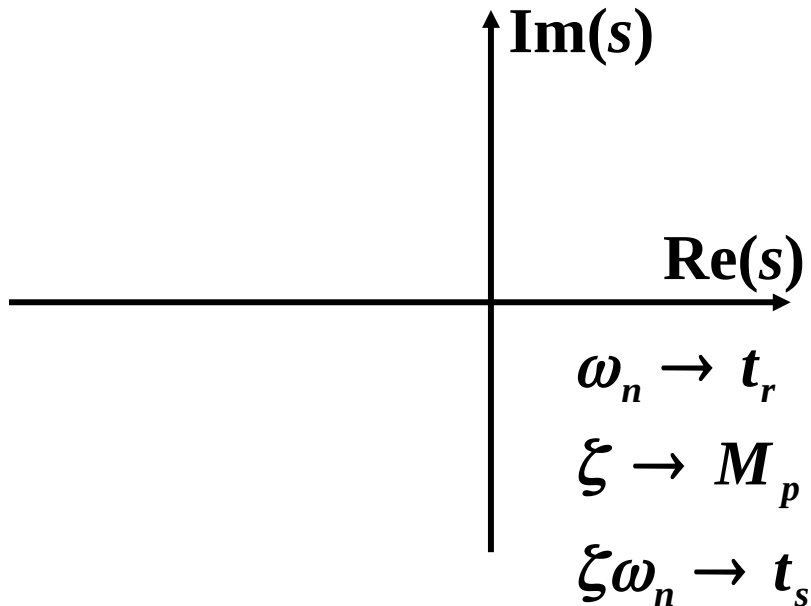
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- Discrete-time compensator design using Bode plots
- $Z$ -plane Bode plotting rule of thumb
- Lead and lag compensators
  - Example
- PID control
  - P, D, PD, I, PI control

# Discrete-Time Compensator Design using Bode Plots

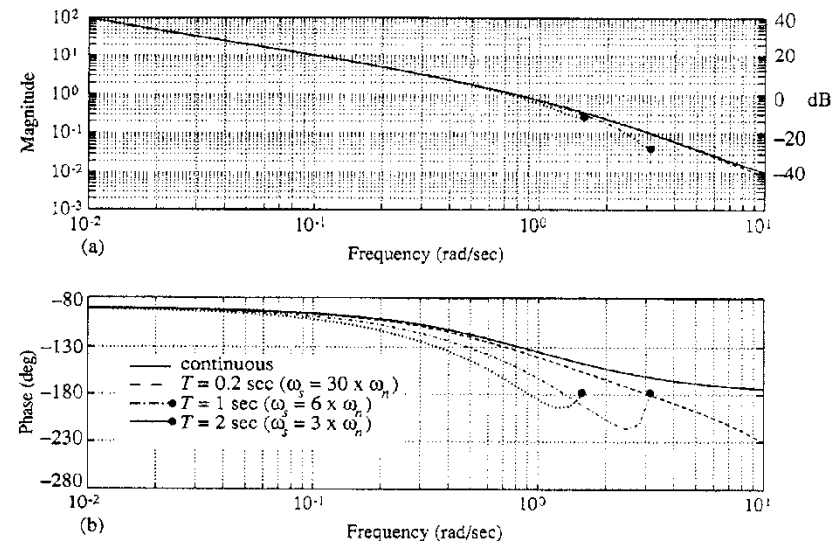
What is correspondence of previous design parameters with quantities determined from Bode plots?

