

1. In the active mixer of Fig. 6.1, $I_{n,M1}$ contains all frequency components. Prove that the convolution of these components with the harmonics of the LO in essence multiplies $4kT\gamma/g_m$ by a factor of $\pi^2/4$.

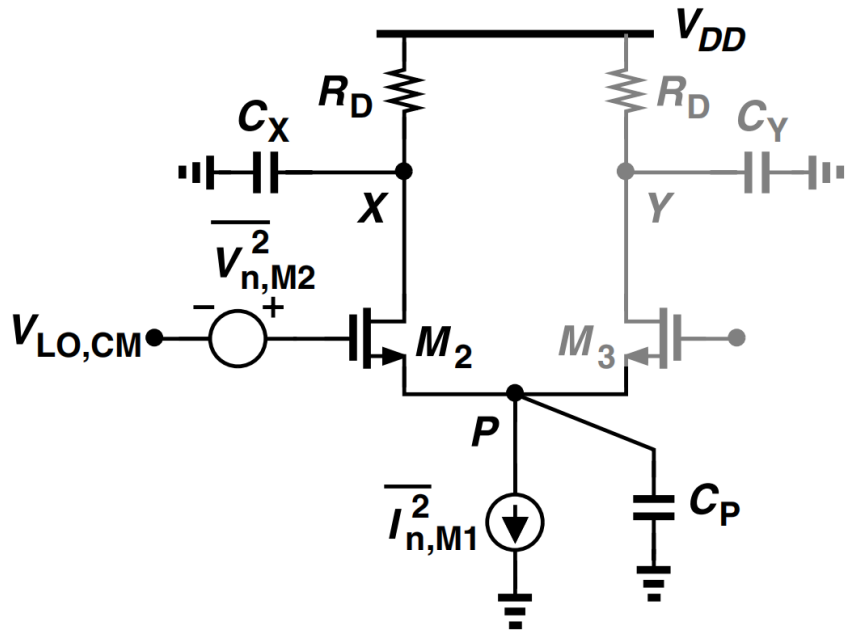
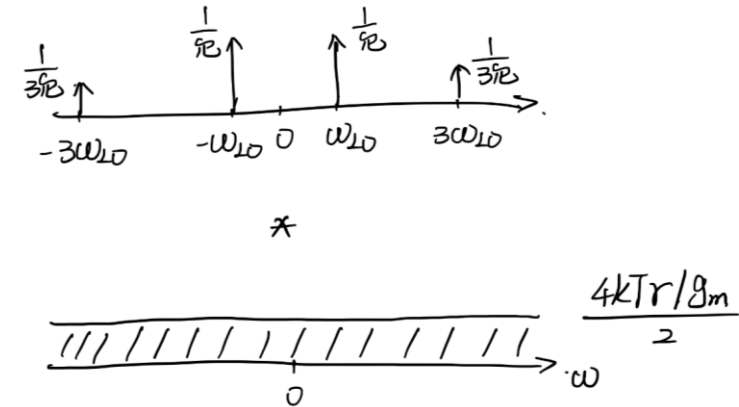


Fig. 6.1

LO: 50% duty cycle square wave



$$\frac{4kT\gamma/g_m}{2} \cdot \left[\frac{1}{\pi^2} + \frac{1}{(3\pi)^2} + \frac{1}{(5\pi)^2} + \dots \right] = \frac{4kT\gamma}{g_m} \cdot \frac{1}{\pi^2} \cdot \frac{\pi^2}{16}$$

As there are two sides on the spectrum and two sides in the mixer

$$\Rightarrow 4kT\gamma/g_m \cdot \frac{1}{\pi^2} \cdot \frac{\pi^2}{4}$$

2. Shown in Fig. 6.2 is the front end of a 1.8-GHz receiver. The LO frequency is chosen to be 900 MHz and the load inductors and capacitances resonate with a quality factor of Q at the IF. Assume M_1 is biased at a current of I_1 , and the mixer and the LO are perfectly symmetric.
- Assuming M_2 and M_3 switch abruptly and completely, compute the LO-IF feedthrough, i.e., the measured level of the 900-MHz output component in the absence of an RF signal.
 - Explain why the flicker noise of M_1 is critical here.

