

General Expression for $d\vec{V}/dt$ & $d\vec{\Omega}/dt$



Lockheed U-2S Dragon Lady

Relation between d/dt and $\vec{\Omega}$



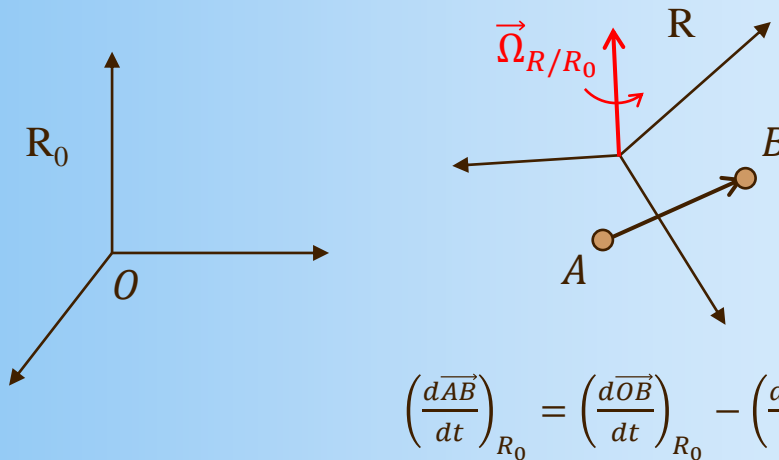
We consider a referential, R_0

We consider another referential R animated with a rotation $\vec{\Omega}_{R/R_0}$

A and B are 2 fix points of the Referential R ,

$$\vec{V}_B = \vec{V}_A + \vec{\Omega}_{R/R_0} \wedge \overrightarrow{AB} \rightarrow \left(\frac{d\overrightarrow{AB}}{dt} \right)_{R_0} = \vec{\Omega}_{R/R_0} \wedge \overrightarrow{AB}$$

The velocity field (of a solid) is a torsor with a resultant $\vec{\Omega}$



Relation between d/dt and $\vec{\Omega}$



We consider a referential, R_0

We consider another referential R animated with a rotation $\vec{\Omega}_{R/R_0}$

If \vec{X} is a fix vector of the Referential R ,

$$\rightarrow \left(\frac{d\vec{X}}{dt} \right)_{R_0} = \vec{\Omega}_{R/R_0} \wedge \vec{X}$$

This relation can be generalised for any vector \vec{X}

$$\rightarrow \left(\frac{d\vec{X}}{dt} \right)_{R_0} = \left(\frac{d\vec{X}}{dt} \right)_R + \vec{\Omega}_{R/R_0} \wedge \vec{X}$$

General Expression of $d\vec{V}/dt$

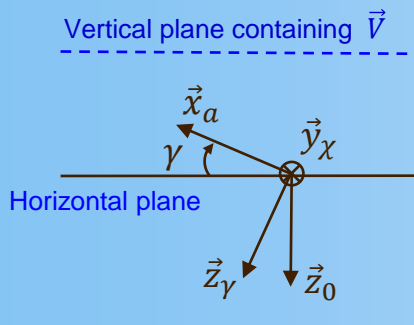


We apply the derivation expression using R_0 and R_a

$$\left(\frac{d\vec{V}}{dt}\right)_{R_0} = \left(\frac{d\vec{V}}{dt}\right)_{R_a} + \vec{\Omega}_{a/0} \wedge \vec{V} = \dot{V} \vec{x}_a + V \vec{\Omega}_{a/0} \wedge \vec{x}_a$$

