# Leveraging Multiple Isolated Maps for Visual Inertial Odometry: Framework and Consistency

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Abstract-Visual Inertial Odometry (VIO) is widely used in autonomous robots to provide the ego-pose of the robot. With the help of pre-built map information, the drift of the VIO can be constrained. However, constructing a globally consistent map is a tough job, especially for large scenes. In this paper, we propose a framework aiming to leverage multiple isolated maps to improve the performance of VIO. In this framework, the relative transformations between the local VIO reference frame and the multiple map reference frames are regarded as pose features to be online estimated. We call these relative transformations as augmented variables. With these augmented variables, the map-based information can be tightly coupled into the VIO system to ease the drift of VIO. To fuse these maps consistently, we theoretically analyze the observability properties of our proposed framework. Based on the analysis, the Schmidt extended Kalman filter (EKF) and the first-estimate Jacobian (FEJ) are employed to maintain the consistency of the system. Simulation and real-world experiments are conducted to demonstrate the effectiveness and consistency of our framework.

#### I. INTRODUCTION

During the recent decade, visual-inertial odometry (VIO) has gained great attention, and a number of excellent VIO systems [1]–[5] have emerged with the efforts of researchers. However, VIO will inevitably suffer drift due to its global unobservable property [6]. To ease the drift, it is required to introduce the measurements beyond self-perception. Pre-built visual maps are commonly employed to relieve the drift of VIO. Especially, it would be favorable if there is more than one visual map available to constrain the drift of VIO and therefore improve positioning accuracy.

There are lots of algorithms improving the performance of VIO by fusing the pre-built map information [7]–[11]. However, the majority of these algorithms only support one global consistent map. Therefore, to assist VIO with multiple maps<sup>1</sup>, some tedious and complicated pre-works are required to concatenate and fuse these maps into one global consistent map. Usually, a single visual map can be generated by simultaneous localization and mapping (SLAM) [12] or structure from motion (SFM) [13]. Nevertheless, for a large scenario, either building a big consistent map directly or merging several maps into one big map is quite time-consuming and complicated. Especially, to consistently fuse multiple maps, it is necessary to consider the covariance

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<sup>1</sup>In the rest of the paper, when we mention "map(s)", it means the prebuilt map(s) instead of the map(s) built online.

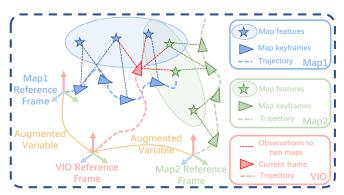


Fig. 1. An intuitive illustration of our proposed Multiple Isolated Maps Based Visual Inertial Odometry (MIMB-VIO). In MIMB, both VIO and the augmented variables are online estimated. When the current frame of the VIO observes the features of the multiple isolated maps, these map-based observations are used to update the state of MIMB-VIO.

matrices of the submaps, which makes the problem more complicated.

An intuitive idea to utilize multiple maps is to regard them as multiple submaps. But how to acquire the relative transformation with covariance matrices between these multiple submaps is a problem. Huang et al. proposed a method to join submaps by performing data association between two adjacent submaps [14]. This method requires the submaps have co-vision areas. Besides, it is an offline map-building algorithm instead of utilizing multiple submaps to assist VIO localization. DuToit et al. proposed a method to compute the relative transformation between two sub-maps by partitioning the original map. After the partition, a relaxation strategy is employed so that these two submaps are independent [9]. However, this method still relies on a pre-built global consistent map, and there is a loss of accuracy in the map because of the relaxation strategy.

Since building a global consistent map from multiple isolated maps is time-consuming and complicated, and partitioning the global map into multiple submaps introduces the approximation, we argue that during the procedure of VIO, it is better to directly utilize multiple isolated (sub)maps and online estimate the relative transformations among them. In order to be lightweight and computationally efficient, a filter-based framework is employed to solve the problem of the multiple isolated maps based VIO (MIMB-VIO). For a filter-based algorithm, how to maintain the consistency of the system is the key. To be specific, on the one hand, because the pre-built maps are not *perfect* (100% accurate), the covariance of these maps needs to be correctly considered. On the other hand, the observability properties of the MIMB-VIO need to be analyzed and correctly maintained. In this

paper, based on the above two points, we investigate how to fuse multiple isolated maps into VIO consistently.

As indicated in Fig. 1, in our proposed framework, MIMB-VIO estimates the robot pose in the VIO reference frame as well as the relative transformations between the VIO reference frame and the multiple isolated maps reference frames (the orange curved arrows)<sup>2</sup> simultaneously. In this way, the multiple maps, i.e., Map1 and Map2 in Fig. 1, can be fused into the VIO system without the need to build a global consistent map. We call the MIMB-VIO system that maintains the augmented variable(s) as the augmented system. By investigating the observability properties of the augmented system, we find that the augmented variables can be regarded as 6 degree-of-freedom (DoF) features maintained by the state. To maintain the consistency of the augmented system, we employ the Schmidt EKF [15] to consider the uncertainties of the maps while keeping the computational complexity at a low level. Besides, the firstestimate Jacobian (FEJ) technique is introduced to preserve the correct observability properties of the system. According to the simulations and experiments, we validated that consistently fusing multiple maps can significantly improve the performance of the VIO whereas the inconsistent augmented system will produce even worse results than the VIO. In summary, the contributions of this paper are four-folded:

- Propose a filter-based framework that fuses multiple isolated maps into the VIO system to improve localization accuracy.
- Analyze the observability properties of our proposed MIMB-VIO system.
- Introduce Schmidt EKF and FEJ to make the system consistent.
- Validate the effectiveness and consistency of the proposed method. The source code of our proposed algorithm is released.<sup>3</sup>

## II. RELATED WORKS

This section gives a brief review of the related works from two perspectives: the map-based localization system and the observability of the VIO system.

## A. Map-based Localization Systems

Map-based localization systems can be classified into optimization-based [7], [10], [16] and filter-based [8], [9], [17]. In these works, a trade-off has been made between the computation and the consideration of map uncertainty. To be specific, most of them [7], [8], [10], [16] highly rely on the accuracy of the pre-built map and neglect the uncertainty of the map. [17] considers the map uncertainty by utilizing the covariance intersection (CI) method. The work [9] considers the map uncertainty through the Schmidt filter. However, all these methods perform localization on a global consistent map. The framework of [9] inspires us to design the framework for the MIMB-VIO system. In [9],

#### TABLE I

THE DECIMITION	OF IMMOLVED	DEFEDENCE I	FRAMES/SENSORS
THE DEFINITION	OF INVOLVED	REFERENCE	EKAMES/SENSUKS

- The local inertial reference frame, which is a fixed frame defined by the initial pose of VIO (c.f. L in Fig. 2).

  The ith map reference frame. All the ith-map-related information (including map keyframes and map features) is based on this frame (c.f.  $G^1$  and  $G^2$  in Fig. 2).

  The IMU (body) frame at timestamp t, which is attached
- $I_t$  to the robot. VIO online estimates the transformation between L and  $I_t$ , i.e.,  ${}^L\mathbf{T}_{I_t}{}^4$ .
- $C_t$  The camera (image) frame at timestamp t. The camera online observes features in  $C_t$ .
- The  $j^{th}$  image keyframe of the ith pre-built map, whose pose  ${}^{i}KF_{j}{}^{G^{i}}\mathbf{T}_{KF_{j}}$  is represented in  $G^{i}$  (cf.  ${}^{2}KF_{1}$  and  ${}^{1}KF_{1}$  in Fig. 2). After the ith map is built, the keyframes  $\{{}^{i}KF_{j}\}$  are fixed.

the relative transformation between the map reference frame and the VIO reference frame (i.e. our defined *augmented variable*) is maintained. To reduce the computational cost, the authors propose a relaxation method to partition the global map into several sub-maps. Nevertheless, as we will demonstrate in Sec. IV, the formulation like [9] will suffer from inconsistency. This problem will be solved in Sec. V. Besides, [9] still needs a global consistent map instead of directly employing several isolated maps.

## B. Observability Analysis of the Visual Inertial Odometry

The filter-based VIO has the demerit of acquiring spurious information along the unobservable direction due to the everchanging linearization points [6]. There are several works trying to relieve the inconsistency of the VIO by fixing the linearization point [18], searching for a linearization point in the observable subspace [6], or reformulating the state error on the manifold [19]. Unfortunately, since our proposed *augmented system* introduces additional variables like the *augmented variables* and map information, the observability properties of the pure VIO cannot reflect that of the *augmented system*. The main contribution of this paper is providing a theoretical analysis of the observability properties of the *augmented system*.

#### III. SYSTEM FRAMEWORK

In this section, we will introduce the involved frame of the *augmented system*, the state of the system, the propagation of the state, and the observation functions used for updating the state. The backbone of our framework is a VIO system Open-VINS [2], which is a state-of-the-art implementation of MSCKF [1].

#### A. Involved Frames

As is shown in Fig. 2 and Table I, for the *augmented* system there are five kinds of frames, i.e., L,  $I_t$ ,  $C_t$ ,  $G^i$ , and  ${}^iKF_j$ , where L,  $I_t$ , and  $C_t$  are VIO-related frames, and  $G^i$  and  ${}^iKF_j$  are map-related frames.

<sup>&</sup>lt;sup>2</sup>For simplicity, we call this kind of relative transformation(s) the *augmented variable(s)*.

<sup>3</sup>https://github.com/zhuqingzhang/C-MIMB-VIO

 $<sup>^4</sup>$ In this paper, we use  ${\bf T}$  to represent a pose or a transformation.  $^L{\bf T}_{I_t}$  means the pose of the frame  $I_t$  in the frame L, or transforming a state from the frame  $I_t$  to the frame L.

## B. System State

We extend the state of Open-VINS [2] to get the *augmented system* state  $\mathbf{x}_t$ :

$$\mathbf{x}_{t} = \begin{bmatrix} \mathbf{x}_{VIO_{t}}^{\top} & \mathbf{x}_{SW_{t}}^{\top} & \mathbf{x}_{\tau_{t}}^{\top} & \mathbf{x}_{KF_{t}}^{\top} \end{bmatrix}^{\top}$$
(1)
$$\mathbf{x}_{VIO_{t}} = \begin{bmatrix} I_{t} \mathbf{q}_{L}^{\top} & L \mathbf{v}_{I_{t}}^{\top} & L \mathbf{p}_{I_{t}}^{\top} & \mathbf{b}_{g_{t}}^{\top} & \mathbf{b}_{a_{t}}^{\top} \end{bmatrix}^{\top}$$

$$\mathbf{x}_{SW_{t}} = \begin{bmatrix} I_{t} \mathbf{q}_{L}^{\top} & L \mathbf{p}_{I_{t}}^{\top} & \cdots & I_{t-B+1} \mathbf{q}_{L}^{\top} & L \mathbf{p}_{I_{t-B+1}}^{\top} \end{bmatrix}^{\top}$$

$$\mathbf{x}_{\tau_{t}} = \begin{bmatrix} G_{t}^{1} \mathbf{q}_{L}^{\top} & G_{t}^{1} \mathbf{p}_{L}^{\top} & \cdots & G_{t}^{N} \mathbf{q}_{L}^{\top} & G_{t}^{N} \mathbf{p}_{L}^{\top} \end{bmatrix}^{\top}$$

$$\mathbf{x}_{KF_t} = \begin{bmatrix} \cdots^{G_t^1} \mathbf{q}_{kf_j}^\top & G_t^1 \mathbf{p}_{kf_j}^\top \cdots G_t^N \mathbf{q}_{kf_k}^\top & G_t^N \mathbf{p}_{kf_k}^\top \cdots \end{bmatrix}^\top$$

where  $\mathbf{x}_{VIO_t}$  and  $\mathbf{x}_{SW_t}$  form the original state of Open-VINS [2],  $\mathbf{x}_{\tau_t}$  and  $\mathbf{x}_{KF_t}$  are the augmented parts. To be specific, for  $\mathbf{x}_{VIO_t}$ ,  $^{I_t}\mathbf{q}_L$  is the unit quaternion that transforms a 3D vector from L to  $I_t$ ,  $^{L}\mathbf{p}_{I_t}$  is the position of  $I_t$  in L,  $^{L}\mathbf{v}_{I_t}$  is the velocity of  $I_t$  in the frame L, and  $\mathbf{b}_{g_t}$  and  $\mathbf{b}_{a_t}$  are the bias of gyroscope and accelerometer. VIO outputs the pose  $^{L}\mathbf{T}_{I_t} \triangleq \{^{I_t}\mathbf{q}_L, ^{L}\mathbf{p}_{I_t}\}$ .  $\mathbf{x}_{SW_t}$  contains B cloned historical body poses, which is the so-called sliding window. Suppose we have N isolated pre-built maps, then the elements  $^{G_t^i}\mathbf{q}_L$ ,  $^{G_t^i}\mathbf{p}_L$ ,  $i=1\cdots N$  represent the relative transformation between the local VIO reference frame L and the ith map reference frame  $G^i$ , i.e., the so-called augmented variable.  $\mathbf{x}_{KF_t}$  contains a set of keyframe poses from N isolated maps. For instance,  $^{G_t^1}\mathbf{q}_{kf_j}$  and  $^{G_t^1}\mathbf{p}_{kf_j}$  represent the rotation and the position of the jth keyframe from the 1st map, respectively.

