

## Euler Angles :

- $\left. \begin{array}{l} \text{① Rotate by } \phi \text{ around } z, R_z(\phi) \\ \text{② Rotate by } \theta \text{ around the new } x\text{-axis, } R_x(\theta) \\ \text{③ Rotate by } \psi \text{ around new } z\text{-axis, } R_z(\psi) \end{array} \right\}$
- z x z  
rotation

$$R = \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix}$$

Then :  $\dot{\omega}_{ab} = (\dot{R} R^{-1})_{ab} = \begin{pmatrix} -\dot{\sin} \theta & \dot{\cos} \theta \\ \dot{\cos} \theta & -\dot{\sin} \theta \end{pmatrix} \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix}$

$$= (\dot{R} R^T)_{ab} = \begin{pmatrix} 0 & \dot{\theta} \\ -\dot{\theta} & 0 \end{pmatrix}$$

For 3D

General Rotation:

$$R(\phi, \theta, \psi) = R_3^z(\psi) R_2^x(\theta) R_1^z(\phi)$$

$$R^{-1}(\phi, \theta, \psi) = R_1^{z(-1)}(\phi) R_2^{x(-1)}(\theta) R_3^{z(-1)}(\psi)$$

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$$R = R_3^z(\psi) R_2^x(\theta) R_1^z(\phi) + R_3^z(\psi) R_2^y(\theta) R_1(\phi) + R_3^z(\psi) R_2(\theta) R_1(\phi)$$

Then  $\omega = (\dot{R}R^{-1})$  In Fixed Frame :  $\begin{aligned}\omega_x &= \dot{\psi} \sin \theta \sin \phi + \dot{\theta} \cos \phi \\ \omega_y &= -\dot{\psi} \sin \theta \cos \phi + \dot{\theta} \sin \phi \\ \omega_z &= \dot{\psi} \cos \theta + \dot{\phi}\end{aligned}$

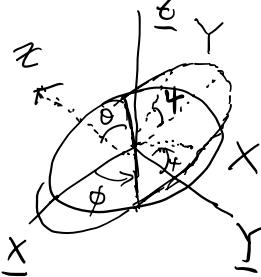


$\omega^x = \omega_{yz} = \dot{\phi} \sin \theta \sin \phi + \dot{\theta} \cos \phi$

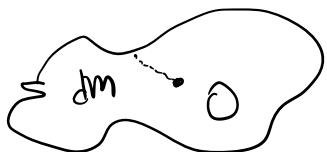
Rotated Frame

$\omega^y = \omega_{zx} = \dot{\phi} \sin \theta \cos \phi - \dot{\theta} \sin \phi$

$\omega^z = \omega_{xy} = \dot{\phi} \cos \theta + \dot{\psi}$



### Kinetic Energy in 3D



O is fixed

$\theta$ : Final tilt angle from  $\underline{z}$  to  $\underline{z}$   
 $\dot{\psi}^2$ : Final spinning rate of  $\underline{z}$   
 $\dot{\phi}$ : Precession rate, spinning rate of  $\underline{z}$

$$T = \sum_i \frac{1}{2} dm_i \left( \frac{d\vec{r}_i}{dt} \right)^2 = \int \frac{1}{2} dm \dot{\vec{r}}^2$$

then  $\dot{\vec{r}}_i = \frac{d\vec{r}_i}{dt} = \vec{\omega} \times \vec{r}_i + \cancel{\left( \frac{d\vec{r}}{dt} \right)} \theta$  since dealing with rigid body its not deforming

$$T = \frac{1}{2} \int dm (\vec{\omega} \times \vec{r}) \cdot (\vec{\omega} \times \vec{r})$$

