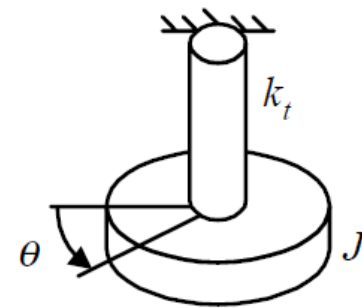
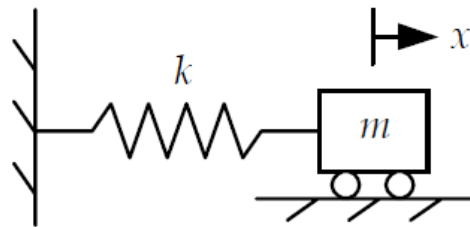


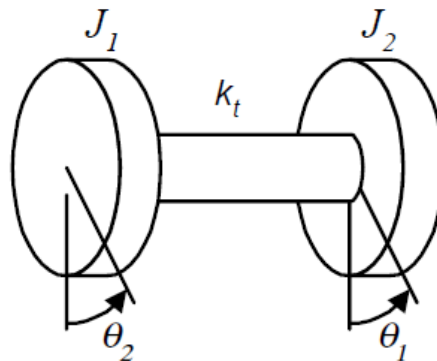
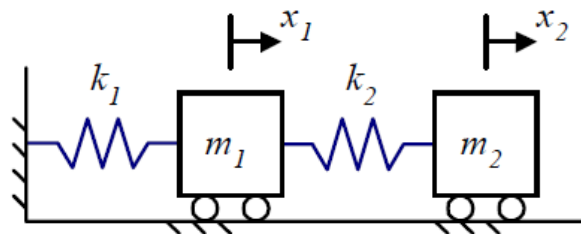
## Mechanical stiffness

Degrees of freedom (DOF)

