

## **Basic example of 1-dimension finite elements**

Develop a code to calculate the displacement of the nodes and plot them in the original and displaced positions of a bar element with 4 nodes, the first and last nodes are restricted and a load of 3000 N is applied to the second node. Data:

$$E = 30e6 \text{ N/m}^2;$$

$$A=1 \text{ m}^2$$
;

$$L = 90 \text{ m};$$

$$[k]^e = \begin{bmatrix} \frac{AE}{L} & -\frac{AE}{L} \\ -\frac{AE}{L} & \frac{AE}{L} \end{bmatrix}$$

## Computational implementation proposal

```
1 clear; clc;
   //-input data
   E = 300000000; A = 1; EA = E*A; L = 90;
   numx = 3;//-number-of-elements
 5 node = linspace(0,L,numx+1);
 6 // Define nodes, elements and DoFs
    -- n=1:numx;
       element(:,1)=n;
       element(:,2)=element+1; // define elements in sequential order
    numnode=size(node,2);
                                                                                              o original nodes
    numelem=size(element,1);
                                                                                              o displaced nodes(x1000)
     ndof = numnode;
    //-Stiffness-matrix
                                                    0.6
   K=zeros (numnode, numnode);
   for e=1:numelem; -//-cover-all-elements
       j=element(e,:); // index nodes to elemen
    length element=node(j(2))-node(j(1));
      k=(EA/length element)*[1 -1;-1 1];>
19 K(j,j)=K(j,j)+k;
20 end;
   //loads-vector
   f = zeros(numnode, 1);
                                                   -0.4
23 f(2) = 3000;
                                                   -0.6
24 U = K\f; // displacement
25 //-to-plot-nodes
26 Y = node'+U*1000;
27 plot (node (1), 0, "ro");
28 plot(Y(2),0,"bo");plot(Y(3),0,"bo");
29 plot (node (2), 0, "ro"); plot (node (3), 0, "ro"); plot (node (4), 0, "ro");
30 hl=legend(['original-nodes','displaced-nodes(x1000)']);
31 xgrid
```



## Isoparametric formulation for finite elements

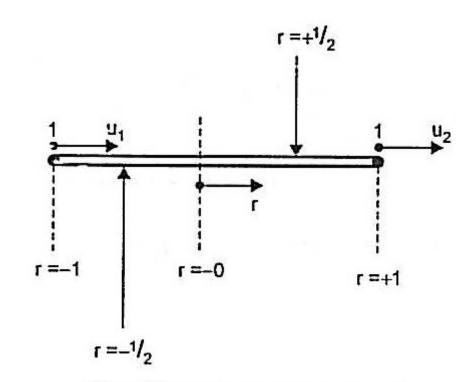
## Interpolation function

# $\begin{array}{c|c} & y & \hline u(x) = u_1 + \frac{u_2 - u_1}{L} \cdot x \\ \hline & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ \end{array}$

# Shape function (h<sub>1</sub> e h<sub>2</sub>)

$$u(x) = h_1 \cdot u_1 + h_2 \cdot u_2 = \sum_{i=1}^{2} h_i \cdot u_i$$

## Isoparametric



$$\leftarrow$$

$$u(x) = \left(\frac{1-r}{2}\right) \cdot u_1 + \left(\frac{1+r}{2}\right) \cdot u_2$$



## **Isoparametric formulation for finite elements**

$$\varepsilon = \frac{\partial u}{\partial x}$$
 strain

By the chain rule, we have:

$$\varepsilon = \frac{\partial x}{\partial u} = \frac{\partial r}{\partial u} \cdot \frac{\partial r}{\partial x}$$

being:

$$\begin{cases} u = \frac{1-r}{2} \cdot u_1 + \frac{1+r}{2} \cdot u_2 \\ x = \frac{1-r}{2} \cdot x_1 + \frac{1+r}{2} \cdot x_2 \end{cases} \qquad \epsilon = \frac{\partial u}{\partial r} \cdot \frac{\partial r}{\partial x} = \frac{u_2 - u_1}{2} \cdot \frac{2}{L}$$

$$\varepsilon = \frac{\partial u}{\partial x} = \frac{\partial u}{\partial r} \cdot \frac{\partial r}{\partial x}$$

