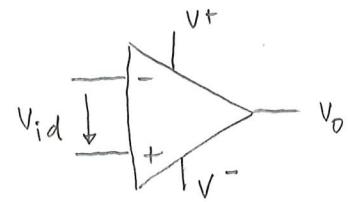
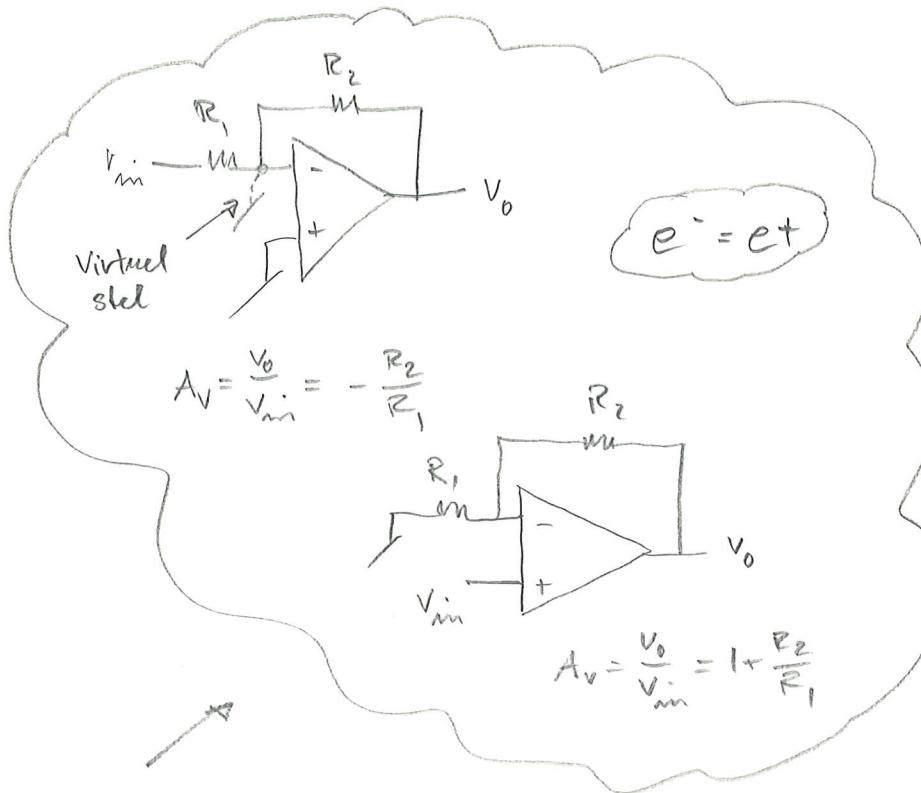


