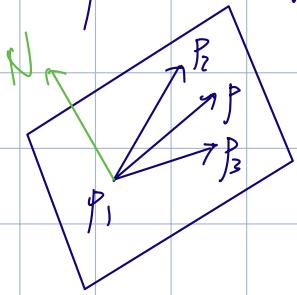


## Lecture 3 plane

3 points to form a plane



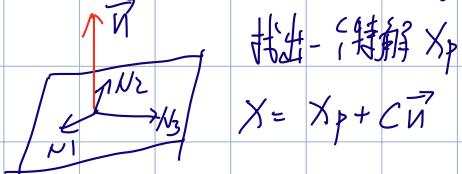
$$(1) \det(\vec{P_1P_2}, \vec{P_1P_3}, \vec{P_1P}) = 0 \quad \det(\vec{a}, \vec{b}, \vec{c}) = \begin{vmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{vmatrix}$$

$$(2) \vec{N} = \vec{P_1P_3} \times \vec{P_1P_2} \quad \text{解 } \vec{P_1P} \cdot \vec{N} = 0$$

≡

$$Ax + By + Cz = D \quad (A, B, C) \text{ 为 normal vector } \vec{N}$$

若  $Ax + By + Cz = D$  且  $\det(A) = 0$ , 则  $\vec{N}_1, \vec{N}_2, \vec{N}_3$  are coplanar



# Lecture 5 Equation of line

1. intersection of 2 planes

2. trajectory of a moving point parametric equation  
ex. line through  $Q_0 = (-1, 2, 2)$ ,  $Q_1 = (1, 3, -1)$

$$\begin{cases} \overrightarrow{Q_0 Q(t)} = t \overrightarrow{Q_0 Q_1} = t \langle 2, 1, -3 \rangle \\ x(t) = -1 + 2t \\ y(t) = 2 + t \\ z(t) = 2 - 3t \end{cases} \quad Q(t) = Q_0 + t \overrightarrow{Q_0 Q_1}$$

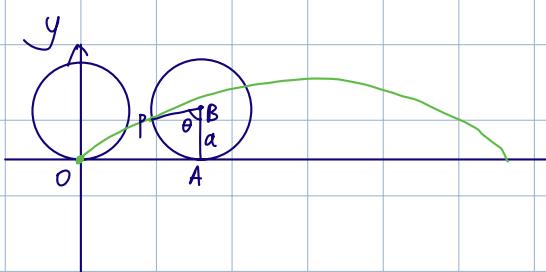


Application:

Intersection with plane? ex.  $x + 2y + 4z = 7$  line through  $(-1, 2, 2), (1, 3, -1)$

the plane divide the space into 2 part:  $x + 2y + 4z > 7$  and  $x + 2y + 4z < 7$  opposite side

$$x(t) + 2y(t) + 4z(t) = -t + 1 + 11 = 7 \quad t = \frac{1}{2} \quad \text{intersection point: } \left(0, \frac{5}{2}, \frac{1}{2}\right)$$



$$\begin{aligned} \overrightarrow{OP} &= \overrightarrow{OA} + \overrightarrow{AB} + \overrightarrow{BP} \\ \overrightarrow{OA} &= \langle a\theta, 0 \rangle \quad \overrightarrow{AB} = \langle 0, a \rangle \quad \overrightarrow{BP} = \langle -a\sin\theta, -a\cos\theta \rangle \\ &= x(\theta) \quad = y(\theta) \\ \overrightarrow{OP} &= \langle a\theta - a\sin\theta, a - a\cos\theta \rangle \end{aligned}$$

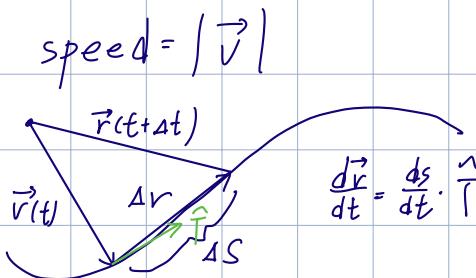
velocity ex  $\vec{r}(t) = \langle t - \sin t, 1 - \cos t \rangle$

$$\vec{v} = \frac{d\vec{r}}{dt} = \left\langle \frac{dx}{dt}, \frac{dy}{dt}, \frac{dz}{dt} \right\rangle = \langle 1 - \cos t, \sin t \rangle$$

unit tangent vector  $\hat{T} = \frac{\vec{v}}{|\vec{v}|}$

$$\vec{v} = \frac{d\vec{r}}{dt} = \frac{d\vec{r}}{ds} \cdot \frac{ds}{dt} = |\vec{v}| \quad \therefore \frac{d\vec{r}}{ds} = \frac{\vec{v}}{|\vec{v}|}$$

Velocity has direction, tangent to traj,  $\hat{T}$   
length: speed,  $\frac{ds}{dt}$



## Lecture 6 Partial derivative

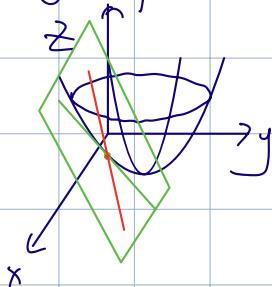
$$f = f(x, y) \quad \frac{\partial f}{\partial x} \Big|_{x_0, y_0} = \lim_{\Delta x \rightarrow 0} \frac{f(x_0 + \Delta x, y_0) - f(x_0, y_0)}{\Delta x}$$

$$\frac{\partial f}{\partial x} = \lim_{\Delta x \rightarrow 0} \frac{f(x + \Delta x, y) - f(x, y)}{\Delta x} = f_x \quad \frac{\partial f}{\partial y} = \lim_{\Delta y \rightarrow 0} \frac{f(x, y + \Delta y) - f(x, y)}{\Delta y} = f_y$$

Approximation:

If we change  $x \rightarrow x + \Delta x$ ,  $y \rightarrow y + \Delta y$ ,  $z = f(x, y)$  then  $\Delta z \approx f_x \Delta x + f_y \Delta y$

Tangent plane



$$L_1 = \begin{cases} z = z_0 + a(x - x_0) & \frac{\partial f}{\partial x}(x_0, y_0) = a \\ y = y_0 \end{cases}$$

$$L_2 = \begin{cases} z = z_0 + b(y - y_0) & \frac{\partial f}{\partial y}(x_0, y_0) = b \\ x = x_0 \end{cases}$$

$$\text{plane: } z = z_0 + a(x - x_0) + b(y - y_0)$$

Application. Optimization problems

At a [local] min or max:  $\frac{\partial f}{\partial x}(x_0, y_0) = \frac{\partial f}{\partial y}(x_0, y_0) = 0$  tangent plane is horizontal

Def:  $(x_0, y_0)$  is a critical point if  $f_x(x_0, y_0) = 0$  and  $f_y(x_0, y_0) = 0$

$$\text{ex: } f(x, y) = x^2 - 2xy + 3y^2 + 2x - 2y$$

$$\begin{cases} f_x = 2x - 2y + 2 = 0 \\ f_y = -2x + 6y - 2 = 0 \end{cases} \Rightarrow \begin{cases} x = -1 \\ y = 0 \end{cases} \text{ critical point } (x, y) = (-1, 0)$$

## Lecture 8 second derivative

critical point  $\begin{cases} \text{local max} \\ \text{local min} \\ \text{saddle} \end{cases}$  global max/min: either critical point or boundary

ex.  $w = ax^2 + bxy + cy^2$

$$w = \frac{1}{4a} [4a^2 (x + \frac{b}{2a}y)^2 + (4ac - b^2)y^2]$$

3 cases: (1)  $4ac - b^2 < 0 \Rightarrow$  saddle point

(2)  $4ac - b^2 = 0 \quad w = x^2$

(3)  $4ac - b^2 > 0 \quad \begin{array}{l} \text{if } a > 0, \text{ minimum} \\ \text{if } a < 0, \text{ maximum} \end{array}$

In general: look at second derivative

$$\frac{\partial^2 f}{\partial x^2} = f_{xx} \quad f_{xy} = \frac{\partial^2 f}{\partial x \partial y} = \frac{\partial^2 f}{\partial y \partial x} = f_{yx} \quad \frac{\partial^2 f}{\partial y^2} = f_{yy}$$

second derivative test

At a critical point  $(x_0, y_0)$  of  $f$

$$\text{let } A = f_{xx}(x_0, y_0), B = f_{xy}(x_0, y_0), C = f_{yy}(x_0, y_0)$$

If  $AC - B^2 > 0$  and  $A > 0$ ,  $f(x_0, y_0)$  is a (local) minimum

If  $AC - B^2 > 0$  and  $A < 0$ , (local) maximum

If  $AC - B^2 < 0$  saddle

If  $AC - B^2 = 0$  can't conclude

proof: quadratic approximation

$$\begin{aligned} \Delta f &= f_x(x - x_0) + f_y(y - y_0) + \frac{1}{2} f_{xx}(x - x_0)^2 + f_{xy}(x - x_0)(y - y_0) + \frac{1}{2} f_{yy}(y - y_0)^2 \\ &= \frac{1}{2} f_{xx}(x_0, y_0)(x - x_0)^2 + f_{xy}(x_0, y_0)(x - x_0)(y - y_0) + f_{yy}(x_0, y_0)(y - y_0)^2 \end{aligned}$$