$$\begin{cases} \frac{\partial u}{\partial r} = -\frac{u_1}{2} + \frac{u_2}{2} = \frac{u_2 - u_1}{2} \\ \frac{\partial r}{\partial x} = \frac{1}{\frac{\partial x}{\partial r}} = -\frac{1}{\frac{x_1}{2} + \frac{x_2}{2}} = \frac{1}{\frac{(x_2 - x_1)}{2}} = \frac{1}{\frac{L}{2}} = \frac{2}{L} \end{cases}$$
1-r 1+r

$$\varepsilon = \frac{\partial u}{\partial r} \cdot \frac{\partial r}{\partial x} = \frac{u_2 - u_1}{2} \cdot \frac{2}{L}$$

$$\varepsilon = \begin{bmatrix} -\frac{1}{L} & \frac{1}{L} \end{bmatrix} \quad \begin{cases} u_1 \\ u_2 \end{cases}$$



## **Isoparametric formulation for finite elements**

$$[B] = \begin{bmatrix} -1 & 1 \\ L & L \end{bmatrix} e [B]^T = \begin{bmatrix} -1/L \\ 1/L \end{bmatrix}$$
 
$$[b] = \int_{Vol}^{K} [B]^T \cdot [D] \cdot [B] \cdot dvol$$
 
$$[k]^B = \int_{Vol}^{X_2} [B]^T \cdot [D] \cdot [B] \cdot A \cdot dx$$
 
$$[D] = E \text{ (uniaxial stress state)}$$
 
$$[From Eq.1: \frac{\partial r}{\partial x} = \frac{2}{L} : \frac{\partial x}{\partial x} = \frac{L}{2} \cdot \partial r$$
 
$$(3)$$

Equation 3 relates the length dx (cartesian system) and the length dr (natural coordinate system).



The domain of Integral (Equation 2) in natural coordinates is given by the range from -1 to +1, according to the equation below.

$$[k]^{2} = \int_{-1}^{+1} \begin{bmatrix} -1/2 \\ 1/2 \end{bmatrix} \cdot E \cdot \begin{bmatrix} -1 & 1 \\ L & L \end{bmatrix} \cdot A \cdot \frac{L}{2} \cdot \partial r$$

where:

$$\partial x = J \cdot \partial r$$

$$\begin{bmatrix} k \end{bmatrix}^e = \begin{bmatrix} \frac{AE}{L} & -\frac{AE}{L} \\ -\frac{AE}{L} & \frac{AE}{L} \end{bmatrix}$$

$$J = \frac{L}{2}$$



## **Example in Scilab**

Develop a code to calculate stresses and plot nodes displacement in the original and displaced positions of an **isoparametric** bar element with 4 nodes. The first and last nodes are restricted and a load of 3000 N is applied to the second node.

#### Data:

$$E = 30e6 \text{ N/m}^2;$$

$$A=1 \text{ m}^2$$
;

