

Nonlinear Dyn. for Nonl. Conf.

1

Lecture IV - Nonlinear Waves I

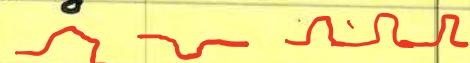
Next goal {
avalanches

turbulence spreading

Add-Prey
LCOs
Transitions
→ Flots
→ Fisher
→ FN

→ What's an avalanche?

pulse train



~ a pulse of a thermodynamic variable T, ρ, \dots , etc., or/and cts flux, which traverses a distance L at a speed c s/t

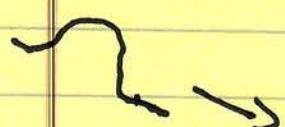
$$\frac{c}{L} > \langle D \rangle / L^2$$



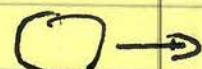
$$\langle D \rangle \sim D_{GR}$$

avg.

Can be a pulse train:



→ Pulse can be fluctuation intensity
→ spreading



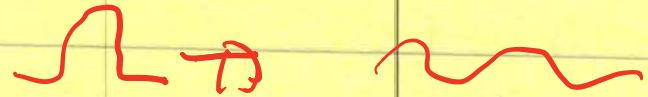
"Spreading" in MFE

=

"Entrainment" in fluids

Structure
of
Turbulent
Shear Flow
A.A. Townsend

→ Why Nonlinear waves \leftrightarrow avalanches?



"The basic idea of wave propagation is that some degenerate feature of the disturbance moves with a finite velocity."

Landau & Lifshitz
Whitham

- G. B. Whitham

"Linear and Nonlinear Waves"

highly recommended!

Cf: Front!



[Nonlinear waves are underpinning for concepts re: avalanches and spreading. → Fundamental!]

β waves - avalanches

So:



= basis: gas dynamics ("simple waves") and plasma solitons
→ collisionless shocks

→ shock, pulse formation

- ⇒ jump conditions
- ⇒ steepening vs. dispersion →
T.n Acoustic shock

Critical Point:

⇒ Entropy production

then:

- (I) - kinematic waves, traffic flow,
Flood waves, buses.
- 
- (II) - Avalanche physics: Micro - Macro.
- (IV) - Turbulence spreading and entrainment physics.

Gas Dynamic Shocks / "Simple Waves"

3

1-D Gas Dynamics

CF { Landau/Lifshitz
Fluids
Whitham &
cont.

Simple Waves

→ steepening
shocks etc.

(continuity)

ideal
1D

$$-\partial_t \rho + \partial_x (\rho v) = 0$$

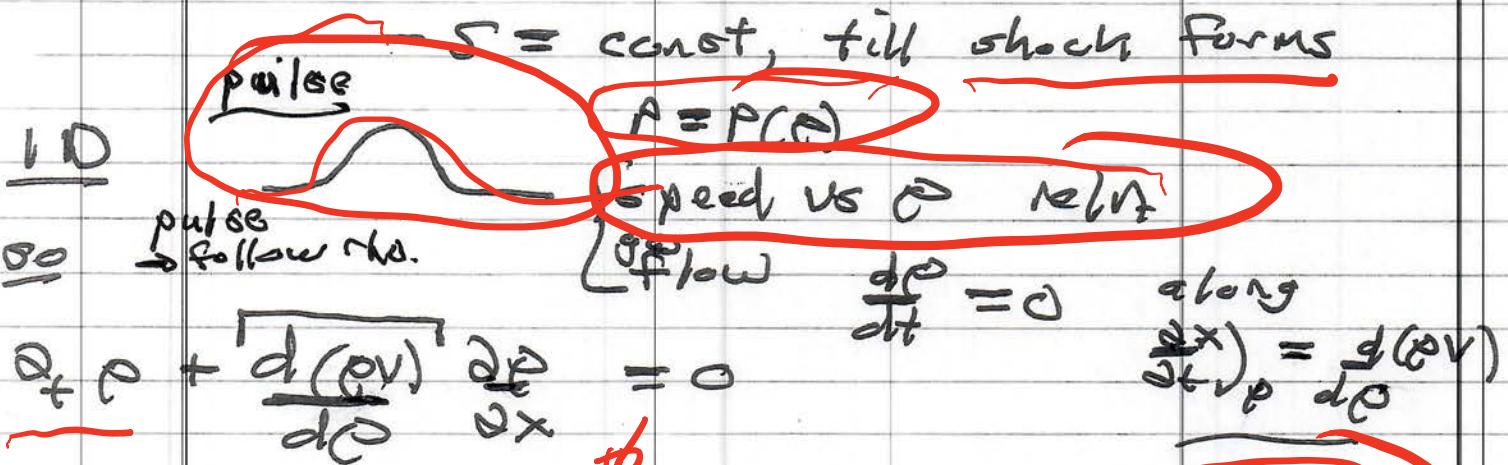
$$-\partial_t v + v \partial_x v + \frac{1}{\rho} \partial_x p = 0$$

mass.

(momentum
balance)

$$p = p(\rho)$$

Entropy: - δ' initially homogeneous



$$\rho_t v + \left(v + \frac{1}{\rho} \frac{dp}{dv} \right) \frac{\partial v}{\partial x} = 0$$

$$p = p(v)$$
 $v = v(p)$

$$\left(\frac{\partial v}{\partial t} \right)_p = v + \rho \frac{dv}{dp}$$

$$\left(\frac{\partial x}{\partial t} \right)_p = \frac{d}{dp} (\rho v) = v + \rho \frac{dv}{dp}$$

1. b get on

$$\frac{dp}{dt} = 0$$

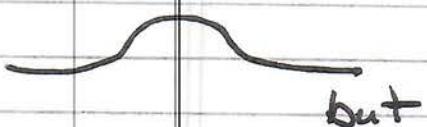
$$\frac{dv}{dt} = 0$$

conservative
for

characteristic
eqn. →
all info

likewise:

$$\left(\frac{\partial x}{\partial t} \right)_V = v + \frac{1}{\rho} \frac{dP}{dV}$$



but

$$v = v(P)$$

$$P = P(P)$$

v_{ig}

$$\left[\left(\frac{\partial x}{\partial t} \right)_P = \left(\frac{\partial x}{\partial t} \right)_{V_0} \right]$$