In degenerate case, depends on higher derivative

## Lecture 9 Least Square

$$y = \hat{a}x + \hat{b}$$

deviation for each point:  $y_i - (\hat{a}x_i + \hat{b})$

$$\text{Minimise } P(a, b) = \sum_{i=1}^n [y_i - (ax_i + b)]^2 = \sum_{i=1}^n [y_i^2 + (ax_i + b)^2 - 2y_i(ax_i + b)]$$

$$\frac{\partial P}{\partial a} = \sum_{i=1}^n [2(ax_i + b) \cdot x_i - 2x_i y_i] = 0 \Leftrightarrow a \sum x_i^2 + b \sum x_i = \sum x_i y_i$$

$$\frac{\partial P}{\partial b} = \sum_{i=1}^n [2(ax_i + b) - 2y_i] = 0 \Leftrightarrow a \sum x_i + b n = \sum y_i$$

solve for  $(a, b)$

$$\left\{ \begin{array}{l} \hat{a} = \frac{n \sum x_i y_i - \sum x_i \sum y_i}{n \sum x_i^2 - (\sum x_i)^2} \\ \hat{b} = \frac{\sum y_i - a \sum x_i}{n} \end{array} \right.$$

## Lecture 11 Differential

Total differential

$$f(x,y,z) \quad df = f_x dx + f_y dy + f_z dz = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy + \frac{\partial f}{\partial z} dz$$

Important:  $df$  is NOT  $\Delta f$

can do ① encode how change in  $x, y, z$  affect  $f$

② placeholder for small variation  $\Delta x, \Delta y, \Delta z$

to get approximation formula  $\Delta f \approx f_x \Delta x + f_y \Delta y + f_z \Delta z$

③ divide by something like  $\Delta t$  to get a rate of change when  $x(t), y(t), z(t)$

$$\frac{df}{dt} = f_x \frac{dx}{dt} + f_y \frac{dy}{dt} + f_z \frac{dz}{dt}$$

$$\text{ex } W = x^2 y + z, \quad x = t, \quad y = e^t, \quad z = \sin t$$

$$\frac{dw}{dt} = 2xy \cdot \frac{dx}{dt} + x^2 \cdot \frac{dy}{dt} + 1 \cdot \frac{dz}{dt}$$

$$= 2te^t + t^2 e^t + \cos t = (t^2 + 2t)e^t + \cos t$$

Prove chain rule with more variables

$$W = f(x, y) \quad x = x(u, v) \quad y = y(u, v)$$

$$W = f(x(u, v), y(u, v)), \quad \text{what about } \frac{\partial w}{\partial x}, \frac{\partial w}{\partial y}$$

$$dw = f_x dx + f_y dy = f_x(x_u du + x_v dv) + f_y(y_u du + y_v dv)$$

$$= (\underbrace{f_x x_u + f_y y_u}_{\text{has to be } \frac{\partial w}{\partial u}}) du + (\underbrace{f_x x_v + f_y y_v}_{\text{has to be } \frac{\partial w}{\partial v}}) dv$$

$$\frac{\partial f}{\partial u} = \frac{\partial f}{\partial x} \cdot \frac{\partial x}{\partial u} + \frac{\partial f}{\partial y} \cdot \frac{\partial y}{\partial u}$$

$$\frac{\partial f}{\partial v} = \frac{\partial f}{\partial x} \cdot \frac{\partial x}{\partial v} + \frac{\partial f}{\partial y} \cdot \frac{\partial y}{\partial v}$$

# Lecture 12 Gradient

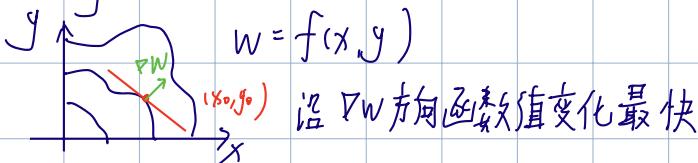
$$w = f(x, y, z)$$

$\nabla w = \langle w_x, w_y, w_z \rangle$  gradient of  $w$  at some point  $(x, y, z)$

$$\frac{d\vec{r}}{dt} = \left\langle \frac{dx}{dt}, \frac{dy}{dt}, \frac{dz}{dt} \right\rangle$$

$$\frac{dw}{dt} = \nabla w \cdot \frac{d\vec{r}}{dt}$$

Theory:  $\nabla w \perp$  level surface ( $w = \text{constant}$ )



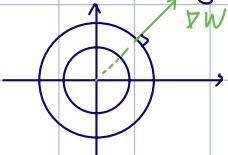
$$\text{ex1. } w = a_1 x + a_2 y + a_3 z$$

$$\nabla w = (a_1, a_2, a_3)$$

level surface:  $a_1 x + a_2 y + a_3 z = C$  plane with normal vector  $\nabla w$

ex2.  $w = x^2 + y^2$  level curve  $w = C$  is a circle  $x^2 + y^2 = C$

$$\nabla w = (2x, 2y)$$



$\nabla w$  always points at higher value of a function

Proof: Take a curve  $\vec{r} = \vec{r}(t)$  that stays on the level  $w = C$

$w(x, y, z) = C$  Take a motion on the surface  $w(x, y, z) = C$

$v = \frac{d\vec{r}}{dt}$  is tangent to the plane  $w(x, y, z) = C$

By chain rule:  $\frac{dw}{dt} = \nabla w \cdot \frac{d\vec{r}}{dt} = \nabla w \cdot \vec{v} = 0$  because  $w(t) = C = \text{constant}$

so  $\nabla w \perp \vec{v}$ , This is true for any motion on  $w = C$

$\vec{v}$  can be any vector tangent to the surface

so  $\nabla w$  is perpendicular to the tangent plane to the level

Applications find the tangent plane to surface  $x^2 + y^2 - z^2 = 4$  at  $(2, 1, 1)$ ?

Level set  $w = 4$  when  $w = x^2 + y^2 - z^2$

gradient  $\nabla w = (2x, 2y, -2z) = (4, 2, -2)$ , which is the normal vector to the plane  $4(x-2) + 2(y-1) - 2(z-1) = 0 \Rightarrow 4x + 2y - 2z = 8$

Another way:  $dw = 2x dx + 2y dy - 2z dz = 4 dx + 2 dy - 2 dz$  at  $(2, 1, 1)$

$$dw \approx 4dx + 2dy - 2dz$$

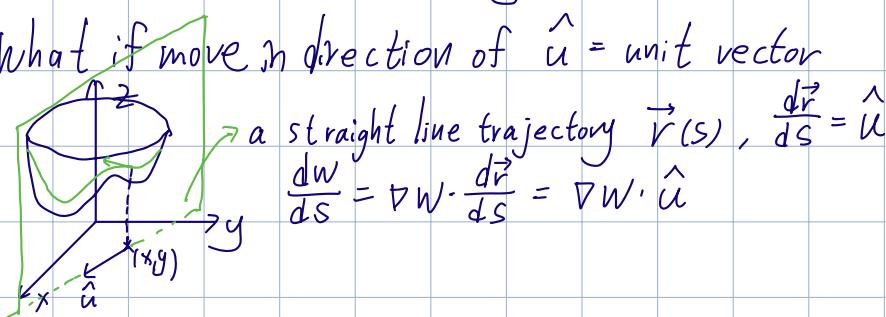
when  $dw = 0$ ; its tangent plane:  $4dx + 2dy - 2dz = 0$

$$4(x-2) + 2(y-1) - 2(z-1) = 0$$

## Directional derivatives

$w = w(x, y) \rightsquigarrow$  know  $\frac{\partial w}{\partial x}, \frac{\partial w}{\partial y}$

What if move in direction of  $\hat{u}$  = unit vector



Def: If  $\hat{u} = \langle a, b \rangle$  (unit vector)

$$\begin{cases} x(s) = x_0 + a s \\ y(s) = y_0 + b s \end{cases}$$

$$\frac{dw}{ds}|_{\hat{u}} = \nabla w \cdot \hat{u} \quad \text{components of } \nabla w \text{ in direction of } \hat{u}$$

## Directional derivative

Geometric view: slice the graph by the plane of the unit vector, slope =  $\frac{dw}{ds}|_{\hat{u}}$

$$\frac{dw}{ds} \Big|_{\hat{u}} = \nabla w \cdot \hat{u} = |\nabla w| \cdot |\hat{u}| \cdot \cos \theta$$

$= |\nabla w| \cdot \cos \theta$

A diagram shows a horizontal vector labeled  $\nabla w$  pointing to the right. A second vector, labeled  $\hat{u}$ , originates from the same point and makes an angle  $\theta$  with the  $\nabla w$  vector. The length of  $\hat{u}$  is indicated by a vertical tick mark.

$\Rightarrow$  be maximal when  $\cos \theta = 1 \Rightarrow \hat{u} = \operatorname{dir}(\nabla w)$

Conclusion:  $\nabla w = \operatorname{dir}$  of fastest increase of  $w$

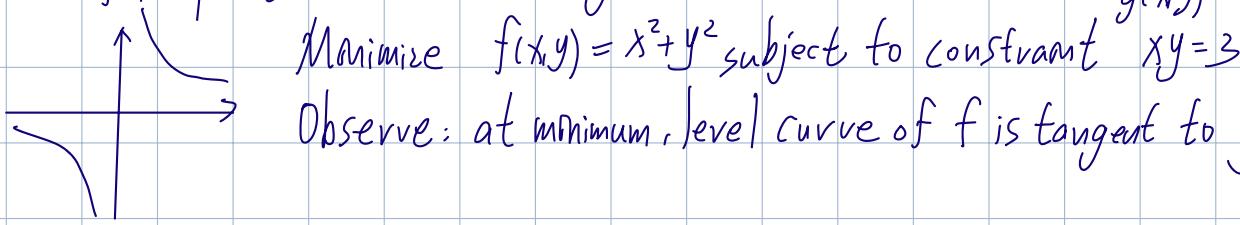
$$|\nabla w| = \frac{dw}{ds} \Big|_{\hat{u}} = \operatorname{dir}(\nabla w)$$

minima when  $\cos \theta = -1 \quad \hat{u} = \operatorname{dir}(\nabla w)$

when  $\frac{dw}{ds} \Big|_{\hat{u}} = 0 \quad \cos \theta = 0 \quad \theta = 90^\circ \quad \hat{u} \perp \nabla w \Leftrightarrow \hat{u} \text{ tangent to level}$

## Lecture 13 Lagrange multipliers

min/max a function  $f(x,y,z)$  where  $x,y,z$  are not independent,  $g(x,y,z) = c$   
ex: find point closest to origin on  $xy=3$



Observe: at minimum, level curve of  $f$  is tangent to  $g=3$

When  $f(x,y)$ 's level curve is tangent to  $g(x,y)$ 's level

curve, normal vectors parallel

$$f = a \quad \nabla f \parallel \nabla g \text{ so } \nabla f = \lambda \nabla g$$

$$\Rightarrow \begin{cases} f_x = \lambda g_x \\ f_y = \lambda g_y \\ xy = 3 \end{cases}$$

from  $\nabla f = \lambda \nabla g$

from the constraint

Why is this method valid?