$$L = 90 \text{ m}.$$

## **Computational implementation proposal**

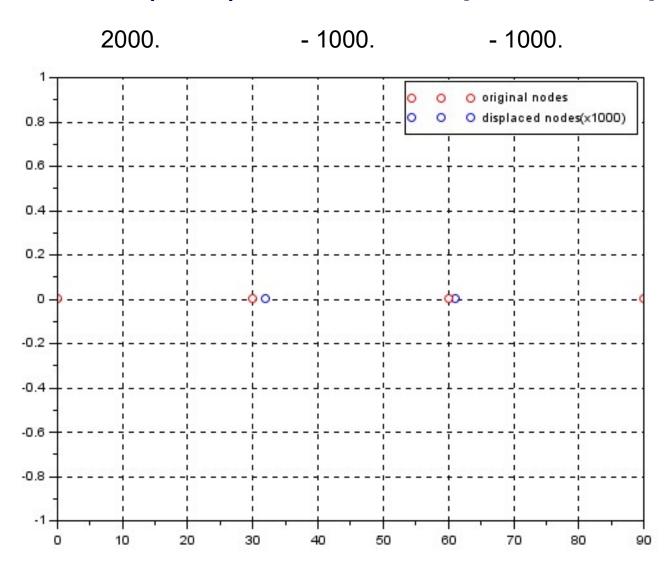
```
1 clear; clc;
   //-input-data
  E = 300000000; A = 1; EA = E*A; L = 90;
   numx = 3;// number of elements
   node = linspace(0,L,numx+1);
   node1=[(node(1:4))', [0.0.0.0]'];
   //-Define-nodes, elements and DoFs
    n=1:numx;
    element(:,1)=n;
    element(:,2)=element+1; // define elements in sequential order
10
    numnode=size(node,2);
11
    numelem=size(element,1);
     ndof = numnode;
       xx=node:
    /-Stiffness-matrix
16 K = sparse([],[],[numnode,numnode]);
   for e = 1:numelem
     index = element(e,:); // vector DoF for each element
     nn = size(index ,"*"); // vector index length
19
     length element = node(index (2))-node(index (1));
     detJ0 = length element/2; // J=L/2
21
     invJ0 = 1/detJ0; -// J^{-1}
     N = ([1,1]/2); -//-shape-function-matrix
23
     dNdxi = [-1:1]/2: // derived from the shape function matrix in relation
24
    -// to the natural coordinates
25
     dNdx = dNdxi*invJ0:
   // derived from the shape function matrix in relation to X (local coordinates)
    // matrix B *** [K] = sum of [B] ^ T. [D]. [B]. | J | , where [D] = E.A ***
    B = [-1/length element 1/length element]; // deformation vector
     K(index,index) = K(index,index) + (B'*E*B*A*detJ0*2); //B*2 = 2/L = dr/dx
31 end;
32 K=full (K)
```



```
33 //Load vector
34 f = zeros (numnode, 1);
35 f(2)=3000;
36 // Boundary conditions
37 fixedNodeW =find(xx==min(node(:)) | xx==max(node(:)))'; dofs=[fixedNodeW];
38
39 //1st and last nodes restricted
40 U = zeros (numnode, 1);
41 act = setdiff((1:ndof)',dofs);
42 U = K(act, act) \f(act);
43 U1 = zeros (ndof, 1);
44 U1 (act) =U;
45 U = U1
46 // stresses calculation
47 stress = zeros (numelem, size (element, 2), 1);
48 stressPoints(1,1) = -1; stressPoints(1,2) = 1;
49 for e = 1: numelem
   index = element(e,:); indexB = index; nn = size(index,"*");
   for q = 1:nn
52
   pt = stressPoints(q);
   N = ([1-pt, 1+pt]/2)';
54 dNdxi = [-1;1]/2;
   dNdx = dNdxi*invJ0; // same as lines of previous looping up to here
   --- // B matrix
57 B = [-1/length_element 1/length_element]; // deformation vector
   strain = B*U(indexB); stress(e,q) = E*strain;
58
59
   end:
60 end;
61 disp (stress(:,1))
62 Y = node'+U*1000;
63 plot (node (1), 0, "ro");
64 plot(Y(2),0,"bo");plot(Y(3),0,"bo");
65 plot (node (2), 0, "ro"); plot (node (3), 0, "ro"); plot (node (4), 0, "ro");
66 hl=legend(['original nodes', 'displaced nodes(x1000)']);
67 xgrid
```



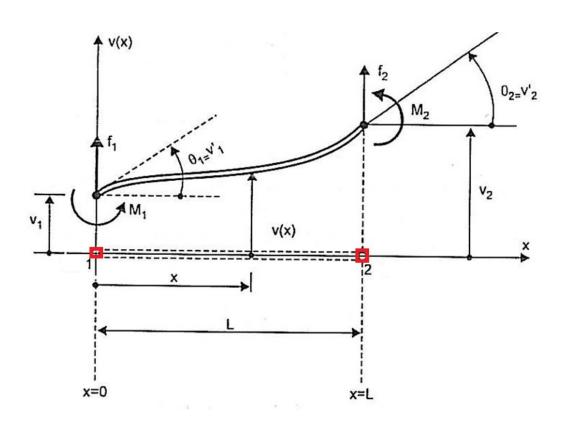
# Stress results (N/m²) and nodes displacements plot

