$$|0\rangle = |0\rangle$$

$$|0\rangle$$

By, applying kVL @ ip loop-
$$-10 + 10K i + 0.8 + 4K i = 0$$

$$10K i + 4K (1+B) i = 9.8$$

$$i = \frac{9.8}{10K + 4K(1+B)}$$

And by applying KVL  $\omega$  olp loop- $-10 + 2K i_{csat} + 0.2 + 4K (i_{\epsilon}) = 0$   $i_{csat} = \frac{9.8}{6K}$ 

for BJT to be in the saturation-

βib > ic sat.

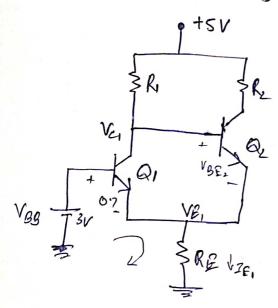
9.28 10K+4K (1+B) 5K

9.2B > 16.3 + 6.5 (1+B)

2.7B > 22.8

β > 8.44 (or) β = 9

62) Gium VBB=3V, hye=100, Q,ON, QLOFF RI= 4KR, Rz=2.5KR



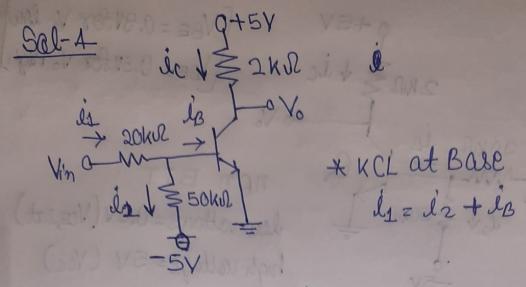
KVL at input of Q1 1-

minimum valtage required to turn ON Q2 153V

$$V_{BE_2} = V_{C_1} - V_{E_1}$$
  
 $0.7 = V_{C_1} - 2.3 \implies V_{C_1} = 3V$ 

from egno -

2 NO > +5V VBE = 0.84 for Vo low VBE = 0.5V fox Vo High Vin a My de Sokar Ja npn BJT low voltage = 0.2V (Vcz, sat) high valtage= 5 V (Vcc) (i) # if Vin=0.2X Assume Q-Off > IB=0 >> VBE = Vin-(-5) x 50K + (-5) = -1.286 V 20K +50K VBE < 0.5V : Assumption correct Icco Vossy (ii) if Vin = 5Y: Assume Q-ON (Scaturation): VBE = 0.8Y IB= 5-0. => l1 = l2 + lB  $J_{12} = \frac{V_{in} = (0.8)}{20K} = \frac{V_{in} - 0.8}{20K} = \frac{5 - 0.8}{20K} = 0.21 \text{ mA} \left( \frac{J_{12}}{20K} = \frac{V_{in} - V_{BE}}{20K} \right)$  $\hat{J}_{2z} = \frac{0.8 - (-5)}{50 \text{K}} = 0.116 \text{ mA} \left( \hat{J}_{2z} = \frac{\text{VBE} - (-5)}{50 \text{K}} \right)$ JB = i1-12 = 0.094 mA >0.2V B Ic = 5-0.2 = 2.4 mA (Ic= 5- VCE, law)  $\Rightarrow \frac{Ic}{F_B} = \frac{2.4}{0.094} \Rightarrow 25.532$  then assumption is correct 7 VO = VCE = 0.2 V



1) Salving for Vil and VoH VBE = 0.5V (given)

$$\Rightarrow$$
  $11 = \frac{Vin - VBE}{20k} = \frac{ViL - 0.5}{20k}$ ;  $12 = \frac{VBE - (-5)}{50k} = \frac{0.5 + 5}{50k}$ 

Assuming o & for Vin=Vil , lBSO; l1=l2

$$\Rightarrow \frac{Vil - 0.5}{20k} = \frac{0.5 + 5}{50k} \Rightarrow \Rightarrow Vil = \frac{20}{50} \times 5.5 + 0.5 = 2.7V$$

> YOH will be 5V :

2) golving for VIH and VOL

$$\Rightarrow$$
 VBE = 0.8 (given)

$$2) \quad \text{$\hat{l}_{1} = \frac{V_{in} - V_{BE}}{20K} = \frac{V_{iH} - 0.8}{20K} + \frac{1}{50K} = \frac{0.8 + 5}{50}}$$

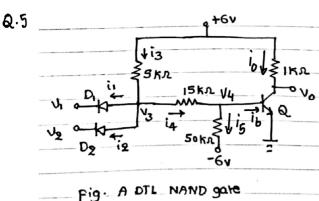
$$\Rightarrow l_B = \frac{l_C}{2} = 0.024 mA$$

$$\frac{39}{20K} = \frac{0.8+5}{50K} + 0.024$$

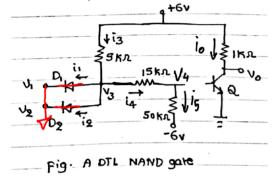
ViH = 20x0.14+0.8 = 3.6

\* input is sufficiently high, 30 Vol & 0.27

## \* Nobe margin

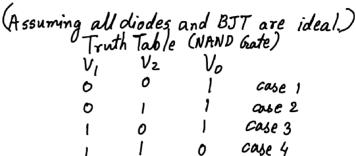


When case 1, case 2, case 3 is considered



Find the power dissipation in the circuit (NAND gate)

For all the NAND gate input/output combinations shown below 1, logic is +6 V and 0, logic is 0 V



-DI and Dz will short circuit the 5km resistor to ground BJT will be in cutoff.  $(i_0=0) \rightarrow V_0=+6V \rightarrow i_0=0$  in A KCL at  $V_3 \rightarrow i_1+i_2=i_3$  | KCL at  $V_4 \rightarrow i_4=i_5$   $\vdots$   $i_3=6-0=1\cdot 2mA$   $\vdots$   $i_5=0+6=0\cdot 092$  mA Power dissipated P1 = 6 x 13 P2 = 6x15 = 6x0.092 = 0.552 mW

Total power dissipated = P = 7.2+0.552 = 7.752 mW

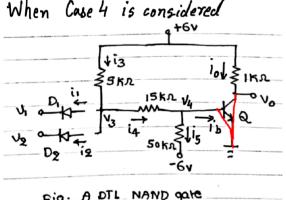


Fig. A DTL NAND gate

Dz and Pz will be open circuitel L> KCLat V3 → 13=14  $\frac{6-V_4}{20KR} = \frac{1}{3}$ 13=0.3 mA P1 = 6xi3 = 1.8mW

KCL at 
$$V_4$$
  
 $i_4 = i_5 + i_b$   
 $: i_5 = V_4 + 6 = 0.12 \text{ mA}$   
 $: i_b = i_4 - i_5 = 0.3 - 0.12 \text{ mA}$   
 $= 0.18 \text{ mA}$   
 $P_3 = 6 \times i_5 = 0.72 \text{ mA}$ 

BJT will be in saturation and act as short to the ground.  $\rightarrow V_4 = V_6 = 0V$  $\frac{6 - V_0}{1 \, \text{K-R}} = i_0$ : 10 = 6 m A P2 = 6xi0 = 36mW