'pulse'

$$\rho \frac{dv}{dp} + v = v + \frac{1}{c^0} \frac{dP}{dV}$$

$$dp = c_s^2 dp$$

$$\rho \frac{dv}{dp} = \frac{c_s^2}{\rho} \frac{dp}{dV}$$

so

$$(dv/dp)^2 = c_s^2 / \rho^2$$

$$v = \pm \int \frac{c_s}{\rho} dp = \pm \int \frac{dp}{\rho c_s}$$

Velocity

solves for flow speed
in terms density

Note:

$$V = \pm \int \frac{C_s}{\rho} dP$$

$$\rho \rho^{-\gamma} = \text{const.} \quad \gamma = 5/3$$

$$dP = C_s^2 d\rho = \alpha \gamma \rho^{\gamma-1} d\rho$$

$$C_s^2 = \alpha \gamma \rho^{\gamma-1} \text{ const.}$$

$$\alpha = \text{const.}$$

$$V = \pm \int \frac{C_s^2}{\rho C_s} d\rho = \pm \alpha \gamma \int \frac{\rho^{1/3}}{\rho} d\rho$$

$$V = \pm 3 \sqrt[3]{\alpha \gamma} \rho^{1/3}$$

- flow speed
circular width
density



→ over-taking

- high density
elements go faster

- then:

$$\left(\frac{\partial x}{\partial t} \right) = V + \frac{1}{\rho} \frac{dP}{dV}$$

$$V = \pm \int \frac{dP}{\rho C_s}$$

$$dV = \frac{dP}{\rho C_s}$$

$$\underline{\underline{\sigma}} \frac{dP}{dv} = \rho c_s$$

$$\rho = \rho(v)$$

$$\frac{\partial x}{\partial t + v} = v = \underline{\underline{c}_s(v)}$$

all cons - 1D-cont, E-N ✓

$$x = t [v \pm c_s(v)] + f(v)$$

"Simple waves" solution

σ cons
nonlinear.

Check: linearized limit

Non linear wave
→ no char.
char. scale

$$x = t [\gamma \pm c_s(c_0)] + f(v) + x_0$$

$$x = x_0 \pm c_s(c_0)t$$

→ Why "Simple"?

No characteristic scale

⇒ alternate approach.

if no characteristic scale
all quantities depend only on

$$\xi = x/t$$

Similarity soln.

$f(x,t)$

$$\underline{v} = f(\Sigma)$$

$$\Sigma = \frac{x}{t}$$

$$F(x/t^2)$$

\hookrightarrow Velocity formed by x/t in absence of shock

$\underline{\underline{\underline{}}}$

$$\partial_x v = \frac{1}{t} \partial_\Sigma v$$

$$\partial_t v = -\frac{\Sigma}{t} \frac{\partial}{\partial \Sigma} v$$

$$\Sigma = \frac{x}{t}$$

$$\Rightarrow \partial_t p + p \partial_x v + v \partial_x p = 0$$

$$\partial_t v + v \partial_x v = -1/p \partial_x p$$

become:

$$-\frac{\Sigma}{t} \rho' + \frac{p}{t} \dot{v} + \frac{v}{t} \rho' = 0$$

$$1 = \partial/\partial \Sigma$$

$$-\frac{\Sigma}{t} \dot{v} + \frac{v}{t} \dot{v} = -\frac{c_s^2}{t} \frac{\partial}{\partial \rho'} \rho'$$

$\underline{\underline{\underline{}}}$

$$(v - \Sigma) \rho' + p \dot{v} = 0$$

$$(v - \Sigma) \dot{v} = -c_s^2 \frac{\partial}{\partial \rho'} \rho'$$

like linear dispersion theory, treat Σ as eigenvalue.

$$(v - \Sigma) \rho' + p \dot{v} = 0$$

$$\frac{dp}{dt}$$

$$-c_s^2 \frac{\partial}{\partial \rho'} \rho' + (v - \Sigma) \dot{v} = 0$$

$$\frac{d\rho'}{dt}$$

$$(V - \varepsilon)^2 = c_s^2$$

2

$$\Sigma = V \pm c_s$$

$$\frac{x}{t} = V \pm c_s$$

$$x = (V \pm c_s) t$$

From "eigenvector", rotate V, ρ etc.

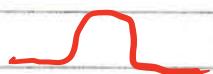
$$V - \varepsilon = -c_s$$

$$(V - \varepsilon)\rho' + \rho'V = 0$$

$$-c_s\rho' + \rho'V$$

$$\rho dv = c_s d\phi$$

$$dv/d\phi = c_s/\rho$$



$$x = \text{c.c.} + t(V \pm c_s)$$

Simple
 $\omega < \omega_c$

✓ $V = \int c_s d\phi / \rho = \int \underline{dP} / c_s \rho$

- equivalent to previous, with
 $f(V) = 0$.

- corresponds to Kundsen's version
of "simple wave".

- Can also write:

$$v = \int + (-dp/dV)^{1/2}$$

$$d(1/p) = d\bar{V} = -\frac{1}{\rho^2} d\rho \quad , \quad dp = c_s^2 d\rho$$

$$\left(v = \int \left(\frac{1}{\rho^2} d\rho c_s^2 d\rho \right)^{1/2} \right.$$

$$= \int \frac{d\rho}{\rho} c_s \quad \left. \right)$$

→ Physics of Simple Wave :

no sub

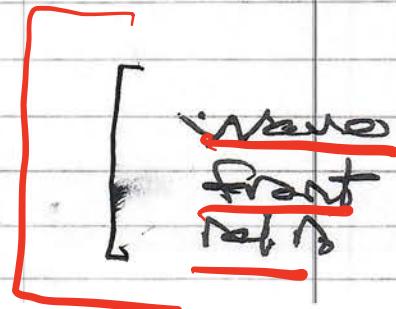
in

shock

- have established simple wave *in gas dynamics* with key element of scales in variation
- now elucidate simple wave physics
⇒ shocks

