

Response to the Decision Letter of the Editor and Reviewers

– Wind veer and speed in turbulent Ekman flow part I: scaling analysis and velocity profile model –

Cedrick Ansorge and Hauke Wurps

April 21, 2025

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Berlin, April 21, 2025

1 Response to the Editor

Dear Professor Anderson,

we thank you very much for the assessment of both parts of this combined manuscript and the commitment of BLM to consider this body of work as a whole.

Below, we detail our responses including changes incurred to the manuscript. We also provide an annotated manuscript (manuscript_diff.pdf) to ease the assessment of changes and expedite the further processing of our manuscript.

As it happens, some changes to this part of the manuscript are required due to Reviewer comments on the second part of the paper. We detail these changes below – before the responses to the individual reviewers.

In our response below, we repeat your original comment in gray font. Next comes *our response in blue font*, and we close by the changes to the manuscript in regular font. Comments are separated by horizontal lines for readability.

Kind Regards,
Cedrick Ansorge and Hauke Wurps

2 Response to Reviewer 1

Dear Reviewer 1,

Many thanks for the positive feedback on our manuscript. We have addressed the minor points raised in your review and hope that you agree with the edits. Please find the detailed responses below.

In our response below, we repeat your original comment in gray font. Next comes *our response in blue font*, and we close by the changes to the manuscript in regular font. Comments are separated by horizontal lines for readability.

Kind regards,

Cedrick Ansorge and Hauke Wurps

The authors analyze wind speed and direction profiles in turbulent Ekman flow using asymptotic theory and DNS data. They found that the streamwise velocity follows classical scaling laws, while outer-layer profiles align with a modified Ekman spiral. They showed that the spanwise component exhibits mixed scaling near the surface and outer scaling farther out.

Overall, the analysis and DNS are conducted rigorously, providing valuable insights and contributing meaningfully to advancements in the field.

We sincerely thank you for the positive assessment of our manuscript and the appreciation of our work.

In line 47, friction velocity is denoted as $u_* = \sqrt{|\tau_{sfc}|/\rho}$. However, in Eq. (1a) (below line 179), τ_{sfc} is defined as the kinematic shear stress. Please make them consistent.

Many thanks for spotting this inconsistency in nomenclature. We have aligned τ_{sfc} with the conventional definition of dynamic shear stress and now include the division by density in Eq. (1b).

$$\underline{\tau}_{sfc} = \begin{pmatrix} \tau_x \\ \tau_y \\ \tau_z \end{pmatrix} = -\rho\nu \left(\frac{\partial U}{\partial z} \hat{e}_x + \frac{\partial V}{\partial z} \hat{e}_y \right) \quad (1a)$$

and labelled by an upper index α as in \underline{U}^α for the velocity vector, and (ii) the coordinate system aligned with the free-atmosphere geostrophic wind labelled by an upper index G as in \underline{U}^G . We

denote the square root of the modulus of surface shear, the surface friction, by

$$u_* = \sqrt{\frac{||-\tau_{\text{sfc}}||}{\rho}} \quad (1b)$$

and let $Z_* = G/u_*$;

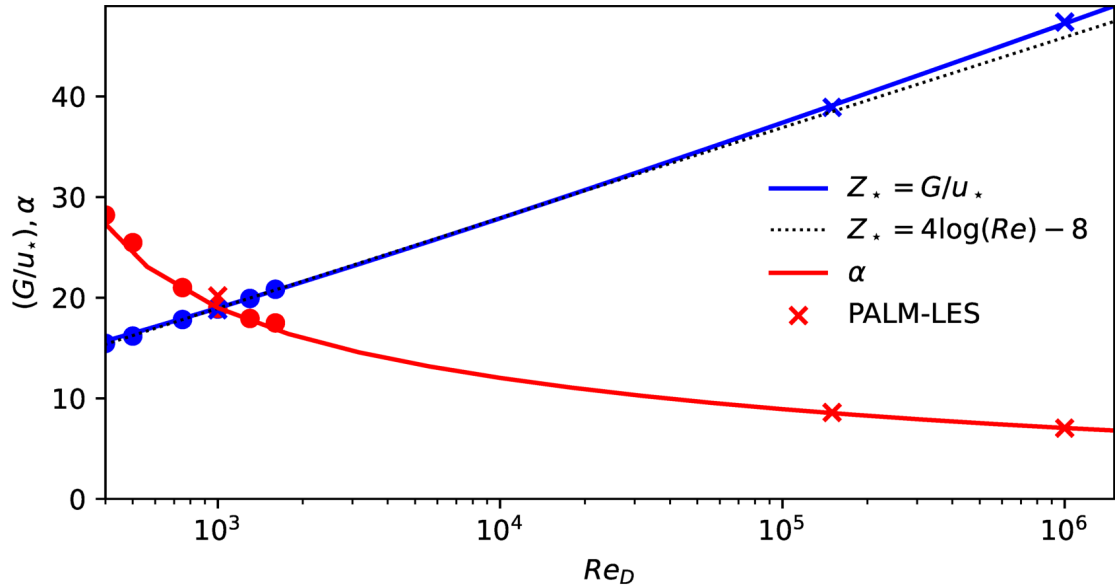
Location for the definition of z^- . The first appearance of z^- is at line 262, and figure 1b, but it was defined on line 307. It would be better to define it close to where it appears.

