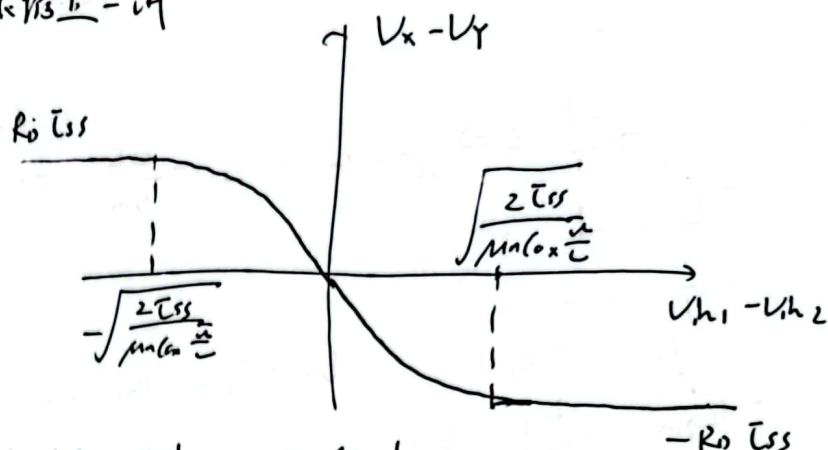


for  $\beta_3 \ll \beta_1$  - ideal



$V_{h1} - V_{h2} \gg \sqrt{2Iss / (\mu_n Cox \frac{W}{L})}$ ,  $V_{h1} \approx V_{h2} \approx V_{TH}$  MOS off of

if  $V_{h1} - V_{h2} \gg \sqrt{2Iss / (\mu_n Cox \frac{W}{L})}$ ,  $M_2$  off

$$V_{h2} - V_{TH} = V_0$$

$$\frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{h1} - V_{TH})^2 = I_{SS} \Rightarrow V_{h1} - V_0 - V_{TH} = \sqrt{\frac{2 I_{SS}}{\mu_n C_{ox} \frac{W}{L}}}$$

$$V_{h1} - V_{h2} = \sqrt{\frac{2 I_{SS}}{\mu_n C_{ox} \frac{W}{L}}}$$

$$\text{又有 } I_{D1} - I_{D2} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{h1} - V_{h2}) \sqrt{\frac{4 I_{SS}}{\mu_n C_{ox} \frac{W}{L}} - (V_{h1} - V_{h2})^2}$$

$$\Rightarrow V_x - V_y = -\frac{R_D}{2} \mu_n C_{ox} \frac{W}{L} (V_{h1} - V_{h2}) \sqrt{\frac{4 I_{SS}}{\mu_n C_{ox} \frac{W}{L}} - (V_{h1} - V_{h2})^2}$$

If  $(V_{h1} - V_{h2})^2 \ll \frac{4 I_{SS}}{\mu_n C_{ox} \frac{W}{L}}$ , at the origin point of

$$V_x - V_y = -\frac{R_D}{2} \mu_n C_{ox} \frac{W}{L} \sqrt{\frac{4 I_{SS}}{\mu_n C_{ox} \frac{W}{L}}} (V_{h1} - V_{h2})$$

$$= -R_D \mu_n C_{ox} \frac{W}{L} \sqrt{\frac{I_{SS}}{\mu_n C_{ox} \frac{W}{L}}} (V_{h1} - V_{h2})$$

$$= -R_D \sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}} (V_{h1} - V_{h2})$$

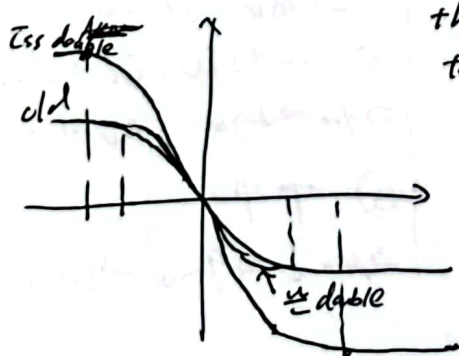
when close to origin point,  $k = -R_D \sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}}$

①  $I_{SS}$  is doubled. slope changes to  $k = -\sqrt{\mu_n C_{ox} \frac{W}{L} 2 I_{SS}} R_D$

the circuit becomes more linear because it can take a larger input difference without "dying".

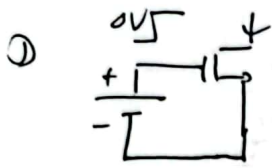
②  $\frac{W}{L}$  is doubled.

The circuit becomes less linear, because it can take only a smaller input difference before it "dies".