At constraint min/max, many directions along  $g=c$ , the rate of change of  $f$  must be 0

For any  $\hat{u}$  tangent to  $g=c$ , we must have  $\frac{df}{ds}|_{\hat{u}} = 0$

$\nabla f \cdot \hat{u} = 0$ , so any such  $\hat{u}$  is  $\perp \nabla f$ , so  $\nabla f \perp$  level set of  $g$

know  $\nabla g \perp$  level set of  $g$ , so  $\nabla f \parallel \nabla g$

WARNING: method don't tell whether it's maximum or minimum (or a saddle)

CAN'T use second derivative test

# Lecture 14 Non-independent variables

$f(x, y, z)$  where  $g(x, y, z) = C$

then  $z = z(x, y)$   $\frac{\partial z}{\partial x}$ ?  $\frac{\partial z}{\partial y}$ ?

ex  $x^2 + yz + z^3 = 8$  at  $(2, 3, 1)$

Take differential:  $2x dx + z dy + (y + 3z^2) dz = 0$

at  $(2, 3, 1)$   $4dx + dy + 6dz = 0$

If we view  $z = z(x, y)$   $dz = -\frac{1}{6}(4dx + dy)$

$$\frac{\partial z}{\partial x} = -\frac{z}{3}/1 = -\frac{z}{3} \quad \frac{\partial z}{\partial y} = -\frac{1}{6}/1 = -\frac{1}{6}$$

( $y$  constant  $dy = 0$ ) ( $x$  constant  $dx = 0$ )

In general:

$g(x, y, z) = C$  then  $dg = g_x dx + g_y dy + g_z dz = 0$

Solve for  $dz$ :  $dz = -\frac{g_x}{g_z} dx - \frac{g_y}{g_z} dy$

so for  $\frac{\partial z}{\partial x}$ , set  $dy = 0$   $dz = -\frac{g_x}{g_z} dx \quad \frac{\partial z}{\partial x} = \frac{-g_x}{g_z}$

ex.  $f(x, y) = x + y \quad \frac{\partial f}{\partial x} = 1$

$x = u$   $y = u + v$ , then  $f = 2u + v \quad \frac{\partial f}{\partial u} = 2$

$x = u$ , but  $\frac{\partial f}{\partial x} \neq \frac{\partial f}{\partial u}$ , because  $\frac{\partial f}{\partial x}$  means keeping  $y$  constant,  $\frac{\partial f}{\partial u}$  means keeping  $v$  constant

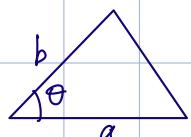
Need clearer Notations

$(\frac{\partial f}{\partial x})_y$  = keep  $y$  constant

$(\frac{\partial f}{\partial u})_v$  = keep  $v$  constant

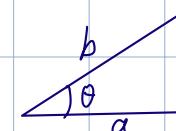
$$\text{so } \underbrace{(\frac{\partial f}{\partial x})_y}_1 \neq \underbrace{(\frac{\partial f}{\partial x})_v}_2 = \underbrace{(\frac{\partial f}{\partial u})_v}_2$$

ex. area of a triangle



$$A = \frac{1}{2}ab \sin \theta$$

Assume it's a right triangle



$$a = b \cos \theta$$

constraint

Rate of  $A$  respect to  $\theta$

(1) treat  $a, b, \theta$  as independent  $\frac{\partial A}{\partial \theta} = (\frac{\partial A}{\partial \theta})_{a,b} = \frac{1}{2}ab \cos \theta$  loss the constraint

(2) keep  $a$  constant  $b = b(a, \theta) (= \frac{a}{\cos \theta})$  to keep right angle  $(\frac{\partial A}{\partial \theta})_a$

(3) keep  $b$  constant,  $a = a(b, \theta) \quad (\frac{\partial A}{\partial \theta})_b$

Compute  $(\frac{\partial A}{\partial \theta})_a$

Method 0: solve for  $b$  then substitute

$$= \frac{\partial}{\partial \theta} \left( \frac{1}{2} a \cdot \frac{a}{\cos \theta} \cdot \sin \theta \right) = \frac{1}{2} a^2 \sec^2 \theta$$

2 systematic methods

Method 1: differentials

keep  $a$  fixed:  $da=0$

constraint  $a=b \cos \theta$   $da = \cos \theta db - b \sin \theta d\theta = 0$

$db = b \tan \theta d\theta$  (To find when  $\theta$  change, how  $b$  change)

function  $A = \frac{1}{2} ab \sin \theta$

$$\begin{aligned} dA &= \frac{1}{2} b \sin \theta da + \frac{1}{2} a \sin \theta db + \frac{1}{2} ab \cos \theta d\theta \\ &= \frac{1}{2} a \sin \theta \cdot b \tan \theta d\theta + \frac{1}{2} ab \cos \theta d\theta = (\frac{1}{2} ab \sin \theta \tan \theta + \frac{1}{2} ab \cos \theta) d\theta = \frac{1}{2} ab \sec \theta d\theta \end{aligned}$$

$$\text{so } (\frac{\partial A}{\partial \theta})_a = \frac{1}{2} ab \sec \theta$$

Summary: (1) write  $dA$  in terms of  $da, db, d\theta$

(2) set  $da = 0$

⊗ (3) differentiate constraint  $\Rightarrow$  solve for  $db$  in terms of  $d\theta$

) plug in

Method 2: Chain Rule  $(\frac{\partial}{\partial \theta})_a$  in formula for  $A$

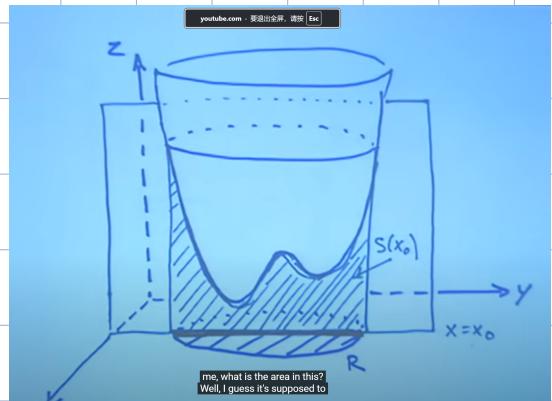
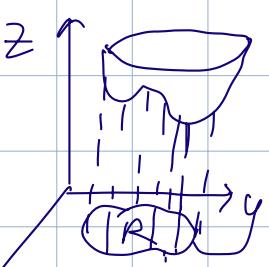
$$(\frac{\partial A}{\partial \theta})_a = A_\theta (\underbrace{\frac{\partial \theta}{\partial \theta}}_1)_a + A_a (\underbrace{\frac{\partial a}{\partial \theta}}_0)_a + A_b (\underbrace{\frac{\partial b}{\partial \theta}}_{\text{use constraint}})_a$$

# Lecture 15 Double integral

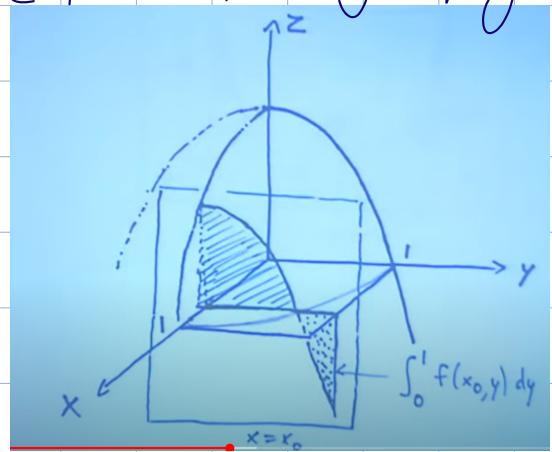
one-variable integral: area of graph

Double integral: volume below the graph

over a region  $R$  in  $xy$  plane  $\iint_R f(x,y) dA$



ex1.  $z = 1 - x^2 - y^2$  region  $0 \leq x \leq 1$ ,  $0 \leq y \leq 1$



move a plane from one axis, take slices  
add all the  $A \cdot dx$

$$V = \int_{x_{\min}}^{x_{\max}} S(x) dx$$

$$\text{For given } x, S(x) = \int_{y_{\min}(x)}^{y_{\max}(x)} f(x,y) dy$$

$$\iint_R f(x,y) dA = \int_{x_{\min}}^{x_{\max}} \left[ \int_{y_{\min}(x)}^{y_{\max}(x)} f(x,y) dy \right] dx$$

$$\begin{aligned} & \int_0^1 \int_0^1 (1 - x^2 - y^2) dy dx \\ &= \int_0^1 \left[ (1 - x^2)y - \frac{1}{3}y^3 \right]_0^1 dx \\ &= \int_0^1 \left( \frac{2}{3} - x^2 \right) dx \\ &= \left( \frac{2}{3}x - \frac{1}{3}x^3 \right) \Big|_0^1 \\ &= \frac{1}{3} \\ & dA = dy dx \end{aligned}$$

ex2: integral in such  $R$

$$\begin{aligned} & \int_0^1 \int_0^{\sqrt{1-x^2}} (1 - x^2 - y^2) dy dx = \int_0^1 \left[ (1 - x^2)\sqrt{1-x^2} - \frac{1}{3}(1 - x^2)\sqrt{1-x^2} \right] dx \\ &= \int_0^1 \frac{2}{3}(1 - x^2)^{\frac{3}{2}} dx = \frac{2}{3} \int_0^{\pi/2} \cos^4 \theta d\theta \\ &= \frac{2}{3} \cdot \frac{3}{16} \pi = \frac{1}{8} \pi \end{aligned}$$