## C. State Propagation

For the *augmented system* with the state defined in (1), we have the following kinematics equations:

$$\begin{cases}
I_{t}\dot{\mathbf{q}}_{L} = \frac{1}{2}\Omega(\boldsymbol{\omega}_{m_{t}} - \mathbf{b}_{g_{t}} - \mathbf{n}_{g_{t}})^{I_{t}}\mathbf{q}_{L} \\
L\dot{\mathbf{v}}_{I_{t}} = C(^{I_{t}}\mathbf{q}_{L})^{\top}(\mathbf{a}_{m_{t}} - \mathbf{b}_{a_{t}} - \mathbf{n}_{a_{t}}) + \mathbf{g} \\
L\dot{\mathbf{p}}_{I_{t}} = ^{L}\mathbf{v}_{I_{t}} \\
\dot{\mathbf{b}}_{g_{t}} = \mathbf{n}_{wg_{t}} \dot{\mathbf{b}}_{a_{t}} = \mathbf{n}_{wa_{t}} \\
G_{t}^{i}\dot{\mathbf{q}}_{L} = \mathbf{0} & G_{t}^{i}\dot{\mathbf{p}}_{L} = \mathbf{0} \\
G_{t}^{i}\dot{\mathbf{q}}_{kf_{j}} = \mathbf{0} & G_{t}^{i}\dot{\mathbf{p}}_{kf_{j}} = \mathbf{0}
\end{cases}$$
(2)

where we argue that the *augmented variable* and the keyframe pose from maps should be static.  $C(\cdot)$  transforms a quaternion to a rotation matrix  $\mathbf{R}$ ,  $\omega_{m_t}$  and  $\mathbf{a}_{m_t}$  are the measurements from IMU in frame L,  $\mathbf{n}_{g_t}$  and  $\mathbf{n}_{a_t}$  are the measurement noises,  $\mathbf{n}_{wg_t}$  and  $\mathbf{n}_{wa_t}$  are the random walk noises,  $\mathbf{g} = \begin{bmatrix} 0 & 0 & -9.81 \end{bmatrix}^{\top} m/s^2$  is the gravitational acceleration in L. For a vector  $\boldsymbol{\omega} \in \mathbb{R}^3$ , we have

$$\Omega(\boldsymbol{\omega}) = egin{bmatrix} -\boldsymbol{\omega}_{ imes} & \boldsymbol{\omega} \\ \boldsymbol{\omega}^{ op} & 0 \end{bmatrix}.$$

By discretizing (2), we can propagate the state from time step t to time step t+1:

$$\mathbf{x}_{t+1|t} = \mathbf{f}(\mathbf{x}_t, \mathbf{a}_{m_t} - \mathbf{n}_{a_t}, \omega_{m_t} - \mathbf{n}_{\omega_t})$$
(3)

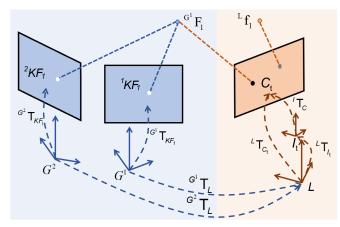


Fig. 2. The observation functions

where  $\mathbf{f}(\cdot)$  is the discretized propagation function derived from (2), the subscript t+1|t means the state is propagated from t to t+1, with all the measurements up to time step t being processed. Then, the state covariance can be propagated by

$$\mathbf{P}_{t+1|t} = \mathbf{\Phi}_{t+1|t} \mathbf{P}_t \mathbf{\Phi}_{t+1|t}^{\top} + \mathbf{G}_{t+1|t} \mathbf{Q}_t \mathbf{G}_{t+1|t}^{\top}$$
(4)

where  $\mathbf{P}_t$  and  $\mathbf{Q}_t$  are the system state covariance and the noise covariance, respectively.  $\mathbf{\Phi}_{t+1|t}$  and  $\mathbf{G}_{t+1|t}$  are the Jacobians of (3) with respect to the system state and the noise, respectively.  $\mathbf{\Phi}_{t+1|t}$  is also called state transition matrix. For the detailed derivation, please refer to [1], [2].

#### D. Observation Functions

As indicated in Fig. 2, there are two kinds of observation functions, the local feature based (the orange shade part) and the map feature based (the blue shade part).

**Local Observation:** For a local feature  ${}^{L}\mathbf{f}_{i}$ , for example,  ${}^{L}\mathbf{f}_{1}$  in Fig. 2, online detected by the camera, we have the following local observation function:

$${}^{loc}\mathbf{y}_t^i = \mathbf{h}({}^{I_t}\mathbf{R}_L({}^L\mathbf{f}_{i_t} - {}^L\mathbf{p}_{I_t})) + {}^{loc}\boldsymbol{\gamma}_t^i$$
 (5)

where for simplicity, we assume the extrinsic  ${}^{I}\mathbf{T}_{L}$  between the IMU and the camera is an identity matrix.  ${}^{I_{t}}\mathbf{R}_{L}$  is the rotation matrix from L to I.  $\mathbf{h}(\cdot)$  is the camera projection function that projects a 3D feature in the camera frame into the 2D image plane.  ${}^{loc}\gamma_{t}^{i}$  is the noise of the local observation.

With (5), the error of the local observation can be computed by:

$$\begin{aligned}
& loc \mathbf{r}_{t}^{i} \triangleq \mathbf{h}(^{I_{t}} \mathbf{R}_{L}(^{L} \mathbf{f}_{i_{t}} - ^{L} \mathbf{p}_{I_{t}})) + ^{loc} \boldsymbol{\gamma}_{t}^{i} - \\
& \mathbf{h}(^{I_{t}} \hat{\mathbf{R}}_{L}(^{L} \hat{\mathbf{f}}_{i_{t}} - ^{L} \hat{\mathbf{p}}_{I_{t}})) \\
& loc \mathbf{r}_{t}^{i} = ^{loc} \mathbf{H}_{\mathbf{x}_{t}}^{i} \tilde{\mathbf{x}}_{t} + ^{loc} \mathbf{H}_{L_{\mathbf{f}_{i_{t}}}}^{L} \tilde{\mathbf{f}}_{i_{t}} + ^{loc} \boldsymbol{\gamma}_{t}^{i}
\end{aligned} \tag{6}$$

where  $\hat{\cdot}$  represents the estimated value of the variable,  $\tilde{\cdot}$  represents the error between the true value and the estimated value of the variable.  $^{loc}\mathbf{H}_{x_t}^i$  and  $^{loc}\mathbf{H}_{L\mathbf{f}_{i_t}}$  represent the Jacobian matrices of h with respect to  $\mathbf{x}_t$  and  $^{L}\mathbf{f}_{i_t}$ , respectively.

Note that in the framework of MSCKF [1] we do not maintain the local features in the state vector, so that the Jacobian matrix of h with respect to the local feature  ${}^{L}\mathbf{f}_{i_t}$ 

should be null-space projected to eliminate. The sliding window  $\mathbf{x}_{SW}$  provides us an opportunity to achieve this purpose: a local feature can be observed not only by the current camera frame but also by the historical successive camera frames. This means for each local feature, there is more than one (say  $n \geq 2$ ) local observation function. By stacking these local observation functions, the row number (2n) of the Jacobian matrix with respect to the local feature  $^L\mathbf{f}_{i_t}$  is larger than its column number (3, the dimension of the local feature), which guarantees the existence of the left null-space of the Jacobian matrix of h with respect to  $^L\mathbf{f}_{i_t}$ . For the details, please refer to [1].

**Map-based Observation:** For a feature from a pre-built map, it can be observed by the current camera  $C_t$  and keyframes  ${}^iKF_j$  from different maps, as indicated by the blue shade part of Fig. 2. Suppose there is a feature  ${}^{G^k}\mathbf{F}_i$  from the kth map, observed by the jth keyframe  ${}^kKF_j$  in the kth map. Besides,  ${}^{G^k}\mathbf{F}_i$  can also be observed by the current camera frame C and the kth keyframe kth in the kth kth map. For example, by setting k1, k2, k3, k4, k5, k6, k7, k8, k9, k9

$$^{cam}\mathbf{y}_{t}^{ki} = \mathbf{h} \left[ {}^{I_{t}}\mathbf{R}_{L} ({}^{G_{t}^{k}}\mathbf{R}_{L}^{\mathsf{T}} ({}^{G^{k}}\mathbf{F}_{i_{t}} - {}^{G_{t}^{k}}\mathbf{p}_{L}) - {}^{L}\mathbf{p}_{I_{t}}) \right] + {}^{cam}\boldsymbol{\gamma}_{t}^{ki}$$

$$(7)$$

$${}^{kKF_{j}}\mathbf{y}_{t}^{ki} = h\left[{}^{G_{t}^{k}}\mathbf{R}_{kf_{j}}^{\top}({}^{G^{k}}\mathbf{F}_{i_{t}} - {}^{G_{t}^{k}}\mathbf{p}_{kf_{j}})\right] + {}^{kKF_{j}}\boldsymbol{\gamma}_{t}^{ki} \quad (8)$$

$$\mathbf{y}_{t}^{ki} = \mathbf{h} \begin{bmatrix} G_{t}^{s} \mathbf{R}_{kfl}^{\top} & G_{t}^{s} \mathbf{R}_{L} & G_{t}^{k} \mathbf{R}_{L}^{\top} & G_{t}^{k} \mathbf{P}_{i_{t}} - G_{t}^{k} \mathbf{p}_{L} \end{pmatrix} + G_{t}^{s} \mathbf{p}_{L} - G_{t}^{s} \mathbf{p}_{kf_{l}} \end{bmatrix} + KF_{l} \boldsymbol{\gamma}_{t}^{ki}$$

$$(9)$$

where  ${}^{cam}\mathbf{y}_t^{ki}$ ,  ${}^{kKF_j}\mathbf{y}_t^{ki}$  and  ${}^{sKF_l}\mathbf{y}_t^{ki}$  represent the observations to the feature  ${}^{G^k}\mathbf{F}_i$  by the current camera, the map keyframe  ${}^kKF_j$  and the map keyframe  ${}^sKF_l$ , respectively.  ${}^{cam}\boldsymbol{\gamma}_t^{ki}$ ,  ${}^{kKF_j}\boldsymbol{\gamma}_t^{ki}$  and  ${}^{sKF_l}\boldsymbol{\gamma}_t^{ki}$  are the corresponding observation noises. For simplicity, we assume the extrinsic  ${}^I\mathbf{T}_C$  between the IMU and the camera is an identity matrix.