Similarity flow $f(v) = 0$ → simple wave with

$$x = t [v \pm c_s(v)]$$



Can write general solution for adiabatic process:

$$P\delta^{-\gamma} = \text{const}$$

$$\checkmark T \delta^{-(\gamma-1)} = \text{const}$$

$$T = C_s^2 = \delta^{\gamma-1}$$

$$\frac{dP}{d\delta} = C_s^2 = T$$

$$\underline{P = \rho T}$$

$$\rho^{-1} T^{1/\gamma-1} = \text{const}$$

$$\text{as } C_s^2 \sim T$$

$$\gamma-1 = 2/3$$

$$\rightarrow \rho = \rho_0 \left(\frac{c}{c_0} \right)^{2/(\gamma-1)}$$

(eliminates
→ clarity
notations)

$$\text{but } V = \pm \int c \frac{dP}{P}$$

$$c = c_f$$

$$\boxed{V = \pm \frac{2}{\gamma-1} (c - c_0)}$$

so finally can write:

$$f(v)$$

$$C = C_0 \pm \frac{1}{2} (\gamma - 1) v$$

$$\rho = \rho_0 \left(1 \pm \frac{(\gamma - 1)}{2} \frac{v}{C_0} \right)^{\frac{2}{\gamma - 1}}$$

$$\rho = \rho_0 \left(1 \pm \frac{1}{2} (\gamma - 1) \frac{v}{C_0} \right)^{\frac{2\gamma}{\gamma - 1}}$$

so then:

$$x = t \left[v \pm C_s(v) \right] + f(v)$$

$$\rightarrow x = t \left[v \pm (C_0 \pm \frac{1}{2} (\gamma - 1) v) \right] + f(v)$$

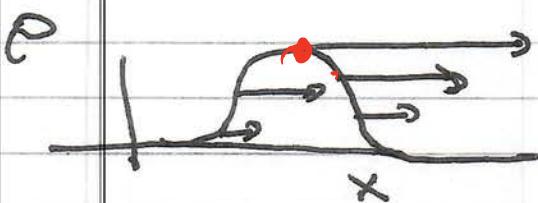
Now:

point on wave profile moves at

$$u = \frac{dx}{dt} = v \pm C_s$$

$\frac{dv}{d\rho} > 0$

and $\frac{dv}{d\rho} > 0$



\rightarrow [speed increases with density!]

12

50

sym

+



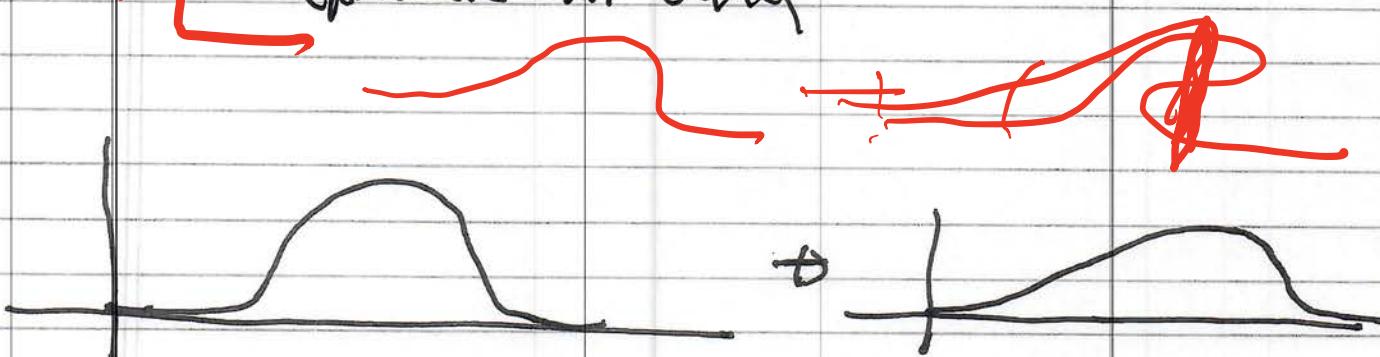
if $d\phi/dx > c$ anywhere in i.v.d.

\Rightarrow overtaking and shock formation

discontinuity forms

disipation no longer negligible
(prevents diff value)

i.e.



clipping resolv.



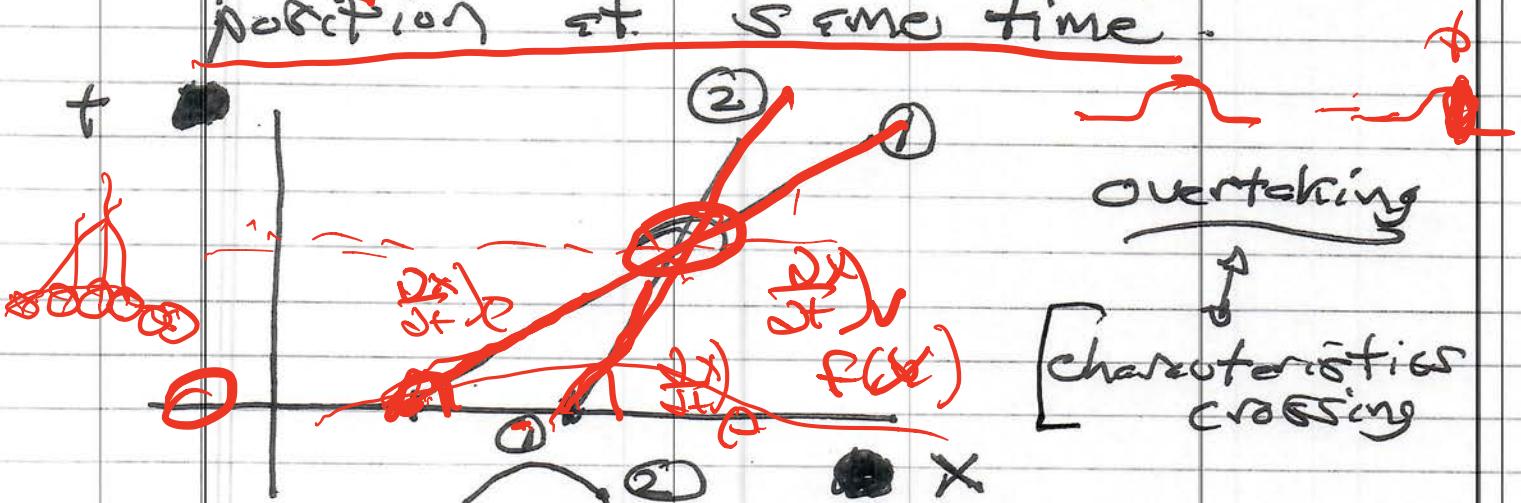
When does breaking / shock
formation occur?

$$V + Cs \leftarrow \frac{\partial x}{\partial t} \Big|_P \rightarrow \text{characteristic eqns}$$

$$\frac{d\theta}{dt} = 0 \rightarrow \frac{d}{dt} P \frac{\partial \theta}{\partial t} \frac{\partial t}{\partial x} = 0$$

Full nonlinear characteristic eqns.