For a 2<sup>nd</sup>-order continuous-time system w/o finite zeros:



# Revisiting Example 7.8 yet again:

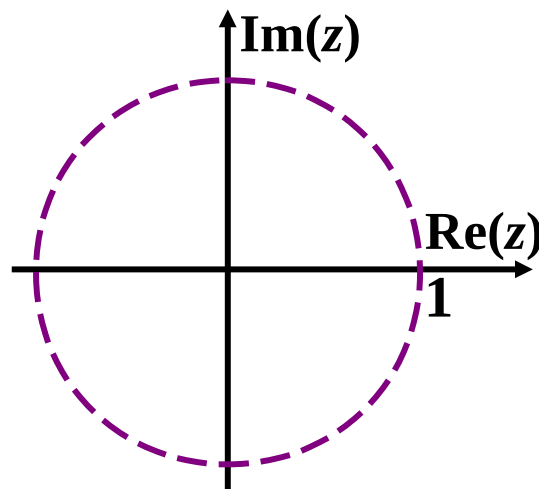
$$H_{CL} = \frac{1}{1 + \frac{1}{s(s+1)}} =$$



See Figure 7.22 of text.

# Z-Plane Bode Plotting Rule of Thumb

- Equivalent idea of “breakpoint” in plotting discrete Bode plots:
  - Magnitude will change slope at a frequency when  $\omega T$ , the angular position on the unit circle in radians, has the same value as the fractional distance of the singularity on the real axis to  $z = +1$ 
    - Rule of thumb accurate for  $\omega T$  relatively small.



For instance,

$$D(z) = K \frac{z - z_1}{z - p_1}$$

$$D(e^{j\omega T}) = K \frac{e^{j\omega T} - z_1}{e^{j\omega T} - p_1}$$

For  $\omega T$  small  $\implies$

$$D(e^{j\omega T}) \approx$$

$$D(e^{j\omega T}) = K \frac{(1 - z_1) + j\omega T}{(1 - p_1) + j\omega T}$$

**Breakpoints for numerator and denominator occur at  $\omega$  where the real and imaginary parts are equal:**

$$\text{Numerator : } |1 - z_1| = \omega T$$

$$\text{Denominator : } |1 - p_1| = \omega T$$

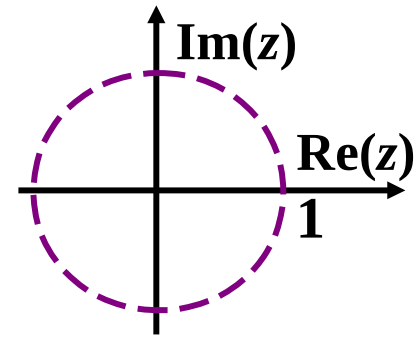
**Very accurate for  $\omega T \leq 0.1$  rad**

**Moderately accurate for  $\omega T \leq 0.8$  rad**

# Lead and Lag Compensators

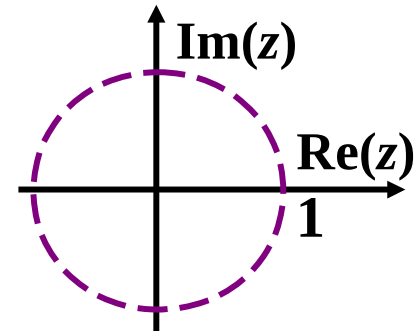
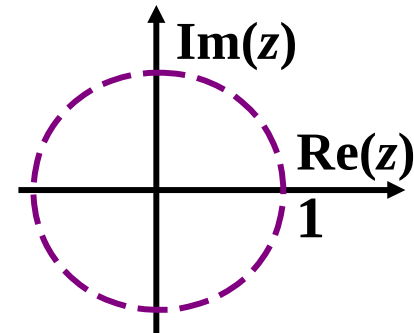
## Lead Compensation