Similar to (6), we have the following map-based observation errors derived from (7)-(9):

$$^{cam}\mathbf{r}_{t}^{ki} = ^{cam}\mathbf{H}_{\mathbf{x}_{t}}^{ki}\tilde{\mathbf{x}}_{t} + ^{cam}\mathbf{H}_{G^{k}}\mathbf{F}_{i_{t}}^{G^{k}}\tilde{\mathbf{F}}_{i_{t}} + ^{cam}\boldsymbol{\gamma}_{t}^{ki} \quad (10)$$

$${}^{kKF_{j}}\mathbf{r}_{t}^{ki} = {}^{kKF_{j}}\mathbf{H}_{\mathbf{x}_{t}}^{ki}\tilde{\mathbf{x}}_{t} + {}^{kKF_{j}}\mathbf{H}_{G^{k}}\mathbf{F}_{i_{t}} {}^{G^{k}}\tilde{\mathbf{F}}_{i_{t}} + {}^{kKF_{j}}\boldsymbol{\gamma}_{t}^{ki}$$

$$\tag{11}$$

$${}^{sKF_{l}}\mathbf{r}_{t}^{ki} = {}^{sKF_{l}}\mathbf{H}_{\mathbf{x}_{t}}^{ki}\tilde{\mathbf{x}}_{t} + {}^{sKF_{l}}\mathbf{H}_{G^{k}}\mathbf{F}_{i,} + {}^{sKF_{l}}\boldsymbol{\gamma}_{t}^{ki}$$
(12)

Again, as we do not maintain the map feature  ${}^{G^k}\mathbf{F}_{i_t}$  in the state vector, the Jacobian matrices related to  ${}^{G^k}\mathbf{F}_{i_t}$  should be null-space projected. Fortunately, as shown in (7)-(9), for each feature  ${}^{G^k}\mathbf{F}_{i_t}$ , it corresponds to at least two observation functions (if the feature  ${}^{G^k}\mathbf{F}_{i_t}$  is observed only by the keyframe in the kth map, (9) vanishes), which means we can find a left null-space matrix to eliminate the  ${}^{G^k}\tilde{\mathbf{F}}_{i_t}$  related parts.

## IV. OBSERVABILITY ANALYSIS

Given the system mentioned in Sec. III, we need to investigate its observability properties, which can indicate the consistency of the system [6], [18].

The unobservable subspace of the system is the right null space of the observability matrix of the system. The observability matrix of the proposed system can be given by:

$$\mathbf{M} \triangleq \begin{bmatrix} \mathbf{H}_{L_0} \\ \mathbf{H}_{G_0} \\ \mathbf{H}_{L_1} \mathbf{\Phi}_{1|0} \\ \mathbf{H}_{G_1} \mathbf{\Phi}_{1|0} \\ \vdots \\ \mathbf{H}_{L_t} \mathbf{\Phi}_{t|0} \\ \mathbf{H}_{G_t} \mathbf{\Phi}_{t|0} \end{bmatrix} \triangleq \begin{bmatrix} \mathbf{M}_{L_0} \\ \mathbf{M}_{G_0} \\ \mathbf{M}_{L_1} \\ \mathbf{M}_{G_1} \\ \vdots \\ \mathbf{M}_{L_t} \\ \mathbf{M}_{G_t} \end{bmatrix}$$
(13)

where  $\mathbf{H}_{L_t}$  represents the Jacobian matrix of the local observation function, corresponding to  $\begin{bmatrix} ^{loc}\mathbf{H}_{\mathbf{x}_t}^i & ^{loc}\mathbf{H}_{L_{\mathbf{f}_{i_t}}} \end{bmatrix}$ .  $\mathbf{H}_{G_t}$  represents the Jacobian matrix of the map-based observation function, which is the stacking matrix along the row direction of  $\begin{bmatrix} ^{cam}\mathbf{H}_{\mathbf{x}_t}^{ki} & ^{cam}\mathbf{H}_{G^k\mathbf{F}_{i_t}} \end{bmatrix}$ ,  $\begin{bmatrix} ^{k}KF_j\mathbf{H}_{\mathbf{x}_t}^{ki} & ^{k}KF_j\mathbf{H}_{G^k\mathbf{F}_{i_t}} \end{bmatrix}$  and  $\begin{bmatrix} ^{s}KF_l\mathbf{H}_{\mathbf{x}_t}^{ki} & ^{s}KF_l\mathbf{H}_{G^k\mathbf{F}_{i_t}} \end{bmatrix}$ . The transition matrix from time step 0 to time step t can be computed by  $\mathbf{\Phi}_{t|0} \triangleq \mathbf{\Phi}_{t|t-1} \dots \mathbf{\Phi}_{2|1}\mathbf{\Phi}_{1|0}^{.5}$ 

As the Jacobian matrices of local and map features are considered here, we need to put these features in the state vector. Besides, for simplicity, the IMU bias and cloned state are omitted. Therefore, the new augmented state is given as:

$$\mathbf{x}_{Aug_t} = \begin{bmatrix} I_t \mathbf{q}_L^\top & L \mathbf{v}_{I_t}^\top & L \mathbf{p}_{I_t}^\top & L \mathbf{f}_{i_t}^\top & G_t^k \mathbf{q}_L^\top & G_t^k \mathbf{p}_L^\top & G_t^s \mathbf{q}_L^\top \\ & & & & & & & & & & & & & \\ G_t^s \mathbf{p}_L^\top & G^k \mathbf{F}_{i_t}^\top & G_t^k \mathbf{q}_{kf_j}^\top & G_t^k \mathbf{p}_{kf_j}^\top & G_t^s \mathbf{q}_{kf_l}^\top & G_t^s \mathbf{p}_{kf_l}^\top \end{bmatrix}^\top$$
(14)

where the elements before the first | are VIO-related, those after the first | are the *augmented variables*, and those after the second | are map-related. We assume all the features are static, i.e., the derivations of their positions are zero.

To investigate the observability properties of the *augmented system*, we should first consider the ideal case where all the values are given by ground truth. Then, the actual case is considered where all the values are given by estimation. If the observability of the actual case is different from that of the ideal case, the system will suffer from inconsistency.

Theorem 1: (Ideal observability properties of the augmented system) For the ideal case, the right null space  $\mathcal{N}_i$  of the observability matrix, where the Jacobian matrices are evaluated with the true values, is spanned by ten (four plus

 $<sup>^5</sup>$ Note that there is a slight abuse of symbol. The dimension of  $\Phi$  in this section is different from that in (4). In this section,  $\Phi$  is augmented by the local feature related and the map feature related parts.

six) directions:

$$\mathcal{N}_i = \begin{bmatrix} {}^{I_0}\mathbf{R}_L\mathbf{g} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -({}^{L}\mathbf{v}_{I_0})_{\times}\mathbf{g} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -({}^{L}\mathbf{p}_{I_0})_{\times}\mathbf{g} & \mathbf{I} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -({}^{L}\mathbf{p}_{I_0})_{\times}\mathbf{g} & \mathbf{I} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -({}^{L}\mathbf{f}_i)_{\times}\mathbf{g} & \mathbf{I} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ -({}^{L}\mathbf{f}_i)_{\times}\mathbf{g} & \mathbf{I} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ {}^{G^k}\mathbf{R}_L\mathbf{g} & \mathbf{0} & \mathbf{I} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & -{}^{G^k}\mathbf{R}_L & \mathbf{0} & \mathbf{I} & \mathbf{0} \\ \mathbf{0} & -{}^{G^k}\mathbf{R}_L & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & ({}^{G^k}\mathbf{F}_i - {}^{G^k}\mathbf{p}_L)_{\times} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{$$

Theorem 2: (Actual observability properties of the augmented system) For the actual case, the right null space  $\mathcal{N}_a$  of the observability matrix, where the Jacobian matrices are evaluated with the estimated values, is spanned by three directions:

$$\mathcal{N}_a = \begin{bmatrix} \mathbf{0}_{3\times15} & \mathbf{I} & \mathbf{0} & \mathbf{I} & \mathbf{I} & \mathbf{0} & \mathbf{I} & \mathbf{0} & \mathbf{I} \end{bmatrix}^{\top}$$
(16)   
Proof: See Appendix I.

From the above two theorems, we can find that compared with the ideal case, seven unobservable directions vanish for the actual case. This means if we use the estimated values to compute Jacobian matrices, the MIMB-VIO system will suffer from inconsistency. Readers can find more detailed analysis in **Appendix I**.

To reveal how the introduced *augmented variables* affect the observability properties of the *augmented system*, we further investigate a special case: when the maps are *perfect*, i.e., the *augmented system* does not need to consider the uncertainty of the maps, then the map-related elements in (14) are removed. In this case, we can derive the following two Theorems:

Theorem 3: (Ideal observability properties of the augmented system with perfect maps) For the ideal case, when system-used maps are perfect, the right null space  $\mathcal{N}_{ip}$  of the observability matrix, where the Jacobian matrices are evaluated with the true values, is spanned by four directions:

$$\mathcal{N}_{ip} = \begin{bmatrix} I_0 \mathbf{R}_L \mathbf{g} & \mathbf{0} \\ -(^L \mathbf{v}_{I_0})_{\times} \mathbf{g} & \mathbf{0} \\ -(^L \mathbf{p}_{I_0})_{\times} \mathbf{g} & \mathbf{I} \\ -(^L \mathbf{f}_i)_{\times} \mathbf{g} & \mathbf{I} \\ G^k \mathbf{R}_L \mathbf{g} & \mathbf{0} \\ \mathbf{0} & -G^k \mathbf{R}_L \\ G^s \mathbf{R}_L \mathbf{g} & \mathbf{0} \\ \mathbf{0} & -G^s \mathbf{R}_L \end{bmatrix}$$
(17)

*Proof:* See **Appendix I**.

Theorem 4: (Actual observability properties of the augmented system with perfect maps) For the actual case, when system used maps are perfect, the original four unobservable directions vanish:

We can find when the maps are *perfect*, for the ideal case, the dimension of the unobservable subspace of the *augmented system* is the same as the dimension of the unobservable subspace of the VI-SLAM system — four dimensions. Actually, the *augmented variables* can be regarded as 6 DoF pose features maintained in the state. Every time a map-based observation occurs, it is equivalent to the *augmented system* observing these pose features, similar to that the VI-SLAM system closes a loop. Therefore, consistently estimating these pose features (i.e., *augmented variables*) can efficiently improve the performance of the VI-SLAM system (i.e., *augmented system*). However, in the actual case, the original four unobservable directions vanish because of the introduced *augmented variables*.

For the case that the maps are *imperfect*, we need to consider their uncertainties, then an additional six-dimensional unobservable subspace is introduced to the *augmented system*, as indicated by (15).

For the detailed derivation and analysis, please refers to **Appendix** I.

#### V. Consistent Estimation

Inconsistency stems from 1) mistakenly considering the uncertainty of the fused information; 2) mistakenly maintaining the observability properties of the system. Aiming to 1), we add the map information (keyframe poses) into the state vector like (1) to consider the uncertainty of the map keyframe poses. However, if we update all the state values like standard EKF, the huge computation would be unaffordable. Aiming to 2), as mentioned in Sec. IV, the ever-changing estimated value of the (3 DoF and 6 DoF) features will break the original observability properties of the system, resulting in inconsistency. Therefore, the Schmidt updating [15] and the first estimate Jacobian (FEJ) [18] techniques are introduced in this section to make the system efficient and consistent.

