

ME 263C, HW#1.

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1. a) consider the mechanical balances at the motor side and the load side:

$$C_m = I_m \dot{\omega}_m + F_m \omega_m + f r_m \quad (1)$$

$$f r = I \dot{\omega} + F \omega + C_l \quad (2)$$

$$\therefore C_m = \left( I_m + \frac{I}{k_r^2} \right) \dot{\omega}_m + \left( F_m + \frac{F}{k_r^2} \right) \omega_m + \frac{C_l}{k_r}$$

$$\text{let } I_{eq} = I_m + \frac{I}{k_r^2}, \quad F_{eq} = F_m + \frac{F}{k_r^2}, \quad C_l = mgl \sin \theta$$

$\therefore$  The inertia of the pair of reduction gears and viscous friction is negligible

$$F_m = 0.$$

$$\therefore C_m = \left( I_m + \frac{I_{load}}{k_r^2} \right) \dot{\omega}_m + \frac{C_l}{k_r}$$

$$I_{total} = I_m + \frac{I_{load}}{k_r^2}$$

$$\text{i) If } k_r = 5, \quad I_{total} = 0.03 + \frac{1}{25} \left( \frac{3 \times 0.5^2}{3} + 2 \times 0.5^2 \right) = 0.06 \text{ kg} \cdot \text{m}^2$$

$$\dot{\omega}_m = \left( C_m - \frac{mgl \sin \theta}{k_r} \right) \cdot \frac{1}{I_{total}}$$

$$= \left( C_m - \frac{9.8 \sin(270^\circ)}{k_r} (m_1 \cdot \frac{L}{2} + m_2 \cdot L) \right) \frac{1}{I_{total}} = \frac{\left[ 12 - \frac{9.8 \sin(270^\circ)}{5} \times (3 \times \frac{0.5}{2} + 2 \times 0.5) \right]}{0.06}$$

$$= 257.2 \text{ rad/s}^2$$

$$\text{ii) If } k_r = 50, \quad I_{total} = 0.03 + \frac{1}{2500} \left( \frac{3 \times 0.5^2}{3} + 2 \times 0.5^2 \right) = 0.0303 \text{ kg} \cdot \text{m}^2$$

$$\dot{\omega}_m = \left[ 12 - \frac{9.8 \sin(270^\circ)}{50} \times (3 \times \frac{0.5}{2} + 2 \times 0.5) \right] \times \frac{1}{0.0303}$$

$$= 407.36 \text{ rad/s}^2$$

b) When  $K_r = 5$ ,  $I_{\text{total}} = 0.06 \text{ kg} \cdot \text{m}^2$ ,  $\dot{W}_m = 257.2 \text{ rad/s}^2$ .

When  $K_r = 50$ ,  $I_{\text{total}} = 0.0303 \text{ kg} \cdot \text{m}^2$ ,  $\dot{W}_m = 407.36 \text{ rad/s}^2$

~~the~~ Higher the gear ratio, lower the impact from load side to the motor side.

2.  $\therefore$  Viscous friction in the system remains negligible

$$(a) \quad C_m = (I_m + I_{gm} + \frac{I_{\text{load}} + I_{gl}}{K_r^2}) \dot{W}_m + \frac{C_l}{K_r}$$

$$I_{\text{total}} = I_m + I_{gm} + \frac{I_{\text{load}} + I_{gl}}{K_r^2}$$

i) when  $K_r = 5$ ,

$$I_{\text{total}} = 0.03 + 0.002 + \frac{1}{25} \left( \frac{3 \times 0.5^2}{3} + 2 \times 0.5^2 + 0.004 \right) = 0.06216 \text{ kg} \cdot \text{m}^2$$

$$\dot{W}_m = \left[ 12 - \frac{9.8 \times \sin(27^\circ)}{5} \times \left( 3 \times \frac{0.5}{2} + 2 \times 0.5 \right) \right] \frac{1}{0.06216} = 248.26 \text{ rad/s}^2$$

ii) When  $K_r = 50$

$$I_{\text{total}} = 0.03 + 0.002 + \frac{1}{2500} \left( \frac{3 \times 0.5^2}{3} + 2 \times 0.5^2 + 0.004 \right) = 0.0323 \text{ kg} \cdot \text{m}^2$$

$$\dot{W}_m = \left[ 12 - \frac{9.8 \times \sin(27^\circ)}{50} \times \left( 3 \times \frac{0.5}{2} + 2 \times 0.5 \right) \right] \cdot \frac{1}{0.0323} = 382.14 \text{ rad/s}^2$$

b) If we consider the inertias of gears, the  $I_{\text{total}}$  will increase, so the maximum angular acceleration values will decrease.