\rightarrow Breaking occurs when 2 critical points arrive at same position at same time.



$$X = t \left[C_0 + \frac{1}{2} (\gamma+1) V \right] + f(V)$$

$$X = + \left[C_0 + \frac{1}{2} (\gamma+1) [V + \delta V] \right] + f(V + \delta V)$$

intervall:

~~$$C_0 t + \frac{1}{2} (\gamma+1) V t + f(V)$$~~

$$= C_0 t + \frac{1}{2} (\gamma+1) t V + \cancel{\delta V} \frac{1}{2} (\gamma+1) t + f(V) + \cancel{\delta V} f'(V)$$

$$(1) = \cancel{\delta V} \left[\frac{1}{2} (\gamma+1) t + \frac{1}{5} \text{shock} + f(V) \right]$$

time for shock formation

145

$$\text{Difference} \rightarrow 0 \quad \underline{\underline{=}}$$

$$x = t(v_{IC}) + f(v)$$

$$\boxed{t_{\text{shock}} = -\frac{2P(v)}{(\gamma+1)}} \quad \rightarrow \quad \begin{array}{l} \text{time to} \\ \text{form} \\ \text{shock} \end{array}$$

- need $f'(v) < 0$ for
over taking

all set by I.C.

- Generally:

need:

$$\left(\frac{\partial x}{\partial v} \right)_+ = 0$$

$$\left(\frac{\partial^2 x}{\partial v^2} \right)_+ = 0 \quad \text{inflection}$$

H.W. \rightarrow work eff

time. \rightarrow shock

get Δx_+ . $\cancel{\Delta x_+}$ high
order

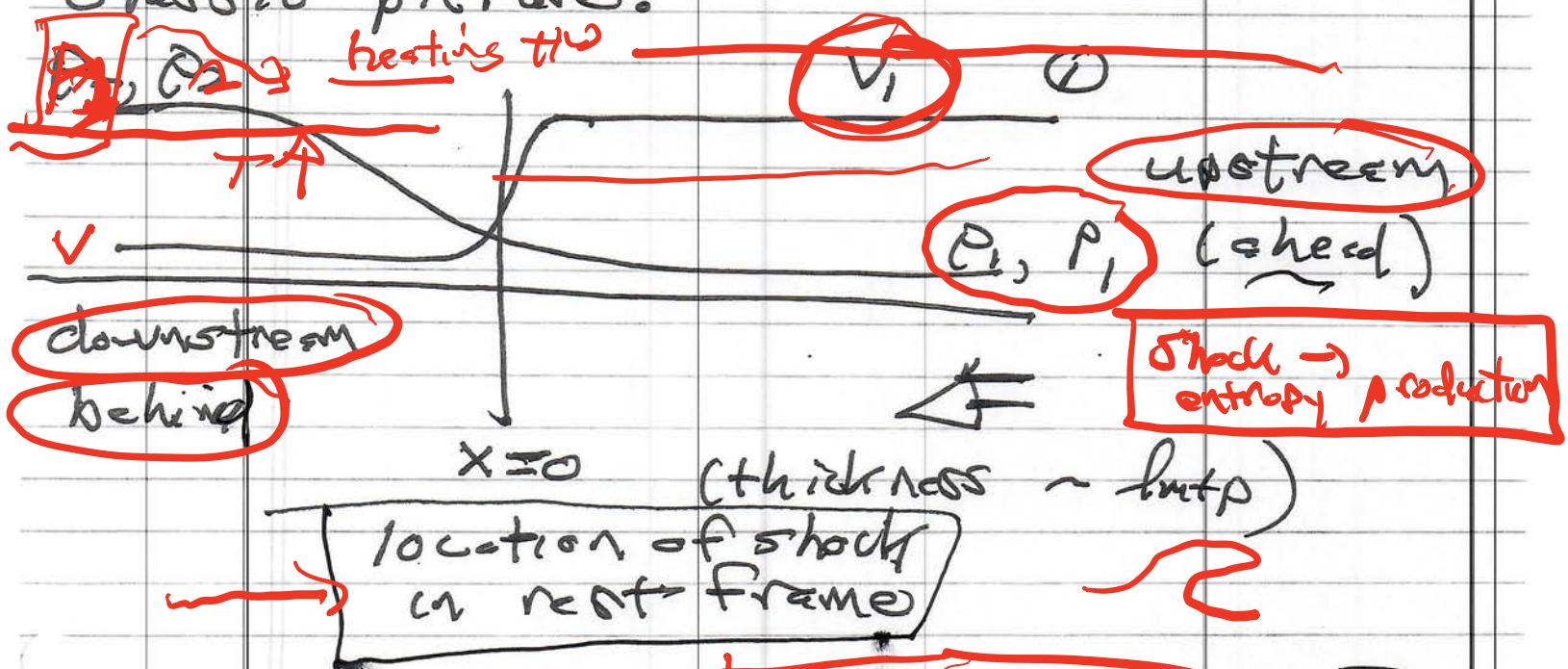
x_{shock}

$$\left(\frac{\partial x}{\partial v} \right)_+ = \frac{1}{2} (\gamma+1) + f' = 0 \quad \checkmark$$

\sim formation.

- **Shocks** - Flows with Discontinuity
- once wave steepen and breaks rapidly up
 - ⇒ discontinuity appears
 - "shock" - localized region of rapid change / discontinuity
 - dissipation (thickness) essentially in shock
 ~ hmp flow \rightarrow shock

Classical picture:



→ Shock converts kinetic energy into thermal energy, compression

(engine) → motion
→ gen elec & heat

~~1.1~~ Entropy Production \rightarrow Insert.

1

Supplement: Gas Dynamic Shocks
Lecture [REDACTED]

a.) Scale

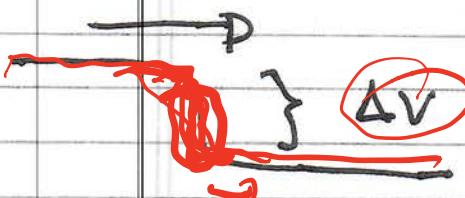
$$P = 0$$

$HV \rightarrow$ Solve
(gen)
for

Burgers
(Waves)

Consider Burgers Eqn.:

$$\partial_t V + V \partial_x V - r \partial_x^2 V = 0$$



$$\frac{V}{W} \sim \frac{\Delta V}{\omega^2}$$
$$\omega \sim \frac{\Delta V}{\Delta V}$$

for shock width

$$\frac{\Delta V}{W} \sim r \frac{\Delta V}{W^2}$$

$$W \sim \frac{\Delta V}{\Delta V}$$

discontinuity
sets shock
thickness

for $r \sim \text{lmp } C_s$

$$\Delta V \sim C_s$$

$$W \sim \text{lmp}$$

{ characteristic
thickness of
shock layer.

