

M263C, HW#3

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$$1. a) L(s) = K_p \frac{1+sT_p}{s} \cdot \frac{k_m}{1+sT_m} \cdot \frac{1}{s} = \frac{K_m K_p (1+sT_p)}{s^2 (1+sT_m)}$$

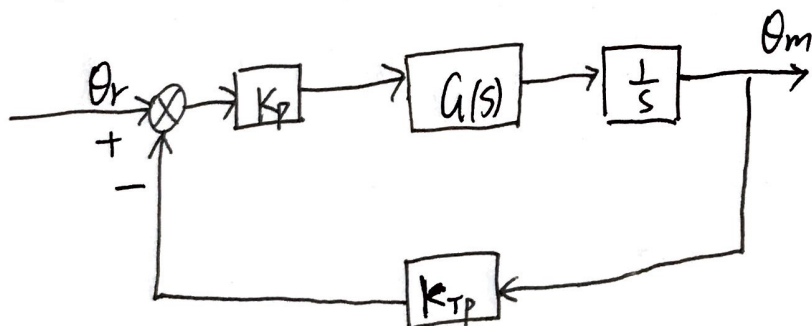
$$b) H(s) = K_{Tp}$$

$$c) \frac{\theta_m(s)}{\theta_r(s)} = \frac{L(s)}{1+L(s)H(s)} = \frac{\frac{K_m K_p (1+sT_p)}{s^2 (1+sT_m)}}{1 + \frac{K_m K_p (1+sT_p) K_{Tp}}{s^2 (1+sT_m)}}$$

$$= \frac{K_m K_p (1+sT_p)}{s^2 (1+sT_m) + K_m K_p K_{Tp} (1+sT_p)}$$

$$d) \frac{\theta_m(s)}{D(s)} = \frac{-\frac{K_m}{1+sT_m} \cdot \frac{1}{s}}{\frac{1}{1+L(s)H(s)}} \cdot \frac{R_a}{K_b} = \frac{R_a K_m \cdot s}{s^2 (1+sT_m) K_b + K_m K_p K_{Tp} (1+sT_p)}$$

2. a) simplify the diagram to be



$$G(s) = \frac{K_v \cdot \frac{1+sT_v}{s} \cdot \frac{K_m}{1+sT_m}}{1 + \frac{K_v (1+sT_v) K_m K_{Tv}}{s(1+sT_m)}} = \frac{K_v K_m (1+sT_v)}{s(1+sT_m) + K_v K_m K_{Tv} (1+sT_v)}$$

$$\frac{\theta_m}{\theta_r} = \frac{K_p G(s) \frac{1}{s}}{1 + K_p G(s) \frac{1}{s} \cdot K_{TP}}$$

$$K_{TP}=1, K_{TV}=1,$$

$$F_m \ll \frac{K_v K_t}{R_a}$$

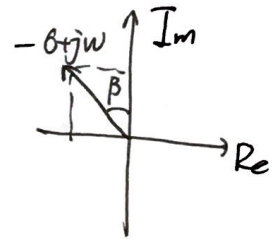
$$\therefore K_m = \frac{1}{K_v} = 2 \text{ rad / (V.s)}, T_m = \frac{K_a Z_m}{K_v K_t} = 7.2 \text{ s}$$

$$\therefore G(s) = \frac{2K_v}{s+2K_v}$$

$$\therefore \frac{\theta_m(s)}{\theta_r(s)} = \frac{\frac{2K_p K_v}{s(s+2K_v)}}{1 + \frac{2K_p K_v}{s(s+2K_v)}} = \frac{2K_p K_v}{s^2 + 2K_v s + 2K_p K_v}$$

b)

$$\begin{cases} 2K_v = 2\xi \omega_n \\ 2K_p K_v = \omega_n^2 \end{cases} \Rightarrow \begin{matrix} K_v = 8 \\ K_p = 25 \end{matrix}$$