## A. Schmidt Updating

Schmidt updating is only used for map-based observations. When there are measurements from maps, we have (10)-(12). By stacking them along the row and performing left null-space projection to eliminate the map feature related part, we have the following concise expression:

$$\mathbf{r}_{t}^{*} = \mathbf{H}_{\mathbf{x}_{t}}^{*} \tilde{\mathbf{x}}_{t} + \boldsymbol{\gamma}_{t}^{*}$$

$$\triangleq \begin{bmatrix} \mathbf{H}_{A_{t}}^{*} & \mathbf{H}_{N_{t}}^{*} \end{bmatrix} \begin{bmatrix} \tilde{\mathbf{x}}_{A_{t}} \\ \tilde{\mathbf{x}}_{N_{t}} \end{bmatrix} + \boldsymbol{\gamma}_{t}^{*}$$
(18)

where we partition the state  $\mathbf{x}_t$  into the two parts,  $\mathbf{x}_{A_t}$  and  $\mathbf{x}_{N_t}$ .  $\mathbf{x}_{A_t}$  is composed of  $\mathbf{x}_{VIO_t}$ ,  $\mathbf{x}_{SW_t}$  and  $\mathbf{x}_{\tau_t}$ .  $\mathbf{x}_{N_t}$  is map keyframe related part, i.e.,  $\mathbf{x}_{KF_t}$ .  $\mathbf{H}_{A_t}^*$  and  $\mathbf{H}_{N_t}^*$  are the Jacobian matrices corresponding to  $\mathbf{x}_{A_t}$  and  $\mathbf{x}_{N_t}$ , respectively.

Then, the Schmidt updating can be performed with the following equations:

$$\hat{\mathbf{x}}_{A_t} = \hat{\mathbf{x}}_{A_{t|t-1}} + \mathbf{K}_{A_t} \mathbf{r}_t^* 
\hat{\mathbf{x}}_{N_t} = \hat{\mathbf{x}}_{N_{t|t-1}}$$
(19)

$$\begin{bmatrix} \mathbf{K}_{A_{t}} \\ \mathbf{K}_{N_{t}} \end{bmatrix} \triangleq \begin{bmatrix} \bar{\mathbf{K}}_{A_{t}} \\ \bar{\mathbf{K}}_{N_{t}} \end{bmatrix} \mathbf{S}_{t}^{-1} = \begin{bmatrix} \mathbf{P}_{AA_{t|t-1}} \mathbf{H}_{A_{t}}^{*\top} + \mathbf{P}_{AN_{t|t-1}} \mathbf{H}_{N_{t}}^{*\top} \\ \mathbf{P}_{NA_{t|t-1}} \mathbf{H}_{A_{t}}^{*\top} + \mathbf{P}_{NN_{t|t-1}} \mathbf{H}_{N_{t}}^{*\top} \end{bmatrix} \mathbf{S}_{t}^{-1} \\
\mathbf{S}_{t} = \mathbf{H}_{\mathbf{x}_{t}}^{*} \mathbf{P}_{t|t-1} \mathbf{H}_{\mathbf{x}_{t}}^{*\top} + \mathbf{R}_{t} \\
\mathbf{P}_{t} = \mathbf{P}_{t|t-1} - \begin{bmatrix} \mathbf{K}_{A_{t}} \mathbf{S}_{t} \mathbf{K}_{A_{t}}^{\top} & \mathbf{K}_{A_{t}} \mathbf{H}_{t}^{*} \begin{bmatrix} \mathbf{P}_{AN_{t|t-1}} \\ \mathbf{P}_{NN_{t|t-1}} \end{bmatrix} \\ \begin{bmatrix} \mathbf{P}_{AN_{t|t-1}} \\ \mathbf{P}_{NN_{t|t-1}} \end{bmatrix}^{\top} \mathbf{H}_{t}^{*\top} \mathbf{K}_{A_{t}}^{\top} & \mathbf{0}_{\mathfrak{m} \times \mathfrak{m}} \end{bmatrix}$$
(21)

where m is the dimension of the map keyframe poses.

We can find that, in Schmidt updating, the map keyframe related part in the state is not updated, and neither is the corresponding covariance. This mechanism guarantees low computation. For the standard EKF updating,  $\mathbf{0}_{m \times m}$  in (21) is replaced by  $\mathbf{K}_{N_t} \mathbf{S}_t \mathbf{K}_{N_t}^{\top}$ , which makes the computational complexity increase from  $\mathcal{O}(m)$  to  $\mathcal{O}(m^2)$ . Besides, the relation between the updated covariance matrices from the Schmidt updating and from the standard EKF updating is that  $\mathbf{P}_{Schmidt} = \mathbf{P}_{EKF} + \begin{bmatrix} \mathbf{0} \\ \bar{\mathbf{K}}_N \end{bmatrix} \mathbf{S}^{-1} \begin{bmatrix} \mathbf{0} & \bar{\mathbf{K}}_N^{\top} \end{bmatrix}$ , which means compared with the covariance from the standard EKF, the covariance from the Schmidt updating will be relative conservative. If the standard EKF is not overconfident about the estimated state, then neither is the Schmidt updating. Hence, by employing the Schmidt updating, we can keep the low computation while not over-optimistically estimating the state.

## B. Observability Maintainance

From the analysis of Sec. IV, we conclude that the everchanging estimated values make the linearization points of nonlinear kinematics and observation functions also change with time, even for those state elements that should be constant. This makes the system think it can obtain information in the original unobservable subspace, leading to inconsistency. To solve this problem, we introduce the FEJ technique to constrain the system only obtaining information in the observable subspace.

To be specific, we carefully extend the traditional first-estimate Jacobian (FEJ) [18] to our *augmented system* with two steps:

- The propagation Jacobian matrix at time step t is evaluated at  $\hat{\mathbf{x}}_{t|t-1}$ .
- The map-based observation Jacobian matrix at time step t is ever evaluated at the first estimate of  ${}^{G^i}\mathbf{p}_L$ ,  ${}^{G^i}\mathbf{R}_L$  and  $\hat{\mathbf{x}}_{t|t-1}$ .

With these two steps, for the actual case, the transition matrix  $\Phi_{t|0}$  can be given by (29). Besides, the linearization points of  $G^i \mathbf{R}_L$  and  $G^i \mathbf{p}_L$  will never change. Moreover, as we do not maintain the map features in the state, their values will also be constant. At this point, the null space of the observability matrix  $\mathbf{M}$  in the actual case keeps the same as that in the ideal case.

## VI. EXPERIMENTS

In this section, we will validate the consistency of our proposed algorithm through simulation experiments. Then,

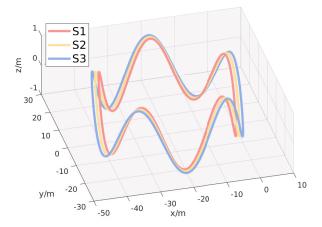


Fig. 3. The trajectories used for simulation.

real-world experiments are conducted to further illustrate the effectiveness of our proposed algorithm.

## A. Simulation Experiments

In this part, we make some adaptations to the simulator of Open-VINS [2] to evaluate the accuracy and consistency of our proposed algorithm. There are three trajectories used in the simulation, which are plotted in Fig. 3. These three trajectories are denoted as S1 (the red one), S2 (the orange one), and S3 (the blue one), respectively. When we online run one of the three trajectories (for example, S1), the other two trajectories (S2, S3) can be used as the two isolated maps. The map keyframe poses and their covariance matrices are generated by running the VIO algorithm Open-VINS [2]. For the maps S1, S2, and S3, the absolute trajectory errors (ATEs) of the map keyframe poses from Open-VINS are  $0.298^{\circ}/0.114m$ ,  $0.165^{\circ}/0.116m$  and  $0.303^{\circ}/0.172m$ , respectively. The map features are randomly extracted and triangulated with the estimated keyframe poses. The triangulated features are then reprojected into the camera frame of the online running trajectory so that we can get the feature matches between the online running trajectory and the maps.

To test the effectiveness of our proposed algorithm (called Consistent MIMB-VIO, denoted as C-MIMB-VIO), we compare it with the one that fails to maintain the correct observability properties of the system (denoted as MIMB-VIO). Furthermore, Open-VINS [2] is used as a benchmark to show that by correctly fusing the multiple isolated maps, the accuracy of the localization can be improved. The overall results are given in Table II.

In Table II, ATE is used to measure the accuracy of the localization results, and normalized estimation error squared (NEES) [2] is used to measure the consistency of the localization results. The value before and after / are corresponding to the orientation ( $^{\circ}$ ) and the position (m), respectively. For ATE, the smaller the value, the better. For NEES, if its value is larger than 1, this means the system is over-optimistic about the estimated results, i.e., the system is inconsistent. For each sequence, there are three settings:

TABLE II The ATES (degree/m) and NEESs of different algorithms on SIMULATION DATA

_	Algorithm Algorithm Algorithm Algorithm								
Seq	Sequence		Open-VINS	MIMB-VIO	C-MIMB-VIO				
	Omap	ATE	0.323/0.191	_	_				
	Omap	NEES	0.301/0.687	_	_				
	1map	ATE	· · · <u> · ·</u> · · · ·	1.142/0.545	0.282/0.154				
S1		NEES	_	19.198/9.353	0.213/0.457				
	2	ATE	· · · <u>- ·</u> · · · ·	1.131/0.541	0.278/0.149				
	2map	NEES	_	19.401/9.445	0.191/0.410				
	average	ATE	0.323/0.191	1.137/0.543	0.280/0.152				
	Omon	ATE	0.314/0.145	_	_				
	0map	NEES	0.357/0.430	_	<u> </u>				
	1map	ATE	· · · <del>· ·</del> · · ·	0.931/0.466	0.275/0.129				
S2		NEES	_	14.373/6.931	0.223/0.346				
	2map	ATE	· · · <u>- ·</u> · · ·	0.934/0.464	0.275/0.128				
		NEES	_	14.914/7.124	0.208/0.295				
	average	ATE	0.314/0.145	0.933/0.465	0.275/0.129				
	Omon	ATE	0.404/0.228	_	_				
	0map	NEES	0.407/0.772	_	<u> </u>				
S3	1,000	ATE	· · · <u> </u>	0.693/0.353	0.345/0.198				
	1map	NEES	_	6.171/3.382	0.275/0.543				
		ATE		0.668/0.351	0.350/0.188				
	2map	NEES	_	5.941/3.446	0.249/0.426				
	average	ATE	0.404/0.228	0.681/0.352	0.348/0.193				

- means there is no such variable to evaluate.

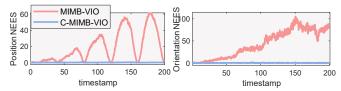


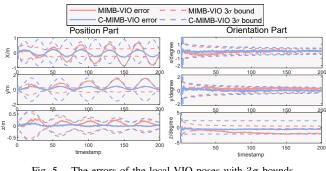
Fig. 4. The NEES of the local VIO poses

Omap means there is no map; 1map means there is one map; 2map means there are two isolated maps. From Table II, we can find that the localization accuracy of MIMB-VIO is much worse than C-MIMB-VIO. Even with the map information, ATE of MIMB-VIO is larger than the pure odometry Openv-VINS. Also, the value of NEES is much larger than 1, which means the system is inconsistent. On the contrary, because C-MIMB-VIO can maintain the correct observability properties of the system, the localization accuracy is improved with the help of external map information, and the value of NEES indicates the good consistency of the system. Fig. 4 also gives the trend of NEES derived from MIMB-VIO and C-MIMB-VIO over time. We can find that the estimation of MIMB-VIO is more and more optimistic, i.e., the estimated uncertainty is much less than the true uncertainty, resulting in a bad estimation. Different from MIMB-VIO, C-MIMB-VIO always keeps NEES at a low value. Moreover, the error of the estimated local VIO pose with its  $3\sigma$  bounds is plotted in Fig. 5. The consistent estimation from C-MIMB-VIO guarantees the estimated errors fall within the  $3\sigma$  bounds, whereas the estimation error of MIMB-VIO is out of bounds.