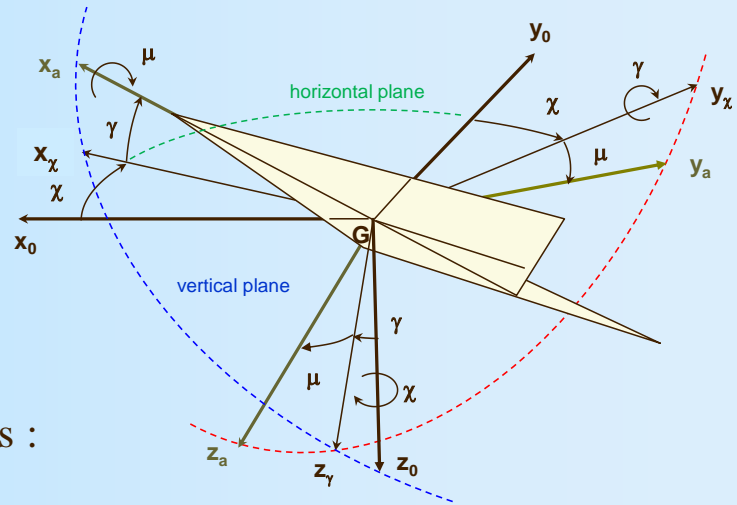
but $\vec{\Omega}_{a/0} = \dot{\chi} \vec{z}_0 + \dot{\gamma} \vec{y}_\chi + \dot{\mu} \vec{x}_a$

$$\left(\frac{d\vec{V}}{dt}\right)_{R_0} = \dot{V} \vec{x}_a + V \dot{\chi} \vec{z}_0 \wedge \vec{x}_a + V \dot{\gamma} \vec{y}_\chi \wedge \vec{x}_a$$



$$\left(\frac{d\vec{V}}{dt}\right)_{R_0} = \dot{V} \vec{x}_a + V \cos \gamma \dot{\chi} \vec{y}_\chi - V \dot{\gamma} \vec{z}_\gamma$$

$$\left(\frac{d\vec{V}}{dt}\right)_{R_0} = \dot{V} \vec{x}_a + V \cos \gamma \dot{\chi} \vec{y}_\chi - V \dot{\gamma} \vec{z}_\gamma$$



The absolute acceleration includes 3 terms :

- 1) along the velocity \vec{V}
- 2) within the horizontal plane, perpendicular to \vec{V}
- 3) within the vertical plane containing \vec{V} , perpendicular to \vec{V}

The 2 last terms correspond to centripetal accelerations for a uniform circular motion :

- within an horizontal plane at a velocity , $V \cos \gamma$ and a rotation rate , $\dot{\chi}$
- within a vertical plane at a velocity , V and a rotation rate , $\dot{\gamma}$

General Expression of $d\vec{\Omega}/dt$



We apply the derivation expression using R_0 and R_b

$$\left(\frac{d\vec{\Omega}}{dt}\right)_{R_0} = \left(\frac{d\vec{\Omega}}{dt}\right)_{R_b} + \vec{\Omega}_{b/0} \wedge \vec{\Omega} = \left(\frac{d\vec{\Omega}}{dt}\right)_{R_b}$$

with

$$\vec{\Omega} = \vec{\Omega}_{ac/R_0} = \vec{\Omega}_{R_b/R_0} = \left. \begin{matrix} p \\ q \\ r \end{matrix} \right|_{R_b}$$

$$\left(\frac{d\vec{\Omega}}{dt}\right)_{R_0} = \left(\frac{d\vec{\Omega}}{dt}\right)_{R_b} = \left. \begin{matrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{matrix} \right|_{R_b}$$

$$\vec{M}_G = [I_G] \cdot \left(\frac{d\vec{\Omega}}{dt} \right)_{R_0} = \begin{bmatrix} A & 0 & -E \\ 0 & B & 0 \\ -E & 0 & C \end{bmatrix}_{R_b} \begin{vmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{vmatrix}$$

The 2nd Newton law can be expressed easily with respect to R_b

We can also neglect the cross product term E

$$\vec{M}_G = [I_G] \cdot \left(\frac{d\vec{\Omega}}{dt} \right)_{R_0} = \begin{vmatrix} A \cdot \dot{p} \\ B \cdot \dot{q} \\ C \cdot \dot{r} \end{vmatrix}_{R_b}$$