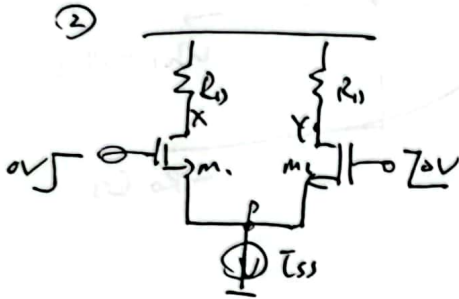


# Small-Signal Behavior of MOS Diff Pair.

A few points.



$$\Delta I \Rightarrow \frac{\Delta I}{\Delta V} = g_m \Rightarrow \Delta V = \frac{\Delta I}{g_m} \Rightarrow$$



$$V_x - V_y = -R_D \sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}} \cdot (2\Delta V)$$

$$\Rightarrow \therefore V_x - V_y = -R_D (I_{D1} - I_{D2})$$

$$\Rightarrow \begin{cases} I_{D1} - I_{D2} = \sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}} (2\Delta V) \\ I_{D1} + I_{D2} = I_{SS} \end{cases}$$

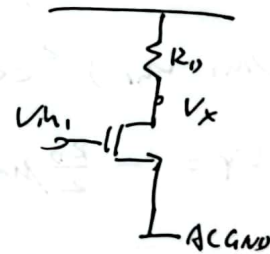
$$\Rightarrow I_{D1} = \frac{I_{SS}}{2} + \sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}} \Delta V$$

$$\therefore \frac{\sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}} \Delta V}{\Delta I} = \Delta V \Rightarrow g_m = \sqrt{\mu_n C_{ox} \frac{W}{L} I_{SS}}$$

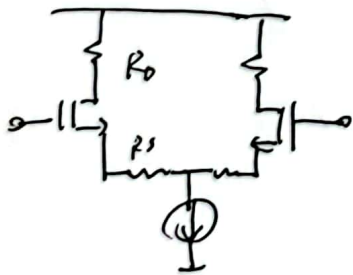
与偏置电压有关

$V_p$  doesn't change  $\Rightarrow$  P is AEGND.  
CS stage

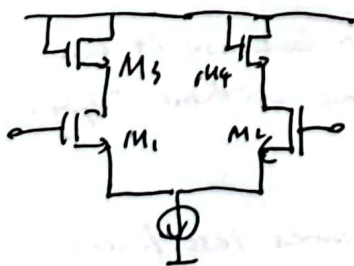
$$\Rightarrow \frac{V_x}{V_{in1}} = -g_m R_D \Rightarrow \frac{V_x - V_p}{V_{in1} - V_{in2}} = -g_m R_D$$



Example



$$\frac{V_x}{V_{in1}} = -\frac{R_D}{\frac{1}{g_m} + R_S} \quad \text{degeneration.}$$



$$\frac{V_x}{V_{in1}} = -\frac{\frac{1}{g_{m2}}}{\frac{1}{g_{m1}} + R_S} = -g_{m1} \frac{1}{g_{m2}}$$

Observations

①  $W \rightarrow 2W$ .

$$\Rightarrow g_m \rightarrow \sqrt{2} g_m$$

$$\Rightarrow A_v \rightarrow \sqrt{2} A_v$$

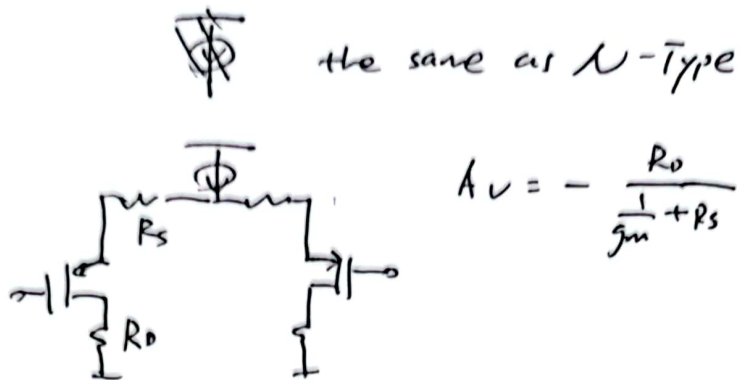
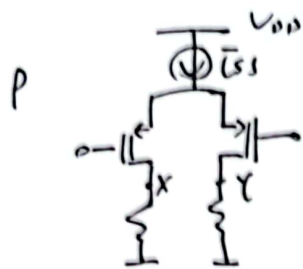
②  $W \rightarrow 2W, I_{SS} \rightarrow 2I_{SS}$

$$\Rightarrow g_m \rightarrow 2g_m, A_v \rightarrow 2A_v$$

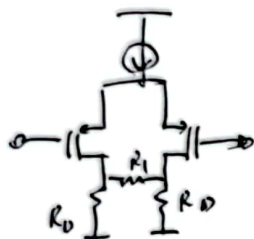
③  $T \uparrow$

$$\Rightarrow \mu_n \downarrow \Rightarrow g_m \downarrow \Rightarrow |A_v| \downarrow$$

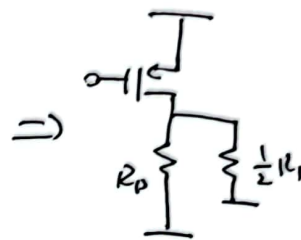
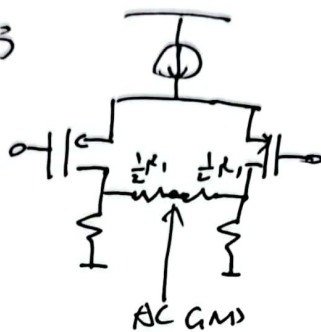
# P-Type Diff Pair



## Example



同样，分析



$$\therefore \frac{V_X}{V_{in}} = -g_m(R_D \parallel \frac{1}{2}R_S)$$