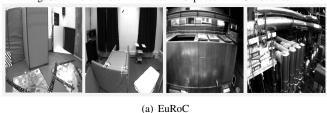
## B. Real-World Experiments

In this part, we will validate our proposed algorithm in two kinds of real-world datasets (c.f. Fig. 6), which cover the scenarios of the aerial vehicle (EuRoC [22]) and the ground vehicle in urban areas (Kaist [23]).

**EuRoC:** EuRoC [22] dataset contains three scenarios, vi-



The errors of the local VIO poses with  $3\sigma$  bounds.

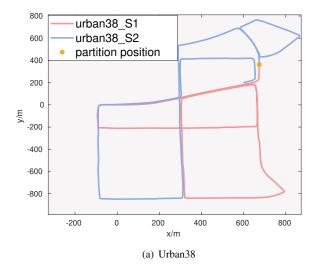


(b) Kaist

Fig. 6. The vehicles and images sampled from the two datasets.

con room 1 (V1), vicon room 2 (V2), and machine hall (MH). For our experiments, we utilize Open-VINS to generate map keyframe poses and their covariance matrices. The 3D map features are triangulated across multiple adjacent images and the corresponding poses. The feature matching procedure is conducted as follows: we first utilize R2D2 [20] to extract new features on the current queried frame and match them with features in map keyframes. The initial matching pairs based on descriptors are then fed into a robust pose estimator [21] to generate accurate feature matching pairs. For each scenario, if one of the sequences is used to query, the other sequences are employed as maps. For instance, if MH01 is the queried sequence, MH02-MH05 are used as maps.

Kaist: Kaist [23] is a dataset collected in urban onthe-road environments with many moving vehicles. In the dataset, there are two sequences, Urban38 and Urban39, having a large overlap. For each sequence, we divide its trajectory into two sessions (denoted as Urban38\_S1, Urban38\_S2, Urban39\_S1, Urban39\_S2), so that for each queried sequence, there are two isolated map sessions from the other sequence can be used. The partitioned trajectory of each sequence is plotted in Fig. 7. Because this dataset is challenging, Open-VINS will suffer significant drift and cannot be used to generate maps. Instead, we utilize the ground truth poses provided by this dataset as the keyframe poses of maps. As the ground truth built upon Virtual Reference Station (VRS)-GPS, we set the deviation of map keyframe pose as 0.1m for position parts and  $2.87^{\circ}$  (0.05rad) for orientation parts. The procedures for generating 3D map



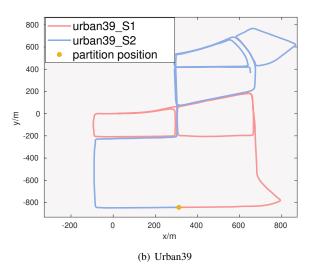


Fig. 7. The partitions of the trajectories in Kaist.

features and feature matches are the same as those in EuRoC dataset.

**Experimental Results:** To validate the accurate estimation of our proposed algorithm, we evaluate the estimated local VIO position (V.P.) as well as the relative transformations between the local VIO reference frame and the different map reference frames (augmented variables, A.V.). Besides, the results of the algorithm that regards the map as perfect (denoted as P-MIMB-VIO) are also given to demonstrate the necessity of considering the uncertainty of the map information. All the results are listed in Table III. For each queried sequence, we run experiments three times with the different numbers of maps. For example, for the queried sequence MH01, one (MH02) to four (MH02-MH05) maps will be used to perform localization. Therefore, the ATEs of V.P. for MH01 are the average of all the experimental results. Similarly, the ATEs of A.V. for MH01 are the average of the transformations between the VIO reference frame and

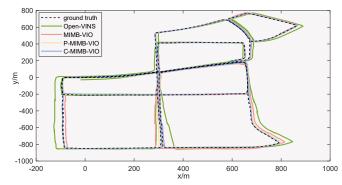


Fig. 8. The trajectory comparison on Kaist Urban38 with different algorithms

reference frames of MH02-MH05 <sup>6</sup>. From Table III, we can find that C-MIMB-VIO has the best performance for almost all cases because it consistently fuses the maps. It is worth noting that even though the map information for Kaist [23] is generated by the ground truth, C-MIMB-VIO also gives better results than P-MIMB-VIO. A trajectory comparison on Urban38 is given by Fig. 8 to provide an intuitive feeling of the performance of different algorithms.

Moreover, the average time consumptions of each step for C-MIMB-VIO in four different scenarios are also given in Table IV, where the pure VIO Open-VINS is compared as a baseline to demonstrate the efficiency of our proposed algorithm.

#### VII. CONCLUSION

In this paper, we propose a framework that can fuse the information of multiple isolated maps into the VIO system, avoiding the tough task of building a big globally consistent map. By analyzing the observability properties of the system, we introduce the Schmidt updating and FEJ to consider the uncertainty of the maps efficiently and maintain the correct observability properties of the system, so that the system can be consistent and gives good localization results. According to simulation and real-world experiments, we demonstrate the consistency of our proposed algorithm and the necessity of keeping the system consistent.

#### APPENDIX I

## OBSERVABILITY ANALYSIS OF THE AUGMENTED SYSTEM

To analyze the observability properties of *augmented system*, we should compute the observability matrix (13), which contains the transition matrices and observation Jacobian matrices.

With the state (14) and the kinematics equation (2), we can derive the transition matrix  $\Phi_{t+1|t}$  defined by:

$$\Phi_{t+1|t} = \begin{bmatrix}
\Phi_1 & 0 & 0 & 0_{3\times30} \\
\Phi_2 & \mathbf{I} & 0 & 0_{3\times30} \\
\Phi_3 & \mathbf{I}\Delta & \mathbf{I} & 0_{3\times30} \\
\mathbf{0}_{30\times3} & \mathbf{0}_{30\times3} & \mathbf{0}_{30\times3} & \mathbf{I}_{30}
\end{bmatrix}, (22)$$

<sup>6</sup>Table VI-B also gives the detailed results for each sequence with the different number of used maps, and Table VI gives the detailed results of the *augmented variables* between the queried sequence and the used prebuilt maps. Table III only lists the average data.

ATES(m) OF LOCAL VIO POSITION (V.P.), ATES(degree/m) OF ROTATION PART (R.) AND POSITION PART (P.) OF augmented variable (A.V.)

		Sequence	MH01	MH02	MH03	MH04	MH05	V101	V102	V103	V201	V202	V203	Urban38	Urban39
Alg	orithn	n —													
		Open-VINS	0.090	0.101	0.144	0.190	0.246	0.046	0.058	0.047	0.073	0.059	0.117	24.886	7.061
V.F	,	MIMB-VIO	0.070	0.063	0.152	0.193	0.280	0.039	0.074	0.047	0.068	0.104	0.083	13.773	10.539
V.F	•	P-MIMB-VIO	0.073	0.074	0.128	0.229	0.218	0.056	0.050	0.081	0.071	0.123	0.105	5.969	5.614
		C-MIMB-VIO	0.056	0.059	0.085	0.161	0.187	0.032	0.043	0.043	0.066	0.056	0.082	5.205	5.376
		MIMB-VIO	1.657	3.126	1.546	3.398	1.747	4.662	5.230	2.169	2.931	9.349	2.494	1.176	1.453
	R.	P-MIMB-VIO	1.567	2.233	1.256	1.784	2.031	1.364	0.736	1.446	2.220	3.300	1.851	0.877	0.760
A.V.		C-MIMB-VIO	1.304	2.301	1.149	1.237	1.388	0.972	0.825	0.993	1.452	3.093	2.038	0.795	0.746
Α. ν.		MIMB-VIO	0.138	0.162	0.137	0.189	0.391	0.049	0.118	0.076	0.099	0.230	0.124	6.437	2.922
	P.	P-MIMB-VIO	0.202	0.173	0.147	0.228	0.544	0.067	0.112	0.114	0.134	0.186	0.133	5.138	1.389
		C-MIMB-VIO	0.123	0.147	0.099	0.182	0.342	0.038	0.107	0.044	0.093	0.209	0.122	4.389	1.387

TABLE IV

The time consumption (s) of each step on real-world datasets

Dataset Algorithm Dataset	МН	V1	V2	urban	average
Open-VINS	0.017	0.016	0.017	0.016	0.017
C-MIMB-VIO	0.024	0.019	0.020	0.024	0.022

where

$$\begin{split} & \boldsymbol{\Phi}_1 = {}^{I_{t+1}} \hat{\mathbf{R}}_L{}^{I_t} \hat{\mathbf{R}}_L^\top, \\ & \boldsymbol{\Phi}_2 = -({}^L \hat{\mathbf{v}}_{I_{t+1}} - {}^L \hat{\mathbf{v}}_{I_t} + \mathbf{g} \boldsymbol{\Delta})_{\times}{}^{I_t} \hat{\mathbf{R}}_L^\top, \\ & \boldsymbol{\Phi}_3 = -({}^L \hat{\mathbf{p}}_{I_{t+1}} - {}^L \hat{\mathbf{p}}_{I_t} - {}^L \hat{\mathbf{v}}_{I_t} \boldsymbol{\Delta} + \frac{1}{2} \mathbf{g} \boldsymbol{\Delta}^2)_{\times}{}^{I_t} \hat{\mathbf{R}}_L^\top \end{split}$$

 $\Delta$  is one time step from time step t to time step t+1. The operation  $(\cdot)_{\times}$  transforms a vector into a skew-symmetric matrix. All the  $\mathbf{0}$  and  $\mathbf{I}$  without the right subscript are with the dimension of 3.

From (5), we have the local observation Jacobian  $\mathbf{H}_{L_t}$  defined by:

$$\mathbf{H}_{L_{t}} = \mathbf{H}_{\pi}^{i} \left[ (^{I_{t}} \hat{\mathbf{R}}_{L} (^{L} \hat{\mathbf{f}}_{i_{t}} - ^{L} \hat{\mathbf{p}}_{I_{t}}))_{\times} \mathbf{0} - ^{I_{t}} \hat{\mathbf{R}}_{L} {}^{I_{t}} \hat{\mathbf{R}}_{L} \mathbf{0}_{3 \times 27} \right]$$
(23)

where  $\mathbf{H}_{\pi}^{i}$  is the Jacobian of the camera projection function, whose dimension is  $2 \times 3$ . The detailed expression is unimportant and omitted here.