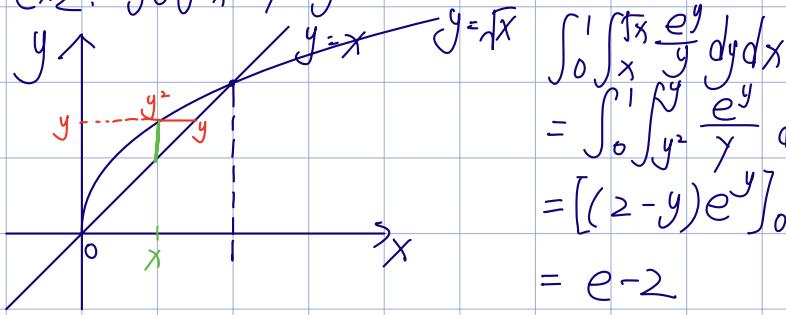
Easier in Polar coordinates



## Exchanging order

$$\text{ex1. } \int_0^1 \int_0^2 dx dy = \int_0^2 \int_0^1 dy dx$$

$$\text{ex2. } \int_0^1 \int_x^2 \frac{e^y}{y} dy dx$$

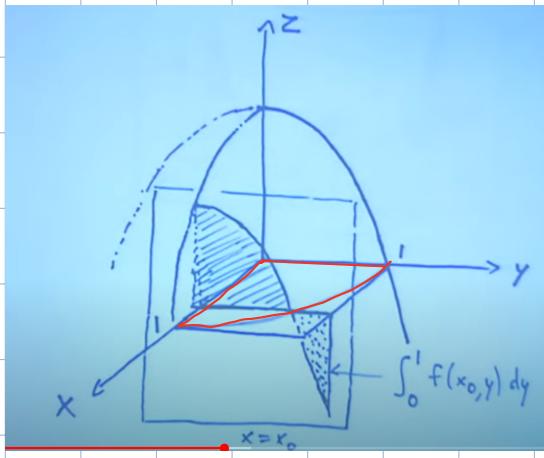


$$\begin{aligned} & \int_0^1 \int_x^2 \frac{e^y}{y} dy dx \\ &= \int_0^1 \int_{y^2}^y \frac{e^y}{y} dy dx = \int_0^1 (1-y) e^y dy \\ &= [(2-y)e^y]_0^1 \\ &= e-2 \end{aligned}$$

$$\bar{x} = \frac{1}{\text{Mass}} \iint x f(\theta, r) dy dx$$

$$\bar{y} = \frac{1}{\text{Mass}} \iint y f(\theta, r) dy dx$$

# Lecture 17 Polar Coordinates



$x = r \cos \theta, y = r \sin \theta$

$\Delta A \approx \Delta r \cdot r \Delta \theta$

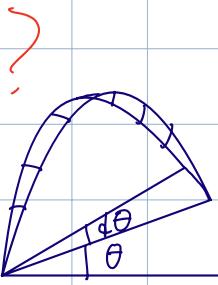
$dA = r dr d\theta$

$$\frac{1}{2} \Delta \theta ((r + \Delta r)^2 - r^2)$$

$$= \Delta \theta r dr$$

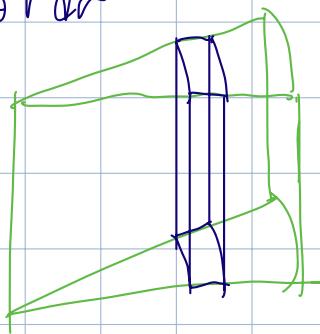
$$\begin{aligned} & \int_0^{\pi/2} \int_0^1 f(\theta, r) r dr d\theta \\ &= \int_0^{\pi/2} \int_0^1 (1-r^2) r dr d\theta \\ &= \int_0^{\pi/2} \left( \frac{1}{2}r - \frac{1}{4}r^4 \right) \Big|_0^1 d\theta \\ &= \int_0^{\pi/2} \frac{1}{4} d\theta = \frac{\pi}{8} \end{aligned}$$

???



$$\iint f(\theta, r) dr \cdot r d\theta \cdot \frac{1}{2}$$

面積 A  
体積 dV



$$\iint f(\theta, r) dr \cdot \frac{1}{2} r d\theta$$

S  
dV

## Application

(1) convert single integral to double integral

$y$   $\text{Area} = \iint_R 1 \cdot dA$

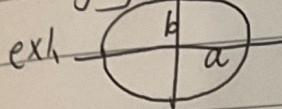
(2) Average value of  $f = \bar{f} = \frac{1}{\text{Area}(R)} \iint_R f dA$

weighted average of  $f$  with density  $\delta$ :  $\bar{f} = \frac{1}{\text{Mass}(R)} \iint_R f \delta dA$

(3) Center of mass of a (planar) object (with density  $\delta$ )

$y$   $(\bar{x}, \bar{y})$   $\bar{x} = \frac{1}{\text{Mass}} \iint_R x \delta dA, \bar{y} = \frac{1}{\text{Mass}} \iint_R y \delta dA$

changing variables in  $\iint \frac{x}{a} + \frac{y}{b} \leq 1$



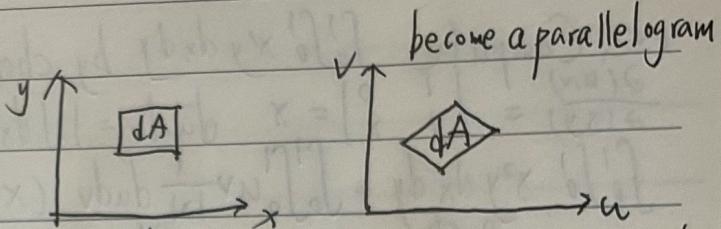
$$\iint_{\frac{x}{a} + \frac{y}{b} \leq 1} dx dy = ab \iint_{u+v \leq 1} du dv = \pi ab$$

set  $\frac{x}{a} = u$   $\frac{y}{b} = v$

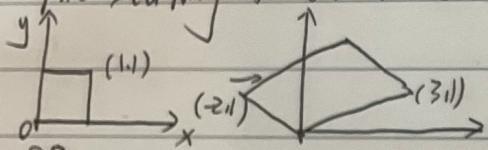
In general: finding scaling factor between  $dx dy \leftrightarrow du dv$

$$\begin{cases} u = 3x - 2y \\ v = x + y \end{cases}$$

$$dA = dx dy \text{ and } dA' = du dv$$



The scaling factor here doesn't depend on choice of rectangle



$$A' = \begin{vmatrix} 3 & 1 \\ -2 & 1 \end{vmatrix} = 5$$

$$\text{so } dA' = 5dA \quad du dv = 5 dx dy$$

$$\iint f(x,y) dx dy = \iint g(u,v) \frac{1}{5} du dv, \text{ bound also needs change}$$

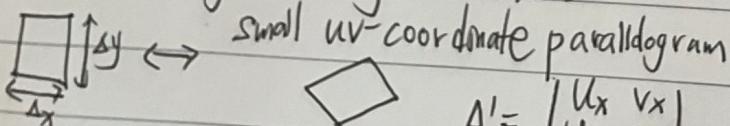
↑ Only for linear transformation

General case:  $u = u(x, y)$   $v = v(x, y)$

$$\Delta u \approx du \approx u_x \cdot \Delta x + u_y \cdot \Delta y$$

$$\Delta v \approx dv \approx v_x \cdot \Delta x + v_y \cdot \Delta y$$

Small rectangle in x-y coordinates



$$A' = \begin{vmatrix} u_x & v_x \\ u_y & v_y \end{vmatrix}$$

can be seen as linear transformation, which changing scalar depends on  $u_x, u_y, v_x, v_y (x_0, y_0)$

$$dA' = \begin{vmatrix} u_x & v_x \\ u_y & v_y \end{vmatrix} dA \quad \text{or} \quad dA' = \begin{vmatrix} u_x & u_y \\ v_x & v_y \end{vmatrix} dA$$

$$\text{Jacobian} : J = \frac{\partial(u, v)}{\partial(x, y)} = \begin{vmatrix} u_x & u_y \\ v_x & v_y \end{vmatrix}$$

$$du dv = |J| dx dy = \left| \begin{vmatrix} u_x & u_y \\ v_x & v_y \end{vmatrix} \right| dx dy$$

ex1 Polar coordinate

$$x = r \cos \theta \quad y = r \sin \theta$$

$$\frac{\partial(x, y)}{\partial(r, \theta)} = \begin{vmatrix} x_r & x_\theta \\ y_r & y_\theta \end{vmatrix} = \begin{vmatrix} \cos \theta & -r \sin \theta \\ \sin \theta & r \cos \theta \end{vmatrix} = r^2$$

$$dx dy = |r| dr d\theta = r dr d\theta$$

ex2. Compute  $\int_0^1 \int_0^1 x^2 y dx dy$  by changing to  $u=x$   $v=xy$

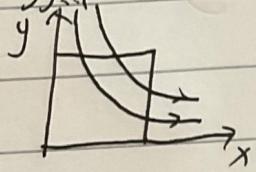
$$\frac{\partial(u, v)}{\partial(x, y)} = \begin{vmatrix} 1 & 0 \\ y & x \end{vmatrix} = x \quad du dv = |x| dx dy = x dx dy$$

$$\int_0^1 \int_0^1 x^2 y dx dy = \int_0^1 \int_0^1 uv \frac{1}{x} du dv \quad (\times)$$

$$= \int_0^1 \int_0^1 v du dv = \int_0^1 v dv = \frac{1}{2} \quad (\times)$$

For bounds

$\iint_{\text{region}} v du dv$  or  $dv du$ ?



