'SMARTPLUS' DOCUMENTATION

SMARTPLUS TEAM

ARTS ET MÉTIERS METZ, TU BERGAKADEMIE FREIBERG

Table des matières

Ta	able	des m	natières	5
Ι	Pra	actica	I documentation	7
1	Ide	ntifica	ation of material parameters	9
	1.1	Descr	iption of the workflow	11
		1.1.1	Definition of the objective function	11
		1.1.2	Optimization algorithm	14
		1.1.3	Identification of the material parameters based on the heterogeneous Meuwis-	
			sen experiments	15
	1.2	Descr	iption of the optimization algorithm utilized	16

Première partie Practical documentation

1

IDENTIFICATION OF MATERIAL PARAMETERS

Sommaire

1.1	Descri	iption of the workflow	11
	1.1.1	Definition of the objective function	11
	1.1.2	Optimization algorithm	14
	1.1.3	Identification of the material parameters based on the heterogeneous Meuwis-	
		sen experiments	15
1.2	Descri	iption of the optimization algorithm utilized	16

With the design of new devices with complex geometry and to take the most advantage of the materials utilized, the local loading paths are often strongly multiaxial while the material often operates a non-linear regime. The development of new structures requires the prediction of their thermomechanical response, for which the calibration of the material parameters for the numerical model is an important step. For other applications, the identification of parameters characteristics of the microstructure (e.g. orientation density function of fiber reinforcements) is crucial to be able to properly describe the effective response of a composite material at a global scale level.

A robust, versatile parameter identification method is thus required. In most cases, the parameter identification do not resume to only find an optimization algorithm that will be able to minimize a given function. An integrated approach that controls all the workflow of the parameter identification procedure is required, with the definition of the function to minimize, the additional constraints and set up the model that will compute the trial numerical values to be compared with experimental data. A typical view of

Various optimization algorithms have been used in identification methods, i.e. deterministic algorithms such as gradient-based Levenberg-Marquardt algorithm (??), real space evolutionary-inspired, genetic algorithms or Bayesian statistical approaches (?). The Levenberg-Marquardt optimization algorithm has been often adopted for the determination of material parameters for metals (????). An hybrid algorithm that used an evolutionary algorithm combined with a gradient-based algorithm has been utilized by ? to determine the parameters of an elastic-plastic constitutive model including an anisotropic criterion (?) coupled with a non-linear kinematical hardening (?). The evolutionary algorithm was used to determine a good initial guess values for the gradient-based approach and therefore ensure that a local minima has been found.

In this chapter, the parameters of a phenomenological model are extracted from tests performed on specimens with non-uniform geometry, which induce heterogeneous strain fields carried out on specimens with the same thermomechanical loading history. The digital image correlation technique is employed to measure the strain fields on the surface of the specimen and to analyze the strain paths of chosen points. Finite element analysis enables the computation of numerical strain fields using a thermodynamical constitutive model for shape memory alloys previously implemented in a finite element code. The strain fields computed numerically are compared with experimental ones obtained by DIC to find the model parameters which best match experimental measurements using a newly developed parallelized mixed genetic/gradient-based optimization algorithm. These numerical simulations are carried out in parallel using a supercomputer to reduce the time necessary to identify the set of model parameters. The major features of this new algorithm is its ability to identify the material parameters which describe the thermomechanical behavior of shape memory alloys from full-field measurements for various loading conditions (different temperatures, multiaxial behavior, heterogeneous test configurations). It is demonstrated that model parameters for the

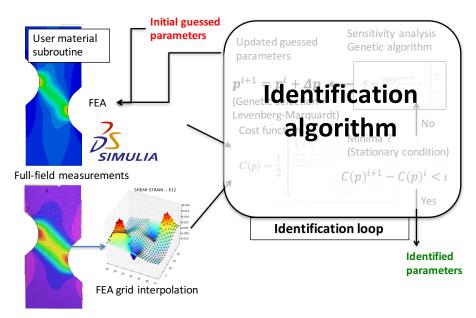


Figure 1.1 – Overview of the identification procedure

simulation of SMA structures are thus obtained based on a reduced number of heterogeneous tests at different temperatures.

1.1 Description of the workflow

1.1.1 Definition of the objective function

Having any type of numerical model with specific set of material parameters, the identification problem consists in the determination of a prescribed set of material parameters that minimize the difference between computed data and a set of experimental data. The numerical model could be typically a Finite Element model, with the same geometry and boundary conditions than the experimental setup. A part of the experimental results is in this case utilized to define (or to complete the definition) of the boundary value problem to solve using the finite element method and another part is utilized to define a cost function to be minimized.