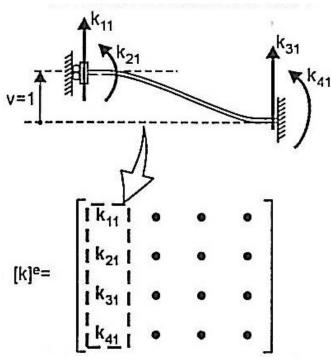




#### STRENGTH MATRIX OF A BAR ELEMENT CONSIDERING

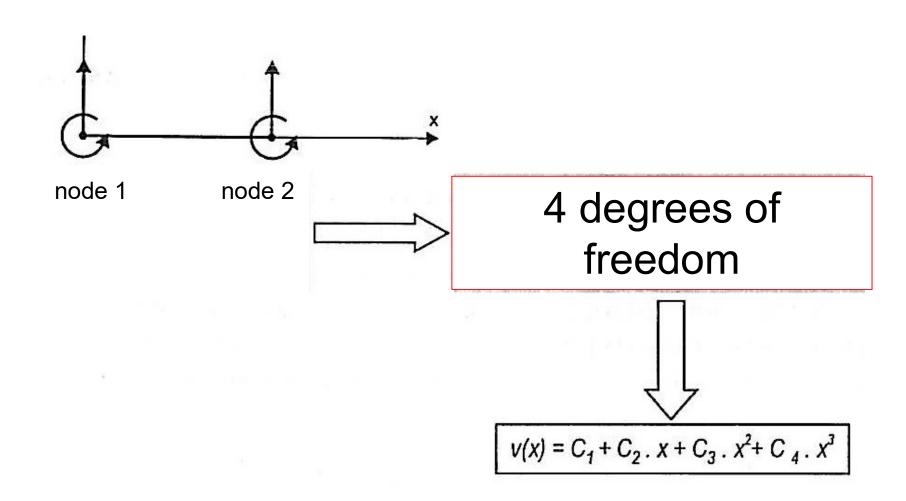
#### **BENDING AND ROTATION**







#### INTERPOLATION FUNCTION



#### **INTERNAL LOADS IN A BEAM**

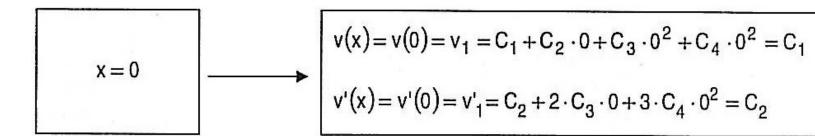
$$v(x) = \begin{bmatrix} 1 & x & x^2 & x^3 \end{bmatrix} \cdot \begin{bmatrix} C_1 \\ C_2 \\ C_3 \\ C_4 \end{bmatrix} \qquad v(x) = \begin{bmatrix} H(x) \end{bmatrix} \cdot \{C\}$$

Matrix which represents displacement and rotation (v'):

$$\{\delta(x)\} = \begin{cases} v(x) \\ v'(x) \end{cases} = \begin{bmatrix} 1 & x & x^2 & x^3 \\ 0 & 1 & 2 \cdot x & 3 \cdot x^2 \end{bmatrix} \cdot \begin{cases} C_1 \\ C_2 \\ C_3 \\ C_4 \end{cases}$$



## Substituting the value of x by 0 and L, we have:



$$v(x) = v(L) = v_2 = C_1 + C_2 \cdot L + C_3 \cdot L^2 + C_4 \cdot L^3$$

$$v'(x) = v'(L) = v'_2 = C_2 + 2 \cdot C_3 \cdot L + 3 \cdot C_4 \cdot L^2$$

$$\{\delta\} = [A].\{C\} \qquad \left\{\delta\} = \begin{cases} v_1 \\ v_1 \\ v_2 \\ v_2 \\ v_2 \end{cases} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & L & L^2 & L^3 \\ 0 & 1 & 2 \cdot L & 3 \cdot L^2 \end{bmatrix} \cdot \begin{bmatrix} C_1 \\ C_2 \\ C_3 \\ C_4 \end{bmatrix} \right\}$$