Pure Longitudinal Flight



Lockheed Constellation

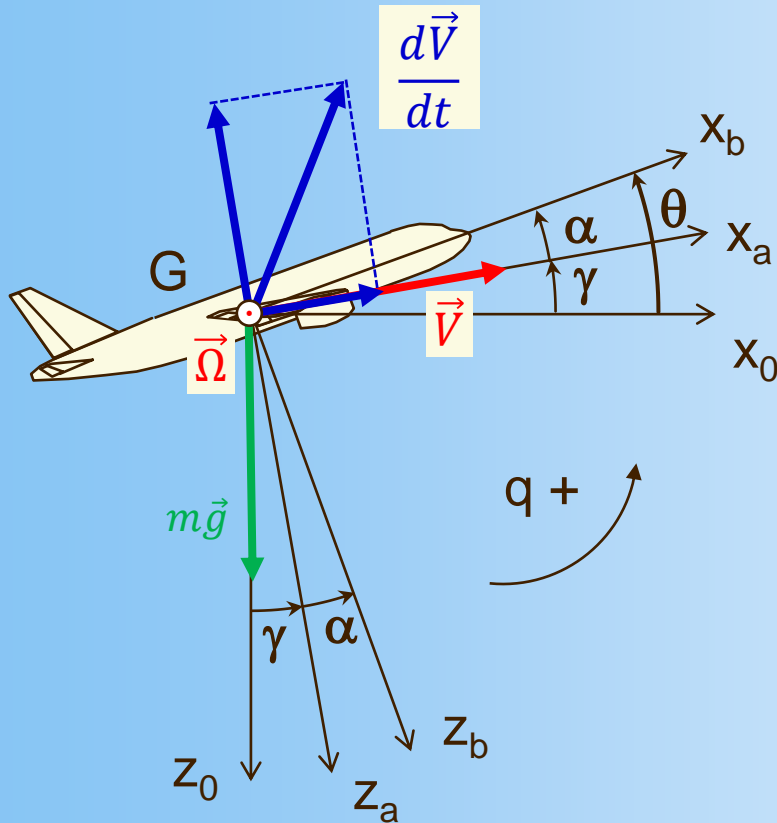
Pure Longitudinal Flight requires that all the forces acting on the a/c are within the a/c plane of symmetry

- all forces within the plane (x_b, z_b) : no lateral forces
- the a/c plane of symmetry is vertical because it contains the vector $m\vec{g}$
- the y_b axis is within the horizontal plane
 - $\phi_1 = 0 \rightarrow \phi = 0$
- the aircraft velocity is within the airplane plane of symmetry
 - $\beta = 0$
- the aircraft acceleration is within the airplane plane of symmetry

$$\rightarrow \left(\frac{d\vec{V}}{dt} \right)_{R_0} = \dot{V} \vec{x}_a + V \cos \gamma \cancel{\dot{\gamma}} \vec{y}_\chi - V \dot{\gamma} \vec{z}_a$$

- the aircraft can only rotate with respect to the y_b axis : it can only rotate within the vertical plane / plane of symmetry → $\vec{\Omega}_{b/0} = \dot{\theta} \vec{y}_b \rightarrow q = \dot{\theta}$

Pure Longitudinal Flight



$$\begin{cases} \beta = 0^\circ \\ \phi = 0^\circ \\ \theta = \alpha + \gamma (*) \\ q = \dot{\theta} \end{cases}$$

$$\left(\frac{d\vec{V}}{dt}\right)_{R_0} = \dot{V} \vec{x}_a - V \dot{\gamma} \vec{z}_a$$

$$\vec{\Omega} = q \cdot \vec{y}_b$$

(*) only valid for pure Longitudinal flight,
see annex

Steady Turn

Lockheed SR-71 Blackbird



The Steady Turn Manoeuvre requires that the rotation vector $\vec{\Omega}$ is a constant vector.

It is a motion performed at constant altitude (steady : no variation).

$$\vec{\Omega}_{a/0} = \vec{\Omega}_{a/b} + \vec{\Omega}_{b/0} = \vec{\Omega}_{b/0}, \text{ because } \vec{\Omega}_{a/b} = \dot{\beta} \vec{z}_a - \dot{\alpha} \vec{y}_b = \vec{0} \text{ (steady condition)}$$