$$= \frac{1}{2} \int dm (\omega r \sin \theta)^2$$

$$= \frac{1}{2} \int dm \omega^2 r^2 (1 - \cos^2 \theta)$$

$$= \frac{1}{2} \int dm \{ \omega^2 r^2 - (\vec{\omega} \cdot \vec{r})^2 \}$$

$$= \frac{1}{2} \int dm W_a W_b r^2 \delta_{ab} - W_a \Gamma_a N_b \Gamma_b$$

$$\left. \begin{aligned} \vec{r}^2 &= \Gamma_a \Gamma_b \delta_{ab} \\ \vec{\omega} \cdot \vec{r} &= W_a \Gamma_a \\ \omega^2 &= W_a W_b \delta_{ab} \end{aligned} \right\}$$

$$= \frac{1}{2} \int dm \omega_a (r^2 \delta_{ab} - r_a r_b) \omega_b$$

\*  $T = \frac{1}{2} \omega_a \omega_b \int dm (r^2 \delta_{ab} - r_a r_b)$

we can pull these terms out since orientation is independent of where you are in the body. Or,  $\omega$  doesn't depend on  $\vec{r}$ .

$I_{ab}$ , moment of inertia tensor for fixed frame.

$$\begin{aligned} I_{ab} &= \int d^3r \rho(r) (r^2 \delta_{ab} - r_a r_b) \\ &\stackrel{!}{=} \int dm (r^2 \delta_{ab} - r_a r_b) \end{aligned}$$

← Moment of inertia tensor for fixed origin.

Ex?

$$I = \int d^3r \rho(r) \begin{pmatrix} x^2 + y^2 + z^2 - x^2 & -xy & -xz \\ -yx & x^2 + y^2 + z^2 - y^2 & -yz \\ -zx & -zy & x^2 + y^2 + z^2 - z^2 \end{pmatrix} \begin{matrix} x \\ y \\ z \end{matrix}$$

$$= \int d^3r \rho(r) \begin{pmatrix} y^2 + z^2 & -xy & -xz \\ -yx & x^2 + z^2 & -yz \\ -zx & -zy & x^2 + y^2 \end{pmatrix} = \begin{pmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{pmatrix}$$

\* Here  $I_{xx}$ ,  $I_{yy}$ , and  $I_{zz}$ , are moment of inertia of  $x$ -,  $y$ -, and  $z$ -axis

For non-fixed origin, use center of mass:  $\vec{R} = \frac{\sum m_a \vec{r}_a}{\sum m_a}$



$$\vec{r}_i = \vec{R}(t) + \Delta \vec{r}_i$$

$$\Delta \vec{r}_i = \vec{r}_i - \vec{R}$$

$$\vec{R}(t) \quad \frac{d\vec{r}_i}{dt} = \frac{d\vec{R}(t)}{dt} + \frac{d\Delta\vec{r}_i}{dt}$$

$$\perp \vec{v}_{cm} + \vec{\omega} \times \vec{r}_i$$

$$KE = \frac{1}{2} \sum m_i \dot{r}_i^2$$

$$= \frac{1}{2} \sum m_i \left\{ v_{cm}^2 + 2 \underbrace{\vec{v}_{cm} \cdot (\vec{\omega} \times \vec{\Delta r}_i)}_{\text{due to center of mass}} + (\vec{\omega} \times \vec{\Delta r}_i)^2 \right\}$$

$$\sum m_i \Delta r_i = 0$$

$$= \frac{1}{2} \sum m_i v_{cm}^2 + \frac{1}{2} \sum m_i (\vec{\omega} \times \vec{\Delta r}_i)^2$$

$$= \frac{1}{2} M_{tot} v_{cm}^2 + \frac{1}{2} \sum m_i \omega^2 \Delta r_i^2 \sin^2 \theta$$

$$= \frac{1}{2} M_{tot} v_{cm}^2 + \frac{1}{2} \sum m_i \underbrace{\omega^2 \Delta r_i^2 (1 - \cos^2 \theta)}_{\omega_a \omega_b I_{ab} \Delta r_i^2 - \Gamma_a \Gamma_b \omega_b \Gamma_b}$$

$$= \omega_a (\Delta r_i^2 \delta_{ab} - \Gamma_a \Gamma_b) \omega_b =$$

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KE	$\downarrow$	$\downarrow$
$= \frac{1}{2} M_{tot} v_{cm}^2 + \frac{1}{2} \omega_a I_{ab} \omega_b^{cm}$		$\leftarrow$ For moving off around center of mass