Thank you - we now introduce the outer length scale much earlier in Sec. 2.1 ("Notation and governing equations"). We also think, this is more appropriate.

The outer normalization (with respect to the boundary-layer depth δ and velocity u_*) is denoted by a superscript $'-'$, i.e. $z^- = z/\delta$.

Figure 4: Should the legend be $Z_* = 4\log(Re_D) - 8$, instead of $u_* = \dots$?

Indeed, there was a typo, please find the revised Figure below.



Berlin, April 21, 2025

3 Response to Reviewer 2

Dear Reviewer 2,

Many thanks for the positive feedback on our manuscript. We have addressed the minor points raised in your review and hope that you agree with the edits. Please find the detailed responses below.

In our response below, we repeat your original comment in gray font. Next comes *our response in blue font*, and we close by the changes to the manuscript in regular font. Comments are separated by horizontal lines for readability.

Kind regards,

Cedrick Ansorge and Hauke Wurps

The authors perform direct numerical simulations of the Ekman layer at moderate Reynolds number, and use their simulations to examine the vertical mean velocity profiles in rotating, neutrally-stratified flows that serve as a proxy for the neutral atmospheric boundary layer. They compare their DNS results to a model that matches the Ekman model (in the outer layer) with the classical results for the inner layer (viscous layer plus log layer) in wall-bounded turbulent flows. Specifically, they examine the scaling of the spanwise velocity profile, and find that a matching procedure—combining both inner- and outer-scaling—is necessary. The article is generally clear and well-written, and addresses the important problem of how velocity profiles behave in the Ekman layer. Despite being an old problem, it has not been resolved, and there are many subtleties that are often neglected in the literature. I am overall supportive of this manuscript, but below I provide some specific comments which I believe will help improve the clarity of communication in the article. I am recommending that the manuscript is accepted in BLM, pending minor revisions.

We appreciate your summary of our work and thank you for the time spent on our manuscript. Below, please find the detailed responses to your comments.

L. 12, 76: discussion of span-wise velocity component. Can you explain how you are defining stream-wise and spanwise here? Are you assuming the streamwise component is aligned with the geostrophic wind direction far above the surface?

This is indeed important and we inserted an apposition phrase for clarification

[...], considered in a wall-stress-aligned reference frame, [...]

L. 16 outer height - do you mean outer length scale?

We mean 'outer height' here, but we realize the phrase may be uncommon to some BLM readers and have clarified as follows

[...] commonly denoted as z^- .

L. 19 "vide Reynolds numbers" - I'm not sure this makes sense to me.

What we mean here is that an increase in scale separation is the same as an increase in Reynolds number. We rephrased

[...], i.e. an increase in Reynolds number.

L. 63 Prandtl-layer height is undefined here

The symbol was superfluous and is not needed. We now describe what the Prandtl-layer height is and trust that the interested reader will be able to find details on the exact definition in the reference that is mentioned here.

[...] they choose the Prandtl-layer depth, a measure for the depth of the surface layer, to match the wind speed profiles. However, this requires external prescription of the veering at that height.

L. 124 - "require one to consider" or "require consideration of"

Thank you! We chose the latter.

[...] require consideration of the height-dependence of the veer and stress misalignment [...].

II. 168-170 - This seems to be contradictory. The authors state that rotation only acts on the horizontal components of velocity, but go on to state that they neglect rotational effects on the horizontal components of velocity.