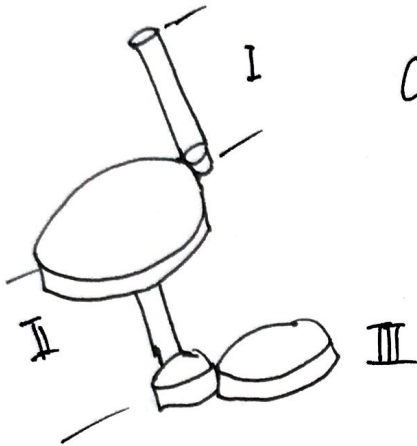
3. Consider the serial connection of two linear springs having stiffness coefficients  $k_1$  and  $k_2$ .

Give the system a torque  $T$ .  $T = k_1 \Delta \theta_1 = k_2 \Delta \theta_2$ ,  $\Delta \theta = \Delta \theta_1 + \Delta \theta_2$

$$K_{\text{serial}} = \frac{T}{\Delta \theta} = \frac{T}{\Delta \theta_1 + \Delta \theta_2} = \frac{T}{\frac{T}{k_1} + \frac{T}{k_2}} = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}}$$

$$\therefore \frac{1}{K_{\text{serial}}} = \frac{1}{k_1} + \frac{1}{k_2}$$

4. Consider the 'serial connection of #1 coupling, connecting rod and #2 Coupling. The serial stiffness  $K_s = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2} + \frac{1}{k_c}} = \frac{1}{\frac{1}{100} + \frac{1}{100} + \frac{1}{400}}$   
 $= 44.44 \text{ N}\cdot\text{m/rad}$



Give the system a torque  $T$ ,  $K_g = 2000 \text{ N}\cdot\text{m/rad}$

$$\text{For I, } \frac{M}{K_s} = \Delta\theta_1$$

$$\text{For II, } \frac{M}{K_g} = \Delta\theta_2$$

$$\text{For III, } \frac{M}{K_g} = \Delta\theta_3$$

$$\Delta\theta = \frac{\frac{\Delta\theta_1}{K_s^2} + \Delta\theta_2}{K_r^2} + \Delta\theta_3$$

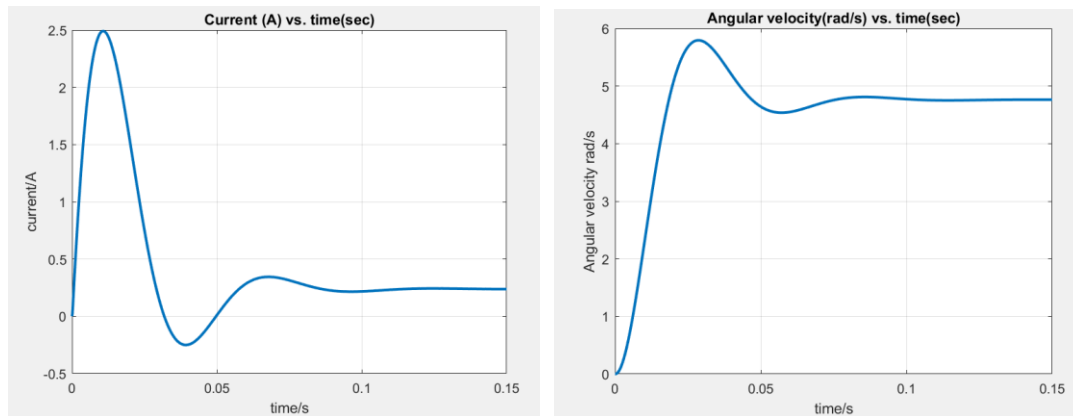
$$= \frac{\Delta\theta_1}{K_r^4} + \frac{\Delta\theta_2}{K_r^2} + \Delta\theta_3 \quad \text{where } K_r = 6.$$

$$\therefore K_4 = \frac{M}{\Delta\theta} = \frac{1}{\frac{1}{K_g} + \frac{1}{K_g K_r^2} + \frac{1}{K_s K_r^4}} = \frac{1}{\frac{1}{2000} + \frac{1}{2000 \cdot 6^2} + \frac{1}{44.44 \cdot 6^4}}$$

$$= 1882.35 \text{ N}\cdot\text{m/rad}$$

Prob5

(a) (b)



%%% Zhaoxing Deng 005024802 %%%

clear all;

clc;

sim HW1

figure(1)

plot(tout,l\_a,'linewidth',2);

grid on;

title('Current (A) vs. time(sec)');

xlabel('time/s');

ylabel('current/A');

figure(2)

plot(tout,omega,'linewidth',2);

grid on;

title('Angular velocity(rad/s) vs. time(sec)');

xlabel('time/s');

ylabel('Angular velocity rad/s');

(c)

