

Notes

LQG optimal control

Linear quadratic Gaussian (LQG) optimal control consists of linear quadratic regulator (LQR) feedback control, and Kalman filter (KF) state observer for stochastic linear system. Consider a stochastic linear system

$$\dot{x} = Ax + Bu + e_x,$$

$$y = Cx + Du + e_y,$$

where e_x and e_y are white noises following

$$e_x \sim N(0, Q), e_y \sim N(0, R), x(0) \sim N(x_0, P_0).$$

Linear quadratic regulator (LQR) designs a feedback control $u = -Kx$, minimizing

$$J = \int_0^{t_f} (x^T Q x + u^T R u) dt + x_f^T F x_f,$$

where $x_f = x(t_f)$. Feedback matrix is computed by

$$K = R^{-1} B^T P,$$

where P is the solution of Riccati equation

$$\dot{P} = -PA - A^T P + PBR^{-1}B^T P - Q.$$

For a time-invariant system that $\dot{P} = 0$, hence

$$-PA - A^T P + PBR^{-1}B^T P - Q = 0,$$

$$\dot{x} = (A - BK)x = (A - BR^{-1}B^T P)x,$$

$$J = \frac{1}{2} x_0^T P x_0.$$

In LQR controller, P can be solved by iteration from $P(t_f) = F$ or $P(0) = P_0$. When $\dot{P} = 0$, P can be solved by least square method, Hamilton matrix method, dynamic programming (DP), linear matrix inequality (LMI), etc. Based on this LQR system, Kalman filter requires observation y to obtain optimal estimation of state x from noised data. Let T denotes time step, the discretization of linear system is

$$x(k+1) = (I + AT)x(k) + TBu(k) + Te_x(k).$$

Then, Kalman filter is performed iteratively by maximizing $p(x(k+1)|y(k), x(k))$.

Proposed algorithm

Inspired by our previous work [Incorporating Transformer and LSTM to Kalman Filter with EM algorithm for state estimation](#) (Fig. 1), this repository combines deep learning models, Transformer and LSTM, for KF in LQG.

