

# Equivalence of Stiffness Matrix Calculated in Current and Reference Configuration

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We use  $\mathbf{F}$  to denote the deformation gradient,  $\mathbf{P}$  to denote the First Piola Kirchhoff stress,  $\mathbf{S}$  to denote the Second Piola Kirchhoff stress,  $\boldsymbol{\sigma}$  to denote the Cauchy stress,  $\mathbf{x}$  to denote the current position,  $\mathbf{X}$  to denote the reference position,  $N$  to denote the shape function in the FEM discretization,  $\mathbf{E} = \frac{1}{2}(\mathbf{F}^T \mathbf{F} - \mathbf{I})$  to denote the Green-Lagrangian strain tensor, and  $C_{IJKL} = \frac{\partial S_{IJ}}{\partial E_{KL}}$  to denote the elasticity tensor in the reference configuration. We use subscripts  $i, j, k, l, m, n, p, q$  and their upper case counterparts to denote spacial dimension indices which can take values from 1, 2 and 3. We use superscripts  $a, b$  to denote local element indexes, ranging from 1 to the number of element nodes.

The stiffness matrix given by [?] without the external force component is

$$[K_{ab}]_{mn} = [K_{ab}^c]_{mn} + [K_{ab}^\sigma]_{mn}. \quad (1)$$

$[K_{ab}^c]_{mn}$  is given by (9.35) in [?]:

$$[K_{ab}^c]_{mn} = \int \frac{\partial N^a}{\partial x_i} c_{minj} \frac{\partial N^b}{\partial x_j} d\mathbf{x},$$

in which  $c_{ijkl}$  is the current configuration elasticity tensor that satisfies  $J c_{ijkl} = F_{iI} F_{jJ} F_{kK} F_{lL} C_{IJKL}$  ((8.12d) in [?]).

$[K_{ab}^\sigma]_{mn}$  is given by (9.44c) in [?]

$$[K_{ab}^\sigma]_{mn} = \int \frac{\partial N^a}{\partial x_i} \sigma_{ij} \frac{\partial N^b}{\partial x_j} \delta_{mn} d\mathbf{x}.$$

The stiffness matrix in our implementation is given by

$$[K_{ab}]_{mn} = \int \frac{\partial F_{iI}}{\partial x_m^a} \frac{\partial P_{iI}}{\partial F_{jJ}} \frac{\partial F_{jJ}}{\partial x_n^b} d\mathbf{X}. \quad (2)$$

We will show that the stiffness matrix we implement in Equation ?? is analytically equivalent to the one in Equation ??.

To see the equivalence, we make use of the identity  $\mathbf{P} = \mathbf{F}\mathbf{S}$ , which implies

$$\begin{aligned} \frac{\partial P_{iI}}{\partial F_{jJ}} &= \frac{\partial F_{iK} S_{KI}}{\partial E_{PQ}} \frac{\partial E_{PQ}}{\partial F_{jJ}} \\ &= \frac{\partial F_{iK}}{\partial E_{PQ}} S_{KI} \frac{\partial E_{PQ}}{\partial F_{jJ}} + F_{iK} C_{KIPQ} \frac{\partial E_{PQ}}{\partial F_{jJ}} \\ &= \delta_{ij} \delta_{KJ} S_{KI} + F_{iK} C_{KIPQ} \left( \frac{1}{2} (\delta_{PJ} F_{jQ} + F_{jP} \delta_{QJ}) \right) \\ &= \delta_{ij} S_{IJ} + F_{iK} C_{KIJL} F_{jL} \end{aligned} \quad (3)$$

where the last equality uses the symmetries  $S_{IJ} = S_{JI}$  and  $C_{IJKL} = C_{IJLK}$ .

Plugging Equation ?? into Equation ?? and using the fact that  $\frac{\partial F_{KL}}{\partial x_j^a} = \delta_{jk} \frac{\partial N^a}{\partial X_L}$ , we get:

$$\begin{aligned}
[K_{ab}]_{mn} &= \int \frac{\partial F_{iI}}{\partial x_m^a} \frac{\partial P_{iI}}{\partial F_{jJ}} \frac{\partial F_{jJ}}{\partial x_n^b} d\mathbf{X} \\
&= \int \delta_{im} \frac{\partial N^a}{\partial X_I} \frac{\partial P_{iI}}{\partial F_{jJ}} \delta_{jn} \frac{\partial N^b}{\partial X_J} d\mathbf{X} \\
&= \int \delta_{im} \frac{\partial N^a}{\partial X_I} \delta_{ij} S_{IJ} \delta_{jn} \frac{\partial N^b}{\partial X_J} d\mathbf{X} \int \delta_{im} \frac{\partial N^a}{\partial X_I} F_{iK} C_{KIJL} F_{jL} \delta_{jn} \frac{\partial N^b}{\partial X_J} d\mathbf{X} \\
&= \int \delta_{im} \frac{\partial N^a}{\partial x_i} F_{iI} \delta_{ij} S_{IJ} \delta_{jn} \frac{\partial N^b}{\partial x_j} F_{jJ} d\mathbf{X} \\
&\quad + \int \delta_{im} \frac{\partial N^a}{\partial x_p} F_{pI} F_{iK} C_{KIJL} F_{jL} \delta_{jn} \frac{\partial N^b}{\partial x_q} F_{qJ} d\mathbf{X} \\
&= \int \delta_{mn} \frac{\partial N^a}{\partial x_i} F_{iI} S_{IJ} \frac{\partial N^b}{\partial x_j} F_{jJ} d\mathbf{X} \\
&\quad + \int \frac{\partial N^a}{\partial x_p} F_{pI} F_{mK} C_{KIJL} F_{nL} F_{qJ} \frac{\partial N^b}{\partial x_q} d\mathbf{X} \\
&= \int \frac{\partial N^a}{\partial x_i} \sigma_{ij} \frac{\partial N^b}{\partial x_j} \delta_{mn} d\mathbf{x} + \int \frac{\partial N^a}{\partial x_p} c_{mpqn} \frac{\partial N^b}{\partial x_q} d\mathbf{x} \\
&= \int \frac{\partial N^a}{\partial x_i} \sigma_{ij} \frac{\partial N^b}{\partial x_j} \delta_{mn} d\mathbf{x} + \int \frac{\partial N^a}{\partial x_i} c_{minj} \frac{\partial N^b}{\partial x_j} d\mathbf{x} \\
&= [K_{ab}^c]_{mn} + [K_{ab}^\sigma]_{mn} ,
\end{aligned}$$

where the sixth equality uses the identity  $\boldsymbol{\sigma} = \frac{1}{J} \mathbf{F} \mathbf{S} \mathbf{F}^T$  and the seventh equality uses the symmetry  $c_{ijkl} = c_{ijlk}$  in the elasticity tensor.

## References

- [1] Bonet, J., Gil, A.J. and Wood, R.D *Nonlinear solid mechanics for finite element analysis: statics*. Cambridge University Press, 2016.