Translational KE      Rotational KE

Angular Momentum:

$$L = \sum m_i \vec{r}_i \times \dot{\vec{r}}_i$$

$$= \sum m_i \vec{r}_i \times (\vec{\omega} \times \vec{r}_i)$$

$$\text{use } \vec{A} \times (\vec{B} \times \vec{C}) = \vec{B}(\vec{A} \cdot \vec{C}) - \vec{C}(\vec{A} \cdot \vec{B})$$

$$\begin{aligned} L &= \sum m_i \{ \vec{w}(\vec{r}_i \cdot \vec{r}_i) - \vec{r}_i(\vec{r}_i \cdot \vec{w}) \} \\ &= \sum m_i \{ w_b r_i^2 \delta_{ab} - r_a r_b w_b \} \\ &= \underbrace{\sum m_i (r_i^2 \delta_{ab} - r_a r_b)}_{I_{ab}} w_b \end{aligned}$$

$$L_a = I_{ab} w_b \quad \leftarrow \text{Angular momentum around some fixed coordinate.}$$

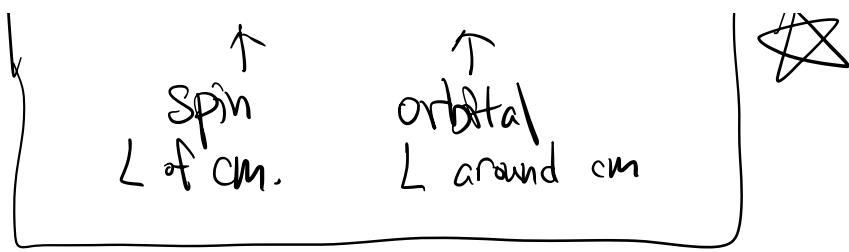
For CoM or moving coordinate-

$$\vec{r}_i = \vec{R}(t) + \vec{\Delta r}_i$$

$$\dot{\vec{r}}_i = \dot{\vec{R}}(t) + \vec{w} \times \vec{\Delta r}_i$$

$$\begin{aligned} L &= \sum m_i \vec{r}_i \times \dot{\vec{r}}_i \\ &= \sum m_i (\vec{R} + \vec{\Delta r}_i) \times (\dot{\vec{R}} + \vec{w} \times \vec{\Delta r}_i) \\ &= \sum m_i (\vec{R} \times \dot{\vec{R}} + \underbrace{\vec{R} \times (\vec{w} \times \vec{\Delta r}_i)}_{=0} + \underbrace{\vec{\Delta r}_i \times \dot{\vec{R}}}_{=0} + \vec{\Delta r}_i \times (\vec{w} \times \vec{\Delta r}_i)) \\ &\text{Since } \sum m_i \vec{\Delta r}_i = 0 \end{aligned}$$

$$L_a = L_{cm,a} + I_{ab} w_b$$



### Summary:

For fixed origin (fixed object):

$$I_{ab} = \int d\vec{r} \rho(\vec{r}) (r^2 \delta_{ab} - r_a r_b)$$

$$T = \frac{1}{2} w_a I_{ab} w_b$$

$$L_a = I_{ab} w_b$$

For moving origin (use center of mass):

$$T = \frac{1}{2} M_{tot} V_{cm}^2 + \frac{1}{2} w_a I_{ab}^{cm} w_b$$

$$L_a = \underbrace{M_{tot} \vec{R} \times \vec{V}_{cm}}_{L_{cm}} + I_{ab} w_b$$

Since  $I_{ab}$  is a matrix, find some axis orientation or find principal axes such that  $I_{ab}$  is diagonalized, or non-diagonal elements go zero.