## Being:

## and considering the inverse of A:

$$\mathbf{v}(\mathbf{x}) = \begin{bmatrix} \mathbf{I} & \mathbf{x} & \mathbf{x}^2 & \mathbf{x}^3 \end{bmatrix} \cdot \begin{bmatrix} \mathbf{C}_1 \\ \mathbf{C}_2 \\ \mathbf{C}_3 \\ \mathbf{C}_4 \end{bmatrix}$$

$$[A]^{-1} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -\frac{3}{L^2} & -\frac{2}{L} & \frac{3}{L^2} & -\frac{1}{L} \\ \frac{2}{L^3} & \frac{1}{L^2} & -\frac{2}{L^3} & \frac{1}{L^2} \end{bmatrix}$$

$$v(x) = [H(x)] \cdot \{C\}$$

$$v(x) = [V(x)] \cdot \{C\}$$

$$v(x) = [H(x)] \cdot [A]^{-1} \cdot \{\delta\}$$

$$[H(x)].[A]^{-1} = [N(x)]$$



#### **SHAPE FUNCTION**

$$N(x) = \begin{bmatrix} 1 & x & x^2 & x^3 \end{bmatrix}_{1x4} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -\frac{3}{L^2} & -\frac{2}{L} & \frac{3}{L^2} & -\frac{1}{L} \\ \frac{2}{L^3} & \frac{1}{L^2} & -\frac{2}{L^3} & \frac{1}{L^2} \end{bmatrix}_{4x4}$$

$$N(x) = \left[ \underbrace{\left[ \underbrace{1 + 0 \cdot x - 3 \cdot \frac{x^2}{L^2} \cdot x^2 + 2 \cdot \frac{x^3}{L^3}}_{N(x) = [\eta_{11} \ \eta_{12} \ \eta_{13} \ \eta_{14} \ ]_{1x4}}^{1 \cdot 0 + x \cdot 0 + 3 \frac{x^2}{L^2} - 2 \frac{x^3}{L^3}} \underbrace{\left[ \underbrace{1 \cdot 0 + x \cdot 0 - \frac{x^2}{L} + \frac{x^3}{L^2}}_{N(x) = [\eta_{11} \ \eta_{12} \ \eta_{13} \ \eta_{14} \ ]_{1x4}}^{1 \cdot 0 + x \cdot 0 + 3 \frac{x^2}{L^2} - 2 \frac{x^3}{L^3}} \right]} \right]$$

#### **CURVATURE CALCULATION**

$$\frac{1}{\rho} = \frac{M}{E \cdot I} = \frac{d^2v}{dx^2} = v^*(x)$$

$$v^*(x) = 2 \cdot C_3 + 6 \cdot C_4 \cdot x$$

$$v''(x) = \begin{bmatrix} 0 & 0 & 2 & 6 \cdot x \end{bmatrix} \begin{cases} C_1 \\ C_2 \\ C_3 \\ C_4 \end{cases}$$
 being:  $\{C\} = [A]^{-1} \cdot \{\delta\}$ , we have:

$$v''(x) = [0 \ 0 \ 2 \ 6 \cdot x] \cdot [A]^{-1} \cdot \{\delta\}$$

being: 
$$[B(x)] = [0 \ 0 \ 2 \ 6 \cdot x] \cdot [A]^{-1}$$

$$v''(x) = [B(x)].\{\delta\}$$



Performing the matrix multiplication, we have:

$$[B] = \left[ \left( -\frac{6}{L^2} + 12 \cdot \frac{x}{L^3} \right) \left( -\frac{4}{L} + 6 \cdot \frac{x}{L^2} \right) \left( \frac{6}{L^2} - 12 \cdot \frac{x}{L^3} \right) \left( -\frac{2}{L} + 6 \cdot \frac{x}{L^2} \right) \right]$$

By means of  $[B]^T$ . [B] and integrals, it is obtained:

$$\{k\}^e = \begin{bmatrix} \frac{12.E.I}{L^3} & \frac{6.E.I}{L^2} & \frac{-12.E.I}{L^3} & \frac{6.E.I}{L^2} \\ \frac{6.E.I}{L^2} & \frac{4.E.I}{L} & \frac{-6.E.I}{L^2} & \frac{2.E.I}{L} \\ \frac{-12.E.I}{L^3} & \frac{-6.E.I}{L^2} & \frac{12.E.I}{L^3} & \frac{-6.E.I}{L^2} \\ \frac{6.E.I}{L^2} & \frac{2.E.I}{L} & \frac{-6.E.I}{L^2} & \frac{4.E.I}{L} \end{bmatrix}$$

The matrix [B] allows to change nodal displacements into deformations within the element.