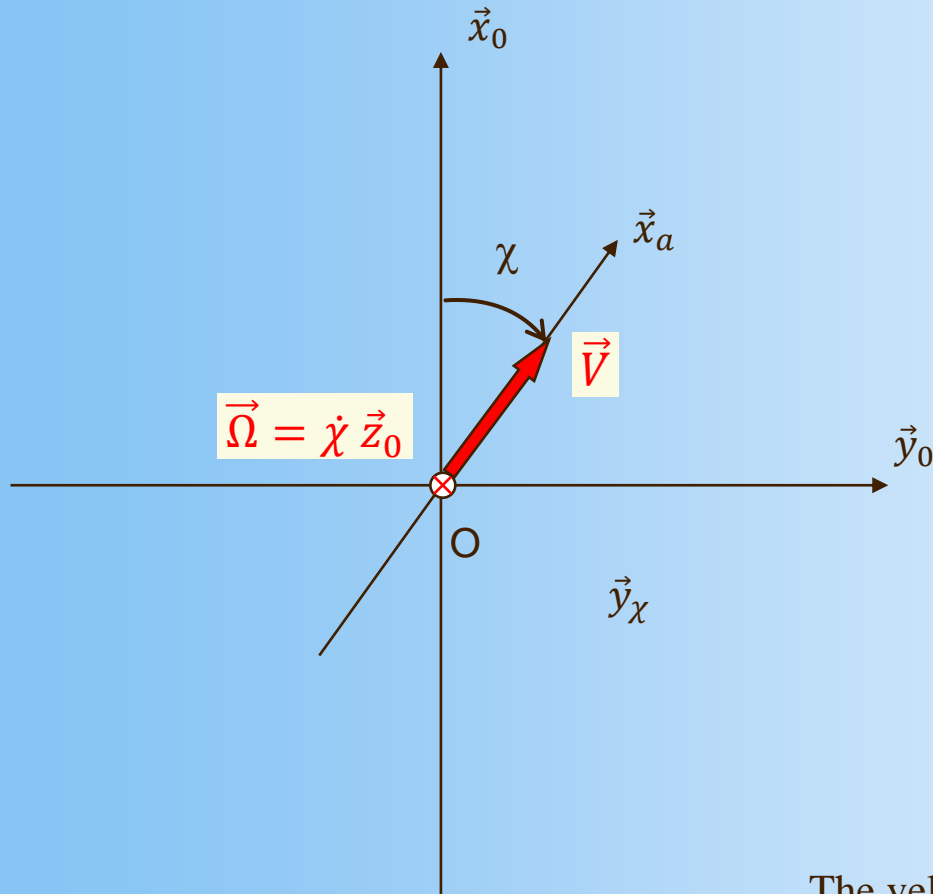
$$\dot{\chi} \vec{z}_0 + \dot{\gamma} \vec{y}_\chi + \dot{\mu} \vec{x}_a = \dot{\psi} \vec{z}_0 + \dot{\theta} \vec{y}_\psi + \dot{\phi} \vec{x}_b$$

$$\text{By identification : } \dot{\chi} = \dot{\psi} = \Omega \quad \text{and} \quad \dot{\gamma} = \dot{\mu} = \dot{\theta} = \dot{\phi} = 0$$

The rotation vector $\vec{\Omega}_{a/0} = \vec{\Omega}_{b/0}$ is vertical

$$\vec{\Omega} = \Omega \vec{z}_0 = \dot{\chi} \vec{z}_0 = \dot{\psi} \vec{z}_0$$