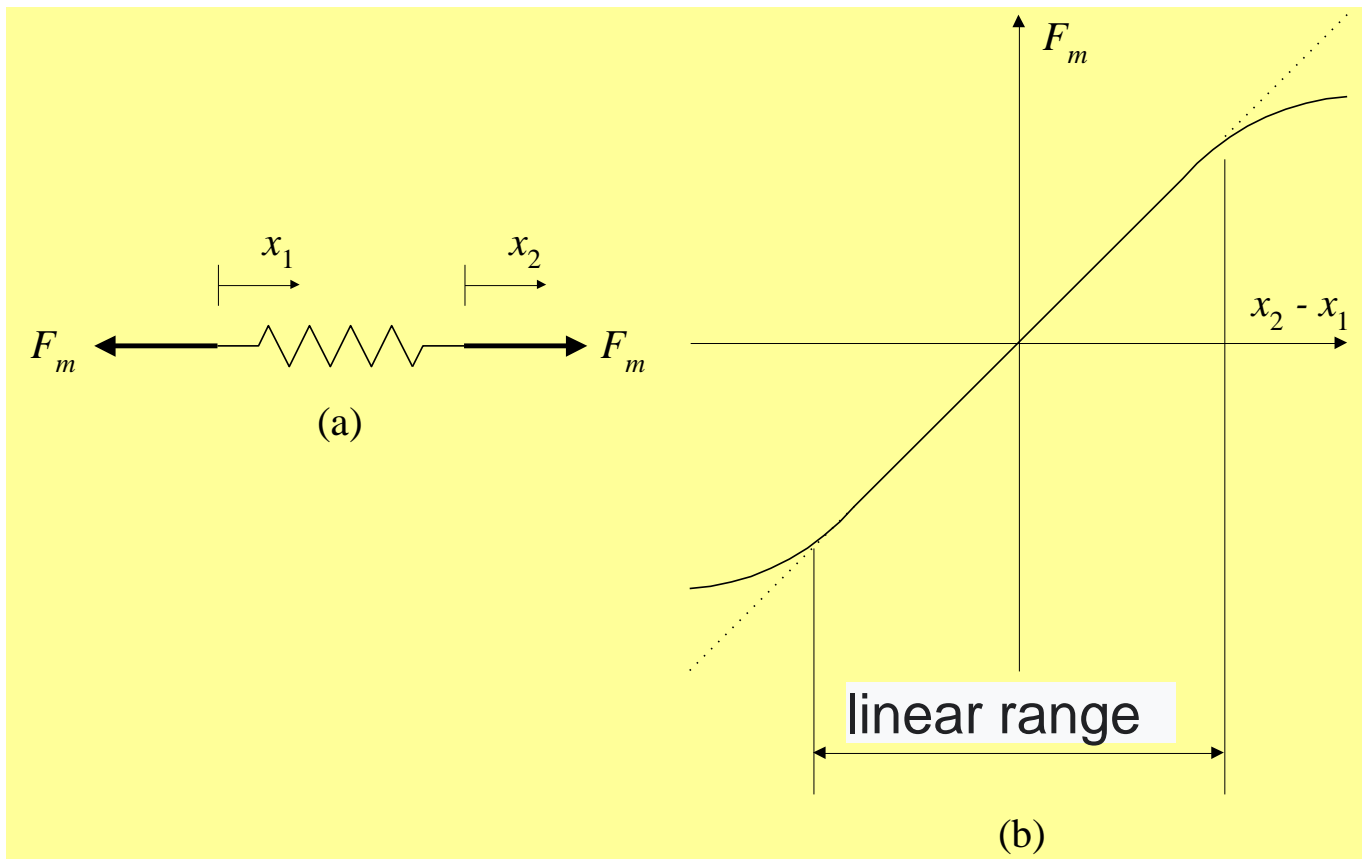
1 DOF



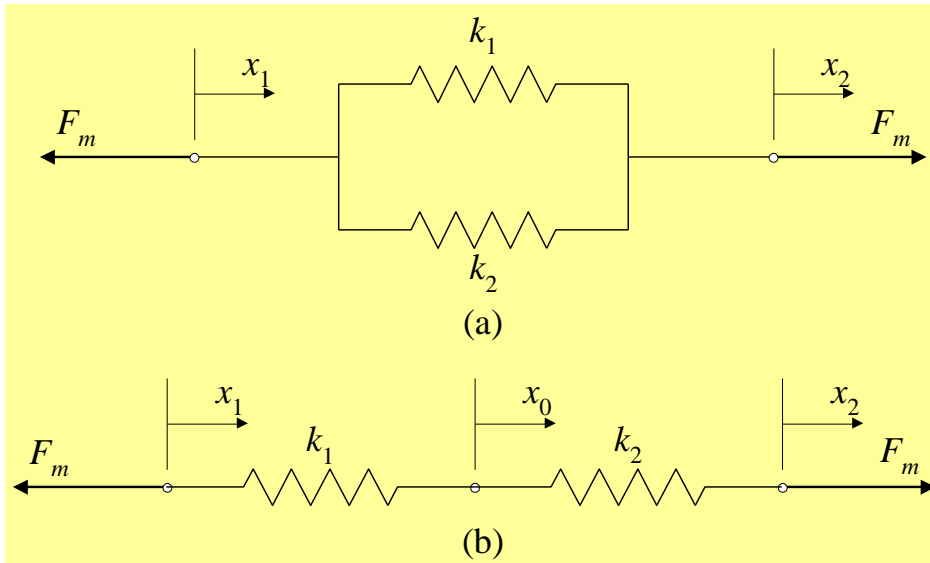
2 DOFs



## Spring element



## Springs association



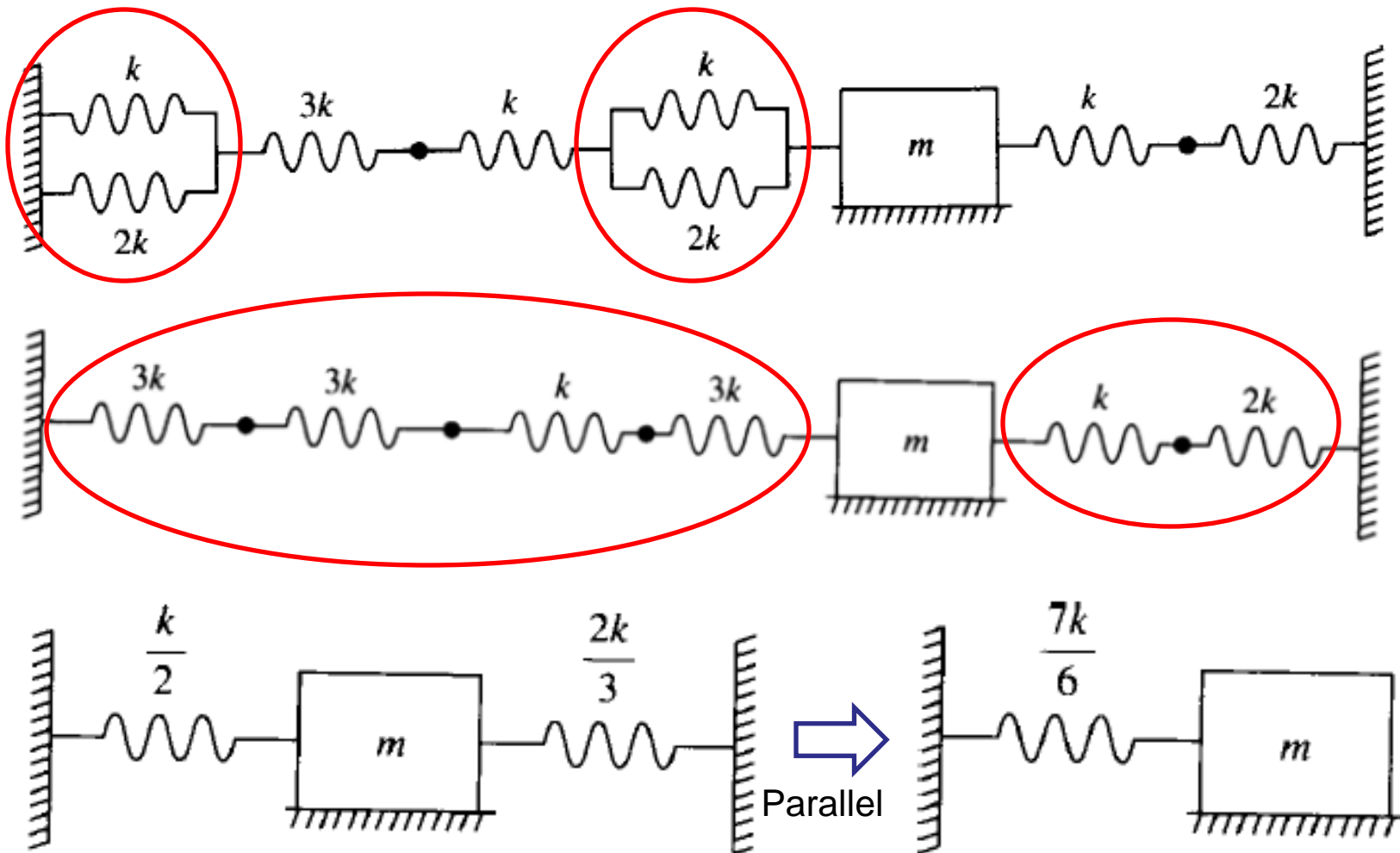
$$k_{eq} = k_1 + k_2$$

$$k_{eq} = \sum_{i=1}^n k_i$$

$$k_{eq} = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}}$$

$$k_{eq} = \frac{1}{\sum_{i=1}^n \frac{1}{k_i}}$$

## Example



## On Scilab

Determine the equivalent stiffness of the system:

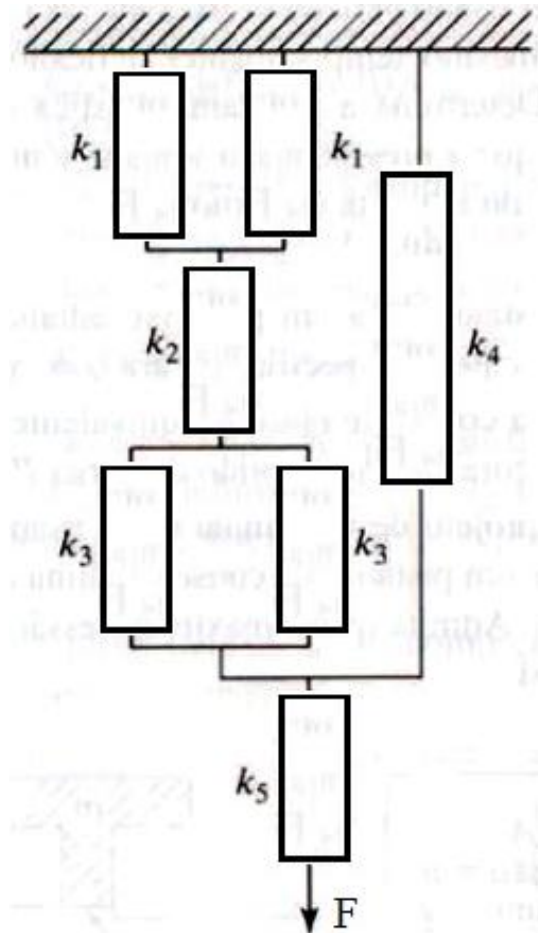
$$K_1 = 100 \text{ N/m}$$

$$K_2 = 200 \text{ N/m}$$

$$K_3 = 300 \text{ N/m}$$

$$K_4 = 400 \text{ N/m}$$

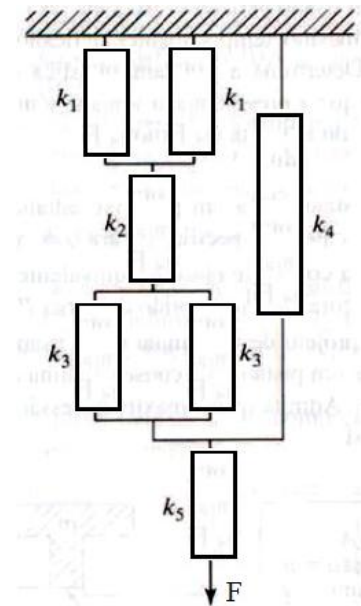
$$K_5 = 500 \text{ N/m}$$



## Solution

```

1 clear; clc;
2 K1 = 100; % N/m
3 K2 = 200; % N/m
4 K3 = 300; % N/m
5 K4 = 400; % N/m
6 K5 = 500; % N/m
7 keq1 = K1+K1; % N/m
8 keq3 = K3+K3; % N/m
9 keq123 = 1 / ( (1/keq1) + (1/K2) + (1/keq3) );
10 keq1234 = keq123 + K4; % N/m
11 keq = 1 / ( (1/keq1234) + (1/K5) )
    
```



K1	100
K2	200
K3	300
K4	400
K5	500
keq	246
keq1	200
keq123	85.7
keq1234	486
keq3	600

## Torsional stiffness

$$k_t = \frac{M_t}{\theta} = \frac{GI}{L}$$

S.I. [Nm]

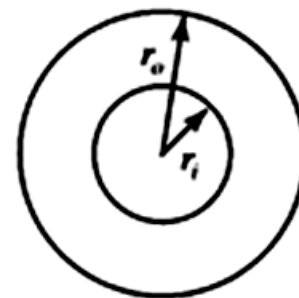
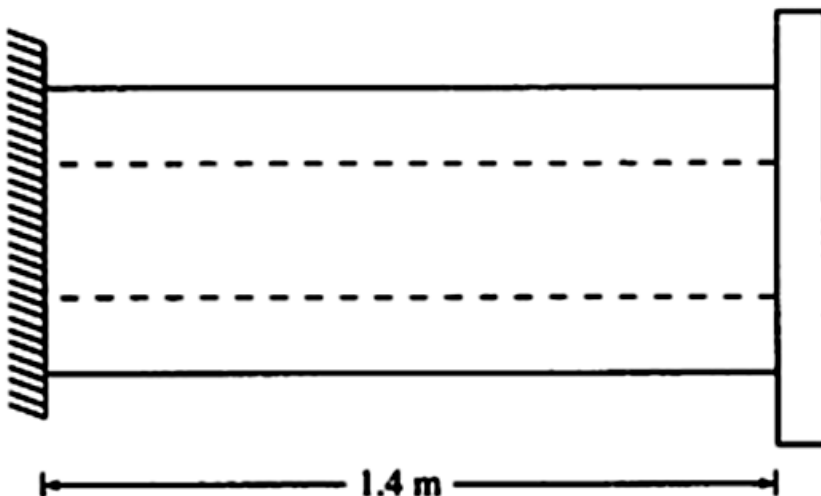
- Hollow shaft:

$$I = \frac{\pi}{32} (d_e^4 - d_i^4)$$

- Solid shaft :

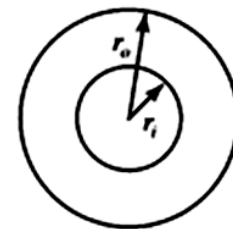
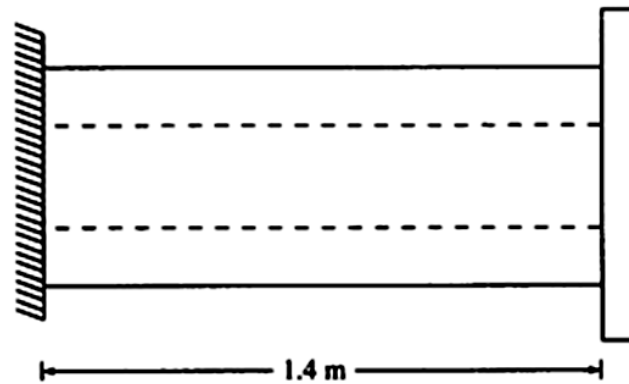
$$I = \frac{\pi}{2} (r^4) = \frac{\pi}{32} (d^4)$$