5.) Entropy Production

In gas-dynamics

- initially ideal dynamics
- entropy constant

but



pulse steepen and shocks

- sharp gradients produced on shock

\Rightarrow couple to diffusive dissipation

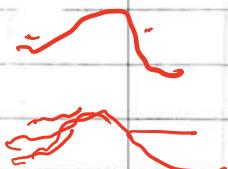
\Rightarrow drive collisional transport

\Rightarrow produce entropy

N.B.: - Entropy production required
in shock

- Sets arrow of time.

- A.I. expansion unstable.



Flex-force

- to calculate:

$$\frac{dS}{dt} = \left(\right) \underbrace{- \Gamma_x}_{k_B} \underbrace{\nabla X}_{\rightarrow \text{thermodynamic force}} \rightarrow$$

$\nabla X \rightarrow$ thermodynamic force

$$\Gamma_x \rightarrow f/\mu x \quad \text{fixes low}$$

i.e. $\Gamma_x = - D_x \nabla X$

$$\frac{dS}{dt} \sim \left(\right) D_x (\nabla X)^2$$

$\overset{\circ}{\text{entropy production rate density}}$

then, for Burgers shock:

$$\left. \begin{aligned} \frac{dS}{dt} &\sim r (\partial_x v)^2 \\ &\sim r \frac{(\Delta v)^2}{w^2} \sim r \frac{(\Delta v)^2}{v^2} \frac{(\Delta v)^2}{v^2} \end{aligned} \right\} \frac{1}{w} \sim \frac{\Delta v}{v}$$

$$\frac{dS}{dt} \sim \frac{(\Delta v)^4}{w^2} \quad \begin{aligned} &\text{action} \\ &\text{force} \end{aligned} \quad D_x (\nabla X)^2 d(\text{shock})$$

but, total entropy production ~~is zero~~

is integrated over shock thickness

$$\int dx \frac{dS}{dt} \sim \frac{dS'}{dt} \sim \frac{W ds}{dt}$$

$$\frac{1}{\rho} w \sim \left(\frac{\Delta v}{\Delta u}\right)^{-1}$$
$$w \sim \left(\frac{\Delta u}{\Delta v}\right)^{-1}$$
$$w \sim \frac{1}{\Delta v}$$

$$\sim \frac{1}{\Delta v} \frac{(\Delta v)^2}{\Delta v^2} (\Delta v)^2$$

$$\frac{dS_{tot}}{dt} \sim (\Delta v)^3$$

total entropy prod
rate const.
of γ

so total entropy production:

$$dS/dt \sim (\Delta v)^3$$

entropy production
independent
of γ though
 γ required
for heating.

- independent $\sqrt{!}$

- entropy / heating produced by
collisions but total dS/dt

independent of γ .

shocks \leftrightarrow Turbulence \rightarrow coriolis to
finite time scale t_{shock} \sim \sqrt{L}

$$f(t) \rightarrow \frac{\partial x}{\partial t} = \underset{a.c.}{x} = f(t) + f(0)$$

15.

Conservation relations \Rightarrow jump conditions

$$\partial_t \rho + \nabla \cdot (\rho \underline{v}) = 0 \quad \text{continuity}$$

$$\partial_t \left(\frac{1}{2} \rho \underline{v}^2 + \rho \epsilon \right) + \nabla \cdot \left(\rho \underline{v} \left(\frac{\underline{v}^2}{2} + \frac{\gamma p}{(\gamma-1)\rho} \right) \right)$$



energy

$$\frac{\gamma p}{\gamma-1} = \frac{\rho}{\gamma-1} + P \quad \begin{matrix} \hookrightarrow \\ \text{PV work on} \\ \text{surroundings} \end{matrix}$$

of
energy density

$$\frac{\partial \rho v_i}{\partial t} = - \frac{\partial}{\partial x_k} \Pi_{ik} \quad \begin{matrix} \hookrightarrow \\ \text{stress tensor} \end{matrix}$$

$$\Pi_{ik} = P \delta_{ik} + \rho v_i v_k$$

\Rightarrow tangential components \vee continuous

- so integrating,

work in shock frame $U = 0$

$$\partial_t \rho = -U \partial_x \rho$$

$$-\int \partial_x \rho = (\rho_2 - \rho_1) U$$

but $U = 0$, frame

~~mass~~

~~flux~~

$$\boxed{\rho v_x \Big|_2 = \rho v_{x0} \Big|_1} \quad \textcircled{1}$$

continuity
mass flux

energy

$$v_n \equiv v_{\perp} \text{ plane}$$

$$\rho v_n \left(\frac{1}{2} v^2 + \frac{\gamma P/\rho}{\gamma - 1} \right) \Big|_2 = \rho v_n \left(\frac{v^2}{2} + \frac{\gamma P/\rho}{\gamma - 1} \right) \Big|_1$$

but

$$\rho v \Big|_2 = \rho v \Big|_1 \quad \textcircled{1}$$

and continuity parallel \Rightarrow

$$\frac{V_y^2}{2} \textcircled{2} = \frac{V_y^2}{2} \textcircled{1}$$

Oz

$$\left[\left(\frac{V_x^2}{2} + \frac{\gamma P/\rho}{\gamma - 1} \right) \textcircled{2} = \left(\frac{V_x^2}{2} + \frac{\gamma P/\rho}{\gamma - 1} \right) \textcircled{1} \right]$$



and momentum conservation:

$$\left[(\rho V_x^2 + P) \right] \textcircled{2} = \left[(\rho V_x^2 + P) \right] \textcircled{1}$$

normal component, only, varied.

have 3 Rankine-Hugoniot jumps/continuity conditions

$$[\Gamma] = C_{\textcircled{2}} - C_{\textcircled{1}}$$

$$\boxed{[\rho v_x] = 0}$$

$$\boxed{\left[\frac{v_x^2}{2} + \frac{\gamma p/\rho}{\gamma - 1} \right] = 0}$$

$$\boxed{[\rho v_x^2 + p] = 0}$$

in shock frame
 relate upstream/
 downstream
 quantities

in fixed coordinate frame:

$$v_x = v_{in} - U$$

\downarrow

normal v
in fixed coords

\rightarrow shock velocity

then on to:

- shock adiabat. \rightarrow entropy production
- $v_2/v_1, \rho_2/\rho_1, P_2/P_1$
 - \uparrow compression
 - \uparrow compression
 - heat transfer

Shock - illustration - schematic
 & use.