$$\iint v du dv$$

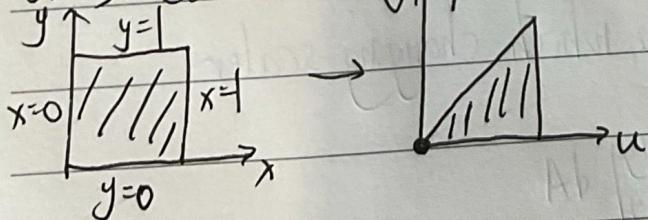
u change, v constant  
 $xy = C$

when v is constant, find scope of u

$$y=1 \quad v=x, \quad u=v \quad \int_v^1 v du$$

$$= \int_0^1 \int_v^1 v du dv$$

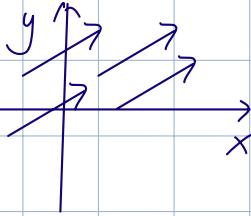
or switch to u-v picture



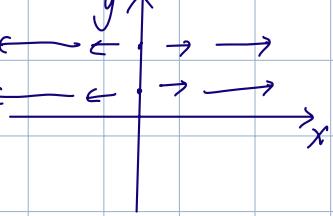
# Lecture 19 Vector fields

$\vec{F} = M\vec{i} + N\vec{j}$ ,  $M, N$  are functions of  $x, y$

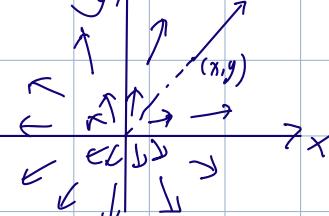
ex:  $\vec{F} = 2\vec{i} + \vec{j}$



$\vec{F} = x\vec{i}$



$\vec{F} = xy\vec{i} + y\vec{j}$

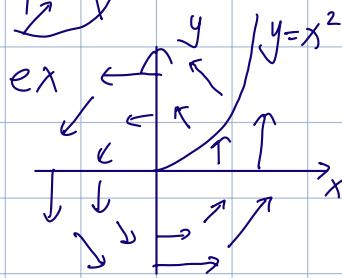


line integral

$$W = \vec{F} \cdot d\vec{r} \quad \text{Along a trajectory } C \quad \vec{F} = M\vec{i} + N\vec{j}$$



$$W = \int_C \vec{F} \cdot d\vec{r} = \int_{t_1}^{t_2} \vec{F} \cdot \frac{d\vec{r}}{dt} dt = \int_C M dx + N dy$$



$\vec{F} = -y\vec{i} + x\vec{j}$

$C: x = t$

$y = t^2 \quad (0 \leq t \leq 1)$

$$\begin{aligned} \int_C \vec{F} \cdot d\vec{r} &= \int_0^1 (-y, x) \cdot (1, 2t) dt \\ &= \int_0^1 (-t^2, t) \cdot (1, 2t) dt \\ &= \int_0^1 t^2 dt = \frac{1}{3} \end{aligned}$$

Special case, when  $\vec{F}$  is gradient of a function  $f(x, y)$

Fundamental theorem of Calculus for line integral

$$\int_C \nabla f \cdot d\vec{r} = f(P_1) - f(P_0)$$



proof:  $\int_C \nabla f \cdot d\vec{r} = \int_C f_x dx + f_y dy = \int_C df = f(P_1) - f(P_0)$

proof:  $\int_C \nabla f \cdot d\vec{r} = \int_C f_x dx + f_y dy \quad C: x = x(t), y = y(t)$

$$= \int_C \left( f_x \frac{dx}{dt} + f_y \frac{dy}{dt} \right) dt = \int_{t_0}^{t_1} \frac{df}{dt} dt = f(x(t_1), y(t_1)) \Big|_{t_0}^{t_1} = f(P_1) - f(P_0)$$

Only works if  $\vec{F}$  is a gradient field

(1) Path-independence  $\int_{C_1} \nabla f \cdot d\vec{r} = \int_{C_2} \nabla f \cdot d\vec{r}$  if  $C_1$  and  $C_2$  have same start/end points

$\Leftrightarrow$  (2)  $\vec{F}$  is a gradient field

$\Leftrightarrow$  (3)  $M dx + N dy$  is an exact differential (can be expressed in  $df$ )

## Lecture 2 | Exact differential

if  $\vec{F} = \nabla f$ ,  $M = f_x$   $N = f_y$ , then  $f_{xy} = f_{yx} \Rightarrow M_y = N_x$

Then: if  $\vec{F} = \langle M, N \rangle$  defined, differentiable everywhere

and  $M_y = N_x$ , then  $\vec{F}$  is a gradient field

ex.  $\vec{F} = -y\hat{i} + x\hat{j}$

$\frac{\partial M}{\partial y} = -1$   $\frac{\partial N}{\partial x} = 1$  are not the same, not a gradient field

ex.  $\vec{F} = (4x^2 + axy)\hat{i} + (3y^2 + 4x^2)\hat{j}$

$\frac{\partial M}{\partial y} = ax = \frac{\partial N}{\partial x} = 8x$   $a=8$

Then, how do we find the potential (only if  $M_y = N_x$ )

(1) Computing line integral

$$\int_C \vec{F} d\vec{r} = f(x_1, y_1) - f(0, 0) \text{ choose a constant}$$
$$\int_C \vec{F} d\vec{r} = (4x^2 + 8xy) dx + (3y^2 + 4x^2) dy$$
$$C_1: y=0 \quad dy=0 \quad \int_{C_1} \vec{F} d\vec{r} = \int_0^{x_1} 4x^2 dx = \frac{4}{3} x_1^3$$
$$C_2: y: 0 \rightarrow y_1 \quad x=x_1 \quad dx=0 \quad \int_{C_2} \vec{F} d\vec{r} = \int_0^{y_1} (3y^2 + 4x_1^2) dy = y_1^3 + 4x_1^2 y_1$$
$$f(x_1, y_1) = \frac{4}{3} x_1^3 + y_1^3 + 4x_1^2 y_1 + C \quad f(x, y) = \frac{4}{3} x^3 + y^3 + 4x^2 y + C$$

(2) Antiderivatives

Want to solve  $\begin{cases} f_x = 4x^2 + 8xy & \textcircled{1} \\ f_y = 3y^2 + 4x^2 & \textcircled{2} \end{cases}$

$\textcircled{1}: f = \frac{4}{3} x^3 + 4x^2 y + g(y)$

$\Rightarrow f_y = 4x^2 + g'(y) \quad \text{match with } \textcircled{2} \quad g'(y) = 3y^2 \quad g(y) = y^3 + C$

$f = \frac{4}{3} x^3 + 4x^2 y + y^3 + C$

$\vec{F}$  is a conservative field, then  $\oint_C \vec{F} d\vec{r} = 0$

Definition  $\text{curl}(\vec{F}) = Nx - My$  and  $Nx = My \Rightarrow \text{curl}(\vec{F}) = 0$

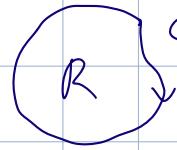
For a velocity field,  $\text{curl}$  measures rotation component of motion

ex.  $\vec{F} = \langle -y, x \rangle$   $\text{curl}(\vec{F}) = \frac{\partial}{\partial x}(x) - \frac{\partial}{\partial y}(-y) = 2$

$\text{curl}$  measures  $(2\pi)$  angular velocity of rotation component of velocity field

in a force field,  $\text{curl}$  measure torque  $\frac{\text{torque}}{\text{moment of inertia}} = \frac{d}{dt}(\text{angular velocity})$

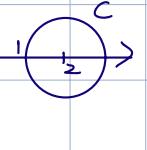
## Lecture 22 Green Theorem

 If  $C$  is a closed curve enclosing a region  $R$ , counter-clockwise

$\vec{F}$  vector field defined and differentiable in  $R$

$$\text{Then } \oint_C \vec{F} \cdot d\vec{r} = \iint_R \operatorname{curl}(\vec{F}) dA$$

$$\oint_C M dx + N dy = \iint_R (N_x - M_y) dA$$

ex. 

$$\begin{aligned} & \oint_C ye^{-x} dx + (\frac{1}{2}x^2 - e^{-x}) dy \\ &= \iint_R (x + e^{-x} - e^{-x}) dA \\ &= 2\pi \end{aligned}$$