## Ideal Performance

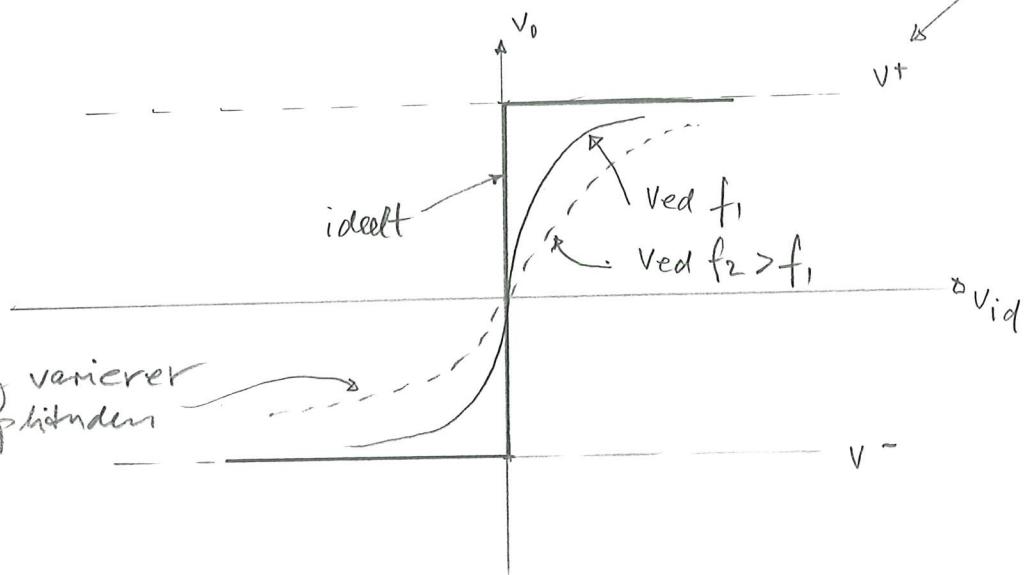


$$V_o = A_{OL} \cdot V_{id}$$

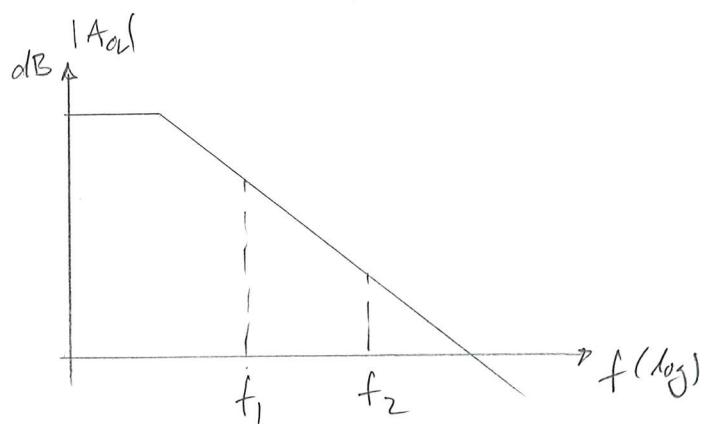
$$\frac{\partial V_o}{\partial V_{id}} = A_{OL}$$

All datter er bestinget af, at  $A_{OL} \rightarrow \infty$

Hældnings-koeff.

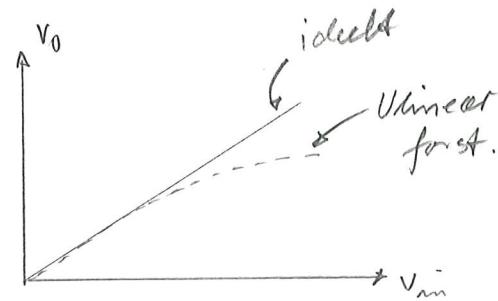
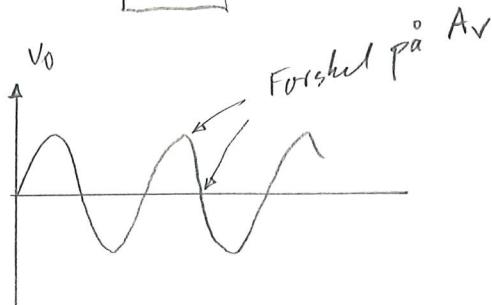
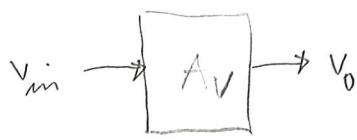


## Datablad



Hvis forstørrelsen varierer med amplitude  $\Rightarrow$

### Forsvængning



### Forstørker med negativ feedback (se nede)

$$V_o = A_{OL} \cdot V_{id} = A_{OL} \cdot (\alpha \cdot V_{in} - \beta \cdot V_o) \Rightarrow$$

$$V_o (1 + \beta A_{OL}) = A_{OL} \cdot \alpha \cdot V_{in} \Rightarrow V_o = \frac{\alpha \cdot A_{OL}}{1 + \beta A_{OL}} \cdot V_{in} \Rightarrow$$

$$A_{CL} = \frac{V_o}{V_{in}} = \frac{\alpha \cdot A_{OL}}{1 + \beta A_{OL}} = \frac{\alpha}{\beta} \cdot \frac{A_{OL}}{\frac{1}{\beta} + A_{OL}} = \frac{\alpha}{\beta} \left( \frac{1}{1 + \frac{1}{\beta A_{OL}}} \right)$$

$$= \frac{\alpha}{\beta} \cdot K_f$$

Fejlfaktor  $K_f$

NB! Ideel opAmp

$$\downarrow$$

$$A_{OL} \rightarrow \infty$$

$$\downarrow$$

$$K_f = 1$$

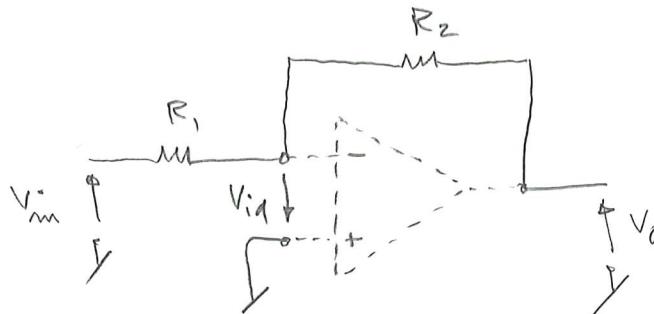
$$V_{id} = \alpha \cdot V_{in} - \beta \cdot V_o$$

$$\alpha = \left. \frac{V_{id}}{V_{in}} \right|_{V_o=0}$$

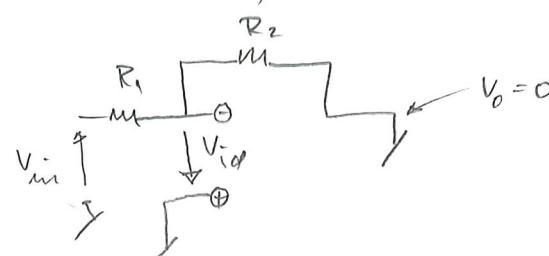
$$\beta = - \left. \frac{V_{id}}{V_o} \right|_{V_{in}=0}$$