The flow is ~~scale invariant~~

Small \rightarrow non-dispersive \rightarrow no shock is problem 1.

Nonlinear Waves II

gas dyn shock

- initial study: gas-dynamic 'simple waves'
 { scale free
 { non-dispersive

- now: dispersive
 scale
 solitons \rightarrow ion acoustic
 (simpler, not first)

Point: $\omega^2 = c_s^2 k^2 / (1 + k^2 \lambda_D^2)$

$$\left(\frac{\omega}{k}\right)^2 = c_s^2 / (1 + k^2 \lambda_D^2)$$

dispersion

$\lambda_D \rightarrow 0$: gas dynamic limit
 { non-dispersive

\Rightarrow all harmonics have same phase
velocity

$$\left(\frac{\omega}{k}\right)^2 = c_s^2$$

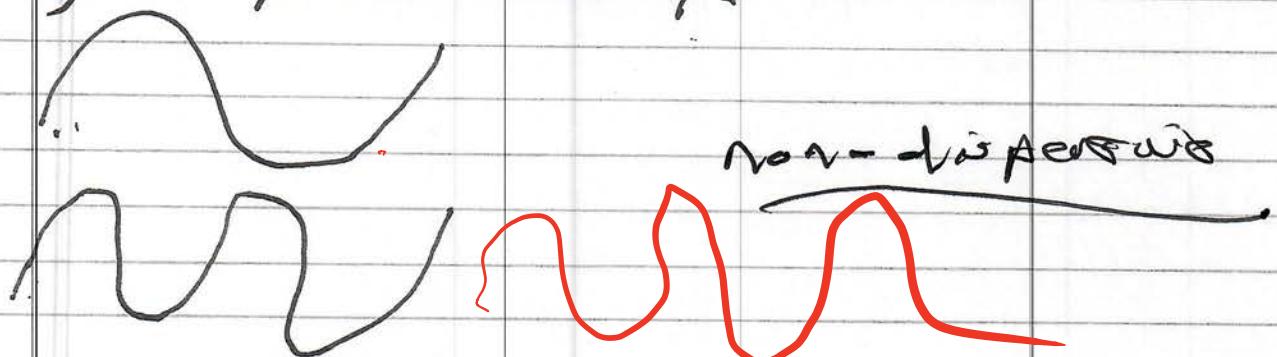
on dispersion

self-test:

$$\left(\frac{\omega}{k}\right)^2 = c_s^2$$

etc.

As wave steepens by non-linear interaction, all harmonics move at Cg. at phase velocity.



but with dispersion:

$$(\omega/k)^2 = C_s^2 / (1 + k^2 \lambda_D^2)$$

$$\left(\frac{\omega}{k}\right)^2 = C_s^2 / (1 + (k^2 \lambda_D^2))$$

$$\frac{\omega^2}{k^2} = C_s^2 / (1 + 2n(k^2 \lambda_D^2))$$

then fundamental and self-beats disperse \rightarrow spread in speeds.

\therefore 2 routes to balance of steepened fronts:

N.b. steepening vs. dissipation $\propto V$

$V \propto$ dissipative structure

\rightarrow Shock (conventional)

A.I. steepening vs. dispersion

→ soliton (1D)

i.e. Schematic:

→ "is called

"collisionless shock"

recall 1D compressible hydro - Burgers Eqn.

$$\partial_t V + V \partial_x V = \nu \partial_x^2 V$$



$$\frac{\Delta V}{\Delta x} \sim \nu \frac{\Delta V}{(\Delta x)^2}$$

$$\boxed{\Delta x \sim \nu / \Delta V} \rightarrow \text{shock layer thickness}$$

↓
dispersion acts

→ ν vs collisions.

Now, can generalize:

$$\omega^2 \equiv k^2 C_s^2 / (1 + k^2 \lambda_D^2)$$

$$\omega \approx k C_s \left(1 - \frac{k^2 \lambda_D^2}{2} \right)$$

~~Σ~~

$$\boxed{\frac{\partial \Sigma}{\partial t} + C_s \partial_x \Sigma + \Sigma \partial_x \Sigma = \nu \partial_x^2 \Sigma + \frac{C_s \lambda_D^2}{2} \partial_x^3 \Sigma}$$

~~done~~

distortion

dispersive

steepness
vs dispersion

4:

$$\underline{c_s} \quad \underline{\lambda_D} \rightarrow \infty$$

Burgers

$$v \rightarrow 0$$

$$\frac{kdV}{dt}$$

Korteweg - de Vries

kdV

$$\frac{\partial}{\partial t} \Sigma + c_s \frac{\partial}{\partial x} \Sigma + \sum \frac{\partial}{\partial x} \Sigma = \frac{c_s \lambda_D^2}{2} \frac{\partial^3}{\partial x^3} \Sigma$$

stuff

$$\frac{\Sigma}{\Delta} \Sigma \sim c_s \frac{\lambda_D^2}{2} \frac{\Sigma}{\Delta^3}$$

dispersion
controls steepening

$$\Delta \sim \frac{c_s \lambda_D^2}{2 \Sigma}$$

$$\Delta \sim \left(\frac{c_s}{2 \Sigma} \right)^{1/2} \lambda_D$$

Collisions

shock

steepness vs dispersion

scale.

n.b. Where does kdV come from in hydro?

- surface wave: $\omega^2 = g k$

- surface wave with finite depth:

$$\omega^2 = g k \tanh(kd)$$

Td

then expanding:

$$\omega^2 = k^2 g d + g k^3 \left(-\frac{k^2 d^2}{3} \right)$$

shallow H_2O

$$\omega^2 = \kappa \frac{g d}{3}$$

5.

$$\omega^2 = k^2 g d \left(1 - \frac{k^2 d^2}{3} \right)$$

$$\omega^2 = \frac{k^2 c_s^2}{1 + k^2 d^2} \rightarrow k^2 c_s^2 \left(1 - \frac{k^2 d^2}{2} \right)$$

6.

$$\partial_t \Sigma + \mathbf{v}_0 \partial_x \Sigma + \Sigma \partial_x \Sigma = - v_0 d \frac{\partial^3 \Sigma}{\partial x^3}$$

$$v_0 = (gd)^{1/2}$$

(bal V)