**Example:** Determine the torsional stiffness of the hollow shaft, as shown in the Figure below.



$$\begin{aligned} r_i &= 15 \text{ mm} \\ r_o &= 25 \text{ mm} \\ G &= 80 \times 10^9 \frac{\text{N}}{\text{m}^2} \end{aligned}$$

## On Scilab:



$$\begin{aligned} r_i &= 15 \text{ mm} \\ r_o &= 25 \text{ mm} \\ G &= 80 \times 10^9 \frac{\text{N}}{\text{m}^2} \end{aligned}$$

```

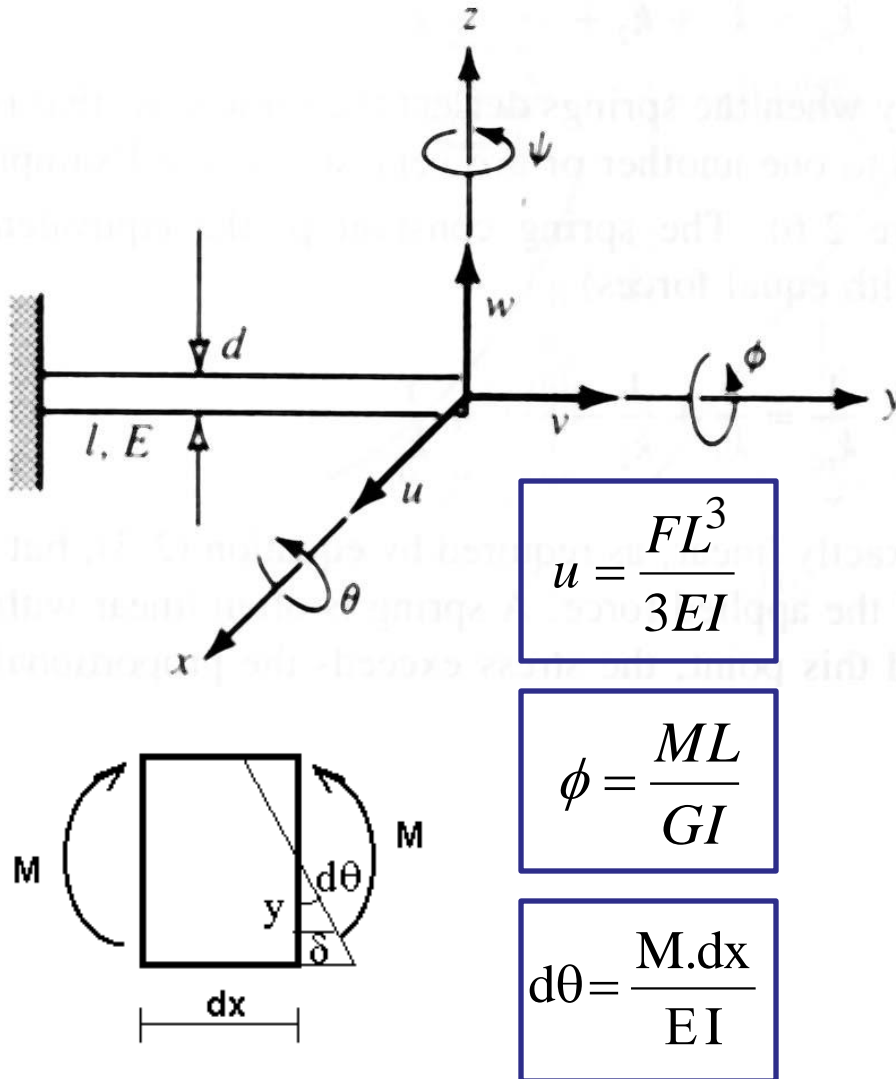
1 clear; clc;
2 ri=15; // mm
3 re=25; // mm
4 L=1400; // mm
5 G=-80000; // MPa
6 J=-(%pi/2)*(((re).^4)-((ri).^4));
7 k=(G*J/L)/1000; // 10^-3 (mm to m)
8 printf("k=%g Nm\n",k);

```

G	8e+04
J	5.34e+05
L	1.4e+03
k	3.05e+04
re	25
ri	15



## Elastic systems



$$F_v = \frac{EA v}{L}, \quad k_{vv} = \frac{EA}{L}$$

$$F_u = \frac{3EI_z u}{L^3}, \quad k_{uu} = \frac{3EI_z}{L^3}$$

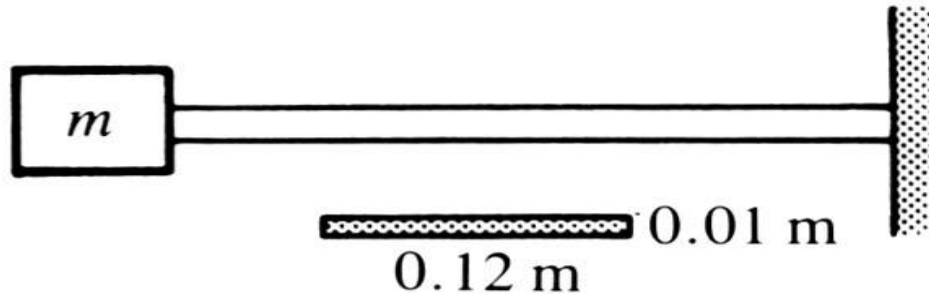
$$F_w = \frac{3EI_x w}{L^3}, \quad k_{ww} = \frac{3EI_x}{L^3}$$

$$M_\phi = \frac{GI_y \phi}{L}, \quad k_{\phi\phi} = \frac{GI_y}{L}$$

$$M_\psi = \frac{EI_z \psi}{L}, \quad k_{\psi\psi} = \frac{EI_z}{L}$$

$$M_\theta = \frac{EI_x \theta}{L}, \quad k_{\theta\theta} = \frac{EI_x}{L}$$

## Example: cantilever beam



$$m_{viga} = 100 \text{ kg}$$

$$m_{eff} = 3.12 \text{ kg}$$

$$L = 1 \text{ m}$$

$$E = 2.1 \times 10^{11} \text{ N/m}^2$$

$$I = \frac{bh^3}{12} = \frac{0.12 \times 0.01^3}{12} = 1 \times 10^{-8} \text{ m}^4$$

$$k = \frac{3EI}{L^3} = \frac{3 \times 2.1 \times 10^{11} \times 10^{-8}}{1^3} = 6300 \text{ N/m}$$

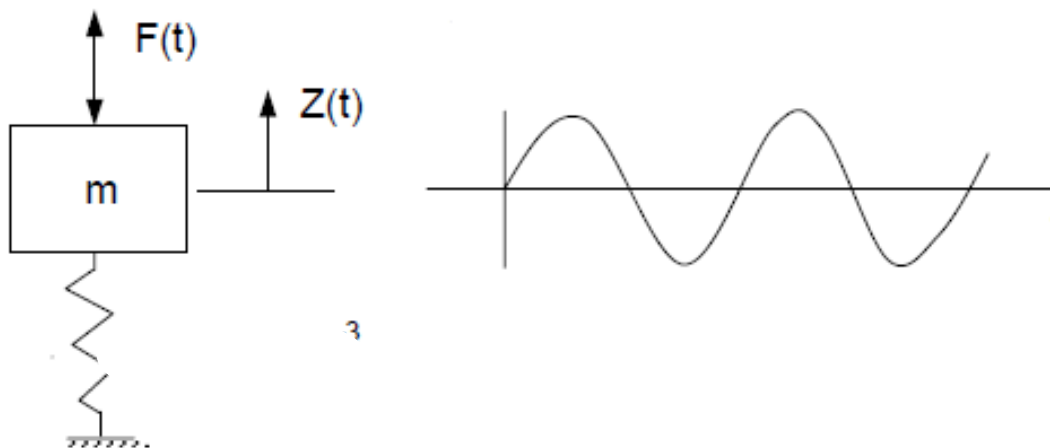
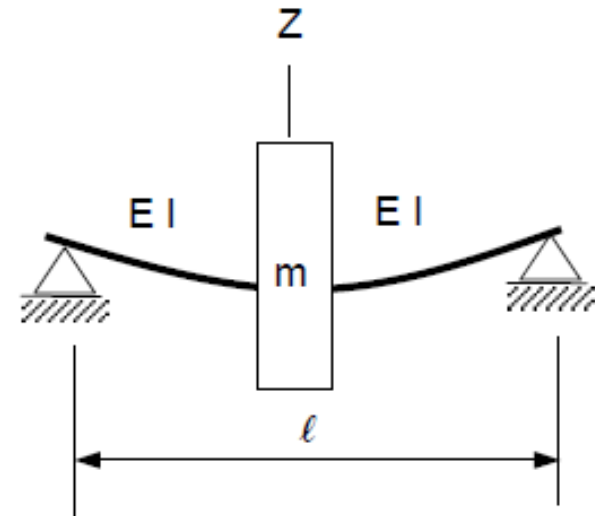
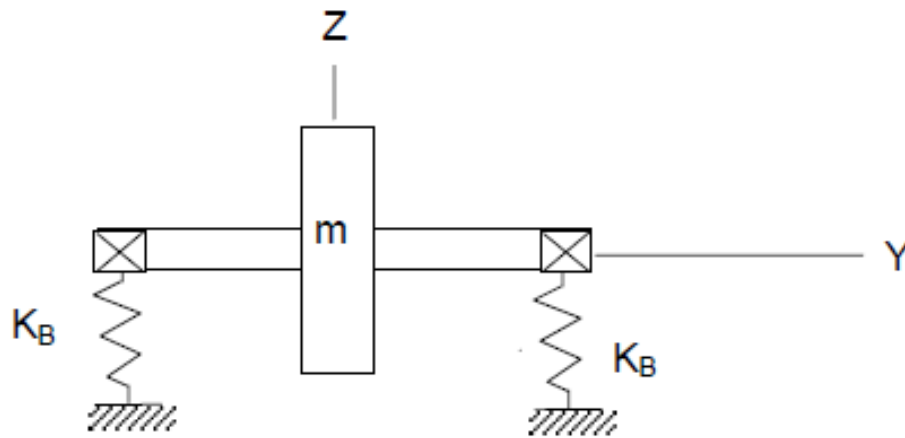
Without mass (m)