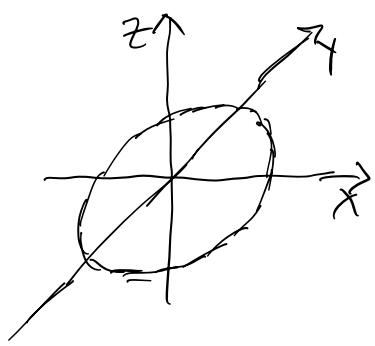
$$I' = R I R^T$$

then

$$I' = \begin{pmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{pmatrix}$$

In principal axis

Ex: Here we see that off-diagonal are all zero.



$$I_{xy} = M \langle xy \rangle = M \frac{\int d^3r f(r) xy}{M} = 0$$

$$I_{xz} = 0$$

$$I_{xx} = \int d^3r f(r) (y^2 + z^2)$$

$$= M \langle y^2 \rangle$$

$$I_{yy} = M \langle x^2 \rangle$$

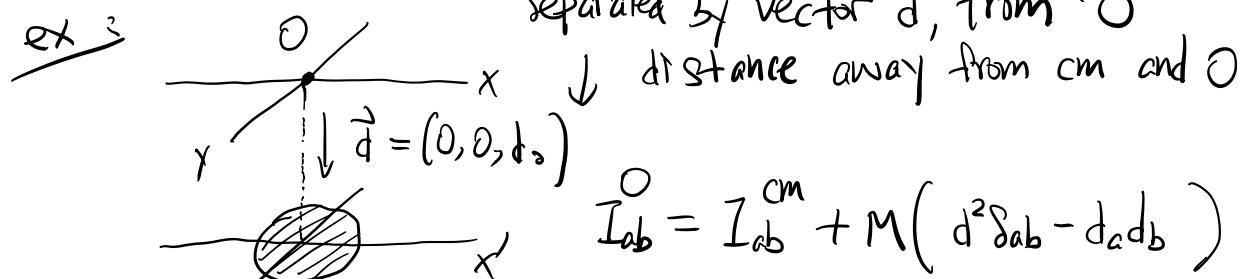
$$I_{zz} = M \langle x^2 + y^2 \rangle = \int f(r) dr (x^2 + y^2)$$

$$= \int r d\theta dr \frac{M}{\pi r^2} r^2$$

$$= \frac{2\pi M}{\pi} \frac{R^2}{2}$$

### Parallel-Axis Theorem:

ex:



$$I_{ab}^O = \left( \frac{1}{4} MR^2 - \frac{1}{4} MR^2 \right) + M \begin{pmatrix} d^2 & 0 & 0 \\ 0 & d^2 & 0 \\ 0 & 0 & d^2 \end{pmatrix}$$

$$\frac{1}{2}MR^2 / \begin{pmatrix} 0 & 0 & 0 \end{pmatrix}$$

Parallel Axis Theorem:

$$I_{ab}^{\circ} = I_{ab}^{cm} + M(d^2\delta_{ab} - d_a d_b)$$

where  $\vec{d}$  is separation vector between  $\circ$  and cm

Then Suppose  $\vec{\omega} = \omega(0, 1, 0)$

$$\begin{aligned} T &= \frac{1}{2} \omega_y I_{yy} \omega_y \\ &= \frac{1}{2} \omega^2 \left( I_{ab}^{cm} + M(d^2\delta_{ab} - d_a d_b) \right) \\ &= \frac{1}{2} \omega^2 \left( \frac{1}{4}MR^2 + Md_o^2 \right) \\ &= \underbrace{\frac{1}{8}M\omega^2 R^2}_{KE \text{ about cm}} + \underbrace{\frac{1}{2}M\omega^2 d_o^2}_{\text{KE about CM}} \end{aligned}$$