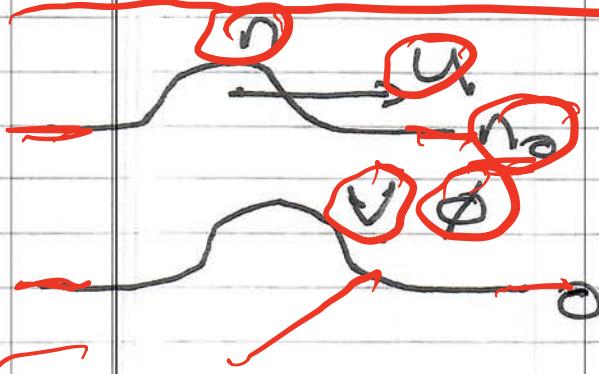
check for
solitons

Now, for ion-acoustics:

$\rightarrow N_L$ ion-acoustic
soliton

$$N_e = N_0 \exp \left[e \phi / T_e \right]$$

Balanced
electrons



$$\partial_t n_i + \partial_x (n_i v_i) = 0$$

$$\partial_t v_i + v_i \partial_x V_i = - \frac{e \phi}{m_i} \frac{\partial \phi}{\partial x}$$

fluid
cons.

form

$$\left\{ \begin{array}{l} N_i \\ V_i \\ \phi \end{array} \right\} = \boxed{F(x - ut)} \quad \xrightarrow{\text{speed}} \boxed{\text{standard form of NL pulse.}}$$

$$-uN_i' + (N_iV)' = 0$$

$$(V-u)V' = -\frac{q}{m_i}\phi'$$

integrate; $\left. \begin{array}{l} \phi \rightarrow 0 \\ V \rightarrow 0 \\ N \rightarrow N_0 = 1 \end{array} \right\}$ $|x| \rightarrow \infty$

$$-uN_i + N_0V = -u \quad (\text{b.c.})$$

$$(u - v)N_i = u$$

$$N_i = u / (u - v)$$

take wise:

$$-\frac{q\phi}{m_i} = \frac{v^2}{2} - \frac{2evV}{2} + \frac{u^2}{2} - \frac{u^2}{2}$$

$$\frac{q\phi}{m_i} = -\frac{1}{2}(u-v)^2 + \frac{u^2}{2}$$

b.c. v.

$$\underline{\underline{U}} = \underline{\underline{U}} - \frac{2\phi}{M_0 c} = \left(U^2 - \frac{2\phi}{M_0 c} \right)^{1/2}$$

#

$$\partial_x^2 \phi = -4\pi n_e \Sigma (n_i - n_e)$$

$$\partial_x^2 \left(\frac{2\phi}{T} \right) = -\frac{1}{\lambda_D^2} \left(\frac{1}{(1 - 2\phi/T)(c_s^2/U^2)^{1/2}} - \exp\left(\frac{2\phi}{T}\right) \right)$$

$$\frac{2\phi}{T} \rightarrow \phi$$

EQU

$$\boxed{\partial_x^2 \phi = -\frac{1}{\lambda_D^2} \left(\frac{1}{(1 - 2\phi/c_s^2)^{1/2}} - e^\phi \right)}$$

$$\underline{\underline{m}} = \underline{\underline{U}} / c_s^2$$

NL wave
e.m.

Mech #

Motion in Potential
(Sagdeev)

$$\begin{aligned} \phi' \partial_x^2 \phi &= -\frac{1}{\lambda_D^2} \frac{\phi'}{(1 - \frac{2\phi}{c_s^2})^{1/2}} - e^\phi \phi' \\ &= -(\partial V/\partial \phi) \phi' \end{aligned}$$

and integrate:

Sagdeev potential

$$V(\phi) = -\frac{1}{2} \frac{\eta^2}{\lambda_D^2} \left\{ \frac{\eta^2}{2} \left(1 - \frac{2\phi}{\eta^2} \right)^{1/2} - e^\phi \right\} + C$$

↓

$$\frac{\phi''}{2} + V(\phi) = 0$$

integration const.
→ sets possibility

$$\phi'' = dV/d\phi$$

⇒ ion acoustic problem reduced to particle orbit.

$$\phi'' = dV/d\phi$$

$$\ddot{x} = -dU/dx$$

81

$$\eta^2 > 2 \frac{e\lambda_D}{T} \phi$$

critical velocity
for solitay.

→ small ϕ

$$V(\phi) \approx -\frac{1}{2} \frac{\eta^2}{\lambda_D^2} \left\{ (1 + \eta^2) + \phi - \phi \cdot \frac{1}{2} \phi^2 \left(\frac{-1}{\eta^2} + 1 \right) \right\}$$

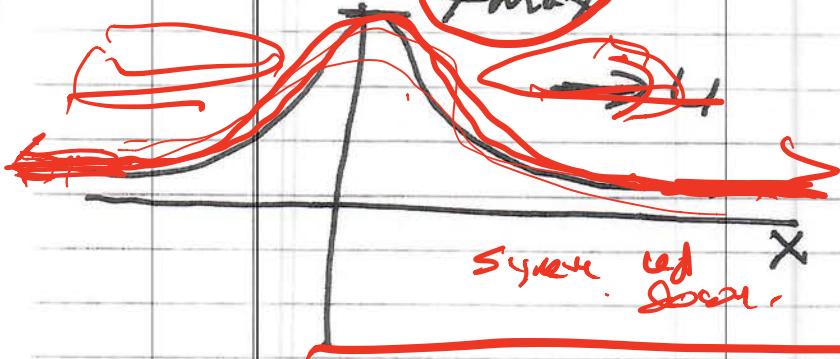
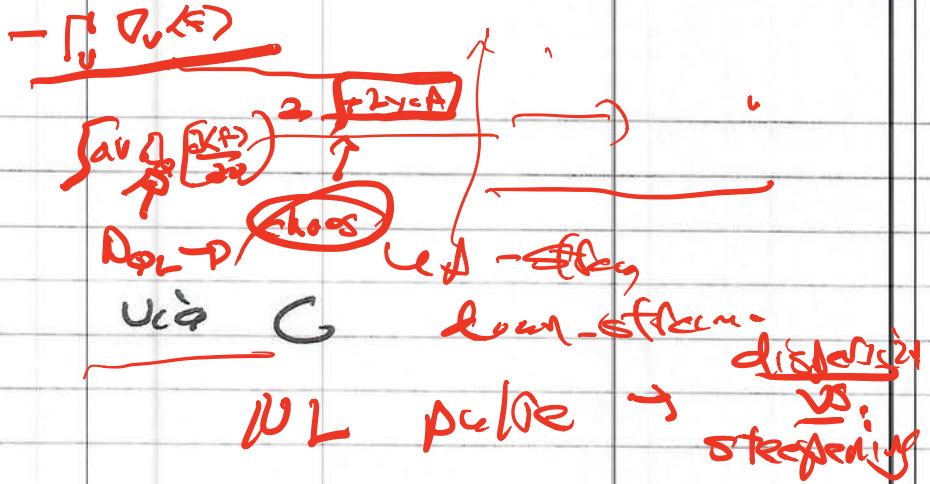
so need $\eta^2 > 1$