Being  $\{k\}^e$ , the stiffness matrix, we have:  $\{k\}^e = E.I.\int_0^L [B]^T.[B]dx$ 

Considering the stiffness matrix of the element for axial loads and bending moments simultaneously, we have:

$$\{k\}^e = \{k\}_{axial}^e + \{k\}_{bending}^e$$

$$\begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 \\ 0 & 12b & 6bL & 0 & -12b & 6bL \\ 0 & 6bL & 4bL^2 & 0 & -6bL & 2bL^2 \\ -a & 0 & 0 & a & 0 & 0 \\ 0 & -12b & -6bL & 0 & 12b & -6bL \\ 0 & 6bL & 2bL^2 & 0 & -6bL & 4bL^2 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 2 \\ 3 \\ 4 \\ -1 \end{bmatrix}$$

$$\delta = \begin{cases} K_1 \\ K_2 \\ K_2 \\ K_2 \\ K_2 \\ K_2 \end{cases}$$

$$\delta = \begin{cases} K_1 \\ K_1 \\ K_2 \\ K_2 \\ K_2 \\ K_2 \end{cases}$$

$$\delta = \begin{cases} K_1 \\ K_1 \\ K_2 \\ K_2 \\ K_2 \\ K_2 \end{cases}$$



## **Example in Scilab**

Develop a code to calculate displacements (u, v) and curvature of a 2-nodes single element. The first node is restricted and loads (fx = 3000 and fy = -500 N) and a moment of 50 Nm are applied to the second node.

Please consider:

$$E = 30e6 \text{ N/m}^2;$$

$$A=6.8 \text{ m}^2$$
;

$$L = 90 \text{ m};$$

$$I = 65 \text{ m}^4.$$



## **Computacional implementation proposal**

```
1 |clear; clc;
 2 //- Input data
 3 E = 30000000; A = 6.8; I = 65; EA = E*A; EI = E*I;
  node = [0,0;1,0];
 5 | xx = node(:,1);yy = node(:,2);
 6 |element = [1,2];
 7 numnode = size(node,1);
 g | numelem = size(element, 1);
   // Matrix initialization
10 U = zeros (3*numnode, 1);
11 f = zeros (3*numnode, 1);
12 K = sparse([], [], [3*numnode, 3*numnode]);
13 // Load
14 f(4)=3000; f(5)=-500; f(6)=50;// fx; fy; Moment
15 for e = 1: numelem
16 index = element(e,:);
17 indexB = [index, index+numnode, index+2*numnode];
18  xa = xx(index(2))-xx(index(1));
   ya = yy(index(2))-yy(index(1));
   L = sqrt(xa*xa+ya*ya); //cosa=xa/L; sina=ya/L;
    a = EA/L; b = EI/(L^3);
    k1 = [a, 0, 0, -a, 0, 0;
    ----0,12*b, (6*b) *L,0,-12*b, (6*b) *L;
24
    0, (6*b) *L, (4*b) * (L^2), 0, - (6*b) *L, (2*b) * (L^2);
25
    ------a,0,0,a,0,0;
    .....0,-12*b,-(6*b)*L,0,12*b,-(6*b)*L;
    0, (6*b) *L, (2*b) * (L^2), 0, - (6*b) *L, (4*b) * (L^2) ];
   K(indexB, indexB) = K(indexB, indexB)+k1;
28
29 end;
30 // - Contourn - conditions
31 b = [1,1,1,0,0,0];
32 K([1,2,3],:) = []; // delete 1st, 2nd and 3rd lines of K which displacement = 0
33 K(:,[1,2,3]) = []; // delete 1st, 2nd and 3rd column of K which displacement = 0
34 f([1,2,3],:) = []; // delete 1st, 2nd and 3rd lines of f which displacement = 0
35 d1 = K\f; // // Displacements calculation
36 disp (d1)
```