$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{6300}{100}} = 7.94 \text{ rad/s}$$

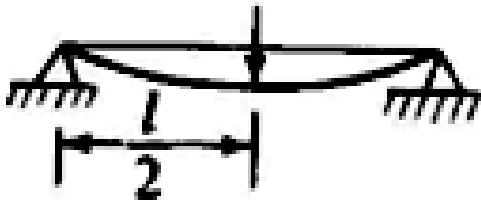
With mass (m)

$$\omega_n = \sqrt{\frac{k}{m_{eq}}} = \sqrt{\frac{6300}{100 + 3.12}} = 7.82 \text{ rad/s}$$

## Point load stiffness



## Equations development



$$M_{max} = R_A x$$

$$R_A = R_B = P / 2$$

Applying the double integration method, we have :

$$EI \frac{d^2 v}{dx^2} = (P / 2) x$$

$$EI \frac{dv}{dx} = \frac{Px^2}{4} + C_1 \quad (1)$$

$$EI v = \frac{Px^3}{12} + C_1 x + C_2 \quad (2)$$

Considering the boundary conditions, we have:

$$\checkmark \quad \frac{dv}{dx} = 0 \quad \text{in} \quad x = L/2$$

$$0 = \frac{PL^2}{16} + C_1 \quad \text{From Equation (1)}$$

$$\checkmark \quad v = 0 \quad \text{in} \quad x = 0$$

$$0 = \frac{Px^3}{12} + C_1 \cdot x + C_2 \quad \text{From Equation (2)}$$

Isolating the value of  $C_1$  e  $C_2$ , we have:  $C_1 = -\frac{PL^2}{16}$  ;  $C_2 = 0$

Replacing values of  $C_1$  e  $C_2$  in the Equation (2), we have:

$$EIv = \frac{Px^3}{12} - \frac{PL^2}{16}x + 0$$

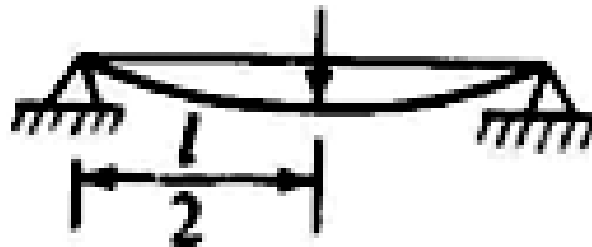
Knowing that the maximum displacements occur in  $L/2$ :

$$EIv = \frac{PL^3}{96} - \frac{PL^3}{32}$$

$$v = \frac{(-P)L^3}{48EI} \Rightarrow -P = \frac{48EIv}{L^3}$$

$$k = \frac{48EI}{L^3}$$

**Example:** Determine the stiffness of a bar of length  $L = 300$  mm and  $E = 210$  GPa, with a rectangular cross section ( $10 \times 5$  mm<sup>2</sup>). Check what happens when the original position of the bar is rotated 90 degrees (cross section =  $5 \times 10$  mm<sup>2</sup>) .

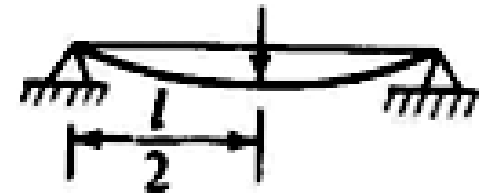


## Solution on Scilab

```

1 clear; clc;
2 E = 210000; // MPa
3 L = 300; // mm
4 b1 = 10; // mm
5 h1 = 5; // mm
6 I1 = (b1 * (h1^3)) / 12; // mm^4
7 k1 = (48 * E * I1) / (L^3); // N/mm
8 printf("k1 = %g N/mm\n", k1);
9 b2 = 5; // mm
10 h2 = 10; // mm
11 I2 = (b2 * (h2^3)) / 12; // mm^4
12 k2 = (48 * E * I2) / (L^3); // N/mm
13 printf("k2 = %g N/mm\n", k2);

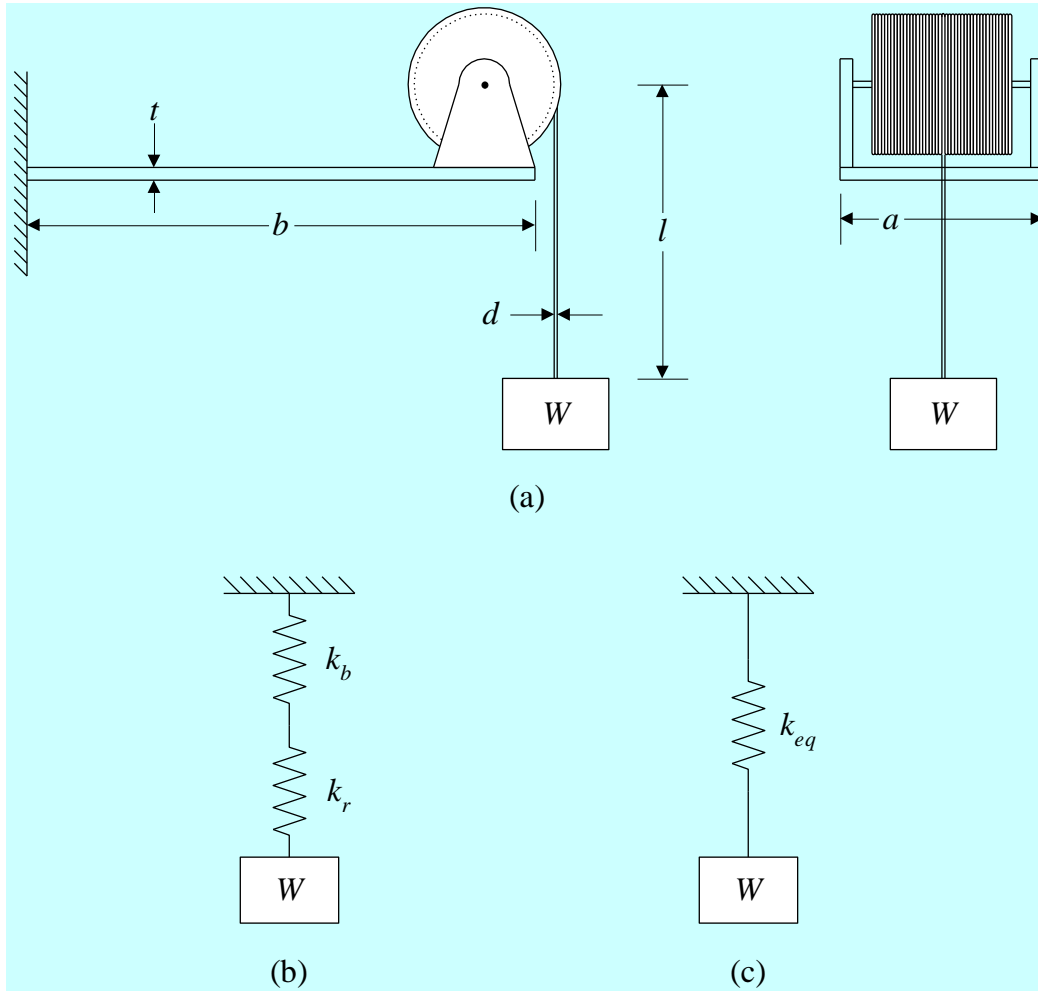
```