$$D(z) = K \frac{z - z_1}{z - p_1}, \quad z_1 > p_1$$



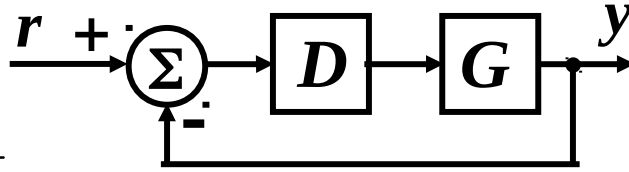
## Lag Compensation

$$D(z) = K \frac{z - z_1}{z - p_1}, \quad z_1 < p_1$$



**Example**

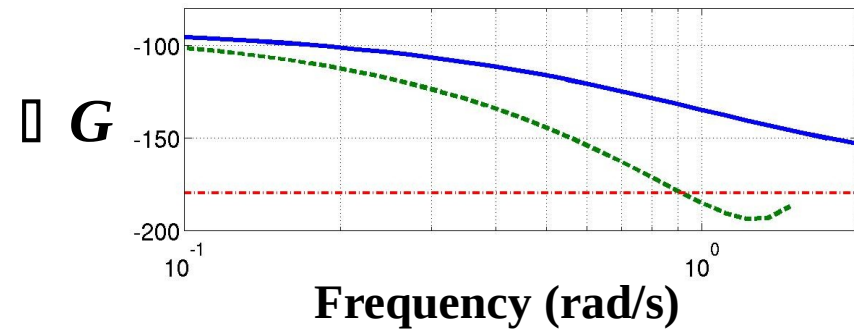
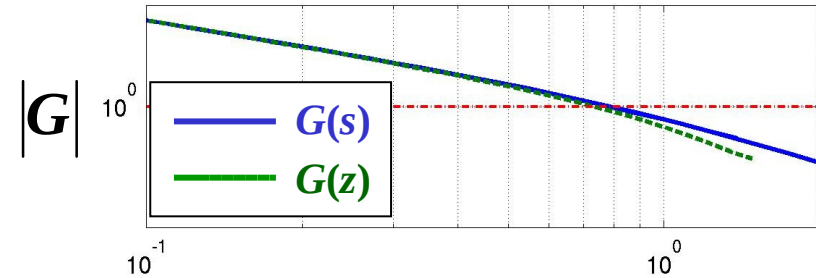
$$G(s) = \frac{1}{s(s+1)}$$



$T = 2$  sec:

$$G(z) = 1.135 \frac{z + 0.523}{(z - 1)(z - 0.135)}$$

Uncompensated ( $D(z) = 1$ ):



Type 1 system:  $K_v = \lim_{z \rightarrow 1} \frac{(z - 1)D(z)G(z)}{Tz} =$

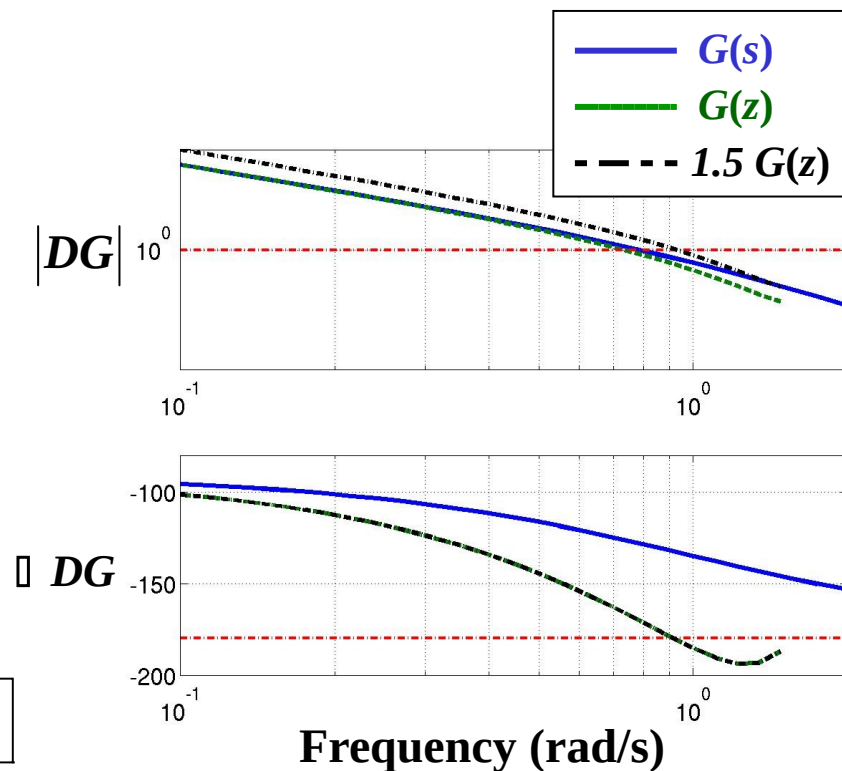
$K_v \approx \implies e_{ss}$  to unit ramp