Proof: Special case:  $\operatorname{curl}(\vec{F}) = 0$

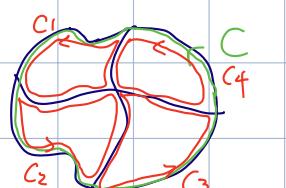
$$\oint_C \vec{F} \cdot d\vec{r} = \iint_R \operatorname{curl}(\vec{F}) dA = 0 \text{ if } \operatorname{curl}(\vec{F}) = 0$$

Proof:  $\oint_C M dx + N dy = \iint_R (N_x - M_y) dA$

Observe: first prove  $\oint_C M dx = \iint_R -M_y dA$  (special case when  $N=0$ )

Similarly:  $\oint_C N dy = \iint_R N_x dA$  ( $M=0$ )

Observe 2: decompose  $R$  into simple regions

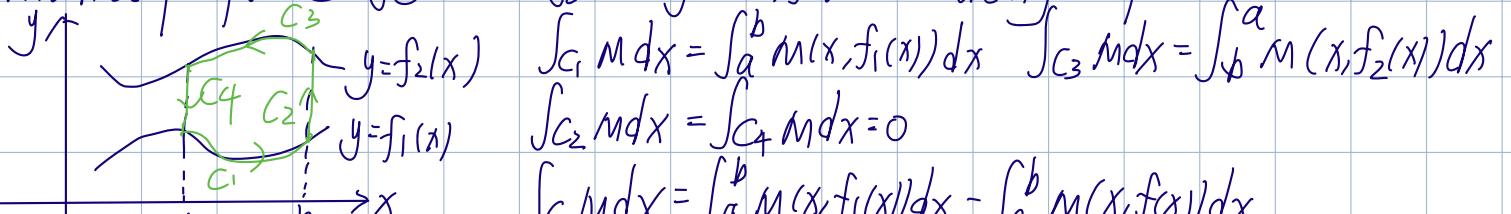


$$\begin{aligned} \oint_C M dx + N dy &= \sum_{i=1}^n \oint_{C_i} M dx + N dy \\ \iint_R (N_x - M_y) dA &= \sum_{i=1}^n \iint_{R_i} (N_x - M_y) dA \end{aligned}$$

(go twice along boundary, cancelled out)

Cut  $R$  into pieces that for  $a \leq x \leq b$ ,  $f_1(x) \leq y \leq f_2(x)$

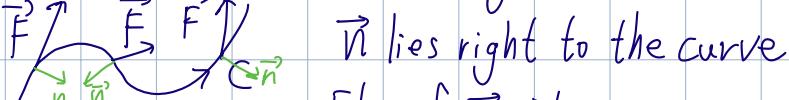
Main step: prove  $\oint_C M dx = \iint_R -M_y dx$  if  $R$  vertically simple



$$\iint_R -M_y dA = - \int_a^b \int_{f_1(x)}^{f_2(x)} \frac{\partial M}{\partial y} dy dx = - \int_a^b [M(x, f_2(x)) - M(x, f_1(x))] dx = \int_a^b [M(x, f_1(x)) - M(x, f_2(x))] dx$$

## Lecture 23 Flux

Flux: another line integral:  $\int_C \vec{F} \cdot \hat{n} \cdot d\vec{s}$



Flux:  $\int_C \vec{F} \cdot \hat{n} \cdot d\vec{s}$  measure normal component of  $\vec{F}$

Interpretation: For  $\vec{F}$  a velocity field, Flux measure how much fluid passes through  $C$

Calculation:  $d\vec{r} = \hat{T} d\vec{s} = \langle dx, dy \rangle$

$\hat{n}$  is  $\hat{T}$  rotate  $90^\circ$  clockwise:  $\hat{n} d\vec{s} = \langle dy, -dx \rangle$

$$\text{if } \vec{F} = \langle P, Q \rangle \quad \int_C \vec{F} \cdot \hat{n} \cdot d\vec{s} = \int_C \langle P, Q \rangle \cdot \langle dy, -dx \rangle = \int_C -Q dx + P dy$$

Green Theorem for flux

If  $C$  encloses a region  $R$  counterclockwise and  $\vec{F} = \langle P, Q \rangle$  defined in  $R$   
then  $\int_C \vec{F} \cdot \hat{n} \cdot d\vec{s} = \iint_R \operatorname{div} \vec{F} dA$  (divergence of  $\vec{F}$ )

$$\operatorname{div} \langle P, Q \rangle = P_x + Q_y$$

$$\int_C -Q dx + P dy = \iint_R (P_x + Q_y) dA \quad \text{the same as Green Theorem}$$

$$\text{ex. } \vec{F} = x\hat{i} + y\hat{j} \quad C = \text{circle of } r=a$$

$$\operatorname{div} \vec{F} = \frac{\partial}{\partial y}(y) + \frac{\partial}{\partial x}(x) = 2$$

$$\int_C \vec{F} \cdot \hat{n} \cdot d\vec{s} = \iint_R 2 dA = 2\pi a^2$$

Interpretation

(1) how much the flow is "expanding"

(2) the source rate = amount of fluid added to the system per unit time and area

line integral:  $\int_C \vec{F} \cdot d\vec{r} = \int_C M dx + N dy$

line integral Flux:  $\int_C \vec{F} \cdot \hat{n} \cdot d\vec{s} = \int_C -Q dx + P dy$

$\operatorname{curl} \vec{F} = N_x - M_y \quad \int_C \vec{F} \cdot d\vec{r} = \iint_R (N_x - M_y) dA$

$\operatorname{div} \vec{F} = P_x + Q_y \quad \int_C \vec{F} \cdot \hat{n} \cdot d\vec{s} = \iint_R (P_x + Q_y) dA$

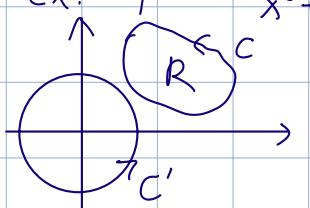
$\langle dx, dy \rangle \cdot \hat{T} \cdot d\vec{s}$

$\langle dy, -dx \rangle \cdot \hat{n} \cdot d\vec{s}$

More validity of Green's Theorem

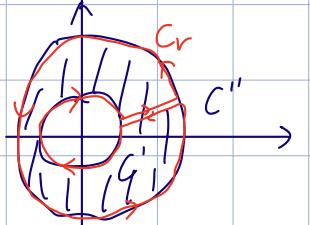
Only work if  $\vec{F}$  (and derivative) defined everywhere

ex.  $\vec{F} = \frac{-y\hat{i} + x\hat{j}}{x^2 + y^2}$  For not  $x=y=0$ ,  $\text{curl } \vec{F} = 0$



$\oint_C \vec{F} d\vec{r} = \iint_R \text{curl } \vec{F} dA = 0$

$\oint_{C'} \vec{F} d\vec{r} = ?$  can't use Green theorem directly

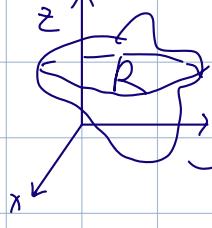


$$\oint_{C''} \vec{F} d\vec{r} - \oint_{C'} \vec{F} d\vec{r} = \iint_R \text{curl } \vec{F} dA$$

take line integral for  $C_r$  to prove

If  $\text{curl } \vec{F} = 0$  and domain where  $\vec{F}$  defined is simply connected,  $\vec{F}$  is conservative and is a gradient

# Lecture 25 Triple Integrals



$$\iiint_R f(x, y, z) dz dy dx$$

ex. region between  $z = x^2 + y^2$   $z = 4 - x^2 - y^2$

$$\begin{aligned} \text{volume} &= \iiint_R dV = \int \int \int_{x^2+y^2}^{4-x^2-y^2} dz dy dx \\ &= \int_{-12}^{12} \int_{-\sqrt{12-x^2}}^{\sqrt{12-x^2}} \int_{x^2+y^2}^{4-x^2-y^2} dz dy dx \\ &= \int_{-12}^{12} \int_{-\sqrt{12-x^2}}^{\sqrt{12-x^2}} (4-x^2-y^2) dy dx \end{aligned}$$

find whenever  $z_{\text{bottom}} < z_{\text{top}}$   $x^2 + y^2 \leq 4 - x^2 - y^2$ ,  $x^2 + y^2 \leq 2$

*project*

switch to polar coordinate

Better: Polar coordinates

$$\int_0^{2\pi} \int_0^{\sqrt{2}} \int_{r^2}^{4-r^2} dz \cdot r dr d\theta \quad \text{cylindrical coordinate}$$

$$\begin{aligned} &\begin{array}{l} z \uparrow \\ r \\ (r, \theta, z) \quad x = r \cos \theta \\ \theta \\ r \\ z \uparrow \\ y \\ y = r \sin \theta \end{array} \\ &dx dy dz = dV = r dr d\theta dz \end{aligned}$$

Average value of  $f(x, y, z)$  on  $x, y, z$

$$\bar{f} = \frac{1}{\text{Vol}(R)} \iiint_R f dV \quad \text{or with weighted } \bar{f} = \frac{1}{\text{Mass}(R)} \iiint_R f \delta dV$$

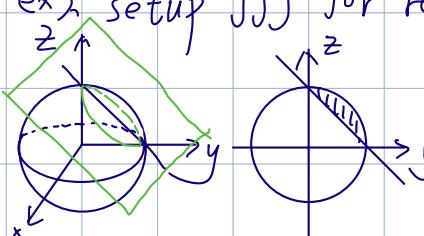
$$\text{Center of Mass } (\bar{x}, \bar{y}, \bar{z}), \quad \bar{x} = \frac{1}{\text{Mass}} \iiint_R x \delta dV \quad \bar{y} = \frac{1}{\text{Mass}} \iiint_R y \delta dV \quad \bar{z} = \frac{1}{\text{Mass}} \iiint_R z \delta dV$$