$$KE \text{ about CM } \frac{1}{2}MV_{cm}^2 \Rightarrow V_{cm} = \omega d_o$$

$$\begin{aligned} (\vec{L})_a &= \vec{d} \times (m\vec{r}_{cm}) + I_{ab}^{cm} \omega_b \\ &= \vec{d} \times (\vec{\omega} \times \vec{d}) m + I_{ab}^{cm} \omega_b \\ &= \left\{ \vec{\omega}(\vec{d} \cdot \vec{d}) - \vec{d}(\vec{d} \cdot \vec{\omega}) \right\} m + I_{ab}^{cm} \omega_b \\ &= (\omega_b d^2 \delta_{ab} - d_a d_b \omega_b) m + I_{ab}^{cm} \omega_b \\ &= \omega_b (d^2 \delta_{ab} - d_a d_b) m + I_{ab}^{cm} \omega_b \\ &= 0 \end{aligned}$$

$$\doteq I_{ab} \omega_b$$

Euler Eqns: ← Rotating frame.

In fixed frame  $\frac{d\vec{L}}{dt} = \left( \frac{d\vec{L}}{dt} \right)_r + \vec{\omega} \times \vec{L}$

For  $\vec{L} = L_a \vec{e}_a(t)$  0 for free motion

$$I_{ab} \dot{\omega}_b = \left( \frac{d\vec{L}}{dt} \right)_a = \left( \frac{dL_a}{dt} \right)_r \vec{e}_a + \epsilon_{abc} \omega^b L^c \vec{e}_a = \cancel{\left( \vec{r}_{ext} \right)_a}$$

$$I_a \dot{\omega}_a = -\epsilon_{abc} \omega^b L^c \vec{e}_a$$

$$\left. \begin{array}{l} I_1 \dot{\omega}_1 = \omega_2 \omega_3 (I_2 - I_3) \\ I_2 \dot{\omega}_2 = \omega_3 \omega_1 (I_3 - I_1) \\ I_3 \dot{\omega}_3 = \omega_1 \omega_2 (I_1 - I_2) \end{array} \right\} \text{Euler Eqns.}$$

For plate:  $I_x = I_y = \frac{1}{4}MR^2$   $I_z = \frac{1}{2}MR^2$

then

$$I_3 \dot{\omega}_3 = \omega_1 \omega_2 (I_1 - I_2) = 0 \quad \text{for } I_1 = I_2$$

$$I_1 \dot{\omega}_1 = \omega_2 \omega_3 (I_2 - I_3)$$

$$I_2 \dot{\omega}_2 = \omega_3 \omega_1 (I_3 - I_1) = \omega_3 \omega_1 (I_3 - I_2)$$

then

$$\dot{\omega}_2 = \frac{\omega_3(I_3 - I_2)}{I_2} \quad \omega_1 = \Omega \omega_1$$

$$\dot{\omega}_1 = \frac{\omega_3(I_2 - I_3)}{I_2} \quad \omega_2 = -\Omega \omega_2$$

Solve, get?  $(\omega_1, \omega_2) = \omega_T (-\sin \Omega t, \cos \Omega t)$

$\omega_3 = \text{constant}$

$$\vec{L} = I_1 \omega_1 \vec{e}_1 + I_2 \omega_2 \vec{e}_2 + I_3 \omega_3 \vec{e}_3$$

$$= I_1 (\omega_1 \vec{e}_1 + \omega_2 \vec{e}_2) + I_3 \omega_3 \vec{e}_3$$

$$= I_1 \vec{\omega}_T + I_3 \vec{\omega}_3$$

$$\frac{\vec{L}}{I_3} = \frac{1}{2} \vec{\omega}_T + \vec{\omega}_3 \quad \begin{array}{l} \downarrow \\ I_1 = I_2 \\ I_3 = 2 I_1 \end{array}$$

know  $\vec{\omega}_3$  is constant,  $\vec{L}$  is constant

$$\vec{L} \cdot \vec{\omega}_3 = L \omega_3 \cos \theta = \text{constant}$$

then  $\theta$  is constant.