Design a compensator so  $e_{ss}$  to unit ramp  $< 2/3$ .

$$\text{If } D(z) = K = \frac{3}{2} \implies K_v = \lim_{z \rightarrow 1} \frac{(z-1)D(z)G(z)}{Tz} =$$

Are there any problems with doing this?



Useful MATLAB command: `margin`

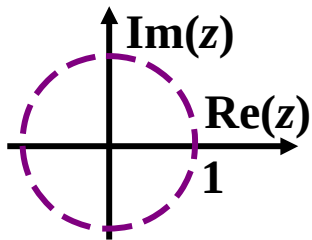
Design a lag compensator to achieve  $e_{ss}$  to unit ramp  $< 2/3$ .

$$D_{lag}(z) = K \frac{z - z_1}{z - p_1}, \quad z_1 < p_1$$

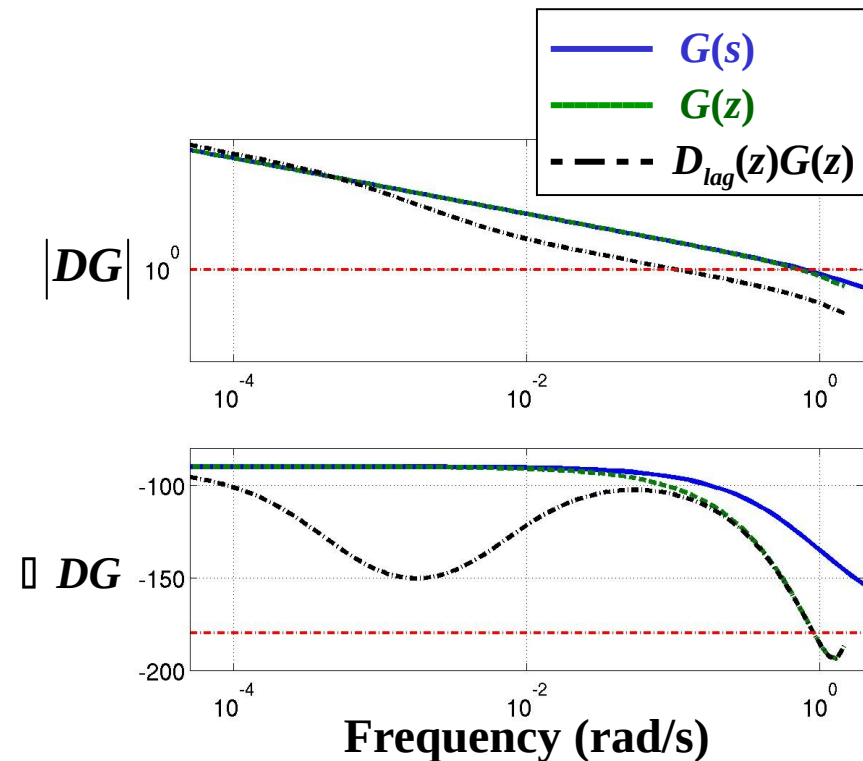
Choose pole at  $1 - \omega T$  such that

Choose zero at  $1 - \omega T$  such that

$$D_{lag}(z) = 0.1071 \frac{z - 0.9870}{z - 0.9991}$$



$e_{ss}$  to unit ramp  $< 2/3$ .