Now, choose:

$$\phi' \rightarrow 0$$

$$\phi \rightarrow 0$$

$$\phi_{\max}$$



$$M^2 = \frac{1}{2} \left[\exp \phi_{\max} - 1 \right]^2$$

$$\exp \phi_{\max} - 1 = \phi_{\max}$$

low amplitude

$$\phi \approx \frac{3}{2} \left(1 - \frac{1}{M^2} \right) \operatorname{sech}^2 \left\{ \sqrt{\frac{\pi M^2}{2}} \sqrt{1 - \frac{x}{M^2}} \right\}$$

$$\text{need } M^2 \geq 1.6.$$

For Acoustic
Collisionless Shock

can consider case,

→ Need discuss wave-particle interaction
to deal with heating, entropy production
etc

→ Sagdeev → Res. Pl. flux
V.L. 4

→ More general discussion (KdV):

Recall, had general:

Ans to: (Fluid waves
kinematics)

KdV

$$\partial_t \mathcal{E} + (c_s + \varepsilon) \partial_x \mathcal{E} + c_s \frac{\lambda_0^2}{2} \partial_x^3 \mathcal{E} = 0$$

$$a = \varepsilon$$

$$y = x - cst$$

$$\boxed{\partial_t q + a \partial_y q + \beta \frac{\partial^3 q}{\partial y^3} = 0}$$

Simple
KdV.

$$l_{\text{shock}} \sim (\beta/a)^{1/2}$$

scale amplitude reln.

Solving (reduced) KdV (integrating)

$$a = a(y - ct)$$

⇒

$$\beta a'' - ca' + qa' = 0$$

invariant
additv
const C + V

$$\beta a'' - ca' + \frac{a'^2}{2} = \frac{\pm C_1}{2}$$

$n \sim 1/5$

const

$\gg t_{\text{shock}}$

~~(written)~~ ~~(typed)~~

1

~~4-9~~ ~~gut~~ ~~rekt~~ ~~-~~ ~~1.1~~

11.

$$(2a') * \left(\beta a'' - c_0 + \frac{a'^2}{2} = \frac{c_1}{2} \right)$$

$$2\beta a' a'' - 2c_0 a' + a' a^2 = c_1 a'$$

intr.

$$\beta a'^2 = -\frac{1}{3} a^3 + c_1 a^2 + c_2 a + c_3$$

and can now reduce to quadrature.

→ Convenient to factorize:

$$c_1, c_2, c_3 \rightarrow q_1, q_2, q_3$$

$$\beta a'^2 = -\frac{1}{3} (q-q_1)(q-q_2)(q-q_3)$$

$$c = \frac{1}{3} (q_1 + q_2 + q_3)$$

3 roots
again!

For: → bounded ($a \cdot c_y$)

need q_1, q_2, q_3 real

if: $q_1 > q_2 > q_3$

$\Rightarrow q_1 \geq q \geq q_3$

$c_{13} = 0$ no loss generality

\Rightarrow

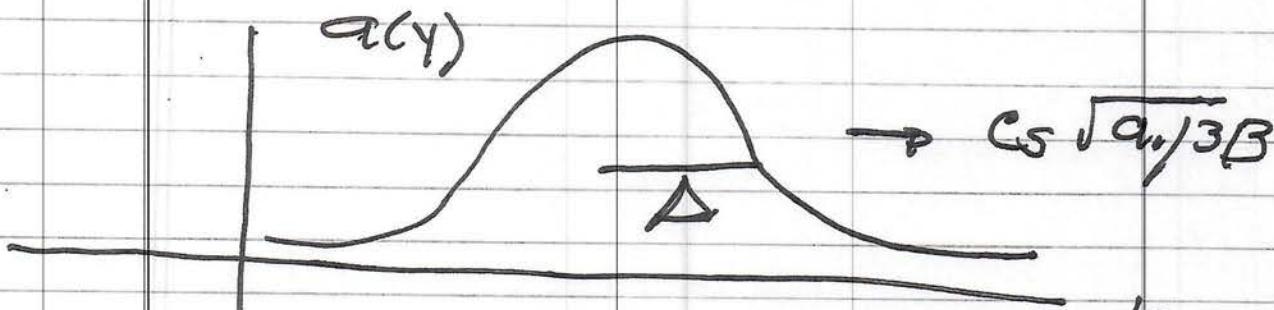
$$\beta d^2 = \frac{1}{3} (a_1 - a_2) (a_1 - a_2) q$$

if $a_2 = 0$

$$a(y) = a_1 \cosh^{-2} \left(\frac{1}{2} y \sqrt{a_1/3\beta} \right)$$

$$\rightarrow a_1 \cosh^{-2} \left(\frac{1}{2} (x - ct) \sqrt{a_1/3\beta} \right)$$

Q:, have (as before)



$$\Delta \sim (3\beta/a_1)^{1/2}$$

Note:

$$\rightarrow U \sim c_5 \sqrt{a_1/3\beta}$$

speed - amplitude

$$\rightarrow \Delta \sim (3\beta/a_1)^{1/2}$$

width - amplitude

B

Note:

→ Soliton has finite width

$$\Delta \sim (3B/a_1)^{1/2} \sim \lambda_{De}$$

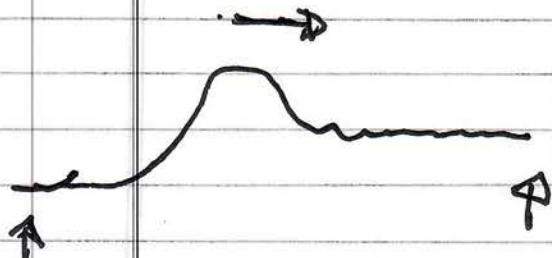
Contract shock

→ bigger solitons go faster

$$v \sim U_0 (a_1/3B)^{1/2}$$

Soliton → symmetric PBC
 up/down stream
 symmetric.

Collision less → collision less, asymmetry
 shock



entropy production?

TBC