*Thank you for spotting this inconsistency, of course rotational effects on the **horizontal** components of velocity are considered, they are only neglected for the **vertical** components.*

The f-plane approximation is applied, i.e. rotation acts on the horizontal components of velocity alone; rotational effects on the vertical component of velocity and dynamical effects due to latitudinal variation of the rate of rotation are neglected.

I. 176 - I do not think that Ensemble should be capitalized

adopted.

L. 193 "this state is defined by a Reynolds number, the only non-dimensional parameter that governs

the system.” Shouldn’t the Rossby number also enter as a non-dimensional parameter? Given a domain height, geostrophic wind speed G , and Coriolis parameter f , one can also define the Rossby number. The problem would depend on Reynolds number alone in the absence of rotation, but if there is rotation, the relevant dimensionless parameters should be both Re and Ro .

In general, this is true. However, when Ekman flow is considered, the ratio of Rossby and Reynolds number (which is the Ekman number) is fixed. To clarify the impact of this constraint: it also implies that - given the Coriolis parameter f , i.e. a latitude - the geostrophic wind defines the Rossby radius. That is, Ekman flow is a rather strong constraint from the perspective of large-scale dynamics. Nonetheless, it is a widely adopted simplification in the context of boundary-layer dynamics. We add a phrase clarifying the uniqueness of the problem given Re . For clarification, one may see that the Ekman-based Reynolds number Re_D can be written as Ratio of the Rossby Radius Λ_{Ro} and laminar Ekman-layer scale D , which is another illustration of the link between large-scale and boundary-layer dynamics:

$$Re_D = \frac{GD}{\nu} = \frac{G\sqrt{2\nu}}{\sqrt{f\nu}} = \sqrt{\frac{2G^2}{f\nu}} = \sqrt{\frac{G^2}{f^2} \frac{2f}{\nu}} = \sqrt{4\Lambda_{Ro}^2 \frac{f}{2\nu}} = 2\Lambda_{Ro}/D. \quad (2)$$

Analogously, one may see that $Ro = \frac{G}{\Lambda_{Ro}f} = 1$ for the definition of the Rossby number. Alternatively – when replacing Λ_{Ro} by D , which also yields a valid definition of Rossby number from the perspective of boundary-layer dynamics– it is (cf. Eq. 2)

$$Ro_D = \frac{G}{Df} = Ro \frac{D}{\Lambda_{Ro}} = \frac{2}{Re_D} \quad (3)$$

L. 221 - It might be better to use scientific notation here.

As we do need five significant digits for the middle number, we do not see the benefit of moving to scientific notation

// no change incurred //

L. 277, 281 - the notation is a bit awkward here, e.g. $V^{\alpha_*+}(z^+)$. Is there a way to make it clearer?

We have thought a lot about this notation and checked many different approaches. It is very important to note that the index α_ cannot simply be omitted (in fact, above it has been demanded to clarify the alignment, which is the sole purpose of the index α_*). At the moment, we do not see a better option - if there may be more aesthetic options, all of them which come to our mind, would sacrifice clarity.*

// no change incurred //

Fig. 1a - Does the solid black line correspond to the $Re=1600$ case? If so, why is there a discontinuity just above 10^1 ? Or are you also using a solid black line to denote the inner layer velocity

profile, $u^+ = z^+$?

L. 308 Eddy should not be capitalized

adopted

The eddy viscosity [...].

L. 311 - The assumptions of horizontal homogeneity and $W=0$ are not exactly the same thing as symmetries in the flow.

We realize that this was an imprecise phrasing and clarified.

For the assumptions of horizontal homogeneity and incompressibility (which implies $W = 0$, i.e. no mean wall-normal velocity), it is [...].

Fig. 3: It would be better to present heights in terms of z^+ values rather than the index of the vertical coordinate.

We believe that both ways of conveying this information have their value and added the requested distance from the wall in inner units.

Fig. 3 Horizontal slices of turbulence kinetic energy in the Buffer layer ($i=10$, $z^+ \approx 10.5$), logarithmic layer ($i=100$, $z^+ \approx 150$), and outer layer ($i=400$, $z^+ \approx 1200$) of the case with $Re_\tau = 2978$; coloring between percentiles 4 and 96 of the respective image. Lower panel: streamwise-vertical intersect through the domain

4 Response to Reviewer 3 (Prof. Sukanta Basu)

Dear Professor Basu,

we like to extend our sincere thanks for your assessment of our manuscript. We understand your criticism of our somewhat bold claim of universality and have amended the manuscript.