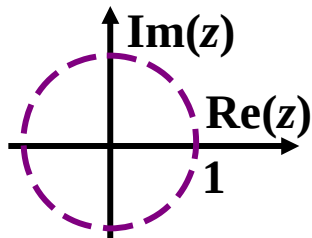
Design a lead compensator to achieve  $t_r < 2$  sec and  $M_p < 40\%$ .

$$D_{lead}(z) = K \frac{z - z_1}{z - p_1}, \quad z_1 > p_1$$

Choose pole at  $1 - \omega T$  such that

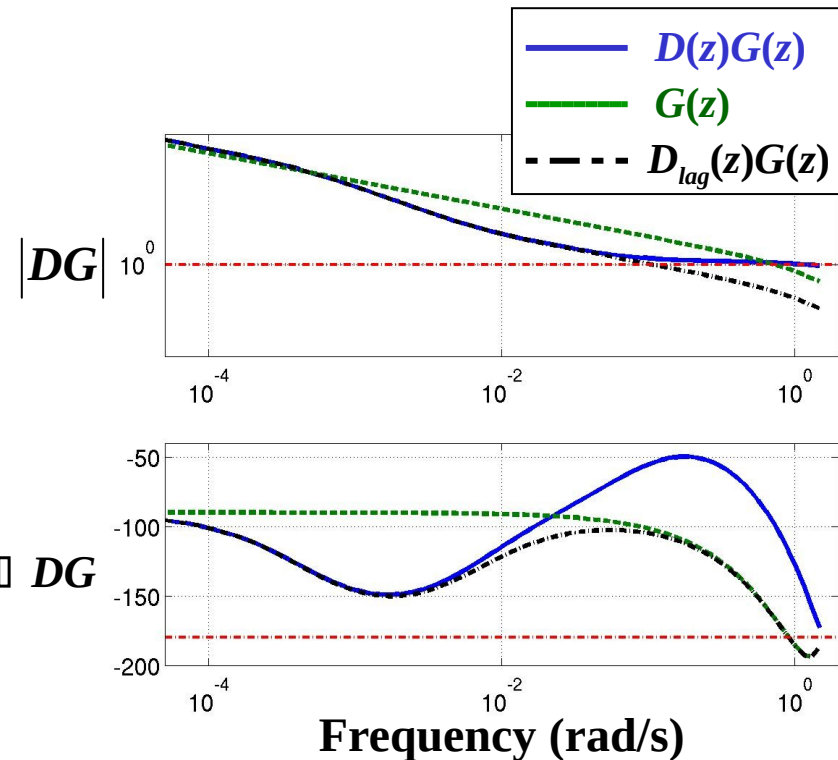
Choose zero at  $1 - \omega T$  such that

$$D_{lead}(z) = 10 \frac{z - 0.8517}{z + 0.4830}$$

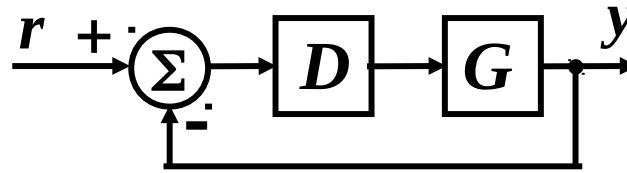


$$D(z) = D_{lag}(z) D_{lead}(z)$$

$$= 1.071 \frac{z - 0.9870}{z - 0.9991} \frac{z - 0.8517}{z + 0.4830}$$



# P and D Control



## P: Proportional Control

Continuous:  $u(t) = Ke(t) \implies D(s) = K$

Discrete:  $u(k) = Ke(k) \implies D(z) = K$

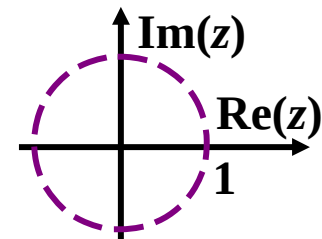
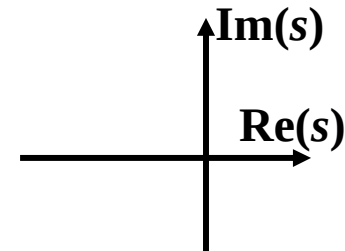
Increases  $K_p$  or  $K_v$  (decreases  $e_{ss}$ ), but can destabilize the system.