$$\omega_x = \dot{\phi} \sin \theta \sin \psi + \cancel{\dot{\theta} \cos \psi} = -\omega_T \sin \Omega t$$

$$\omega_y = \dot{\phi} \sin\theta \cos\psi - \cancel{\dot{\phi} \sin\psi} = \omega_1 \cos\Omega t$$

$$\omega_z = \dot{\phi} \cos\theta + \dot{\psi} = \text{constant}$$

By matching,  $\psi = -\Omega t \Rightarrow \dot{\psi} = -\Omega$

$$\omega_z = \text{constant}$$

$\uparrow$   
precession rate  
in body frame

$$\dot{\phi} \cos\theta + \dot{\psi} = \dot{\phi} \cos\theta - \Omega = \omega_3$$

$$\boxed{\dot{\phi} = \frac{\omega_3 + \Omega}{\cos\theta}}$$

$\leftarrow$  precession rate.  
in lab frame.

For  $\theta \ll 1$

$$\dot{\phi} \approx \omega_3 + \Omega$$

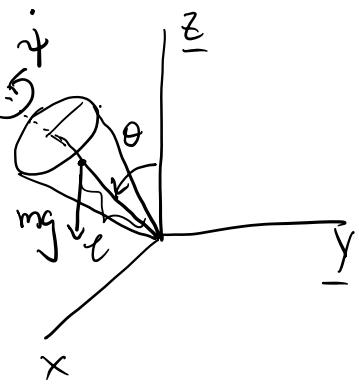
### Symmetric Top Problem

(base is fixed)

Meaning:  $\rightarrow I^o = \begin{pmatrix} I_{11}^o & 0 & 0 \\ 0 & I_{22}^o & 0 \\ 0 & 0 & I_{33}^o \end{pmatrix}$

Moment of inertia

w.r.t. base point, O.



Lagrangian:

$$L = \frac{1}{2} \omega_a I_{ab} \omega_b$$

$$= \frac{1}{2} \omega_1^2 I_1 + \frac{1}{2} \omega_2^2 I_2 + \frac{1}{2} \omega_3^2 I_3$$

Symmetry in  $\vec{e}_1$  and  $\vec{e}_2$ , so  $I_1 = I_2$

$$= \frac{1}{2} I_1 (w_1^2 + w_2^2) + \frac{1}{2} w_3^2 I_3$$



Rotating Frame.

$$\omega^x = \omega_{yz} = \dot{\phi} \sin\theta \sin\phi + \dot{\theta} \cos\phi$$

$$\omega^y = \omega_{zx} = \dot{\phi} \sin\theta \cos\phi - \dot{\theta} \sin\phi$$

$$\omega^z = \omega_{xy} = \dot{\phi} \cos\theta + \dot{\psi}$$

$$L = \frac{1}{2} I_1 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) + \frac{1}{2} I_3 (\dot{\phi} \cos\theta + \dot{\psi})^2 - mg l \cos\theta$$

$l$ : distance  
to center  
of mass

$$P_4 = \frac{2L}{2\dot{\psi}} = I_3 (\dot{\phi} \cos\theta + \dot{\psi}) = \text{constant}$$

$$P_\phi = \frac{2L}{2\dot{\phi}} = I_1 \dot{\phi} \sin^2 \theta + \underbrace{I_3 (\dot{\phi} \cos\theta + \dot{\psi})}_{P_4} \cos\theta = \text{constant}$$

$$\hookrightarrow \dot{\phi} = \frac{P_\phi - P_4 \cos\theta}{I_1 \sin^2 \theta} \Rightarrow \text{precession rate around } z$$

$$\hookrightarrow \dot{\psi} = \frac{P_4}{I_3} - \dot{\phi} \cos\theta \Rightarrow \text{spinning rate around } z$$

$$P_\theta = \frac{2L}{2\dot{\theta}} = I_1 \dot{\theta}$$

In order to get  $\dot{\phi}$ , need  $\theta$ .