For the map-based observation Jaocbian  $\mathbf{H}_{G_t}$ , it consists of three parts (denoted as  ${}^{cam}\mathbf{H}_{G_t}$ ,  ${}^{k}K^{F_j}\mathbf{H}_{G_t}$  and  ${}^{s}K^{F_l}\mathbf{H}_{G_t}$ ) that are derived from (10)-(12):

$$^{cam}\mathbf{H}_{G_t} = \mathbf{H}_{\pi}^{ki} \left[ H_1 \ \mathbf{0} \ -^{I_t} \hat{\mathbf{R}}_L \ \mathbf{0} \ H_2 \ -H_3 \ \mathbf{0}_{3 \times 6} \ H_3 \ \mathbf{0}_{3 \times 12} \right]$$
(24)

$${}^{k}KF_{j}\mathbf{H}_{G_{t}} = \mathbf{H}_{\pi}^{ki'} \left[ \mathbf{0}_{3\times24} \ {}^{G_{t}^{k}} \hat{\mathbf{R}}_{kf_{j}}^{\top} \ H_{4} \ -{}^{G_{t}^{k}} \hat{\mathbf{R}}_{kf_{j}}^{\top} \ \mathbf{0}_{3\times6} \right]$$
 (25)

$${}^{sKF_{l}}\mathbf{H}_{G_{t}} = \mathbf{H}_{\pi}^{ki''} \left[ \mathbf{0}_{3 \times 12} \ H_{5} \ -H_{6} \ H_{7} \ {}^{G_{t}^{s}} \hat{\mathbf{R}}_{kf_{l}}^{\top} \ H_{6} \right]$$

$$\mathbf{0}_{3 \times 6} \ H_{8} \ -{}^{G_{t}^{s}} \hat{\mathbf{R}}_{kf_{l}}^{\top} \right]$$
(26)

$$\begin{split} H_{1} &= \begin{bmatrix} I_{t} \hat{\mathbf{R}}_{L} (G^{k}_{t} \hat{\mathbf{R}}_{L}^{\top} (G^{k} \hat{\mathbf{F}}_{i_{t}} - G^{k}_{t} \hat{\mathbf{p}}_{L}) - {}^{L} \hat{\mathbf{p}}_{I_{t}} ) \end{bmatrix}_{\times} \\ H_{2} &= I_{t} \hat{\mathbf{R}}_{L} G^{k}_{t} \hat{\mathbf{R}}_{L}^{\top} (G^{k} \hat{\mathbf{F}}_{i_{t}} - G^{k}_{t} \hat{\mathbf{p}}_{L})_{\times} \quad H_{3} = I_{t} \hat{\mathbf{R}}_{L} G^{i}_{t} \hat{\mathbf{R}}_{L}^{\top} \\ H_{4} &= -G^{k}_{t} \hat{\mathbf{R}}_{kf_{j}}^{\top} (G^{k} \hat{\mathbf{F}}_{i_{t}} - G^{k}_{t} \hat{\mathbf{p}}_{kf_{j}})_{\times} \\ H_{5} &= -G^{s}_{t} \hat{\mathbf{R}}_{kf_{l}}^{\top} G^{s}_{t} \hat{\mathbf{R}}_{L} G^{k}_{t} \hat{\mathbf{R}}_{L}^{\top} (G^{k} \hat{\mathbf{F}}_{i_{t}} - G^{k}_{t} \hat{\mathbf{p}}_{L})_{\times} \\ H_{6} &= G^{s}_{t} \hat{\mathbf{R}}_{kf_{l}}^{\top} G^{s}_{t} \hat{\mathbf{R}}_{L} G^{k}_{t} \hat{\mathbf{R}}_{L}^{\top} \\ H_{7} &= G^{s}_{t} \hat{\mathbf{R}}_{kf_{l}}^{\top} \left[ G^{s}_{t} \hat{\mathbf{R}}_{L} G^{k}_{t} \hat{\mathbf{R}}_{L}^{\top} (G^{k} \hat{\mathbf{F}}_{i_{t}} - G^{k}_{t} \hat{\mathbf{p}}_{L}) \right]_{\times} \\ H_{8} &= -G^{s}_{t} \hat{\mathbf{R}}_{kf_{l}}^{\top} \left[ G^{s}_{t} \hat{\mathbf{R}}_{L} G^{k}_{t} \hat{\mathbf{R}}_{L}^{\top} (G^{k} \hat{\mathbf{F}}_{i_{t}} - G^{k}_{t} \hat{\mathbf{p}}_{L}) + G^{s}_{t} \hat{\mathbf{p}}_{L} - G^{s}_{t} \hat{\mathbf{p}}_{kf_{l}} \right] \end{split}$$

We first consider the ideal case that all the estimated values are equal to the true values. With this assumption, we can investigate the observability properties that the system should have. Then, on this basis, we will further demonstrate the inconsistency of the system under the actual case.

## The Proof of Theorem 1

*Proof:* Under the ideal case, the following two conditions are satisfied: a) The propagated state  $\hat{\mathbf{x}}_{Aug_t|t-1}$  is equal to the updated state  $\hat{\mathbf{x}}_{Aug_t}$  and is equal to the true state  $\mathbf{x}_{Aug_t}$ ; b) All the features, *augmented variables*, and map keyframe poses do not change with time and are equal to the constant true values. For instance, the map feature  $G^k\hat{\mathbf{F}}_{i,} = G^k\mathbf{F}_i$ .

With condition a) and (22), the transition matrix  $\Phi_{t|0}$  can be given as:

$$\Phi_{t|0} = \begin{bmatrix}
\Phi(1) & \mathbf{0} & \mathbf{0} & \mathbf{0}_{3\times30} \\
\Phi(2) & \mathbf{I} & \mathbf{0} & \mathbf{0}_{3\times30} \\
\Phi(3) & \mathbf{I}\Delta_t & \mathbf{I} & \mathbf{0}_{3\times30} \\
\mathbf{0}_{30\times3} & \mathbf{0}_{30\times3} & \mathbf{0}_{30\times3} & \mathbf{I}_{30}
\end{bmatrix},$$
(27)

where  $\Delta_t$  is t time steps from time setp 0 to time setp t,

$$\begin{split} & \boldsymbol{\Phi}(1) = {}^{I_t} \mathbf{R}_L {}^{I_0} \mathbf{R}_L^\top, \\ & \boldsymbol{\Phi}(2) = -({}^L \mathbf{v}_{I_t} - {}^L \mathbf{v}_{I_0} + \mathbf{g} \boldsymbol{\Delta}_t)_\times {}^{I_0} \mathbf{R}_L^\top, \\ & \boldsymbol{\Phi}(3) = -({}^L \mathbf{p}_{I_t} - {}^L \mathbf{p}_{I_0} - {}^L \mathbf{v}_{I_0} \boldsymbol{\Delta}_t + \frac{1}{2} \mathbf{g} \boldsymbol{\Delta}_t^2)_\times {}^{I_0} \mathbf{R}_L^\top. \end{split}$$

Substituting (23)-(29) into (13), we can get the observability matrix, whose right null space is given by (15).

We can find that for the ideal case, the dimension of the unobservable subspace is ten: four dimensions for the VIO system, and six dimensions for the introduced *imperfect* maps.

## The Proof of Theorem 2

TABLE V  $\label{eq:atention} ATE(M) \mbox{ of the local VIO position on different datasets with } \\ DIFFERENT \mbox{ algorithms}$ 

	Algorithm	Open	MIMB	P-MIMB	C-MIMB
Sequence		-VINS	-VIO	-VIO	-VIO
	0map	0.090	_	_	_
	1map	_	0.067	0.062	0.066
MH01	2map	_	0.086	0.080	0.053
WIIIOI	3map	_	0.062	0.078	0.057
	4map	_	0.065	0.070	0.048
	average	0.090	0.070	0.073	0.056
	0map	0.101	_	_	_
	1map	_	0.070	0.074	0.066
MH02	2map	_	0.064	0.070	0.060
WIIIOZ	3map	_	0.059	0.073	0.051
	4map	_	0.060	0.077	0.058
	average	0.101	0.063	0.074	0.059
	0map	0.144	_	_	_
	1map	_	0.187	0.125	0.083
MH03	2map	_	0.174	0.137	0.113
WITIOS	3map	_	0.130	0.122	0.072
	4map	_	0.115	0.127	0.073
	average	0.144	0.152	0.128	0.085
	0map	0.190	_	_	_
	1map	_	0.199	0.225	0.163
MH04	2map	_	0.158	0.253	0.159
WIIIO	3map	_	0.168	0.225	0.157
	4map	_	0.247	0.212	0.164
	average	0.190	0.193	0.229	0.161
	0map	0.246	_	_	_
	1map	_	0.301	0.224	0.186
MH05	2map	_	0.317	0.239	0.189
1411105	3map	_	0.266	0.264	0.183
	4map	_	0.237	0.145	0.191
	average	0.246	0.280	0.218	0.187
	0map	0.046	_		
V101	1map	_	0.040	0.058	0.032
	2map	_	0.037	0.054	0.032
	average	0.046	0.039	0.056	0.032
	0map	0.058			
V102	1map	_	0.072	0.044	0.044
	2map	-	0.075	0.056	0.041
	average	0.058	0.074	0.050	0.043
	0map	0.047		0.050	
V103	1map	_	0.047	0.058	0.043
	2map	0.047	0.046	0.104	0.042
	average	0.047	0.047	0.081	0.043
	0map	0.073	0.070	0.060	0.060
V201	1map	_	0.070 0.066	0.069 0.073	0.069 0.063
	2map average	0.073	0.068	0.073	0.065
		0.073	0.008	0.071	0.000
	0map 1map	0.039	0.093	0.132	0.049
V202		_	0.093	0.132	0.049
-	2map average	0.059	0.117	0.114	0.062
		0.039	0.104	0.123	0.030
	0map	0.117	0.086	0.106	0.084
V203	1map	_	0.086	0.106	0.084
-	2map	0.117			0.079
	average	0.117	0.083	0.105 <b>0.082</b>	
Urban38	0map	24.886			
	2map		13.773	5.969	5.205
	average	24.886	13.773	5.969	5.205
Urban39	0map	7.061			
	2map		10.539	5.614	5.376
	average	7.061	10.539	5.614	5.376

*Proof:* Under the actual case, conditions a) and b) are not satisfied. Without condition a),  $\Phi$  does not have the elegant form of (29), which leads to the vanishment of the first column block of (15). Without condition b),

TABLE VI  $\label{table} \mbox{ATE(degree/m) of the } \mbox{augmented variables on different datasets}$  With different algorithms