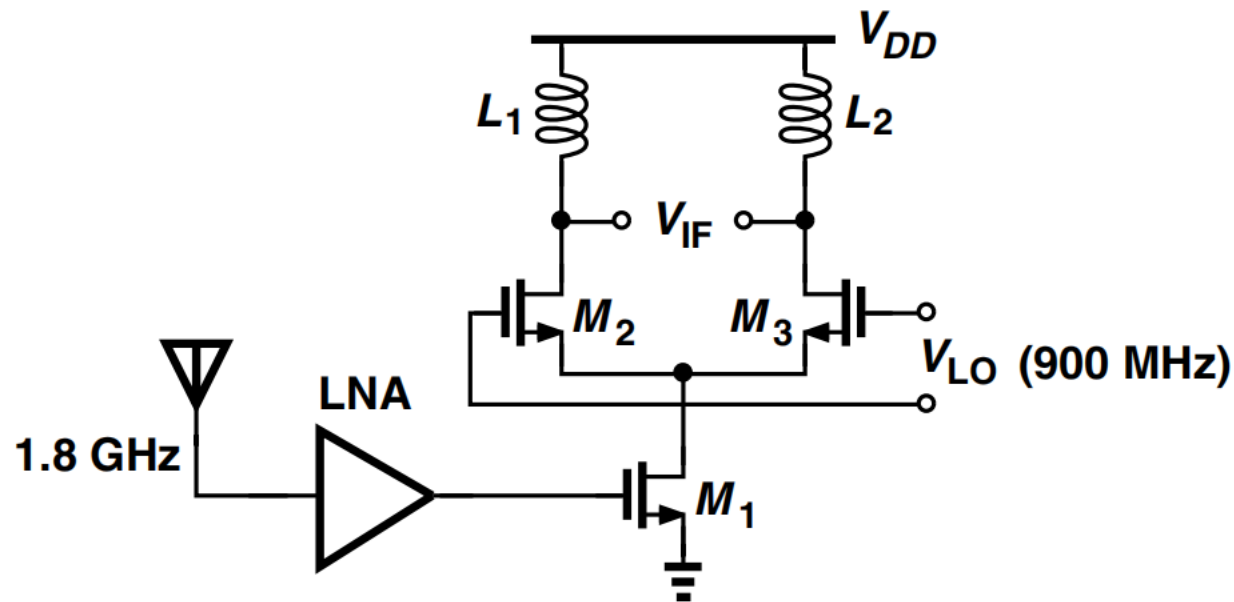
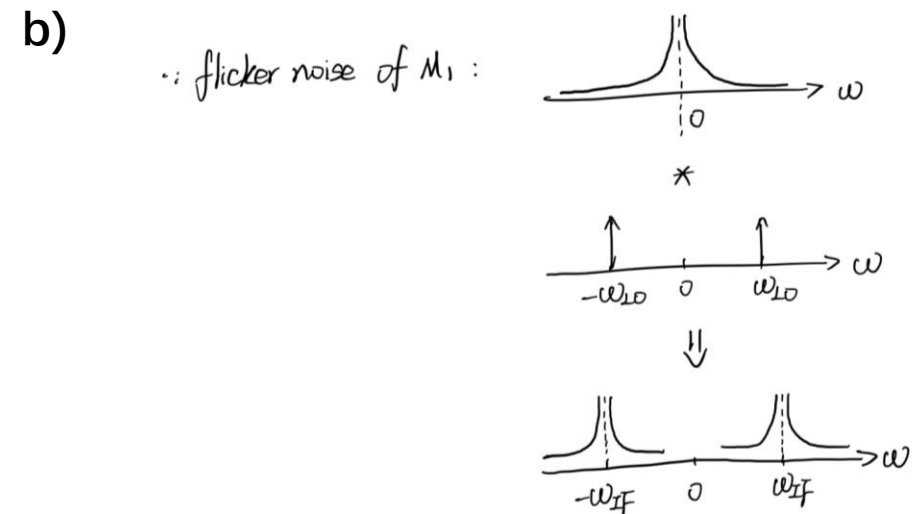
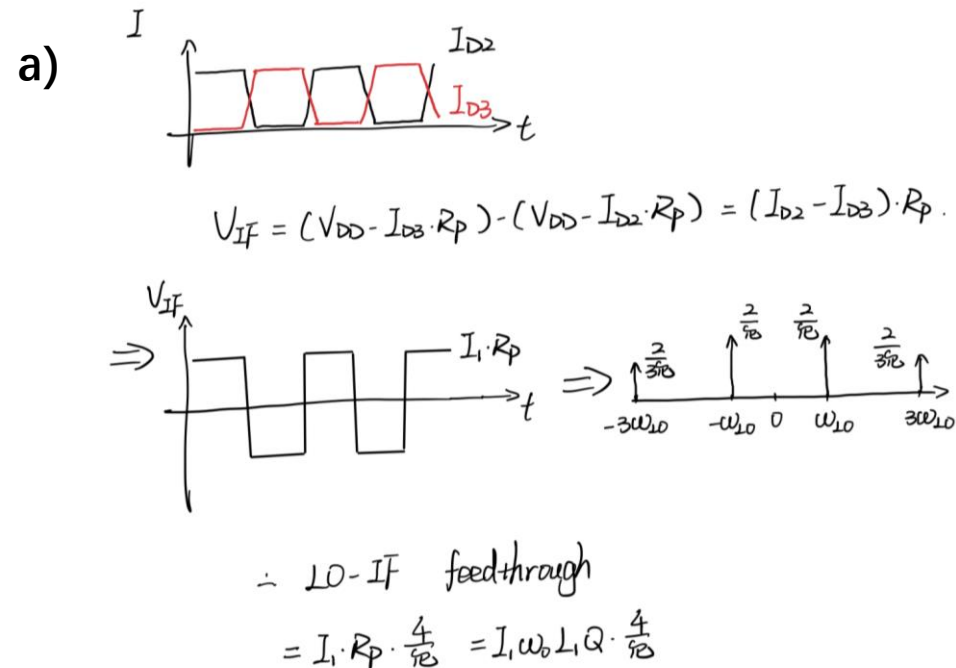


Fig. 6.2

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So the flicker noise is transferred to IF band