Use  $E = h = P(\dot{q})\dot{q} - L$  since  $L$  independent of  $t$ , energy conservation

$$= I_1 \dot{\theta}^2 + I_3 \dot{\psi} (\dot{\phi} \cos\theta + \dot{\psi}) + I_1 \dot{\phi}^2 \sin^2 \theta + I_3 \dot{\phi} (\dot{\phi} \cos\theta + \dot{\psi}) \cos\theta$$

$$-\left\{ \frac{1}{2} I_1 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) + \frac{1}{2} I_3 (\dot{\phi} \cos \theta + \dot{\psi})^2 - mgl \cos \theta \right\}$$

$$E = \frac{1}{2} I_1 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) + \frac{1}{2} I_3 (\dot{\phi} \cos \theta + \dot{\psi})^2 + mgl \cos \theta$$

Express E in integral of motion (constants):

$$E = \frac{1}{2} I_1 \dot{\theta}^2 + \frac{1}{2} I_1 \sin^2 \theta \left( \frac{P_\phi - P_4 \cos \theta}{I_1 \sin^2 \theta} \right)^2 + \frac{1}{2} \frac{P_4^2}{I_3} + mgl \cos \theta.$$

$$\frac{1}{2} I_1 \dot{\theta}^2 + \frac{1}{2} \frac{(P_\phi - P_4 \cos \theta)^2}{I_1 \sin^2 \theta} + \underbrace{\frac{1}{2} \frac{P_4^2}{I_3}}_{\text{constant}} + mgl \cos \theta$$

$$\frac{1}{2} I_1 \dot{\theta}^2 + \underbrace{\frac{(P_\phi - P_4 \cos \theta)^2}{2 I_1 \sin^2 \theta}}_{\text{term}} + mgl \cos \theta$$

$U_{\text{eff}}(\theta)$

$$\text{Routhian: } L_{\text{eff}} = \frac{1}{2} I_1 \dot{\theta}^2 - U_{\text{eff}}(\theta) = -R$$

$$\frac{d}{dt} \frac{\partial R}{\partial \dot{\theta}} = \frac{\partial R}{\partial \theta} \quad \frac{d}{dt} \frac{\partial L}{\partial \dot{\theta}} = \frac{\partial L}{\partial \theta}$$

$$\hookrightarrow I_1 \ddot{\theta} = - \frac{\partial}{\partial \theta} U_{\text{eff}}(\theta)$$

At fixed angle  $\theta$ ,  $\frac{\partial}{\partial \theta} U_{\text{eff}}(\theta) = 0$ , so  $U_{\text{eff}}$  is at minimum.  
(initial condition is at  $\theta_{\min}$ )

$$\frac{\partial}{\partial \theta} U_{\text{eff}} = \frac{\partial}{\partial \theta} \left\{ \frac{(P_\phi - P_4 \cos \theta)^2}{2 I_1 \sin^2 \theta} + mgl \cos \theta \right\} = 0$$

$$\text{define } \bar{g} = \frac{mgL}{P_4^2/I_1} \quad \text{and} \quad \beta = \frac{P_\phi}{P_4}$$

$$\frac{U_{\text{eff}}}{P_4^2/I_1} = \bar{g} \cos \theta + \frac{(\beta - \cos \theta)^2}{2 \sin^2 \theta}$$

For  $\bar{g} \ll 1$ , zeroth approximation:

$$\frac{U_{\text{eff}}}{P_4^2/I_1} = \frac{(\beta - \cos \theta)^2}{2 \sin^2 \theta}$$

$$\begin{aligned} \frac{\partial}{\partial \theta} \left( \frac{U_{\text{eff}}}{P_4^2/I_1} \right) &= \frac{4(\beta - \cos \theta) \sin^2 \theta - (\beta - \cos \theta)^2 2 \cos \theta}{4 \sin^3 \theta} \\ &\stackrel{!}{=} \frac{(\beta - \cos \theta) \{ 4 \sin^2 \theta - 2 \beta \cos \theta + 2 \cos^2 \theta \}}{4 \sin^3 \theta} \end{aligned}$$