Nome	Value
E	2.1e+05
I1	104
I2	417
L	300
b1	10
b2	5
h1	5
h2	10
k1	38.9
k2	156



## Load lifting system

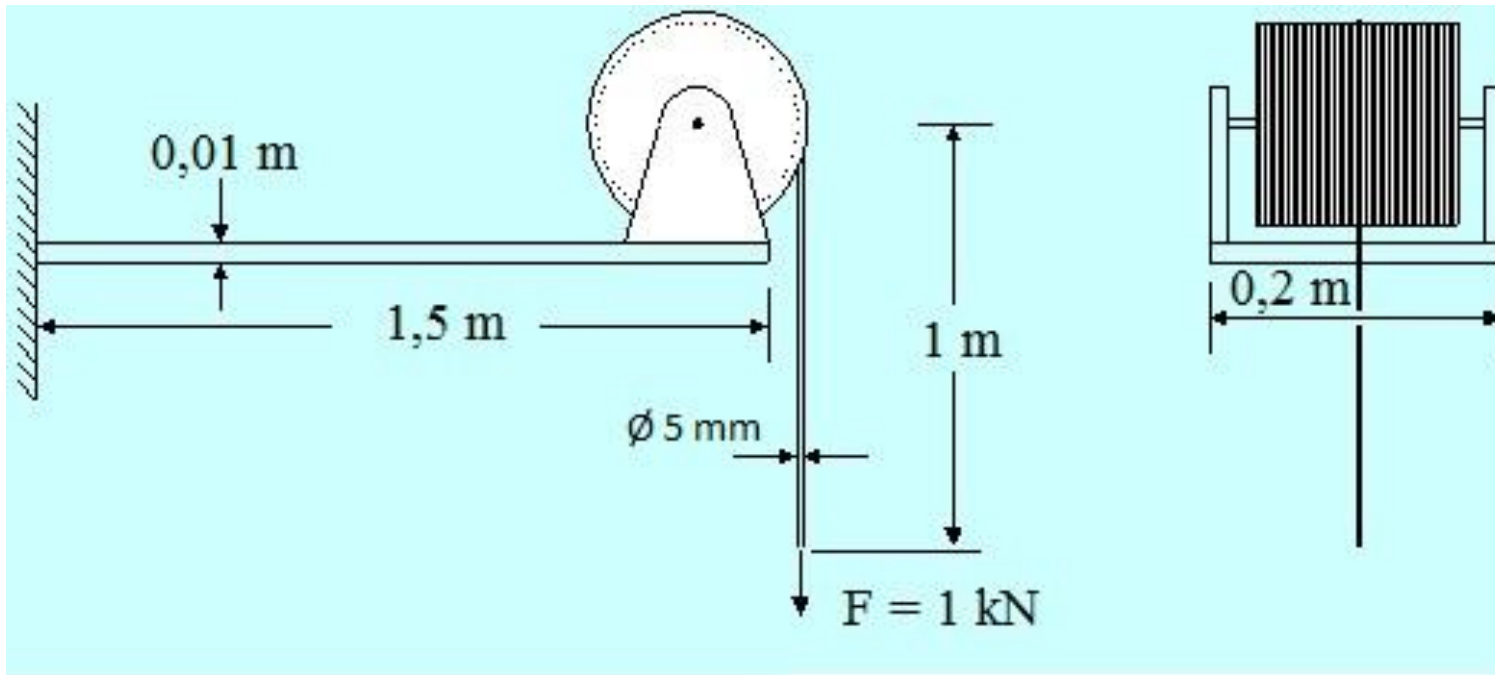


$$k_b = \frac{3EI}{L^3}$$

$$k_r = \frac{EA}{L}$$

$$k_{eq} = \frac{k_b k_r}{k_b + k_r}$$

## Example:



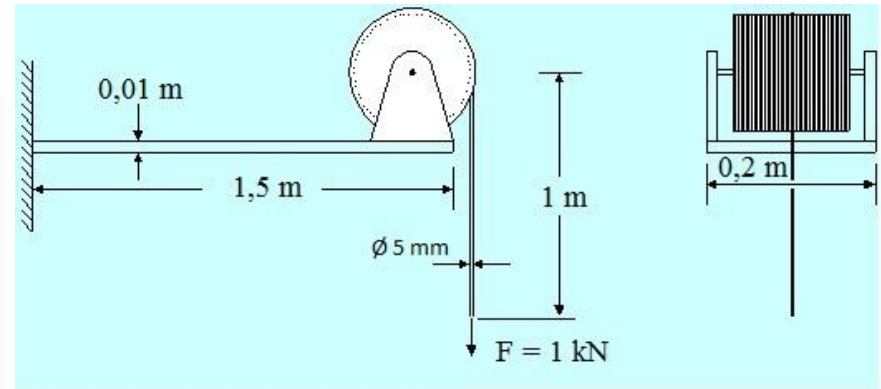
Considering  $E = 210 \text{ GPa}$  for the entire lifting system, calculate the equivalent stiffness.

## Solution on Scilab

```

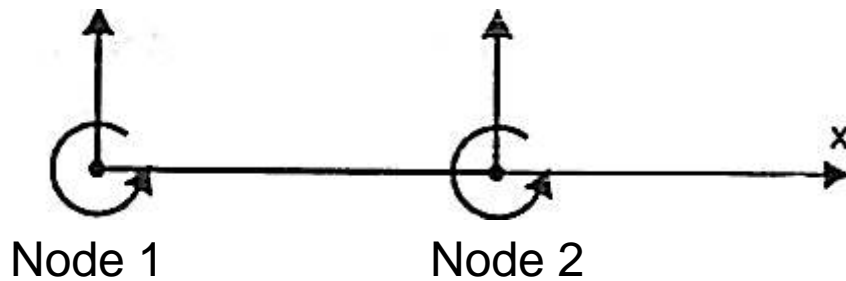
1 clear; clc;
2 E = 210000; // MPa
3 // beam (bending)
4 Lb = 1500; // mm
5 b = 200; // mm
6 h = 10; // mm
7 I = (b*(h^3))/12; // mm^4
8 kb = (3*E*I)/(Lb^3); // N/mm
9 // cable (traction)
10 r = 2.5; // mm
11 Lr = 1000; // mm
12 A = %pi*(r^2); // mm^2
13 kr = (E*A)/Lr; // N/mm
14 keq = (kb*kr)/(kb+kr)
15 printf("k = %g N/mm\n", keq);

```



A	19.6
E	2.1e+05
I	1.67e+04
Lb	1.5e+03
Lr	1e+03
b	200
h	10
kb	3.11
keq	3.11
kr	4.12e+03
r	2.5