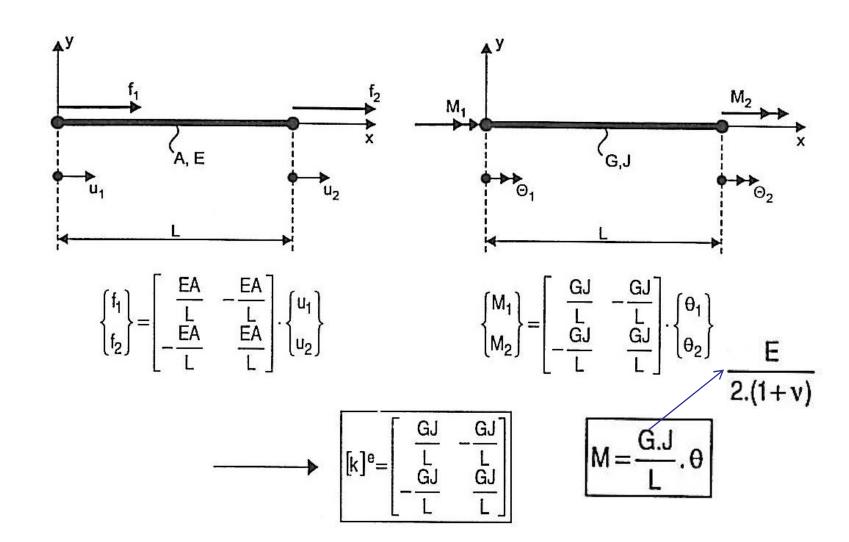
d1 = 0.0000147

- 7.265D-08

- 0.000001

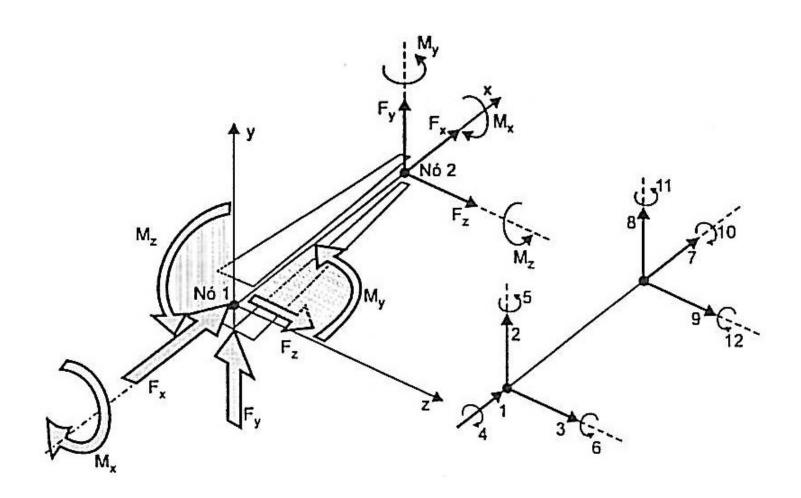


#### STIFFNESS MATRIX CONSIDERING TORSION





# **DoFs**



### **GLOBAL STIFFNESS MATRIX**

	a										a=	<u>EA</u>	
[k] <sup>e</sup> =	0	12bz									====	L	
	0	0	12by								b <sub>z</sub> =	Elz	
	0	0	0	t								-	
	0	0	–6by∙L	0	4by L <sup>2</sup>						$b_y = \frac{E \cdot l_y}{13}$		
	0	6b <sub>Z</sub> ⋅L	0	0	0	4 <sub>bz</sub> ·L <sup>2</sup>					L		
	-a	0	0	0	4b <sub>y</sub> ·L <sup>2</sup> 0 0	0	а				$t = \frac{GJ}{L}$		
	0	-12bz	0	0	0	–6b <sub>z</sub> ⋅L	0	12bz					
	0	0	-12by	0	-6by⋅L	0	0	0	12by				
	0	0	0	_t	0	0		0	0	t			
	0	0	–6by⋅L	0	2·by L <sup>2</sup>	0	0	0	6by ·L	0	4by ·L <sup>2</sup>		
	0	6b <sub>Z</sub> ⋅L	0	0		$2b_z \cdot L^2$						4bz·L <sup>2</sup>	

#### **Exercise on Scilab**

```
Based on the previous code data, calculate displacements and torsion being: E=30e6; A=6.8; Iz=65; Iy=45; G=80e6; J=50; f(7)=3000.0; f(8)=500; f(9)=300; f(10)=500; f(11)=300; f(12)=400.
```