queried sequence         map sequence         MIMB control         P-MIMB control         C-MIMB control           MH02         2.730/0.113         2.652/0.202         2.147/0.100           MH03         1.372/0.141         0.598/0.224         0.808/0.109           MH01         MH04         1.167/0.169         1.598/0.263         0.927/0.123           MH01         3.740/0.203         2.472/0.153         2.842/0.160           MH03         3.134/0.136         2.421/0.118         2.320/0.106           MH04         2.642/0.141         1.795/0.197         1.916/0.160           MH05         2.986/0.167         2.242/0.255         2.127/0.163           average         3.126/0.162         2.223/0.173         2.301/0.147           MH01         1.357/0.158         0.929/0.166         0.672/0.096           MH02         2.150/0.183         2.735/0.110         2.502/0.134           MH03         MH04         1.247/0.092         0.790/0.096         0.724/0.084           MH03         3.107/0.172         1.256/0.147         1.149/0.099           MH04         1.429/0.116         0.5680.214         0.696/0.080           average         1.546/0.137         1.256/0.147         1.149/0.099           MH04<					
MH01	queried	map	MIMB	P-MIMB	C-MIMB
MH01         MH03         1.372/0.141         0.598/0.224         0.808/0.109           MH01         1.358/0.129         1.419/0.120         1.334/0.131           MH05         1.167/0.169         1.598/0.263         0.927/0.150           average         1.657/0.138         1.567/0.202         1.304/0.123           MH01         3.740/0.203         2.472/0.153         2.842/0.160           MH02         MH04         2.642/0.141         1.795/0.197         1.916/0.160           MH02         MH05         2.986/0.167         2.242/0.255         2.127/0.163           average         3.126/0.162         2.233/0.173         2.301/0.147           MH03         MH04         1.257/0.158         0.929/0.166         0.672/0.096           MH03         MH04         1.247/0.092         0.790/0.096         0.724/0.084           MH03         MH04         1.249/0.116         0.5680.214         0.696/0.080           MH05         3.479/0.272         2.264/0.333         1.393/0.274           MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH04         MH03         3.917/0.172         1.23/0.089         0.628/0.163           Average         3.398/0.189         1.784/0.222	sequence	sequence		-VIO	-VIO
MH01		MH02	2.730/0.113	2.652/0.202	2.147/0.100
MH05		MH03	1.372/0.141	<b>0.598</b> /0.224	0.808/ <b>0.109</b>
Average	MH01	MH04	1.358/0.129	1.419/ <b>0.120</b>	<b>1.334</b> /0.131
MH01   3.740/0.203   2.472/0.153   2.842/0.160   MH03   3.134/0.136   2.421/0.118   2.320/0.106   MH05   2.986/0.167   2.242/0.255   2.127/0.163   average   3.126/0.162   2.233/0.173   2.301/0.147   MH01   1.357/0.158   0.929/0.166   0.672/0.096   MH02   2.150/0.183   2.735/0.110   2.502/0.134   MH03   MH04   1.247/0.092   0.790/0.096   0.724/0.084   MH05   1.429/0.116   0.5680.214   0.696/0.080   average   1.546/0.137   1.256/0.147   1.149/0.099   MH01   3.479/0.272   2.264/0.333   1.393/0.274   MH02   3.801/0.149   2.195/0.222   1.923/0.137   MH04   MH03   3.204/0.162   1.553/0.269   1.005/0.154   MH05   3.107/0.172   1.123/0.089   0.628/0.163   average   3.398/0.189   1.784/0.228   1.237/0.182   MH01   1.606/0.413   2.416/0.625   1.483/0.370   MH02   2.276/0.430   2.323/0.577   1.983/0.341   MH05   MH03   1.911/0.442   2.516/0.595   1.439/0.433   MH04   1.196/0.280   0.869/0.378   0.648/0.222   average   1.747/0.391   2.031/0.544   1.388/0.342   V101   V103   4.513/0.051   0.950/0.059   0.911/0.038   average   4.662/0.049   1.364/0.067   0.972/0.038   V101   V103   4.513/0.051   0.950/0.059   0.911/0.038   average   5.230/0.118   0.736/0.112   0.825/0.107   V103   4.513/0.076   1.665/0.114   1.279/0.055   V103   V102   2.026/0.076   1.226/0.113   0.707/0.033   average   2.169/0.076   1.226/0.113   0.707/0.033   average   2.169/0.076   1.246/0.114   0.993/0.044   V202   2.946/0.102   2.025/0.140   1.426/0.079   V201   6.778/0.233   3.000/0.233   2.837/0.244   V202   V203   11.920/0.227   3.598/0.138   3.349/0.173   average   2.156/0.135   1.640/0.144   1.911/0.131   average   2.156/0.335   3.000/0.233   2.837/0.244   V202   V203   11.920/0.227   3.598/0.138   3.349/0.173   average   2.156/0.135   1.640/0.144   1.911/0.131   average   1.176/6.437   0.887/1.375   0.854/1.463   Urban38.S1   1.516/3.374   0		MH05	1.167/0.169	1.598/0.263	0.927/0.150
MH02         MH03 MH04         3.134/0.136 2.642/0.141         2.421/0.118 1.795/0.197         2.320/0.106 1.916/0.160           MH05         2.986/0.167         2.242/0.255         2.127/0.163           average         3.126/0.162         2.233/0.173         2.301/0.147           MH01         1.357/0.158         0.929/0.166         0.672/0.096           MH02         2.150/0.183         2.735/0.110         2.502/0.134           MH03         MH04         1.247/0.092         0.790/0.096         0.724/0.084           MH05         1.429/0.116         0.5680.214         0.696/0.080           average         1.546/0.137         1.256/0.147         1.149/0.099           MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH02         3.801/0.149         2.195/0.222         1.923/0.137           MH03         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.784/0.228         1.237/0.182           MH05         MH01         1.606/0.413         2.416/0.625         1.439/0.433           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.341           MH05         MH04         1.196/0.280         0.869/0.377		average	1.657/0.138	1.567/0.202	1.304/0.123
MH02         MH04         2.642/0.141         1.795/0.197         1.916/0.160           MH05         2.986/0.167         2.242/0.255         2.127/0.163           average         3.126/0.162         2.233/0.173         2.301/0.147           MH01         1.357/0.158         0.929/0.166         0.672/0.096           MH02         2.150/0.183         2.735/0.110         2.502/0.134           MH03         MH04         1.247/0.092         0.790/0.096         0.724/0.084           MH05         1.429/0.116         0.5680.214         0.696/0.080           average         1.546/0.137         1.256/0.147         1.149/0.099           MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH02         3.801/0.149         2.195/0.222         1.923/0.137           MH03         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.784/0.228         1.237/0.182           MH05         MH01         1.606/0.413         2.416/0.625         1.483/0.370           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433 <t< td=""><td></td><td>MH01</td><td>3.740/0.203</td><td>2.472/0.153</td><td>2.842/0.160</td></t<>		MH01	3.740/0.203	2.472/0.153	2.842/0.160
MH05		MH03	3.134/0.136	2.421/0.118	2.320/0.106
Average	MH02	MH04	2.642/ <b>0.141</b>	<b>1.795</b> /0.197	1.916/0.160
MH01		MH05	2.986/0.167	2.242/0.255	2.127/0.163
MH03         MH04         1.247/0.092         0.790/0.096         0.724/0.084           MH05         1.4247/0.092         0.790/0.096         0.724/0.084           MH05         1.429/0.116         0.5680.214         0.696/0.080           average         1.546/0.137         1.256/0.147         1.149/0.099           MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH02         3.801/0.149         2.195/0.222         1.923/0.137           MH04         MH03         3.204/0.162         1.553/0.269         1.005/0.154           MH05         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.744/0.625         1.483/0.370           MH05         MH001         1.606/0.413         2.416/0.625         1.483/0.341           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V103         4.513/0.014         1.364/0.067         0.972/0.038           V101         V103         5.157/0.127         0.762/0.133         0.681/0.1		average	3.126/0.162	<b>2.233</b> /0.173	2.301/ <b>0.147</b>
MH03         MH04         1.247/0.092         0.790/0.096         0.724/0.084           MH05         1.429/0.116         0.5680.214         0.696/0.080           average         1.546/0.137         1.256/0.147         1.149/0.099           MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH04         MH03         3.801/0.149         2.195/0.222         1.923/0.137           MH04         MH03         3.204/0.162         1.553/0.269         1.005/0.154           MH05         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.784/0.228         1.237/0.182           MH05         MH01         1.606/0.413         2.416/0.625         1.483/0.341           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.343           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           V102         V103         5.157/0.127		MH01	1.357/0.158	0.929/0.166	0.672/0.096
MH05   1.429/0.116   0.5680.214   0.696/0.080     average   1.546/0.137   1.256/0.147   1.149/0.099     MH01   3.479/0.272   2.264/0.333   1.393/0.274     MH02   3.801/0.149   2.195/0.222   1.923/0.137     MH04   MH03   3.204/0.162   1.553/0.269   1.005/0.154     MH05   3.107/0.172   1.123/0.089   0.628/0.163     average   3.398/0.189   1.784/0.228   1.237/0.182     MH01   1.606/0.413   2.416/0.625   1.483/0.370     MH02   2.276/0.430   2.323/0.577   1.983/0.341     MH05   MH03   1.911/0.442   2.516/0.595   1.439/0.433     MH04   1.196/0.280   0.869/0.378   0.648/0.222     average   1.747/0.391   2.031/0.544   1.388/0.342     V102   4.810/0.047   1.777/0.075   1.032/0.038     V101   V103   4.513/0.051   0.950/0.059   0.911/0.038     average   4.662/0.049   1.364/0.067   0.972/0.038     V101   5.302/0.108   0.709/0.090   0.968/0.093     V102   V103   5.157/0.127   0.762/0.133   0.681/0.120     average   5.230/0.118   0.736/0.112   0.825/0.107     V103   V102   2.026/0.076   1.226/0.113   0.707/0.033     average   2.169/0.076   1.446/0.114   0.993/0.044     V202   2.946/0.102   2.025/0.140   1.426/0.079     V201   V203   2.916/0.096   2.415/0.128   1.477/0.106     average   2.931/0.099   2.220/0.134   1.452/0.093     V201   V203   3.300/0.233   3.309/0.233   2.837/0.244     V202   V203   11.920/0.227   3.598/0.138   3.349/0.173     average   9.349/0.230   3.300/0.186   3.093/0.209     V201   V203   2.156/0.135   1.640/0.144   1.911/0.131     average   2.494/0.112   1.851/0.133   2.039/0.122    Urban38   Urban39_S1   1.556/7.003   1.295/6.161   1.164/5.861     Urban38   Urban38_S2   1.390/2.470   0.887/1.375   0.854/1.463		MH02	<b>2.150</b> /0.183	2.735/0.110	2.502/0.134
average         1.546/0.137         1.256/0.147         1.149/0.099           MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH02         3.801/0.149         2.195/0.222         1.923/0.137           MH03         3.204/0.162         1.553/0.269         1.005/0.154           MH05         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.784/0.228         1.237/0.182           MH01         1.606/0.413         2.416/0.625         1.483/0.370           MH02         2.276/0.430         2.323/0.577         1.983/0.341           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V101         5.302/0.108         0.709/0.090         0.968/0.093           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           V103         5.1	MH03	MH04	1.247/0.092	0.790/0.096	0.724/0.084
MH01 MH02 MH02 MH03 3.801/0.149         3.479/0.272 2.195/0.222         2.264/0.333 1.293/0.137         1.393/0.274 1.923/0.137           MH04 MH03 Average         3.801/0.149 3.107/0.172         1.153/0.089 1.553/0.269         1.005/0.154 1.005/0.154           MH05 Average         3.398/0.189 3.398/0.189         1.784/0.228 1.237/0.182         1.237/0.182           MH01 MH02 Average         2.276/0.430 2.276/0.430 2.323/0.577         1.983/0.341           MH05 MH03 MH04 1.196/0.280 Average         0.869/0.378 0.869/0.378         0.648/0.222 0.869/0.378           Average Average         1.747/0.391 4.513/0.051 0.950/0.059         0.911/0.038 0.950/0.059 0.911/0.038           V101 V103 Average         4.662/0.049 4.662/0.049 1.364/0.067         0.972/0.038 0.972/0.038           V102 V103 Average         5.230/0.118 5.157/0.127 5.230/0.018 0.7062/0.133 0.681/0.120 0.7062/0.133 0.681/0.120 0.825/0.107           V103 Average         2.169/0.076 1.226/0.114 0.707/0.033 0.707/0.034 0.707/0.034 0.707/0.034 0.707/0.034 0.707		MH05	1.429/0.116	<b>0.568</b> 0.214	0.696/ <b>0.080</b>
MH01         3.479/0.272         2.264/0.333         1.393/0.274           MH02         3.801/0.149         2.195/0.222         1.923/0.137           MH03         3.204/0.162         1.553/0.269         1.005/0.154           MH05         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.784/0.228         1.237/0.182           MH01         1.606/0.413         2.416/0.625         1.483/0.370           MH02         2.276/0.430         2.323/0.577         1.983/0.341           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           v103         5.157/0.127         0.762/0.133         0.681/0.120           v104         2.312/0.076         1.665/0.114         1.279/0.055           v105         2.169/		average	1.546/0.137	1.256/0.147	1.149/0.099
MH04         MH03         3.204/0.162         1.553/0.269         1.005/0.154           MH05         3.107/0.172         1.123/0.089         0.628/0.163           average         3.398/0.189         1.784/0.228         1.237/0.182           MH01         1.606/0.413         2.416/0.625         1.483/0.370           MH02         2.276/0.430         2.323/0.577         1.983/0.341           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V103         V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.47			3.479/ <b>0.272</b>	2.264/0.333	1.393/0.274
MH05   3,107/0.172   1.123/0.089   0.628/0.163     average   3.398/0.189   1.784/0.228   1.237/0.182     MH01   1.606/0.413   2.416/0.625   1.483/0.370     MH02   2.276/0.430   2.323/0.577   1.983/0.341     MH03   1.911/0.442   2.516/0.595   1.439/0.434     MH04   1.196/0.280   0.869/0.378   0.648/0.222     average   1.747/0.391   2.031/0.544   1.388/0.342     V102   4.810/0.047   1.777/0.075   1.032/0.038     V101   V103   4.513/0.051   0.950/0.059   0.911/0.038     average   4.662/0.049   1.364/0.067   0.972/0.038     V102   V103   5.157/0.127   0.762/0.133   0.681/0.120     average   5.230/0.118   0.736/0.112   0.825/0.107     V103   V101   2.312/0.076   1.665/0.114   1.279/0.055     V103   V102   2.026/0.076   1.226/0.113   0.707/0.033     average   2.169/0.076   1.446/0.114   0.993/0.044     V202   2.946/0.102   2.025/0.140   1.426/0.079     V201   V203   2.916/0.096   2.415/0.128   1.477/0.106     average   2.931/0.099   2.220/0.134   1.452/0.093     V201   V203   2.916/0.096   2.415/0.128   1.477/0.106     average   9.349/0.233   3.000/0.233   2.837/0.244     V202   V203   11.920/0.227   3.598/0.138   3.349/0.173     average   9.349/0.230   3.300/0.186   3.093/0.209     V201   2.831/0.112   2.061/0.122   2.164/0.112     V203   V202   2.156/0.135   1.640/0.144   1.911/0.131     average   2.494/0.124   1.851/0.133   2.039/0.122    Urban39_S1   1.556/7.003   1.295/6.161   1.164/5.861     Urban39_S1   1.556/7.003   1.295/6.161   1.164/5.861     Urban38_S1   1.516/3.374   0.634/1.400   0.634/1.310     Urban38_S1   1.516/3.374   0.634/1.400   0.634/1.310     Urban39_S2   1.390/2.470   0.887/1.375   0.854/1.463					
MH05   3.107/0.172   1.123/0.089   0.628/0.163     average   3.398/0.189   1.784/0.228   1.237/0.182     MH01   1.606/0.413   2.416/0.625   1.483/0.370     MH02   2.276/0.430   2.323/0.577   1.983/0.341     MH03   1.911/0.442   2.516/0.595   1.439/0.434     MH04   1.196/0.280   0.869/0.378   0.648/0.222     average   1.747/0.391   2.031/0.544   1.388/0.342     V102   4.810/0.047   1.777/0.075   1.032/0.038     V101   V103   4.513/0.051   0.950/0.059   0.911/0.038     average   4.662/0.049   1.364/0.067   0.972/0.038     V102   V103   5.157/0.127   0.762/0.133   0.681/0.120     average   5.230/0.118   0.736/0.112   0.825/0.105     V103   V101   2.312/0.076   1.665/0.114   1.279/0.055     V103   V102   2.026/0.076   1.226/0.113   0.707/0.033     average   2.169/0.076   1.446/0.114   0.993/0.044     V201   V203   2.916/0.096   2.415/0.128   1.477/0.106     average   2.931/0.099   2.220/0.134   1.452/0.093     V201   V203   2.916/0.096   2.415/0.128   1.477/0.106     average   9.349/0.233   3.000/0.233   2.837/0.244     V202   V203   11.920/0.227   3.598/0.138   3.349/0.173     average   9.349/0.230   3.300/0.186   3.093/0.209     V201   2.831/0.112   2.061/0.122   2.164/0.112     V203   V202   2.156/0.135   1.640/0.144   1.911/0.131     average   2.494/0.124   1.851/0.133   2.039/0.122     Urban39_S1   1.556/7.003   1.295/6.161   1.164/5.861     Urban38_S1   1.516/3.374   0.634/1.400   0.634/1.310     Urban38_S1   1.516/3.374   0.634/1.400   0.634/1.310     Urban39_S2   1.390/2.470   0.887/1.375   0.854/1.463	MH04	MH03	3.204/0.162	1.553/0.269	1.005/0.154
average         3.398/0.189         1.784/0.228         1.237/0.182           MH01         1.606/0.413         2.416/0.625         1.483/0.370           MH02         2.276/0.430         2.323/0.577         1.983/0.341           MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH04         1.196/0.280         0.869/0.378         0.648/0.232           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V103         V101         2.312/0.076         1.665/0.114         1.279/0.053           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093 </td <td></td> <td></td> <td></td> <td></td> <td></td>					
MH01		average	3.398/0.189		1.237/0.182
MH05         MH02         2.276/0.430         2.323/0.577         1.983/0.341           MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V102         4.810/0.047         1.777/0.075         1.032/0.038           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V103         V102         2.026/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.035           V103         2.169/0.076         1.446/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average <td< td=""><td></td><td></td><td></td><td></td><td></td></td<>					
MH05         MH03         1.911/0.442         2.516/0.595         1.439/0.433           MH04         1.196/0.280         0.869/0.378         0.648/0.222           average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V102         4.810/0.047         1.777/0.075         1.032/0.038           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.039           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.018         0.736/0.112         0.825/0.107           V103         V102         2.026/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.					
MH04	MH05				
average         1.747/0.391         2.031/0.544         1.388/0.342           V101         V102         4.810/0.047         1.777/0.075         1.032/0.038           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V101         5.302/0.108         0.709/0.090         0.968/0.093           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V103         V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.246/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230	111105				
V101         V102         4.810/0.047         1.777/0.075         1.032/0.038           V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V101         5.302/0.108         0.709/0.090         0.968/0.093           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.110           V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V203         V201         2.831/0.112         2.061/0.12		-			
V101         V103         4.513/0.051         0.950/0.059         0.911/0.038           average         4.662/0.049         1.364/0.067         0.972/0.038           V101         5.302/0.108         0.709/0.090         0.968/0.093           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.110           V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V203         V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.14		Ü			
average         4.662/0.049         1.364/0.067         0.972/0.038           V101         5.302/0.108         0.709/0.090         0.968/0.093           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V103         V101         2.312/0.076         1.665/0.114         1.279/0.053           average         2.169/0.076         1.266/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V203         V201         2.815/0.135         1.640/0.144         1.911/0.131           v203         V201         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         <	V101				
V101         5.302/0.108         0.709/0.090         0.968/0.093           V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V203         V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V201         2.816/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.29					
V102         V103         5.157/0.127         0.762/0.133         0.681/0.120           average         5.230/0.118         0.736/0.112         0.825/0.107           V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           V203         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban38_S2         0.796/5.871         0.468/4.115         0.427/3.817					
average         5.230/0.118         0.736/0.112         0.825/0.107           V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6	V102				
V103         V101         2.312/0.076         1.665/0.114         1.279/0.055           V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.249           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban38_S1         1.76/6.437         0.877/5.138         0.795/4.839           Urban38_S2         1.390/2.470 <td< td=""><td></td><td></td><td></td><td></td><td></td></td<>					
V103         V102         2.026/0.076         1.226/0.113         0.707/0.033           average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V203         V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban38_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400 <td></td> <td></td> <td></td> <td></td> <td></td>					
average         2.169/0.076         1.446/0.114         0.993/0.044           V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39_S2         1.390/2.470         0.887/1.375         0.854/1.463 </td <td>V103</td> <td></td> <td></td> <td></td> <td></td>	V103				
V201         V202         2.946/0.102         2.025/0.140         1.426/0.079           V201         V203         2.916/0.096         2.415/0.128         1.477/0.106           average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban38_C1         1.76/6.437         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39_Varage         1.390/2.470         0.887/1.375         0.854/1.463		average	2.169/0.076		0.993/0.044
average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463				2.025/0.140	1.426/0.079
average         2.931/0.099         2.220/0.134         1.452/0.093           V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463	V201	V203	2.916/ <b>0.096</b>	2.415/0.128	<b>1.477</b> /0.106
V201         6.778/0.233         3.000/0.233         2.837/0.244           V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463		average			
V202         V203         11.920/0.227         3.598/0.138         3.349/0.173           average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463					
average         9.349/0.230         3.300/0.186         3.093/0.209           V201         2.831/0.112         2.061/0.122         2.164/0.112           V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463	V202	V203			
V201         2.831/0.112         2.061/0.122         2.164/0.112           V203         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463					
V203         V202         2.156/0.135         1.640/0.144         1.911/0.131           average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463					
average         2.494/0.124         1.851/0.133         2.039/0.122           Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463	V203				
Urban39_S1         1.556/7.003         1.295/6.161         1.164/5.861           Urban39_S2         0.796/5.871         0.468/4.115         0.427/3.817           average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463					
Urban38         Urban39_S2         0.796/5.871         0.468/4.115 <b>0.427/3.817</b> average         1.176/6.437         0.877/5.138 <b>0.795/4.839</b> Urban38_S1         1.516/3.374 <b>0.634/1.400 0.634/1.310</b> Urban39         Urban38_S2         1.390/2.470         0.887/ <b>1.375</b> 0.854/1.463					
average         1.176/6.437         0.877/5.138         0.795/4.839           Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463	Hrban 30				
Urban38_S1         1.516/3.374         0.634/1.400         0.634/1.310           Urban39         Urban38_S2         1.390/2.470         0.887/1.375         0.854/1.463	Oluanso				
Urban39 Urban38_S2 1.390/2.470 0.887/ <b>1.375</b> 0.854/1.463					
	Urban20				0100 0 -10 - 0
average 1.433/2.922 0.700/1.369 0.740/1.367	Orban39				
		average	1.43314.744	0.700/1.369	0./40/1.30/