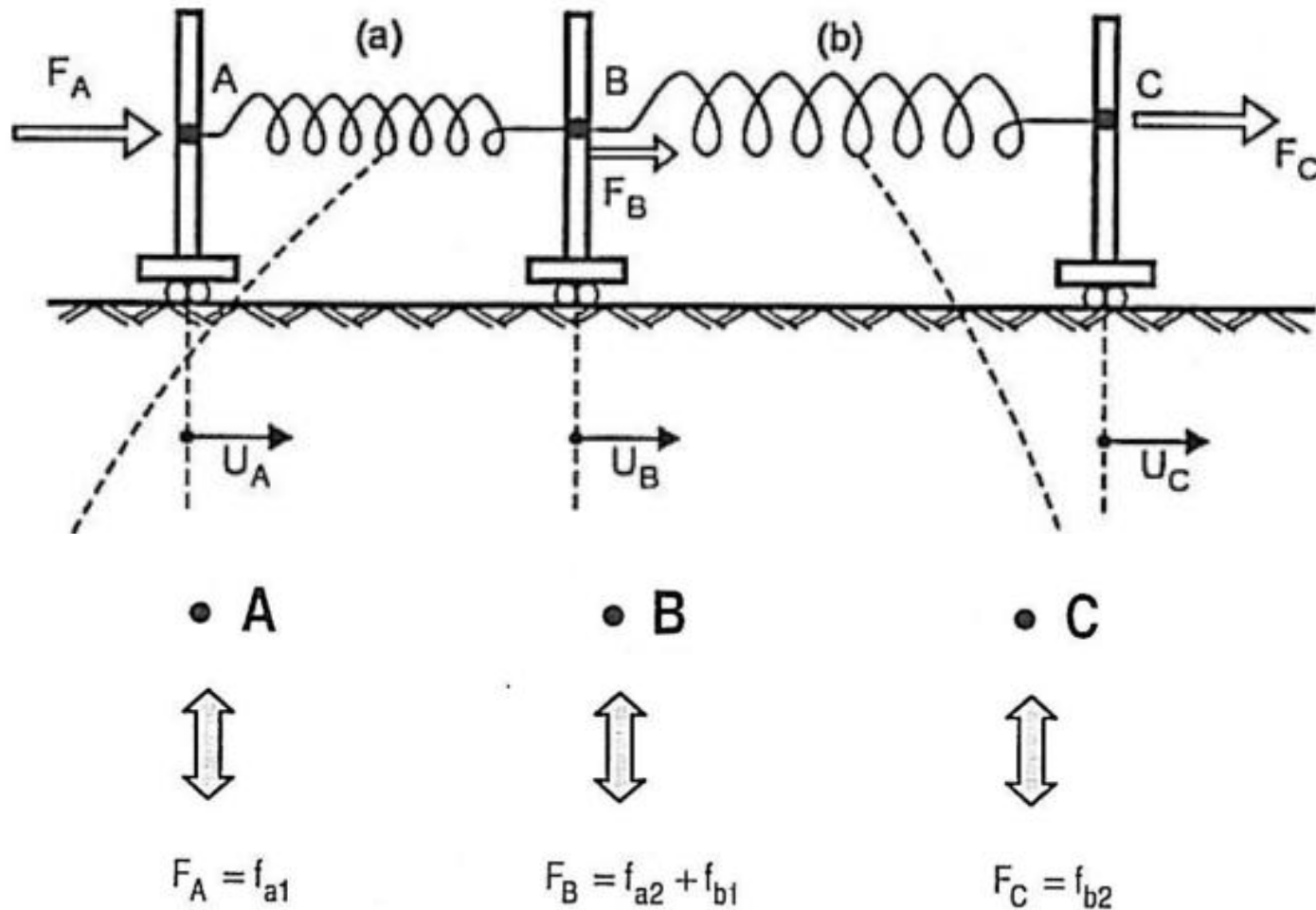
## Stiffness matrix



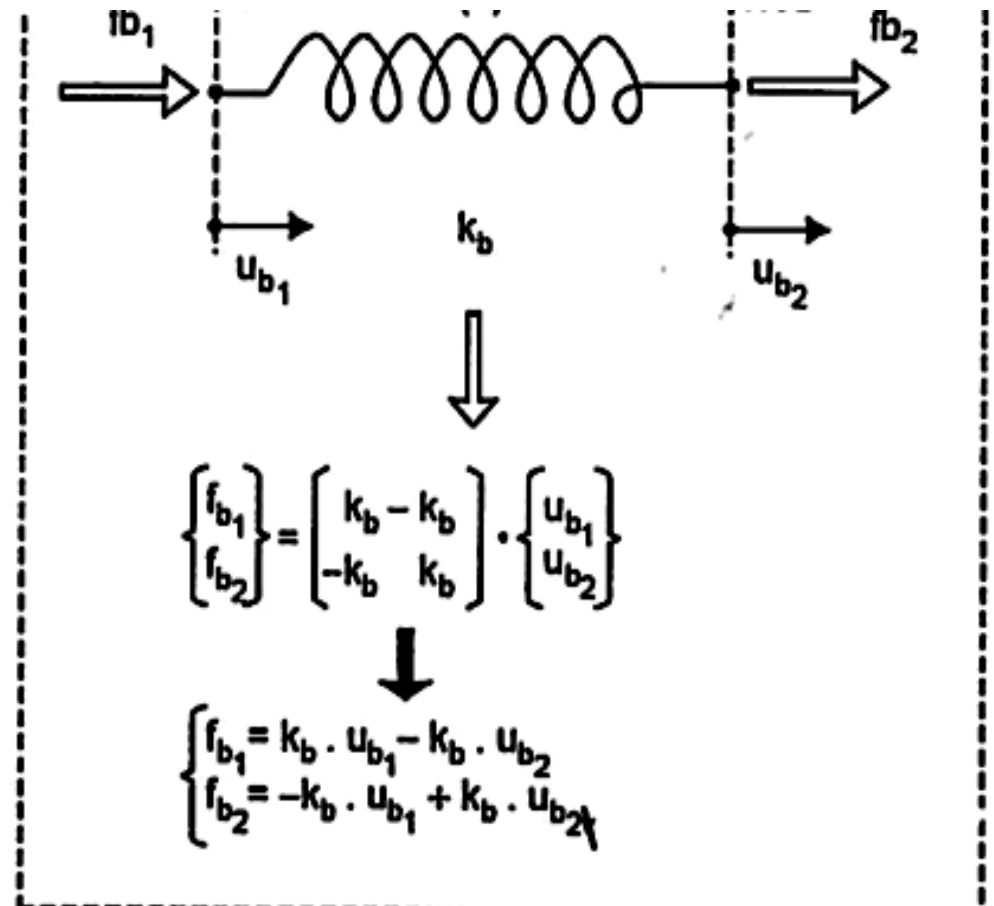
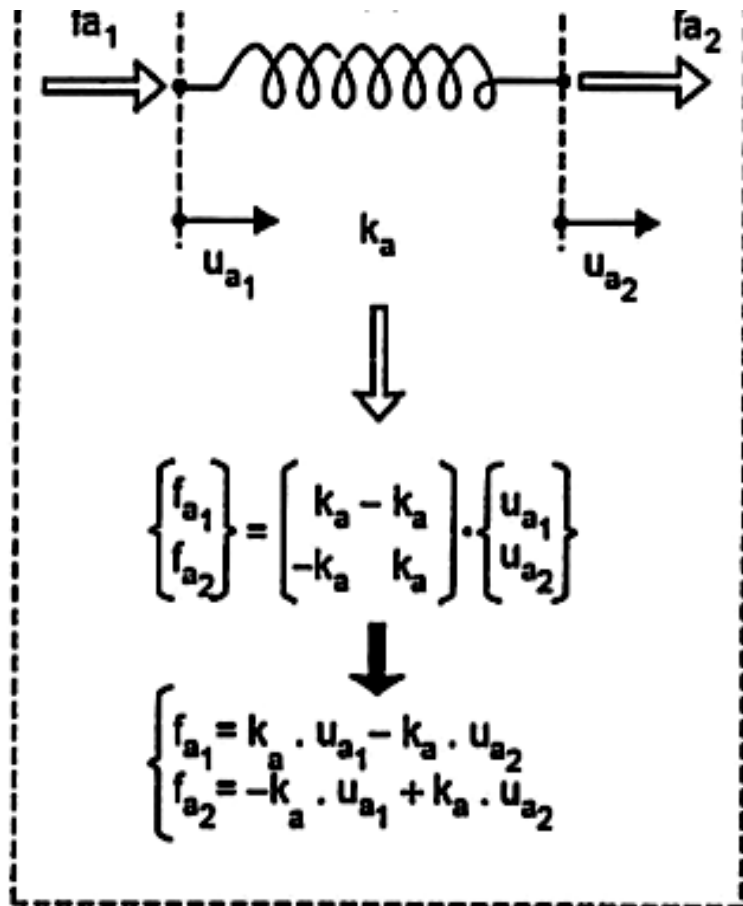
$$\begin{cases} F_1 = \frac{EA}{L} u_1 \\ F_1 = -\frac{EA}{L} u_2 \end{cases} \quad \begin{cases} F_2 = \frac{EA}{L} u_2 \\ F_2 = -\frac{EA}{L} u_1 \end{cases} \Rightarrow \begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} K_{11} & -K_{12} \\ -K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$K_{21}$  is the load from node 2 due to the unit displacement of node 1 ( $u_1 = 1$ ), keeping  $u_2 = 0$ .

## Two elements stiffness matrix



## Two elements stiffness matrix



## Global stiffness matrix

Stiffness matrix  
(Element "a")

Stiffness matrix  
(Element "b")

$$\begin{Bmatrix} F_A \\ F_B \\ F_C \end{Bmatrix} = \begin{bmatrix} \boxed{\begin{matrix} k_a & -k_a \\ -k_a & k_a \end{matrix}} & 0 \\ 0 & \boxed{\begin{matrix} k_b & -k_b \\ -k_b & k_b \end{matrix}} \end{bmatrix} \cdot \begin{Bmatrix} U_A \\ U_B \\ U_C \end{Bmatrix}$$

$$\begin{Bmatrix} F_A \\ F_B \\ F_C \end{Bmatrix} = \begin{bmatrix} k_a & -k_a & 0 \\ -k_a & k_a + k_b & -k_b \\ 0 & -k_b & k_b \end{bmatrix} \cdot \begin{Bmatrix} U_A \\ U_B \\ U_C \end{Bmatrix}$$

## Solution

$$\begin{Bmatrix} F_A \\ F_B \\ F_C \end{Bmatrix} = \begin{bmatrix} k_a & -k_a & 0 \\ -k_a & k_a + k_b & -k_b \\ 0 & -k_b & k_b \end{bmatrix} \cdot \begin{Bmatrix} U_A \\ U_B \\ U_C \end{Bmatrix}$$