## D: Derivative Control

Continuous:  $u(t) = KT_D \dot{e}(t) \implies D(s) = KT_D s$

Discrete: approximate derivative using 1<sup>st</sup>-order difference

$$u(k) = KT_D \left[ \frac{e_k - e_{k-1}}{T} \right] \implies D(z) = KT_D \left[ \frac{1 - z^{-1}}{T} \right]$$



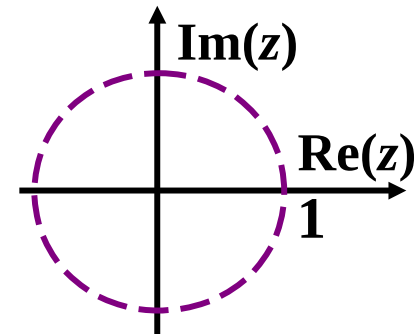
Increases damping (decreases overshoot).

# PD Control

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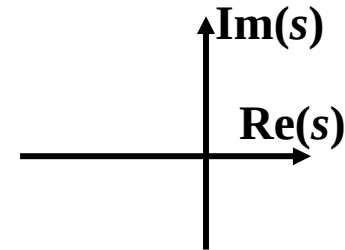
$$D(z) = K + KT_D \frac{z - 1}{Tz}$$

$$D(z) = K_D \frac{z - \alpha}{z}, \quad (0 < \alpha < 1)$$



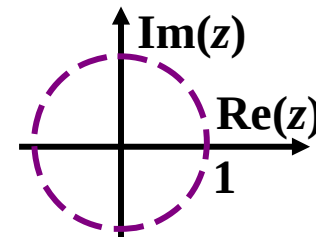
# I: Integral Control

**Continuous:**  $u(t) = \frac{K}{T_I} \int_{t_0}^t e(\tau) d\tau \implies D(s) = \frac{K}{T_I s}$



**Discrete:** one way is to approximate integral using backward rectangular rule

$$u(k) = u(k-1) + \frac{K}{T_I} T e(k) \implies D(z) = \frac{KT}{T_I(1 - z^{-1})}$$



**Decreases  $e_{ss}$ .**

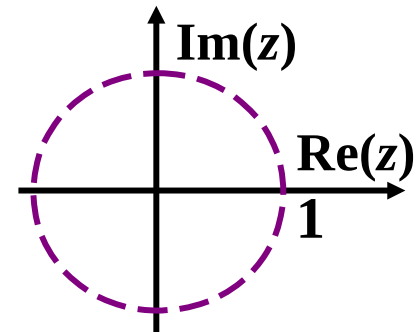
$$K_v = \lim_{z \rightarrow 1} \frac{(z-1)D(z)G(z)}{Tz}, \quad e_{ss} = \frac{1}{K_v}$$

# PI Control

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$$D(z) = K \left[ 1 + \frac{Tz}{T_I(z - 1)} \right]$$

$$D(z) = K_I \frac{z - \beta}{z - 1}, \quad (0 < \beta < 1)$$



# PID Control

$$D(z) = K \left[ 1 + \frac{Tz}{T_I(z - 1)} + T_D \frac{z - 1}{Tz} \right]$$

In general:

$T_I$	↓	⇒	$e_{ss}$	↓	$(t_r ↓)$
$K$	↑	⇒	$e_{ss}$	↓	$(t_r ↓)$
$T_D$	↑	⇒	$M_p$	↓	$(t_r ↓)$