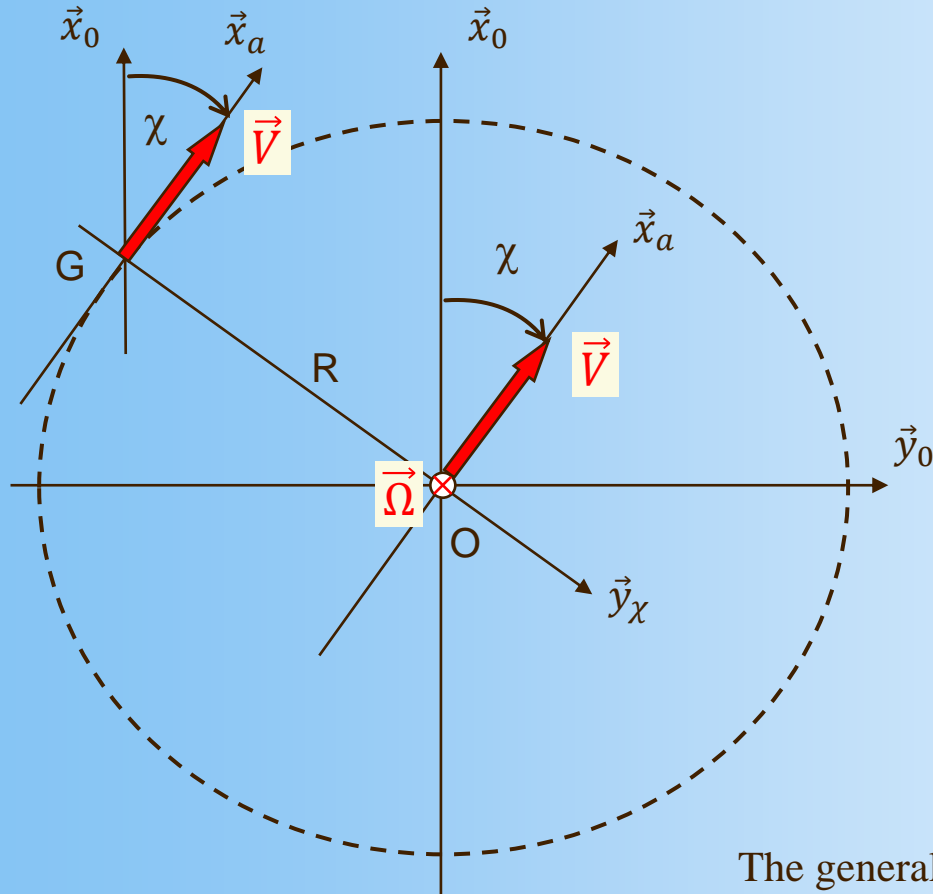
Steady Turn manoeuvre



$$\begin{aligned} \rightarrow \gamma &= 0 \\ \rightarrow \dot{\chi} &= \Omega \end{aligned}$$