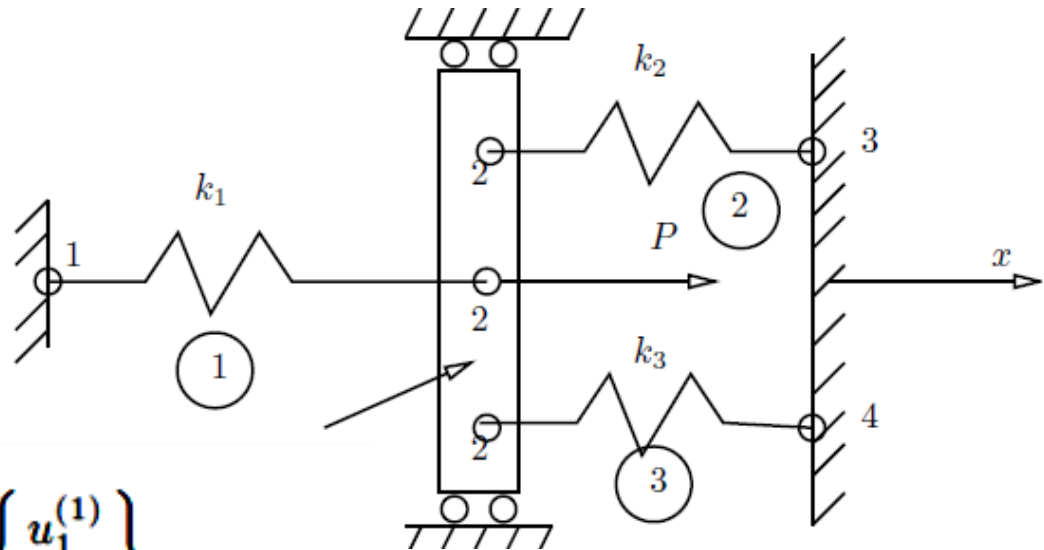
$$\begin{aligned} \{F_A\} &= [k_a] \cdot \{U_A\} + [-k_a \quad 0] \cdot \begin{Bmatrix} U_B \\ U_C \end{Bmatrix} \\ &\quad e \\ \begin{Bmatrix} F_B \\ F_C \end{Bmatrix} &= \begin{bmatrix} -k_a \\ 0 \end{bmatrix} \cdot \{U_A\} + \begin{bmatrix} k_a + k_b & -k_b \\ k_b & -k_b \end{bmatrix} \cdot \begin{Bmatrix} U_B \\ U_C \end{Bmatrix} \end{aligned}$$

↓

$U_A = 0$



## Example



$$\begin{Bmatrix} R_1^{(1)} \\ R_2^{(1)} \end{Bmatrix} = k^{(1)} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1^{(1)} \\ u_2^{(1)} \end{Bmatrix}$$

$$\begin{Bmatrix} R_1^{(2)} \\ R_2^{(2)} \end{Bmatrix} = k^{(2)} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1^{(2)} \\ u_2^{(2)} \end{Bmatrix}$$

$$\begin{Bmatrix} R_1^{(3)} \\ R_2^{(3)} \end{Bmatrix} = k^{(3)} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1^{(3)} \\ u_2^{(3)} \end{Bmatrix}$$

## Solution

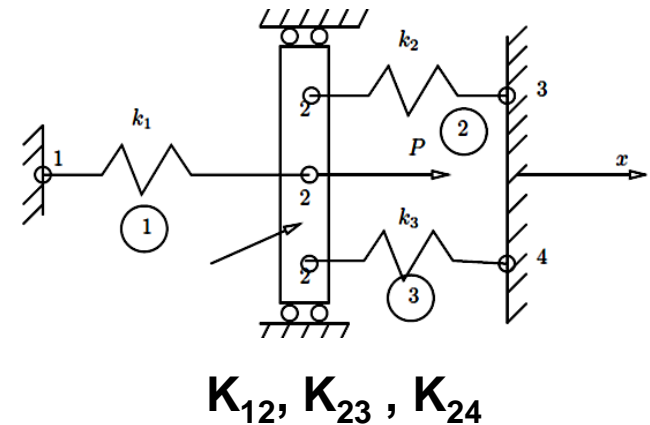
$$\begin{bmatrix} k_1 & -k_1 & 0 & 0 \\ -k_1 & k_1 + k_2 + k_3 & -k_2 & -k_3 \\ 0 & -k_2 & k_2 & 0 \\ 0 & -k_3 & 0 & k_3 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} F_1 \\ P \\ F_3 \\ F_4 \end{Bmatrix}$$

$$u_1 = u_3 = u_4 = 0,$$

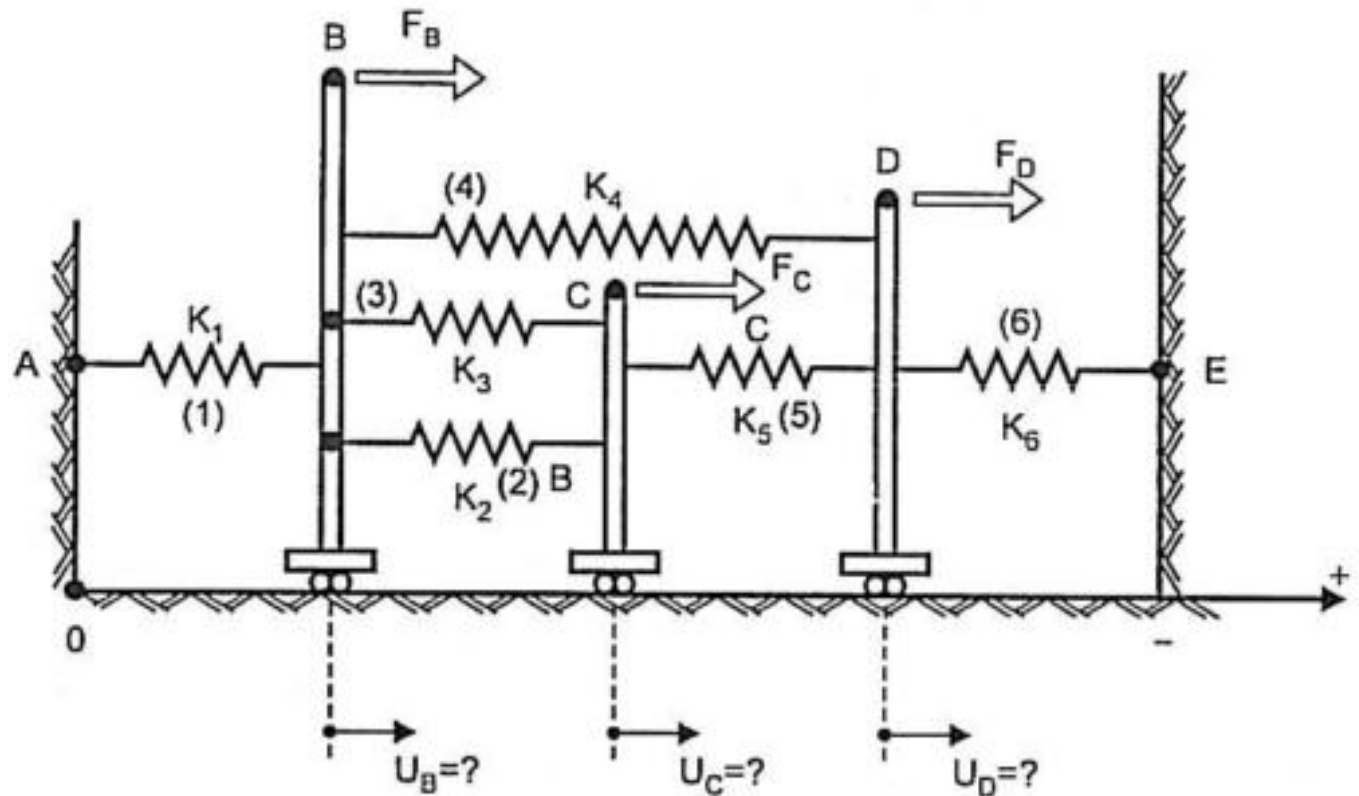
$$\begin{bmatrix} k_1 & -k_1 & 0 & 0 \\ -k_1 & k_1 + k_2 + k_3 & -k_2 & -k_3 \\ 0 & -k_2 & k_2 & 0 \\ 0 & -k_3 & 0 & k_3 \end{bmatrix} \begin{Bmatrix} 0 \\ u_2 \\ 0 \\ 0 \end{Bmatrix} = \begin{Bmatrix} F_1 \\ P \\ F_3 \\ F_4 \end{Bmatrix}$$

$$(k_1 + k_2 + k_3)u_2 = P$$

$$-k_1 u_2 = F_1; \quad -k_2 u_2 = F_3; \quad -k_3 u_2 = F_4$$



## Example 2



$$\begin{aligned} K_1 &= 200 \text{ Kgf/mm} \\ K_2 &= 100 \text{ Kgf/mm} \\ K_3 &= 150 \text{ Kgf/mm} \\ K_4 &= 300 \text{ Kgf/mm} \\ K_5 &= 400 \text{ Kgf/mm} \\ K_6 &= 500 \text{ Kgf/mm} \end{aligned}$$

$$F_B = 400 \text{ Kgf}$$

$$F_C = 300 \text{ Kgf}$$

$$F_D = 500 \text{ Kgf}$$

## Stiffness matrix of each (n) element

$$(1): [K]^1 = \begin{bmatrix} \boxed{A} & \boxed{B} \\ 200 & -200 \\ -200 & 200 \end{bmatrix} \begin{bmatrix} \boxed{A} \\ \boxed{B} \end{bmatrix}$$