$$\text{pole: } \therefore \sin \beta = \xi$$

$$\therefore \frac{a}{\omega_n} = 0.4, \quad a = 8$$

$$\omega = \sqrt{\omega_n^2 - a^2} = \sqrt{400 - 64} = 18.33$$

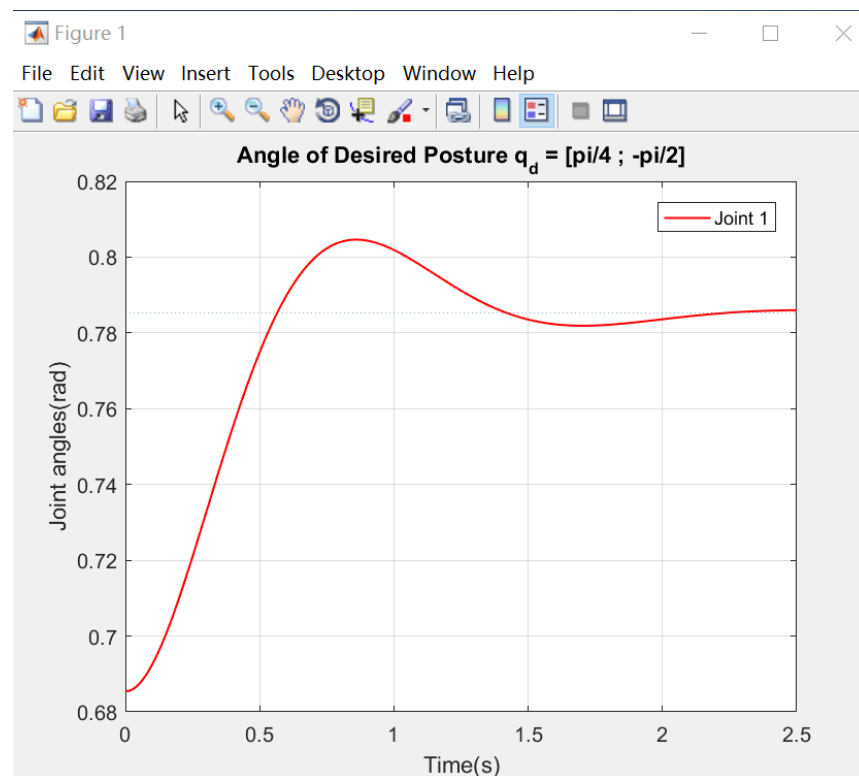
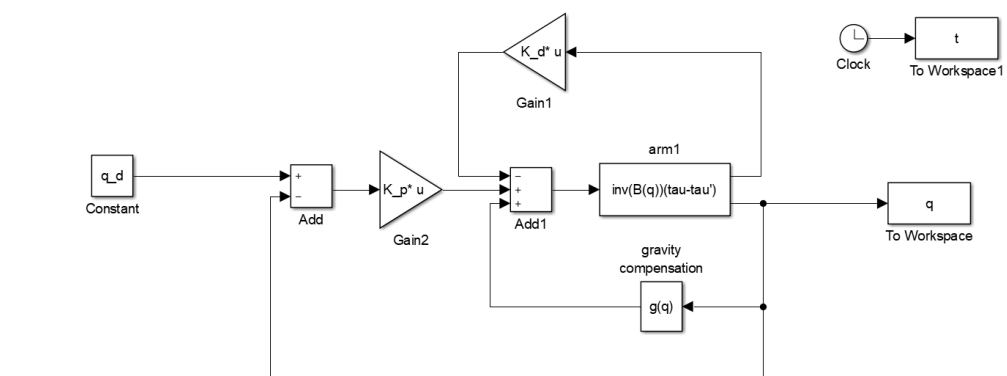
$$\therefore \text{poles: } -8 \pm j18.33$$