Moments of inertia

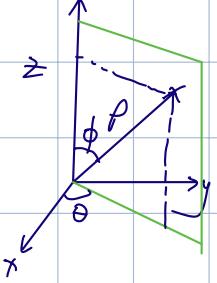
$$I = \iiint_R (\text{distance to the axis})^2 \delta dV \quad \text{ex. } I_z = \iiint_R r^2 \delta dV$$

ex3. setup  $\iiint$  for region  $z > 1-y$  inside unit ball

$$\begin{aligned} &\begin{array}{l} z \uparrow \\ \text{unit ball} \\ z \uparrow \\ y \\ y \end{array} \\ &= \int_0^1 \int_{\sqrt{1-y^2}}^{\sqrt{1-x^2-y^2}} \int_{-y}^{1-y} dz dx dy \\ &\quad (1-y) < \sqrt{1-x^2-y^2} \\ &\quad (1-y)^2 < 1-x^2-y^2 \end{aligned}$$



## Lecture 26 Spherical coordinate

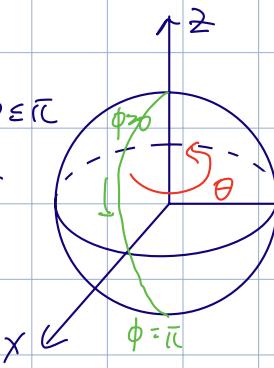


$\phi$ : go down from  $z$ -axis  $0 \leq \phi \leq \pi$

$\theta$ : counterclockwise from  $x$ -axis

$$z = \rho \cos \phi \quad \rho = \sqrt{r^2 + z^2} = \sqrt{x^2 + y^2 + z^2}$$

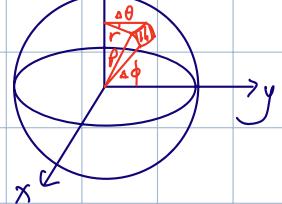
$$r = \rho \sin \phi \quad x = \rho \sin \phi \cos \theta \\ y = \rho \sin \phi \sin \theta$$



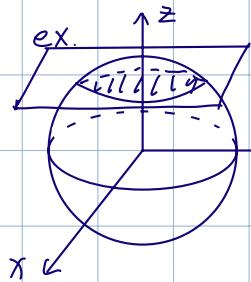
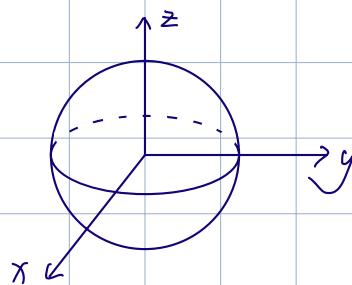
fix  $\rho = a$

$\phi \leftrightarrow$  latitude  
 $\theta \leftrightarrow$  longitude

Triple integral in spherical coordinate



$$dV = \rho d\phi \, r d\theta \, d\rho \\ = \rho \rho \sin \phi \, d\rho \, d\phi \, d\theta \\ = \rho^2 \sin \phi \, d\rho \, d\phi \, d\theta$$



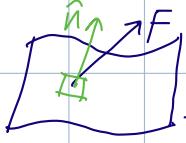
$$= \int_0^{2\pi} \int_0^{\pi/4} \int_{\frac{r}{2} \sec \theta}^1 (1 - \frac{r^2}{2} \sec \theta) \rho^2 \sin \phi \, d\rho \, d\phi \, d\theta \\ = \frac{2\pi}{3} - \frac{5\pi}{6\sqrt{2}}$$

ex.

# Lecture 27 Flux in space

flux through a surface; surface integral

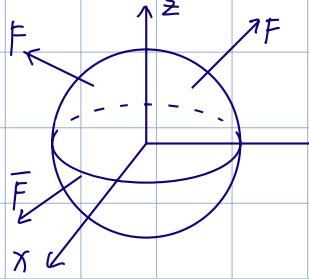
$\vec{F}$  vector field,  $S$  a surface



2 choices for  $\hat{n}$  (orientation)

$$\text{Flux} = \iint_S \vec{F} \cdot \hat{n} dS \quad \text{Notation } d\vec{S} = \hat{n} dS$$

ex1. Flux of  $\vec{F} = \langle x, y, z \rangle$  through sphere of radius  $a$  centered at  $O$



$$\hat{n} = \frac{1}{a} \langle x, y, z \rangle$$

$$\vec{F} \cdot \hat{n} = |\vec{F}| = a$$

$$\iint_S \vec{F} \cdot \hat{n} dS = \iint_S a dS = 4\pi a^3$$

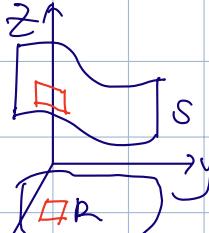
ex2. Same sphere  $\vec{F} = z \hat{k}$

$$\vec{F} \cdot \hat{n} = \langle 0, 0, z \rangle \cdot \langle x, y, z \rangle \cdot \frac{1}{a} = \frac{z^2}{a}$$

$$\iint_S \vec{F} \cdot \hat{n} dS = \iint_S \frac{z^2}{a} dS$$

$$dS = \rho^2 \sin\phi d\phi d\theta = a^2 \sin\phi d\phi d\theta \quad z = a \cos\phi$$

$$\iint_S \frac{z^2}{a} dS = \int_0^{2\pi} \int_0^\pi \frac{a^2 \cos^2\phi}{a} \cdot a^2 \sin\phi d\phi d\theta = \frac{4}{3}\pi a^3$$



graph  $z = f(x, y)$

$$\hat{n} dS = \pm \langle -f_x, -f_y, 1 \rangle \underbrace{dx dy}_{\text{Not } \hat{n}} \underbrace{dS}_{\text{Not } ds}$$

simplifies magically!

To set up bounds on  $\iint \cdots dx dy$ , look at shadow on  $x-y$  plane

$$\pm \vec{u} \times \vec{v} = \Delta S \cdot \hat{n}$$

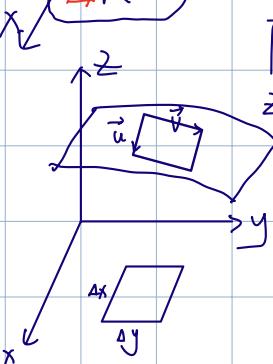
$$\approx f(x, y) + \Delta x \cdot f_x$$

$\vec{u}$ : from  $(x, y, f(x, y))$  to  $(x + \Delta x, y, f(x + \Delta x, y))$

$$\begin{aligned} \vec{u} &= \langle \Delta x, 0, f_x \Delta x \rangle & \vec{v} &= \langle 0, \Delta y, f_y \Delta y \rangle \\ &= \langle 1, 0, f_x \rangle \Delta x & &= \langle 0, 1, f_y \rangle \Delta y \end{aligned}$$

$$\hat{n} \Delta S = \vec{u} \times \vec{v} = \begin{vmatrix} i & j & k \\ 1 & 0 & f_x \\ 0 & 1 & f_y \end{vmatrix} \Delta x \Delta y = \langle -f_x, -f_y, 1 \rangle \Delta x \Delta y$$

$$\hat{n} dS = \pm \langle -f_x, -f_y, 1 \rangle dx dy$$



ex.  $\vec{F} = z\hat{k}$ ,  $z = x^2 + y^2$  above the unit circle

$$= \iint_{S} \langle 0, 0, z \rangle \cdot \langle -2x, -2y, 1 \rangle dy dx \quad \text{choose the unit vector upward}$$

$$= \int_{-1}^1 \int_{-\sqrt{1-x^2}}^{\sqrt{1-x^2}} x^2 + y^2 dy dx \quad \text{get rid of } z$$

$$= \int_0^{2\pi} \int_0^1 r^2 \cdot r dr d\theta = \int_0^{2\pi} \frac{1}{4} d\theta = \frac{\pi}{2}$$

More generally: given parametric description of  $S$

$$S: \begin{cases} x = x(u, v) \\ y = y(u, v) \\ z = z(u, v) \end{cases}$$

Sides:  $\frac{\partial \vec{r}}{\partial u} \cdot \Delta u = \left\langle \frac{\partial x}{\partial u}, \frac{\partial y}{\partial u}, \frac{\partial z}{\partial u} \right\rangle \Delta u$  and  $\frac{\partial \vec{r}}{\partial v} \cdot \Delta v$

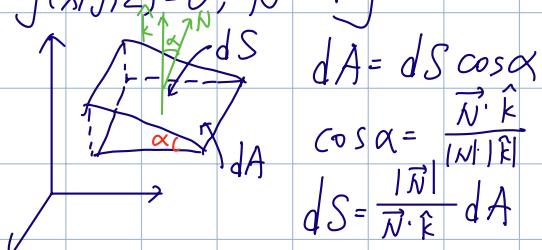
$$\hat{n} \Delta S = \left( \frac{\partial \vec{r}}{\partial u} \cdot \Delta u \right) \times \left( \frac{\partial \vec{r}}{\partial v} \cdot \Delta v \right) = \left( \frac{\partial \vec{r}}{\partial u} \times \frac{\partial \vec{r}}{\partial v} \right) du dv$$

$$\hat{n} dS = \pm \left( \frac{\partial \vec{r}}{\partial u} \times \frac{\partial \vec{r}}{\partial v} \right) du dv$$

$$\langle x, y, z \rangle = \vec{r} = \vec{r}(u, v)$$

If we know a normal vector  $\vec{N}$  (not necessarily unit)

$$g(x, y, z) = 0, \vec{N} = \nabla g$$



$$\text{ex. } z - f(x, y) = 0$$

$$\hat{n} dS = \frac{|\vec{N}| \cdot \vec{n}}{|\vec{N}| \cdot \vec{k}} dA = \pm \frac{\vec{N}}{|\vec{N}| \cdot \vec{k}} dA$$

$$\hat{n} dS = \pm \frac{\vec{N}}{|\vec{N}| \cdot \vec{k}} \cdot dx dy$$

$$n dS = \pm \frac{\vec{N}}{|\vec{N}| \cdot \vec{k}} dx dy$$

$$g = z - f(x, y) = 0 \quad \nabla g = \langle -f_x, -f_y, 1 \rangle$$

$$\pm \frac{\vec{N}}{|\vec{N}| \cdot \vec{k}} dx dy = \pm \langle -f_x, -f_y, 1 \rangle \cdot dx dy$$