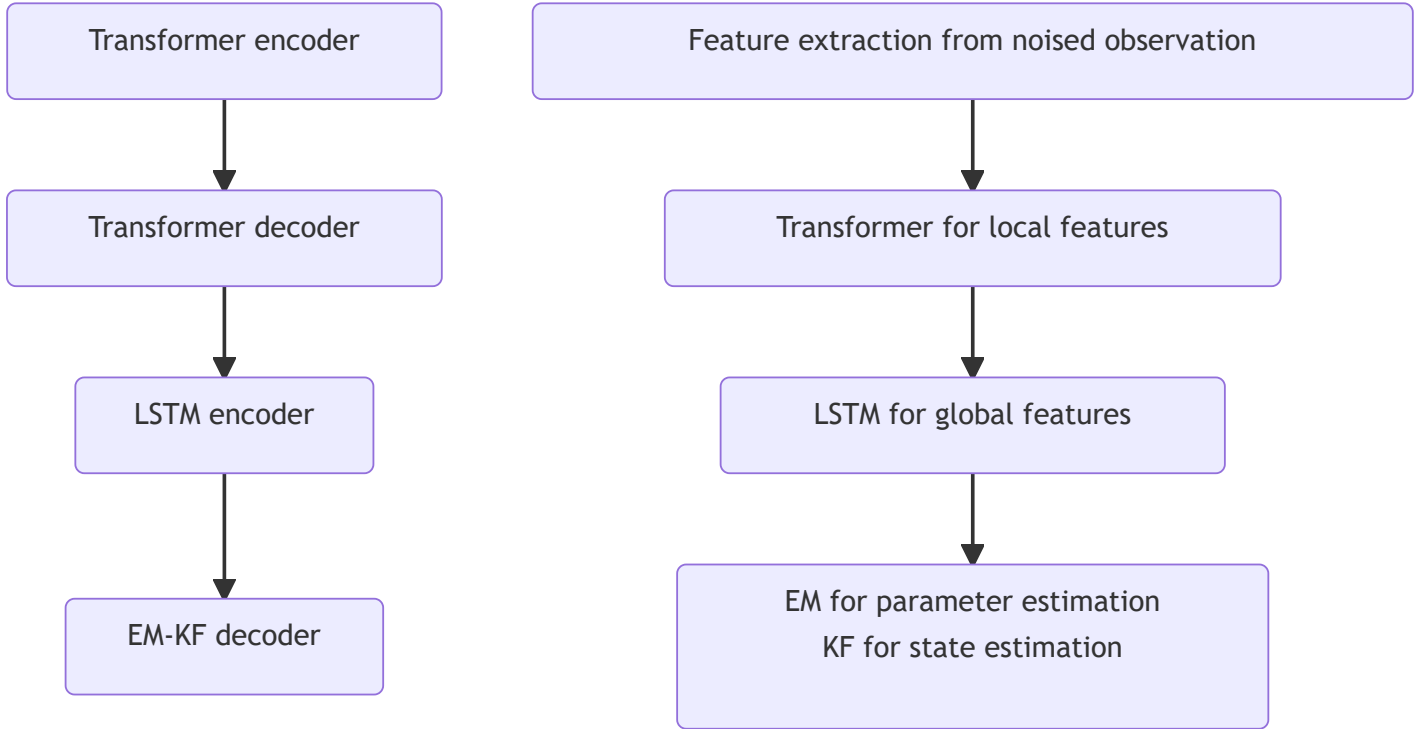


Fig.1 Deep learning-based KF

EM-KF adopts expectation maximization (EM) algorithm for parameters estimation before Kalman filtering. This repository utilizes EM-KF to estimate the feedback matrix of LQR controller, instead of classical Riccati equation-based LQR.

- Classical method: $\dot{x} = \hat{A}x$, $\hat{A} = A - BK = A - BR^{-1}B^TP$, P is the solution of Riccati equation.
- Our method: $\dot{x} = \hat{A}x$. \hat{A} is solved by EM algorithm-based iteration from initial $\hat{A}_0 = A - BR^{-1}B^TP_0$.

AGV system

Example1 Acceration-driven system

Consider an AGV system that position x can be observed, and is driven by acceration u .

$$\begin{pmatrix} \dot{x} \\ \ddot{x} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \end{pmatrix} + \begin{pmatrix} 0 \\ 1 \end{pmatrix} u,$$

$$y = \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \end{pmatrix}.$$

Example2 Temperature control system

In industrial applications, The operation of AGV for biochemical usage usually depends on the stability of environmental factors (e.g. temperature). The transfer function of temperature control system is simulated by

$$G(s) = \frac{Y(s)}{U(s)} = \frac{K \exp(-\tau s)}{Ts + 1} \approx \frac{K}{(Ts + 1)(\tau s + 1)},$$

where y is temperature, u is the control signal. Commonly, u is the output of a PID controller requiring error value as input. Let $a = 1/(T\tau)$, then the state-space model of $G(s)$ is

$$\begin{pmatrix} \dot{x} \\ \ddot{x} \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -a & -a(T + \tau) \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \end{pmatrix} + \begin{pmatrix} 0 \\ 1 \end{pmatrix} u,$$

$$y = \begin{pmatrix} aK & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \end{pmatrix}.$$

Two-wheel differential AGV in cartesian coordinate

An AGV on 2D-plane requires linear velocity v and angular velocity ω to control the position $(x_1, x_2, \theta)^T$ in cartesian coordinate (Fig. 2).