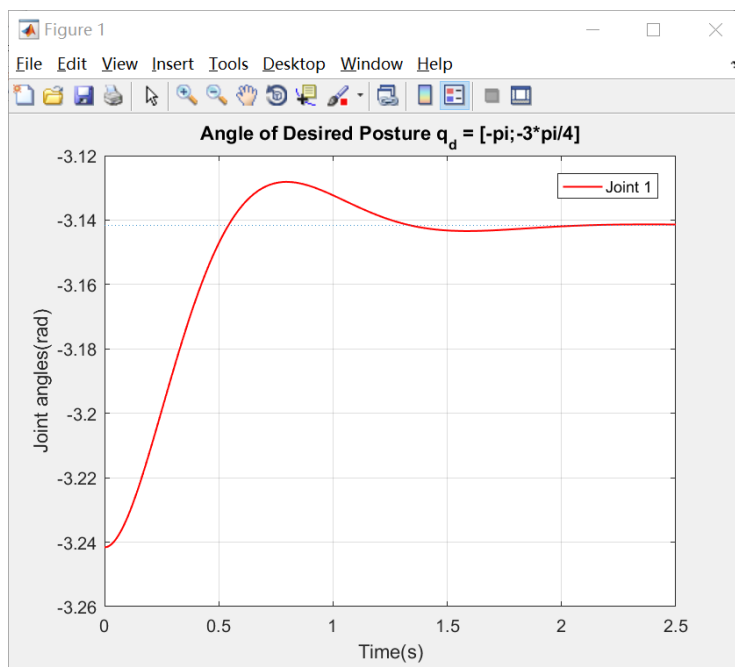
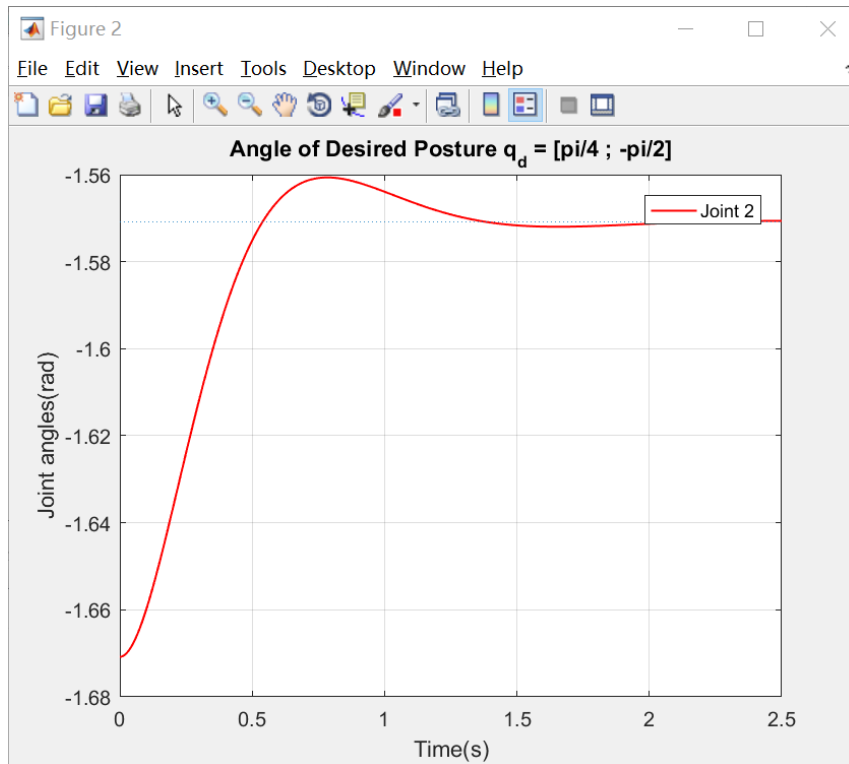
$$c) \quad X_R = K_p K_{TP} K_v = 200$$