A general cost function is considered to be:

$$C(\mathbf{p}) = \frac{1}{2} \sum_{i} w_i \left(v_i^{num}(\mathbf{p}) - v_i^{exp} \right)^2$$
(1.1)

where $C(\mathbf{p})$ is the cost function, $v_i^{num}(\mathbf{p})$ is the i-th information obtained with the numerical simulation, v_i^{exp} is the i-th information obtained from the set of experiments conducted and w_i is a weight factor. Note that all these information are potentially obtained from a number of experiments at different times and at different spatial positions.

In the methodology proposed here, the experimental data are classified in the following:

- Each experiment is considered separately and is determined with the index e
- Within that experiment, there exists a number n of measured quantities

— Within an experiment, there exist a number j of experimental points The cost function is therefore set as :

$$C(\mathbf{p}) = \frac{1}{2} \sum_{e} \sum_{n} \sum_{j} w_{e} w_{e,n} w_{e,j,n} \left(v_{e,j,n}^{num}(\mathbf{p}) - v_{e,j,n}^{exp} \right)^{2},$$
(1.2)

where the three weights factors w_e , $w_{e,n}$, $w_{e,n,j}$ can be set independently.

Information about the experimental points

The information about the experimental points to be compared with have to be set in the file "files_exp.inp". The file that correspond to the example described here is presented below:

```
#Name_of_the_exp_files
  results_0-90.dat
  results\_pm45.dat
  results_pm675.dat
  #EXP_Nb_columns_in_files
  20
  20
  20
  #EXP_Nb_columns_to_identify
  2
  2
  #EXP_colums_to_identify
  8 9
  8 9
  8 9
  #skip_lines
  0
23
  0
```

 $1_Identification/files_exp.inp$

The first part "#Name_of_the_exp_files" is directly followed with the name of the files that are stored in the *exp_data* folder. The number of files should correspond to what indicated in the file "dataident_essentials.inp" and correspond to the {e} index:

- -- results_0-90.dat
- results pm45.dat
- results_pm675.dat

The second part "#EXP_Nb_columns_in_files" is directly followed with the number of columns of the experimental files ¹:

^{1.} this will be suppressed and automatically evaluated in a subsequent version

- --20
- -20
- --20

The three file then are composed of 20 columns.

The third part "#EXP_Nb_columns_to_identify" is directly followed with the number of columns. It directly correspond to the {n} index.

- -2
- 2
- -2

The fourth part "#EXP_colums_to_identify" is directly followed with the index of the columns that contains experimental values for each experimental point. Each column correspond to the {j} index.

- **—** 8 9
- -89
- -89

The fifth and last part "#skip_lines" corresponds to the number of lines that are skipped and usually correspond to a header in the files.

- -0
- --0
- --0

Information about the weight factors

In the file "files_weights.inp", you can enter those weight factors in the following manner:

```
Weight_1_per_file
type_0_no_weight_1_weight_per_file

#if_1_list
2.0

Weight_2_per_columns
type_0_no_weight_1_sum_per_cols_2_weight_per_cols_plus_sum_3_weight_per_cols_no_sum

2

#if_2_or_3_list
4.0 1.0

Weight_3_or_uncertainty_per_point
type_0_no_weight_1_weight_column_for_each_exp_col

##if_1_list_per_file_of_columns
9 10
```

 $1_Identification/files_weights.inp$

The final version of the cost function is written as:

$$C(\mathbf{p}) = \frac{1}{2} \alpha_{\varepsilon} \left(\frac{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{xx}^{num}(\mathbf{p}) - \varepsilon_{xx}^{exp})^{2}}{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{xx}^{exp})^{2}} + \frac{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{yy}^{num}(\mathbf{p}) - \varepsilon_{yy}^{exp})^{2}}{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{yy}^{exp})^{2}} + \frac{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{yy}^{exp})^{2}}{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{xy}^{exp})^{2}} + \frac{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{xy}^{exp})^{2}}{\sum_{i} \sum_{t} \sum_{T} (\varepsilon_{xy}^{exp})^{2}} + \frac{1}{2} \alpha_{F} \left(\frac{\sum_{i} \sum_{t} (F^{num}(\mathbf{p}) - F^{exp})^{2}}{\sum_{i} \sum_{t} (F^{exp})^{2}} \right)$$

$$(1.3)$$

where ε_{xx}^{exp} , ε_{yy}^{exp} and ε_{xy}^{exp} represent the three components of the strain tensor that are extracted at a material point i of coordinates x_i at the time t from an isothermal test performed at the temperature T. The values ε_{xx}^{num} , ε_{yy}^{num} and ε_{xy}^{num} represent the corresponding values computed using a chosen constitutive model. p denotes the set of guessed parameters. The weight parameters α_{ε} and α_{F} are set to equilibrate the influence of the error in strains and the error in reaction force. The total contribution to the cost function of the strain and the force has been set to be about half for each component, which is obtained using $\alpha_{\varepsilon} = 1$ and $\alpha_{F} = 40$.