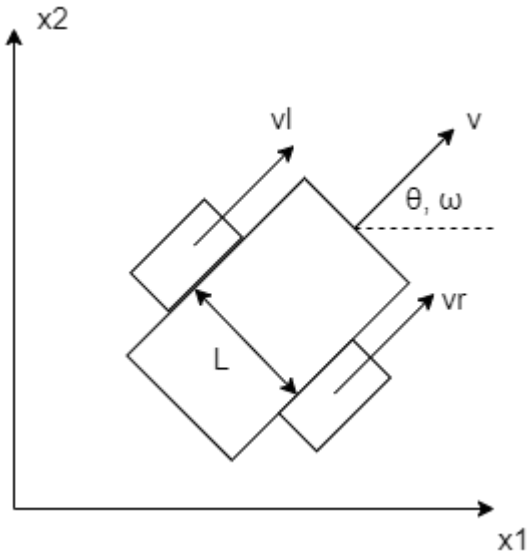


Fig.2 Two-wheel differential AGV

The kinematics equations are

$$\dot{x}_1 = v \cos \theta, \dot{x}_2 = v \sin \theta, \dot{\theta} = \omega.$$

Let v_l and v_r denote the linear velocity of left or right wheel, respectively, and L denotes the width of the vehicle, then

$$v_l = v + \frac{\omega L}{2}, v_r = v - \frac{\omega L}{2}.$$

Hence, linear velocity v can be set as constant to decouple v and θ . Only ω is the control signal for manipulating left or right wheel. Let $(x_{10}, x_{20}, \theta_0)^T$ denotes the initial position, using $\cos \theta \approx 1$, $\sin \theta \approx \theta$, the system can be linearized as

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & v \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ \theta \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \omega + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} v.$$

Using Taylor expansion

$$y = \sqrt{x_1^2 + x_2^2} = \sqrt{x_{10}^2 + x_{20}^2} + \cos \theta_0 (x_1 - x_{10}) + \sin \theta_0 (x_2 - x_{20}),$$

where

$$\cos \theta_0 = \frac{x_{10}}{\sqrt{x_{10}^2 + x_{20}^2}}, \sin \theta_0 = \frac{x_{20}}{\sqrt{x_{10}^2 + x_{20}^2}},$$

Hence

$$y = \begin{pmatrix} \cos \theta_0 & \sin \theta_0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ \theta \end{pmatrix} + \sqrt{x_{10}^2 + x_{20}^2} - \cos \theta_0 x_{10} - \sin \theta_0 x_{20}.$$

Two-wheel differential AGV in polar coordinate

In polar coordinate, x is defined as the offset between the direction the AGV actually travels and the reference direction. This distance can be observed.

$$\dot{x} = v \sin \theta, \dot{\theta} = \omega \Rightarrow \begin{pmatrix} \dot{x} \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} 0 & v \\ 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ \theta \end{pmatrix} + \begin{pmatrix} 0 \\ 1 \end{pmatrix} \omega.$$

$$y = \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} x \\ \theta \end{pmatrix}.$$

Lagrangian mechanics in robotics

Lagrangian mechanics defines the Lagrangian \mathcal{L} as a function of generalized coordinates q describing the complete dynamics of a given system.

$$\mathcal{L} = T - V = \frac{1}{2} \dot{q}^T M(q) \dot{q} - V(q),$$

where T is the kinetic energy and V is the potential energy. M is the inertia matrix. The Euler-Lagrange equation is adopted.

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{q}} - \frac{\partial \mathcal{L}}{\partial q} = \tau,$$

where τ is generalized force. Hence

$$M(q)\ddot{q} + \dot{M}(q)\dot{q} - \frac{1}{2} \frac{\partial \dot{q}^T M(q) \dot{q}}{\partial q} - \frac{\partial V}{\partial q} = \tau.$$

Let Centripetal and Coriolis forces c and gravity g denote

$$c(q, \dot{q}) = \dot{M}(q)\dot{q} - \frac{1}{2} \frac{\partial \dot{q}^T M(q) \dot{q}}{\partial q}, g(q) = -\frac{\partial V}{\partial q},$$

then

$$M(q)\ddot{q} + c(q, \dot{q}) + g(q) = \tau.$$

[Deep Lagrangian Networks: Using Physics as Model Prior for Deep Learning](#) proposes Deep Lagrangian Networks (DeLaN) as a deep network structure for estimating parameters in Lagrangian Mechanics. Inspired by this work, this repository can also be adopted for mechanics modeling of AGV.