We ask for your understanding that, as you already anticipated, a complete reconsideration of our results in the framework of your 2023 paper is not carried out at this point (the detailed reasoning is given below). We, however, would be happy to provide processed and unprocessed data if a colleague or potentially member of your working group is interested in carrying these ideas further.

As you unveiled your identity and you gave your consent to be mentioned, we also thank for your contribution in the acknowledgments of the revised manuscript.

Cedrick Ansorge and Hauke Wurps

This is an excellent paper that should be published in BLM. However, I request the authors to tone down their narrative, including the title. It is an empirical study that tries to fit DNS data using various formulations. Some of these formulations have a physical basis, while others are ad-hoc. Please refrain from calling the results “universal”.

*We critically reassessed our use of the work 'universal' in the manuscript and indeed agree that in some respect, in particular with respect to the derived velocity-profile formulations the use was somewhat overstating. We removed these occurrences in the introduction, conclusion and some parts of the results. Most importantly, we removed the word from the running title and from the section title. However, in the context of some the classic universal scalings *(logarithmic scaling, viscous scaling), we keep the word – also in the context of our results.*

A number of changes was carried out throughout the manuscript in response to this point, we kindly ask you to refer to the annotated pdf file for details. Primarily we undertook the following modifications

- (1) changed title to **Wind veer and speed in turbulent Ekman flow part I: scaling analysis and velocity profile model**
- (2) changed heading of Section 4.1 to **A Reynolds-number-independent velocity profile for the turbulent Ekman layer**
- (3) Conclusions: universal formulation → **closed formulation**

At the heart of this paper is Eq. 10a. Following Etling's work and others, this equation has been derived in Appendix A1.

$$\frac{1}{G} \begin{pmatrix} U_{Ek} \\ V_{Ek} \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \end{pmatrix} + e^{-z_{Ek}} \left[a_{ek} \begin{pmatrix} -\cos z_{ek} \\ \sin z_{ek} \end{pmatrix} + b_{ek} \begin{pmatrix} \sin z_{ek} \\ \cos z_{ek} \end{pmatrix} \right]$$

The problem with this equation is the assumption of constant eddy viscosity. As the authors showed in Figure 2c, the eddy viscosity profile from the DNS is far from constant. It has a clear maximum and a specific shape, which depends on Re. So, the authors took an empirical (engineering) approach on page 14 (line 403). They estimated a bulk eddy viscosity indirectly. This is a major weakness of this paper and could be avoided. Please see the following paper where we analytically derived the eddy viscosity profile from the Ekman equations. Since this is a relatively new paper, the authors might not have come across it. That is why I am revealing my identity.

Basu, Sukanta, and Albert AM Holtslag. "A novel approach for deriving the stable boundary layer height and eddy viscosity profiles from the Ekman equations." *Boundary-Layer Meteorology* 187.1 (2023): 105-115.

The authors might want to revise their derivations based on our analytical eddy viscosity profile. If that is difficult to do, I suggest highlighting the limitations of their current bulk approach. Also, emphasize the limitations of Eq. (10a) as it assumes constant eddy viscosity.

We agree that eddy viscosity is not constant as a function of height. In fact, we even discuss the height dependency of eddy viscosity in Fig. 2c,d / Sec. 2. At the same time, the revised Ekman model / Eq. (10) makes use of Ekman's assumption of height-constant eddy viscosity. The important point here is that this is only used in the upper part of the boundary layer, where variation of the eddy viscosity is not the dominant mechanism for the wind profile. We find excellent agreement above $z^- \approx 0.5$ (cf. Fig. 6a/b in the manuscript). We are aware that deviations from the idealized Ekman profile below $z^- \approx 0.5$ are due to variations of eddy viscosity. The key novelty in our approach regarding the Ekman spiral is, however, to apply it only in parts of the outer layer and to acknowledge its inappropriateness for most of what is commonly considered the turbulent boundary layer (about 2/3 of δ). Across this range, where we argue to apply the Ekman model the eddy viscosity is not constant, but its variation appears limited, also in view of our own results presented in Sec. 2. We do hence not see an advantage to incorporate the model using variable eddy viscosity suggested by Basu et al. (2023) but rather understand this as an alternative approach, which is now mentioned in the revised manuscript.

Could the authors comment on Fig. 6a in the revised manuscript? The discrepancy between DNS and their empirical prediction is large and not explained.