$$\text{at min: } \beta - \cos \theta = 0 \quad \text{or} \quad \beta = \cos \theta_{\min}$$

$$\beta = \frac{P_\phi}{P_4} = \cos \theta_{\min}$$

$$P_\phi = P_4 \cos \theta_{\min}$$

$$\begin{aligned} \text{and } \dot{\phi} &= \frac{P_\phi - P_4 \cos \theta}{I_1 \sin^2 \theta} \quad \downarrow \\ &\stackrel{!}{=} \frac{P_4 \cos \theta - P_4 \cos \theta}{I_1 \sin^2 \theta} = 0. \end{aligned}$$

Therefore need first order:

$$\cos \theta_{\min} = \beta + \delta$$

$\uparrow$   
0th order ans       $\uparrow$   
first order answer

Find  $\delta$  by plug into  $U_{\text{eff}}(\theta)$ :

$$\frac{U_{\text{eff}}}{P_4^2/I_1} = \bar{g}(B+\delta) + \frac{\{B-(B+\delta)\}^2}{2(1-(B+\delta)^2)}$$

$$= \bar{g}(B+\delta) + \frac{\delta^2}{2(1-B^2)}$$

$$\frac{2U_{\text{eff}}}{2\delta} = \bar{g} + \frac{\delta}{1-B^2} = 0$$

$$\Rightarrow \delta = (1-B^2)(-\bar{g})$$

then plug into  $\dot{\phi}$

$$\dot{\phi} = \frac{P_\phi - P_4 \cos \theta_{\min}}{I_1 \sin^2 \theta} = \frac{P_4}{I_1} \left( \frac{B - \cos \theta}{\sin^2 \theta} \right)$$

$$= \frac{P_4}{I_1} \left( \frac{B - (B+\delta)}{1 - (B+\delta)^2} \right)$$

$$= \frac{P_4}{I_1} \frac{-\delta}{1 - B^2}$$

$$= \frac{P_4}{I_1} \frac{(1-B^2)\bar{g}}{1 - B^2}$$

$$\dot{\phi} = \frac{P_4 \bar{g}}{I_1} = \frac{P_4 m g l}{I_1 P_4^2 / I_1}$$

$$\dot{\phi} = \frac{m g l}{P_4}$$

Sleeping Top?



$$U_{\text{eff}}(\theta) = mgl \cos \theta + \frac{(P_\phi - P_4 \cos \theta)^2}{2I_1 \sin^2 \theta}$$

If  $\theta = 0$ , then the eff way to have minimum potential is to have

$$P_\phi = P_4$$

$$\text{then } U_{\text{eff}}(\theta) = mgl \cos \theta + \frac{P_\phi}{2I_1} \frac{(1 - \cos \theta)^2}{\sin^2 \theta}$$

then we expand around  $\theta = 0$

$$U_{\text{eff}}(\theta) = mgl \left(1 - \frac{\theta^2}{2}\right) + \frac{P_\phi^2}{2I_1} \frac{\left\{1 - \left(1 - \frac{\theta^2}{2}\right)\right\}^2}{\theta^2}$$

$$= \underbrace{mgl}_{\text{const}} - mgl \frac{\theta^2}{2} + \frac{P_\phi^2}{2I_1} \frac{\theta^2}{4}$$

$$= \text{const} + \left(\frac{P_\phi^2}{8I_1} - \frac{mgl}{2}\right) \theta^2$$

In order for stability,  $U_{\text{eff}}(\theta)$  must be concave up near  $\theta = 0$

$$\text{or } \left(\frac{P_\phi^2}{8I_1} - \frac{mgl}{2}\right) > 0$$

$\therefore$  need  $D_1 < \sqrt{T_{\text{min}} + T}$

$\tau\phi \supset \tau^m \mathcal{J}^L \perp_1$