The velocity vector is rotating at a constant rate Ω within an horizontal plane

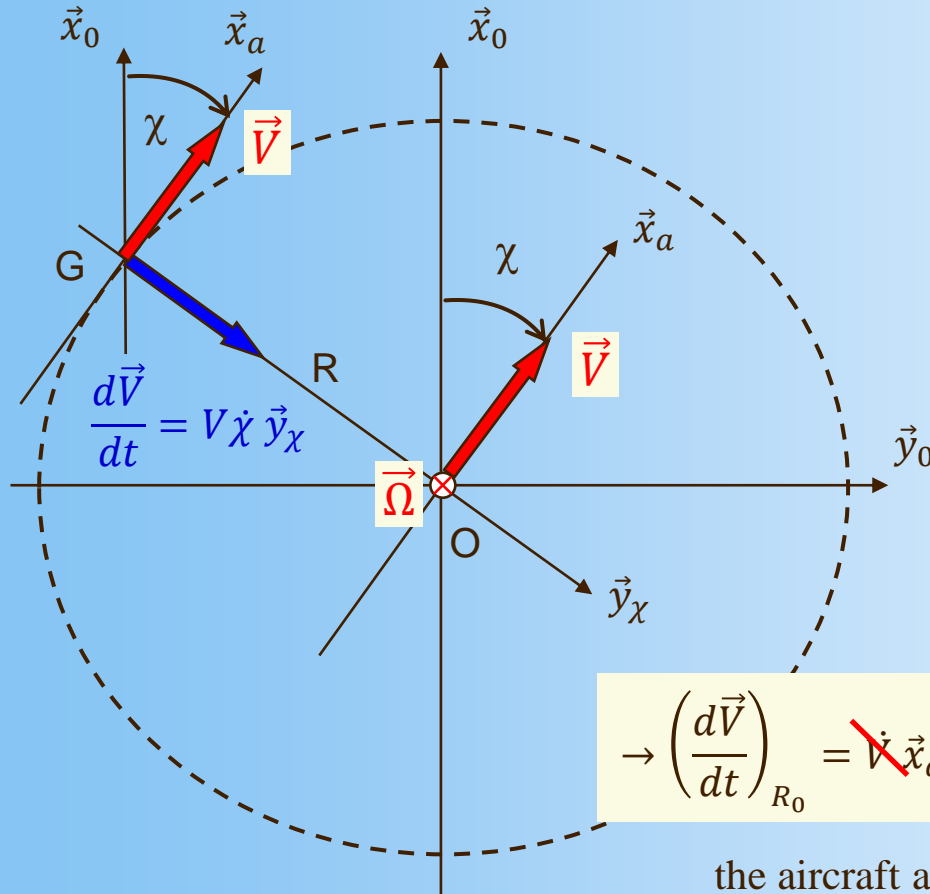
Steady Turn manoeuvre



$$\rightarrow V = \Omega \cdot R$$

The general motion is a uniform circular motion within an horizontal plane

Steady Turn manoeuvre



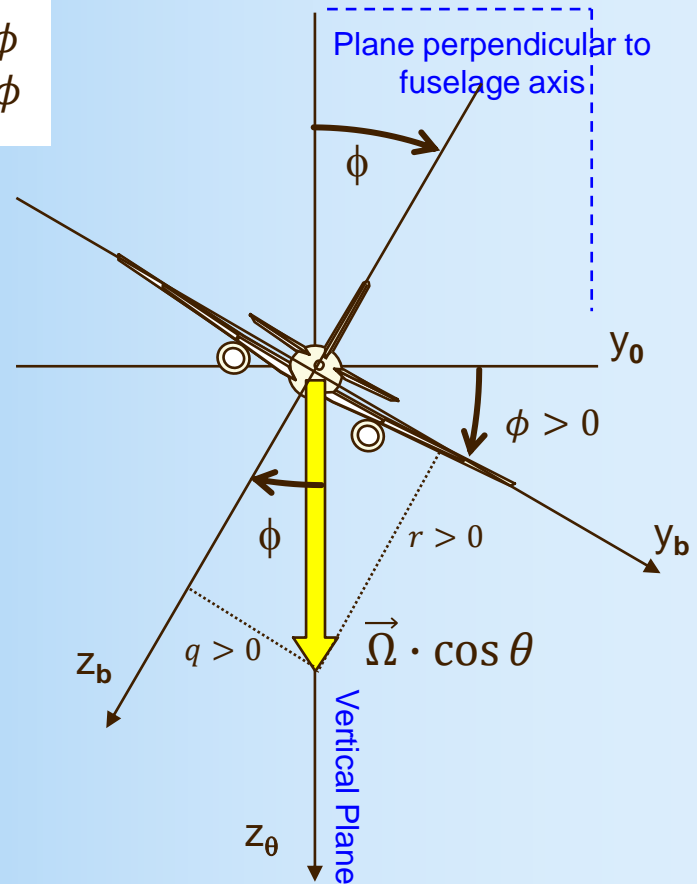
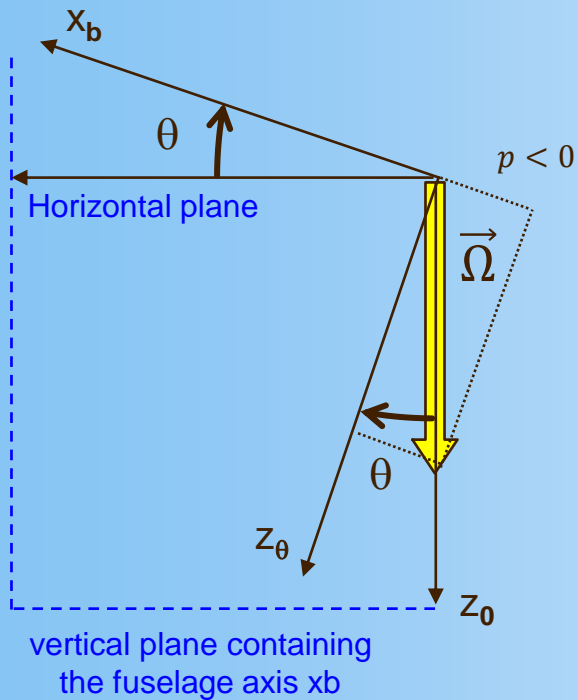
$$\rightarrow \left(\frac{d\vec{V}}{dt} \right)_{R_0} = \cancel{\dot{V} \vec{x}_a} + V\dot{\chi} \vec{y}_\chi - \cancel{V\dot{\chi} \vec{z}_\gamma} = \Omega V \vec{y}_\chi$$

the aircraft acceleration is perpendicular
to \vec{V} within the horizontal plane