1.1.2 Optimization algorithm

The definition of an optimization algorithm has to take into account the computational time necessary to perform a numerical simulation for a given set of parameters. Indeed, it often depends on the model utilized to obtain values entering in the definition of the cost function according to a given set of design variables. Especially, the efficiency of the algorithms depends on the time necessary to compute a numerical solution and then evaluate the corresponding cost to be able to evaluate the prescribed set of parameters within the set of admissible solutions. Also, the form of the cost function might impact the decision of an optimization algorithm, e.g. if local minima are expected. Indeed, the main issue associated with gradient-based techniques is that the method ensures the convergence to a local minima. Heuristic such as genetic algorithm should be therefore utilized in such cases to determine preferential sets of parameters from a large population that are close to the global minima (?). In the approach proposed, the genetic algorithm and the gradient-based method are used simultaneously, with the following procedure:

- 1. An initial population of C_0 individuals (each individual is a set of parameters) is generated. The selection of individuals can be aleatory, given limitations of the material parameters, or can be generated using Design Of Experiments (DOE).
- 2. The numerical simulation for all the individual is computed in parallel.
- 3. All the individuals are scored by computing their cost value.
- 4. The individuals of the initial generation are classified, and a number n of them are selected (the best ones). These constitute the 'current' generation n.
- 5. A set of children of the current generation (with n members) are determined using the crossover technique. A mutation probability has been added to increase the diversity

- of the children generation. For the same purpose a small deviation operator from the parent's parameters is also applied.
- 6. The bests members of the current generation are selected. The set of numerical simulation to apply the finite differences derivation technique is determined.
- 7. The numerical simulation for all the children and the simulations required for the finite differences derivation are computed *in parallel*.
- 8. The cost function of all the individual is determined.
- 9. The parameters of a number N_{GB} of the best members are updated using a Levenberg-Marquardt algorithm.
- 10. The current generation n + 1 is determined from the the best individuals among the current generation n and the children.
- 11. Stationary condition test for the best individual of the current generation compared to the previous best. If needed, reloop from item 5.

On overview of the identification procedure in general is presented in Figure 1.1.

1.1.3 Identification of the material parameters based on the heterogeneous Meuwissen experiments

The identification method presented in section ?? is applied to the case of a set of experimental data corresponding to three isothermal tests performed at 50°C, 60°C and 70°C. Several tests have been conducted with different parameters of the hybrid genetic - gradient based algorithm, which are resumed in Tab. 1.1.

The different control parameters of the algorithm are:

- The initial number of individuals of the first generation N_{init} .
- The number of sons generated and the number of retained individual for the current generation N_{cur} .
- The number of best individuals selected to be optimized via the Levenberg-Marquardt gradient based algorithm N_{GB} .
- The probability of mutation of the parameters, set to 5%. This means that for each parameter of all the new individual, there is a 5% chance that the concerned parameter is set randomly inside the design space rather than being selected from the crossover technique. This low value is generally utilized when a low population is defined to keep a certain stability of the generations, still slowly introducing new parameters to authorize the exploration of new points in the design space.
- The first (best) half of each generation is considered for the crossover technique.

For each case the identification was stopped after a maximum of 30 generations, or after a stabilization of the cost function. The algorithm has been ran on a cluster to be able to parallelize the numerical simulations. This is achieved using a developed software coupled with TORQUE Resource Manager for the management of the simulation on the cluster.

The set of initial parameters is bounded to define the design space (see Tab. 1.2):

 ${\it Table 1.1-Parameters\ of\ the\ hybrid\ genetic\ -\ gradient\ based\ algorithm\ for\ the\ four\ identification\ tests}$

Number	N_{init}	N_{cur}	N_{GB}
1	50	10	1
2	50	10	1
3	150	50	1
4	150	5	3

Table 1.2 – Min and max bounds for the material parameters

	$E\left(\mathrm{MPa}\right)$	ν	H_f (MPa)	ε_{trac}^{T}
\min	50 000	0.2	0.5	0.03
max	80 000	0.45	6	0.05
	$C^M \left(MPa.^{\circ}C^{-1} \right) \right)$	$C^A (\mathrm{MPa^{\circ}C^{-1}})$	M_S (°C)	A_f (°C)
\min	4	4	-73	-33
max	12	12	27	47

1.2 Description of the optimization algorithm utilized