element values that are not supposed to change over time will become ever-changing estimated values. That is to say, the map feature  ${}^{G^k}\hat{\mathbf{F}}_{i_t}{\neq}{}^{G^k}\hat{\mathbf{F}}_{i_{t-1}}{\neq}\cdots{\neq}{}^{G^k}\hat{\mathbf{F}}_{i_0}{\neq}{}^{G^k}\mathbf{F}_i$ , so as  ${}^{G^k}\mathbf{R}_L$ ,  ${}^{G^s}\mathbf{R}_L$ , and  ${}^{G^k}\mathbf{p}_L$ , which leads to the vanishment of the second and the third column block of (15). Therefore, for the actual case, the dimension of the unobservable subspace is only three given by (16), not in accordance with the ideal case. This means if we use the estimated values to compute Jacobian matrices, the *augmented system* will suffer from inconsistency.

When the used maps are *perfect*, the original state (14) shrinks to

$$\mathbf{x}_{Aug_t}^* = \begin{bmatrix} I_t \mathbf{q}_L^\top \ L \mathbf{v}_{I_t}^\top \ L \mathbf{p}_{I_t}^\top \ L \mathbf{f}_{i_t}^\top \end{bmatrix}^G \mathbf{f}_t^k \mathbf{q}_L^\top \ G_t^k \mathbf{p}_L^\top \ G_t^s \mathbf{q}_L^\top \ G_t^s \end{bmatrix}^\top$$
(28)

where the map-related parts are removed. Then, the dimension of the state is reduced from 39 to 24.

#### The Proof of Theorem 3

*Proof:* With the proof of Theorem 1, the derivation of Theorem 3 is straightforward.

Since the dimension of the state changes, so does that of the transition matrix  $\Phi_{t|0}$ . Therefore, (22) becomes to

$$\Phi_{t|0}^* = \begin{bmatrix}
\Phi(1) & \mathbf{0} & \mathbf{0} & \mathbf{0}_{3\times15} \\
\Phi(2) & \mathbf{I} & \mathbf{0} & \mathbf{0}_{3\times15} \\
\Phi(3) & \mathbf{I}\Delta_t & \mathbf{I} & \mathbf{0}_{3\times15} \\
\mathbf{0}_{15\times3} & \mathbf{0}_{15\times3} & \mathbf{0}_{15\times3} & \mathbf{I}_{15}
\end{bmatrix},$$
(29)

where the key elements, i.e., the upper-left  $9 \times 9$  blocks of the transition matrix, remain the same.

Besides, for (23)-(26), the map-related Jacobian blocks are also removed.

Based on these analyses and the unobservable subspace getten from Theorem 1, we can easily derive that the unobservable subspace of the *augmented system* with *perfect* maps is given by (17).

## The Proof of Theorem 4

*Proof:* As analyzed in the proof of Theorem 2, under the actual case, the first column block of (17) vanishes because the updated state  $\hat{\mathbf{x}}^*_{Aug_t}$  is not equal to the true state  $\mathbf{x}^*_{Aug_t}$ . Besides, the ever-changing values of the estimated augmented variables make the second column block of (17) vanish.

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