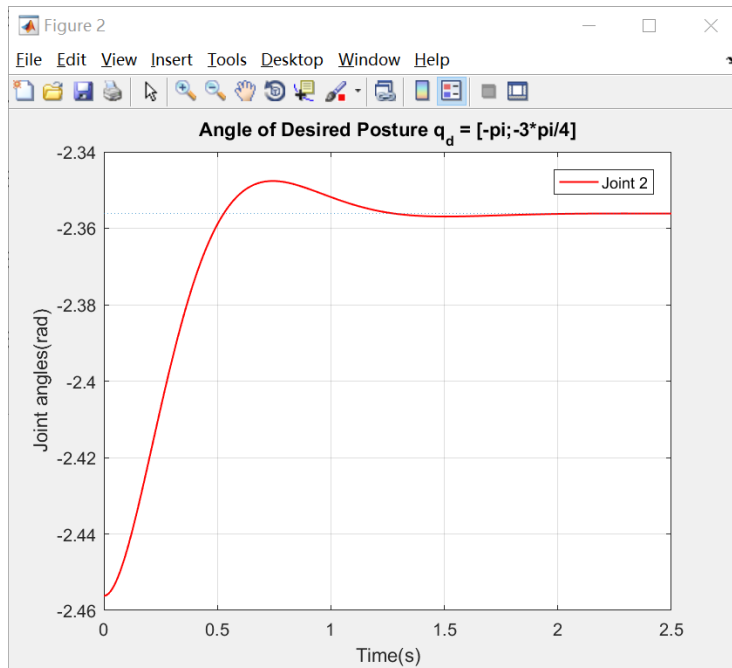
$$T_R = \max \left\{ T_m, \frac{1}{\xi \omega_n} \right\} = 7.2 \text{ s}$$

\therefore We cannot decrease the output recovery time

3.







```
%*****
% VERONICA J. SANTOS
% 4/20/18
% HW3_main.m
%
% This script file was originally created by L. Villani, G. Oriolo, and
% B. Siciliano in Feb. 2009. It has been modified for MAE 263C HW #3.
%*****

% Variable initialization
clear all;
global a k_r1 k_r2 pi_m pi_l

% load manipulator dynamic parameters without load mass
param;
pi_l = pi_m;

% gravity acceleration
g = 9.81;

% friction matrix
K_r = [k_r1,0;0,k_r2];
F_v = K_r*[0.01,0;0,0.01]*K_r;

%
Tc = 0.001;
```

```

% controller gains
K_p = 3700 * eye(2);
K_d = 750 * eye(2);

% desired position
%   q_d = [pi/4;-pi/2];
q_d = [-pi;-3*pi/4];

% initial position
q_i = q_d-0.1;

% duration of simulation
t_d = 2.5;

% sample time for plots
Ts = Tc

% sim hw3
%
% figure(1)
% plot(t,q(:,1),'LineWidth',1,'Color','r'); grid on
% line([0,2.5],[q_d(1),q_d(1)],'linestyle',':');grid on
% xlabel('Time(s)');
% ylabel('Joint angles(rad)');
% title('Angle of Desired Posture q_d = [pi/4 ; -pi/2]')
% legend('Joint 1');
%
% figure(2)
% plot(t,q(:,2),'LineWidth',1,'Color','r'); grid on
% line([0,2.5],[q_d(2),q_d(2)],'linestyle',':');grid on
% xlabel('Time(s)');
% ylabel('Joint angles(rad)');
% title('Angle of Desired Posture q_d = [pi/4 ; -pi/2]')
% legend('Joint 2')

sim hw3

figure(1)
plot(t,q(:,1),'LineWidth',1,'Color','r'); grid on
line([0,2.5],[q_d(1),q_d(1)],'linestyle',':');grid on
xlabel('Time(s)');
ylabel('Joint angles(rad)');
title('Angle of Desired Posture q_d = [-pi;-3*pi/4]')
legend('Joint 1');

```

```
figure(2)
plot(t,q(:,2),'LineWidth',1,'Color','r'); grid on
line([0,2.5],[q_d(2),q_d(2)],'linestyle',':');grid on
xlabel('Time(s)');
ylabel('Joint angles(rad)');
title('Angle of Desired Posture q_d = [-pi;-3*pi/4]')
legend('Joint 2')
```