The more general case, if  $g(x, y, z) = 0$  can't be solved as  $z = f(x, y)$

$$\text{use } \hat{n} dS = \pm \frac{\vec{N}}{|\vec{N}| \cdot \vec{k}} dx dy, \vec{N} = \nabla g$$

# Divergence Theorem (Gauss Theorem)

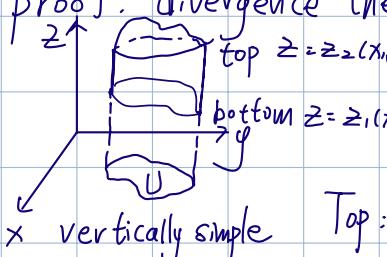
If  $S$  is a closed surface enclosing a space called  $D$ ,  $\hat{n}$  needs to be outward, and  $\vec{F}$  is defined and differentiable in  $D$

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_D \text{div } \vec{F} dV, \text{ where } \text{div} (P\hat{i} + Q\hat{j} + R\hat{k}) = P_x + Q_y + R_z$$

$\nabla$  notation  $\nabla$  "del" =  $\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \rangle$

$$\nabla \cdot \vec{F} = \langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \rangle \cdot \langle P, Q, R \rangle = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

proof: divergence theorem  $\Leftrightarrow \iint_S \langle 0, 0, R \rangle \cdot \hat{n} dS = \iiint_D R_z dV$ , sum up  $x, y, z$  components



$$\iiint_D R_z dV = \iint_U \left( \int_{z_1(x,y)}^{z_2(x,y)} R_z dz \right) dy dx = \iint_U [R(x,y, z_2(x,y)) - R(x,y, z_1(x,y))] dy dx$$

$\iint_S \langle 0, 0, R \rangle \cdot \hat{n} dS$

$\iint_S \langle 0, 0, R \rangle \cdot \hat{n} dS = \iint_{\text{top}} R dxdy = \iint_{\text{top}} R(x,y, z_2(x,y)) dxdy$

Top:  $\hat{n} dS = \langle -\frac{\partial z_2}{\partial x}, -\frac{\partial z_2}{\partial y}, 1 \rangle dxdy$

Bottom:  $\hat{n} dS = \langle -\frac{\partial z_1}{\partial x}, -\frac{\partial z_1}{\partial y}, 1 \rangle dxdy$

$\iint_{\text{bottom}} -R dxdy = \iint_{\text{bottom}} -R(x,y, z_1(x,y)) dxdy$

Sides are vertical,  $\langle 0, 0, R \rangle$  is tangent to sides Flux through sides = 0

Diffusion Equation = Heat Equation (immobile)

$u$  = concentration =  $u(x, y, z, t)$

$$\frac{\partial u}{\partial t} = k \nabla^2 u = k \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

$\vec{F}$  = flow of smoke, smoke flows from high concentration to low

so  $\vec{F}$  directed along  $-\nabla u$   $\vec{F} = -k \nabla u$

(2) Relate  $\vec{F}$  and  $\frac{\partial u}{\partial t}$

$\iint_S \vec{F} \cdot d\vec{S}$  Flux out of  $D$  through  $S$

$$\iint_S \vec{F} \cdot d\vec{S} = \text{amount of smoke pass in per unit time} = -\frac{d}{dt} (\iiint_D u dV) \text{ (smoke we are losing)}$$

$$\iiint_D dV \vec{F} dV = -\frac{d}{dt} \iiint_D u dV = -\iiint_D \frac{\partial u}{\partial t} dV \Rightarrow \text{div } \vec{F} = -\frac{\partial u}{\partial t}$$

$$\Rightarrow \frac{\partial u}{\partial t} = -\text{div } \vec{F} = -\text{div} (-k \nabla u) = k \nabla^2 u$$

## Lecture 29 Line integrals

$$\vec{F} = P\hat{i} + Q\hat{j} + R\hat{k} \quad d\vec{r} = \langle dx, dy, dz \rangle$$

$$\text{Work} = \int_C \vec{F} \cdot d\vec{r} = \int_C Pdx + Qdy + Rdz$$

parametrize C

ex.  $\vec{F} = \langle yz, xz, xy \rangle \quad C: x=t^3, y=t^2, z=t, 0 \leq t \leq 1$

$$\int_C \vec{F} \cdot d\vec{r} = \int_0^1 (t^3, 3t^2 + t^4, 2t + t^5) dt = 1$$

In fact,  $\vec{F}$  is conservative  $\vec{F} = \langle x, y, z \rangle$

$$\vec{F} \text{ is conservative} \Leftrightarrow P_y = Q_x \quad P_z = R_x \quad Q_z = R_y \Leftrightarrow Pdx + Qdy + Rdz = df$$

① Line integrals

② Antiderivatives

$$f_x = 2xy \quad f_y = x^2 + z^3 \quad f_z = 3yz^2 - 4z^3$$

$$f = x^2y + g(y, z)$$

$$f_y = x^2 + g_y = x^2 + z^3 \quad g_y = z^3 \quad g = z^3y + h(z)$$

$$f_z = 3yz^2 - 4z^3 = 3yz^2 + h_z \quad h_z = -4z^3 \quad h = -z^4 + C$$

$$f = x^2y + z^3y - z^4 + C$$

# Lecture 30 Stoke's theorem

curl in 3D

$$\text{if } \vec{F} = P\hat{i} + Q\hat{j} + R\hat{k} \quad \text{curl } \vec{F} = (R_y - Q_z)\hat{i} + (P_z - R_x)\hat{j} + (Q_x - P_y)\hat{k}$$

If  $\vec{F}$  is defined on a simply-connected region,  $\vec{F}$  is conservative  $\Leftrightarrow \text{curl } \vec{F} = 0$

$$\nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle$$

$$\nabla f = \left\langle \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right\rangle$$

$$\nabla \cdot \langle P, Q, R \rangle = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

$$\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = \left( \frac{\partial R}{\partial y} - \frac{\partial Q}{\partial z} \right) \hat{i} - \left( \frac{\partial R}{\partial x} - \frac{\partial P}{\partial z} \right) \hat{j} + \left( \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) \hat{k} = \text{curl } \vec{F}$$

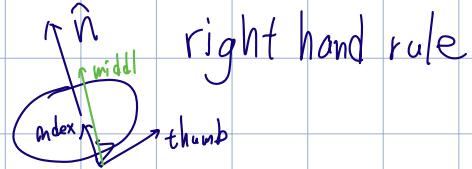
curl measures the rotation component in a velocity field

STOKE'S THM

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_S (\nabla \times \vec{F}) \cdot \hat{n} dS \quad \text{if } C \text{ closed curve} \quad S = \text{any curve bounded by } C$$

Calculate the flux of  $\nabla \times \vec{F}$  (curl is a vector field also)

Orientation: need  $C$  and  $S$  to be compatible



Compare Stokes with Green

$$\oint_C \vec{F} \cdot d\vec{r} = \oint_C P dx + Q dy$$

$$\begin{aligned} \text{Stokes: } &= \iint_S (\nabla \times \vec{F}) \hat{k} dS \quad (\nabla \times \vec{F}) \hat{k} = z \text{ components of curl } \vec{F} \\ &= \iint_S (Q_x - P_y) dx dy \end{aligned}$$

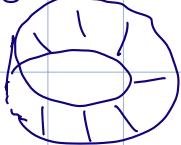
ex.  $\vec{F} = z\hat{i} + x\hat{j} + y\hat{k}$  around unit circle counterclockwise

$$\begin{aligned} S &\text{ is a hemisphere } z = \sqrt{1-x^2-y^2} \\ \oint_C z dx + x dy + y dz &= \int_0^{2\pi} 0 + \cos t \cdot (\cos t dt) + 0 = \int_0^{2\pi} \cos^2 t dt = \pi \end{aligned}$$

$$\hat{n} dS = \langle -f_x, -f_y, 1 \rangle dx dy = \langle 2x, 2y, 1 \rangle dx dy$$

$$\iint_S \langle 1, 1, 1 \rangle \langle 2x, 2y, 1 \rangle dx dy = \iint (2x+2y+1) dx dy = \pi$$

$$\oint_C \vec{F} d\vec{r} = \iint_S (\operatorname{curl} \vec{F}) \hat{n} dS$$



Flux can't be defined

$$\operatorname{div}(\nabla \times \vec{F}) = 0 \text{ always}$$

$$\vec{F} = \langle P, Q, R \rangle$$

$$\operatorname{div}(\nabla \times \vec{F}) = (P_y - Q_z)_x + (P_z - P_x)_y + (Q_x - P_y)_z = 0$$

In space,  $\operatorname{curl}(\vec{F} = \nabla \times \vec{F})$  is a consecutive vector field