Cart-pole as AGV mechanics

Cart-pole describes a classical control question by modeling inverted pendulum mechanics. This question is also widely applied for benchmarking reinforcement learning algorithms. (See classic control environments in [Gym](#) library for details.) The pendulum is assumed to consist of rigid rod of length $2L$ (Fig. 3a), or a point mass m affixed to the end of a massless rigid rod of length L (Fig. 3b). The moment of inertia

$$I_a = \int_0^{2L} \frac{m}{2L} r^2 dr = \frac{4}{3} mL^2, I_b = mL^2.$$

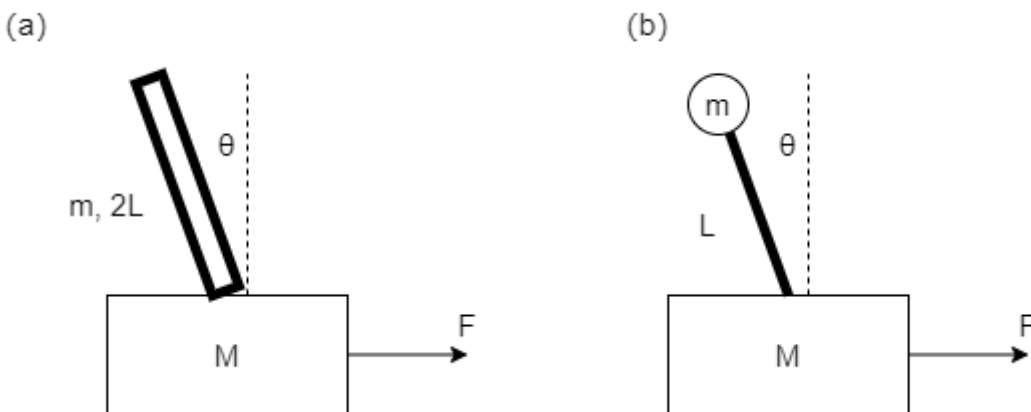


Fig. 3 Cart-pole

Let θ denotes the angle of the pendulum with respect to the vertical direction, cart mass M moves at position x , and F denotes control force in the x -direction.

$$T_M = \frac{1}{2}M\dot{x}^2, T_m = \frac{1}{2}m(v_x^2 + v_y^2) + \frac{1}{2}I\dot{\theta}^2, V = mgL \cos \theta.$$

$$v_x = \dot{x} - L\dot{\theta} \cos \theta, v_y = L\dot{\theta} \sin \theta.$$

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{x}} - \frac{\partial \mathcal{L}}{\partial x} = (M + m) \ddot{x} - mL\ddot{\theta} \cos \theta + mL\dot{\theta}^2 \sin \theta = F.$$

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}} - \frac{\partial \mathcal{L}}{\partial \theta} = (I + mL^2)\ddot{\theta} - mL\ddot{x} \cos \theta - mgL \sin \theta = 0.$$

Using $\cos \theta \approx 1, \sin \theta \approx \theta, \dot{\theta}^2 \approx 0$,

$$(M + m)\ddot{x} - mL\ddot{\theta} = F, (I + mL^2)\ddot{\theta} - mL\ddot{x} - mgL\theta = 0.$$

Set x as observation.

$$\begin{pmatrix} \dot{x} \\ \ddot{x} \\ \dot{\theta} \\ \ddot{\theta} \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{m^2gL^2}{p} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \frac{mgL(M+m)}{p} & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \\ \theta \\ \dot{\theta} \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{I+mL^2}{p} \\ 0 \\ \frac{mL}{p} \end{pmatrix} F,$$

where $p = I(M + m) + mL^2$,

$$y = \begin{pmatrix} 1 & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \\ \theta \\ \dot{\theta} \end{pmatrix}.$$