$$(2): [K]^2 = \begin{bmatrix} \boxed{B} & \boxed{C} \\ 100 & -100 \\ -100 & 100 \end{bmatrix} \begin{bmatrix} \boxed{B} \\ \boxed{C} \end{bmatrix}$$

$$(3): [K]^3 = \begin{bmatrix} \boxed{B} & \boxed{C} \\ 150 & -150 \\ -150 & 150 \end{bmatrix} \begin{bmatrix} \boxed{B} \\ \boxed{C} \end{bmatrix}$$

$$(4): [K]^4 = \begin{bmatrix} \boxed{B} & \boxed{D} \\ 300 & -300 \\ -300 & 300 \end{bmatrix} \begin{bmatrix} \boxed{B} \\ \boxed{D} \end{bmatrix}$$

$$(5): [K]^5 = \begin{bmatrix} \boxed{C} & \boxed{D} \\ 400 & -400 \\ -400 & 400 \end{bmatrix} \begin{bmatrix} \boxed{C} \\ \boxed{D} \end{bmatrix}$$

$$(6): [K]^6 = \begin{bmatrix} \boxed{D} & \boxed{E} \\ 500 & -500 \\ -500 & 500 \end{bmatrix} \begin{bmatrix} \boxed{D} \\ \boxed{E} \end{bmatrix}$$

## Global stiffness matrix

$$[K] = \begin{array}{c|ccccc} & A & B & C & D & E \\ \hline A & 200 & -200 & 0 & 0 & 0 \\ B & -200 & 200+100+150+300 & -100-150 & -300 & 0 \\ C & 0 & -100-150 & 100+150+400 & -400 & 0 \\ D & 0 & -300 & -400 & 300+400+500 & -500 \\ E & 0 & 0 & 0 & -500 & 500 \end{array} \begin{array}{c} A \\ B \\ C \\ D \\ E \end{array}$$



$$\begin{Bmatrix} F_A \\ F_B \\ F_C \\ F_D \\ F_E \end{Bmatrix} = \begin{array}{c|ccccc} & A & B & C & D & E \\ \hline A & 200 & -200 & 0 & 0 & 0 \\ B & -200 & 750 & -250 & -300 & 0 \\ C & 0 & -250 & 650 & -400 & 0 \\ D & 0 & -300 & -400 & 1200 & -500 \\ E & 0 & 0 & 0 & -500 & 500 \end{array} \begin{array}{c} A \\ B \\ C \\ D \\ E \end{array} \begin{Bmatrix} U_A \\ U_B \\ U_C \\ U_D \\ U_E \end{Bmatrix}$$

$$F_A = 200 \cdot U_A - 200 \cdot U_B + 0 \cdot U_C + 0 \cdot U_D + 0 \cdot U_E$$

$$F_B = -200 \cdot U_A + 750 \cdot U_B - 250 \cdot U_C - 300 \cdot U_D + 0 \cdot U_E$$

$$F_C = 0 \cdot U_A - 250 \cdot U_B + 650 \cdot U_C - 400 \cdot U_D + 0 \cdot U_E$$

$$F_D = 0 \cdot U_A - 300 \cdot U_B - 400 \cdot U_C + 1200 \cdot U_D - 500 \cdot U_E$$

$$F_E = 0 \cdot U_A + 0 \cdot U_B + 0 \cdot U_C - 500 \cdot U_D + 500 \cdot U_E$$

$$\begin{Bmatrix} F_A \\ F_B \\ F_C \\ F_D \\ F_E \end{Bmatrix} = \begin{bmatrix} 200 & -200 & 0 & 0 & 0 \\ -200 & 750 & -250 & -300 & 0 \\ 0 & -250 & 650 & -400 & 0 \\ 0 & -300 & -400 & 1200 & -500 \\ 0 & 0 & 0 & -500 & 500 \end{bmatrix} \begin{Bmatrix} U_A \\ U_B \\ U_C \\ U_D \\ U_E \end{Bmatrix}$$

$$\begin{bmatrix} B \\ C \\ D \end{bmatrix}$$

$$\begin{Bmatrix} F_B \\ F_C \\ F_D \end{Bmatrix} = \underbrace{\begin{bmatrix} 750 & -250 & -300 \\ -250 & 650 & -400 \\ -300 & -400 & 1200 \end{bmatrix}}_{[K]_{\Delta}} \cdot \begin{Bmatrix} U_B \\ U_C \\ U_D \end{Bmatrix} \begin{bmatrix} B \\ C \\ D \end{bmatrix}$$

$$\det [K]_{\Delta} = [750 \times 650 \times 1200 + (-250) \cdot (-400) \cdot (-300) + (-250) (-400) (-300)] -$$

$$- [(-300) \cdot (650) (-300) + (750) \cdot (-400) \cdot (-400) + (-250) \cdot (-250) \cdot (1200)]$$

$$\boxed{\det [K]_{\Delta} = 271.500.000}$$



$$(\text{cof } K_{BB}) = (-1)^{1+1} \cdot \begin{vmatrix} 650 & -400 \\ -400 & 1200 \end{vmatrix} = 650 \times 1200 - 400 \times 400 = 620000$$

$$(\text{cof } K_{BC}) = (-1)^{1+2} \cdot \begin{vmatrix} -250 & -400 \\ -300 & 1200 \end{vmatrix} = (-1) [-250 \times 1200 - 300 \times 400] = 420.000$$

$$(\text{cof } K_{BD}) = (-1)^{1+3} \cdot \begin{vmatrix} -250 & 650 \\ -300 & -400 \end{vmatrix} = [400 \times 250 - (-300) \times (650)] = 295.000$$

$$(\text{cof } K_{CB}) = (-1)^{2+1} \cdot \begin{vmatrix} -250 & -300 \\ -400 & 1200 \end{vmatrix} = (-1) [(-250) \times 1200 - 400 \times 300] = 420.000$$

$$(\text{cof } K_{CC}) = (-1)^{2+2} \cdot \begin{vmatrix} 750 & -300 \\ -300 & 1200 \end{vmatrix} = [750 \times 1200 - 300 \times 300] = 810.000$$

$$(\text{cof } K_{CD}) = (-1)^{2+3} \cdot \begin{vmatrix} 750 & -250 \\ -300 & -400 \end{vmatrix} = (-1) \cdot [750 \times (-400) - 300 \times 250] = 375.000$$

$$(\text{cof } K_{DB}) = (-1)^{3+1} \cdot \begin{vmatrix} -250 & -300 \\ 650 & -400 \end{vmatrix} = [400 \times 250 - (650) \times (-300)] = 295000$$

$$(\text{cof } K_{DC}) = (-1)^{3+2} \cdot \begin{vmatrix} 750 & -300 \\ -250 & -400 \end{vmatrix} = (-1) [750 \times (-400) - 250 \times 300] = 375.000$$

$$(\text{cof } K_{DD}) = (-1)^{3+3} \cdot \begin{vmatrix} 750 & -250 \\ -250 & 650 \end{vmatrix} = [750 \times 650 - 250 \times 250] = 425000$$



$$[K]_{\Delta}^{-1} = \frac{1}{271.500.000} \begin{bmatrix} 620000 & 420000 & 295000 \\ 420000 & 810000 & 375000 \\ 295000 & 375000 & 425000 \end{bmatrix} = \begin{bmatrix} 0,0022836 & 0,0015470 & 0,0010866 \\ 0,0015470 & 0,0029834 & 0,0013812 \\ 0,0010866 & 0,0013812 & 0,0015653 \end{bmatrix}$$

$$F_B = +400 \text{ kgf} \quad ; \quad F_C = +300 \text{ kgf} \quad ; \quad F_D = +500 \text{ kgf}$$

$$\{U\} = \begin{Bmatrix} U_B \\ U_C \\ U_D \end{Bmatrix} = \begin{bmatrix} 0,0022836 & 0,0015470 & 0,0010866 \\ 0,0015470 & 0,0029834 & 0,0013812 \\ 0,0010866 & 0,0013812 & 0,0015653 \end{bmatrix} \cdot \begin{Bmatrix} 400 \\ 300 \\ 500 \end{Bmatrix}$$

$$U_B = 0,0022836 \times 400 + 0,0015470 \times 300 + 0,0010866 \times 500 \quad \Rightarrow \quad \boxed{U_B = 1,92084 \text{ mm}}$$

$$U_C = 0,0015470 \times 400 + 0,0029834 \times 300 + 0,0013812 \times 500 \quad \Rightarrow \quad \boxed{U_C = 2,20442 \text{ mm}}$$

$$U_D = 0,0010866 \times 400 + 0,0013812 \times 300 + 0,0015653 \times 500 \quad \Rightarrow \quad \boxed{U_D = 1,63165 \text{ mm}}$$