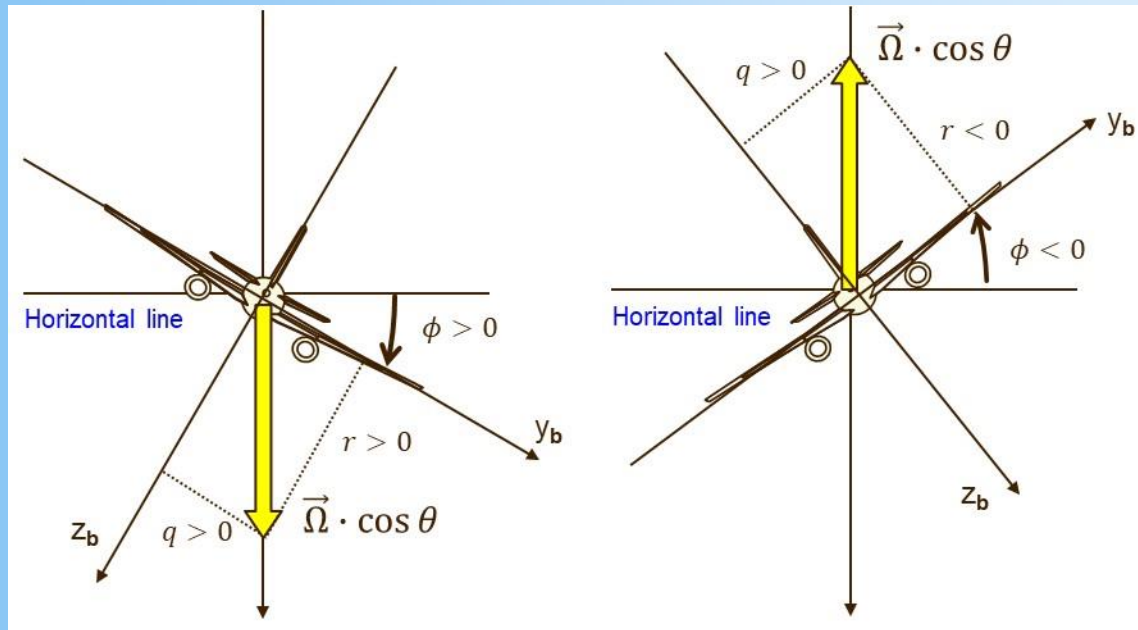
Steady Turn : expression of $\vec{\Omega}_{b/0}$



$$\vec{\Omega}_{b/0} = \begin{matrix} p \\ q \\ r \end{matrix}_{R_b} = \Omega \cdot \begin{matrix} -\sin \theta \\ \cos \theta \cdot \sin \phi \\ \cos \theta \cdot \cos \phi \end{matrix}_{R_b}$$



Steady Turn : positive, pitch up rate, q



During a steady turn manoeuvre, there is a steady pitch-up rate :

$$q = \Omega \cos \theta \cdot \sin \phi = \Omega \cdot \sin \phi_1 > 0$$

Pure Longitudinal Flight / Steady Turn Manoeuvre correspond to trimmed situations.

- If the aircraft is stable (longitudinal stability) and if the pilot doesn't apply any roll / yaw command, at the end, we will converge to a trimmed situation corresponding to the Pure Longitudinal Flight
- If the aircraft is stable (spiral stability) and if the pilot applies a roll / yaw command, at the end, we will converge to a trimmed situation corresponding to the Steady Turn Manoeuvre

These notions of « stability » and « convergence » are linked to the dynamic properties of the aircraft (aircraft eigen modes) that we will study latter in this course.