Eksempel

# Inverterende kobling

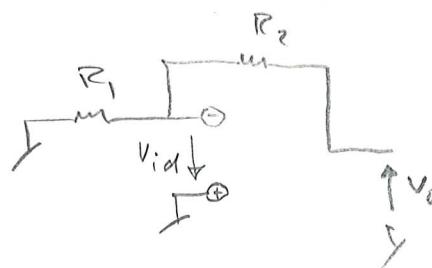


$$\alpha = \frac{V_{id}}{V_{in}} \Big|_{V_o=0}$$



$$V_{id} = -V_{in} \cdot \frac{R_2}{R_1 + R_2} \Rightarrow \underline{\alpha = \frac{V_{id}}{V_{in}} = -\frac{R_2}{R_1 + R_2}}$$

$$\beta = -\frac{V_{id}}{V_o} \Big|_{V_{in}=0}$$

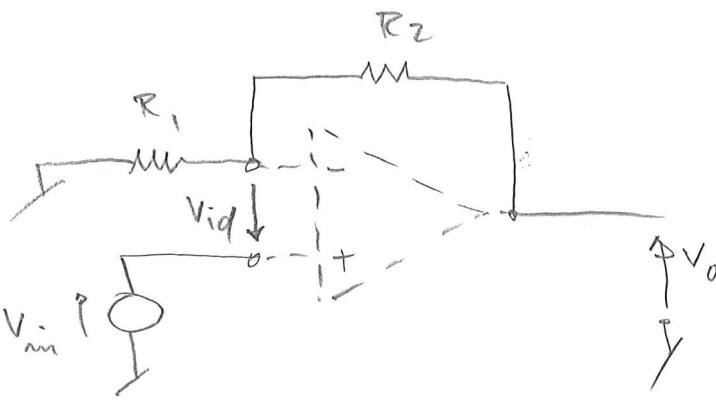


$$V_{id} = -\frac{R_1}{R_1 + R_2} \cdot V_o \Rightarrow \underline{\beta = -\frac{V_{id}}{V_o} = \frac{R_1}{R_1 + R_2}}$$

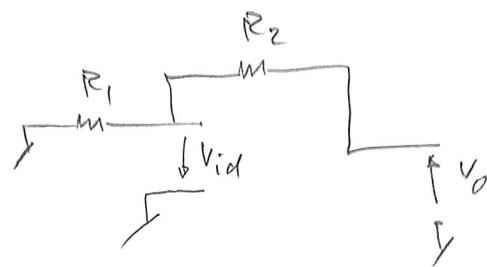
$$\frac{\alpha}{\beta} = A_{CLideal} = -\frac{R_2}{R_1 + R_2} \cdot \frac{R_1 + R_2}{R_1} = -\underline{\underline{\frac{R_2}{R_1}}}$$

Ideel  $A_{CL}$ ; dvs. for  $A_{OL} \rightarrow \infty \Rightarrow k_f = 1$

# Ikke-inverterende kobling

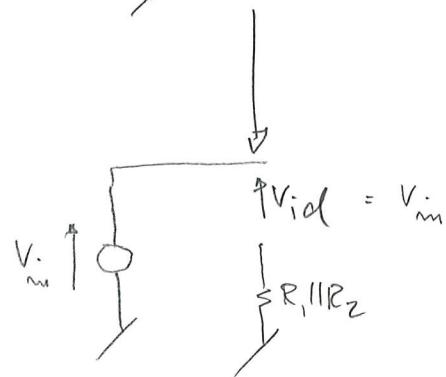
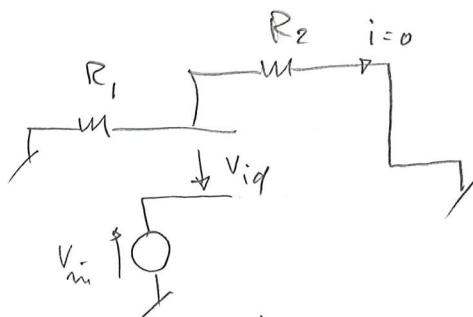


$$\beta = - \frac{V_{id}}{V_o} \Big|_{V_{in}=0}$$



$$V_{id} = -V_o \frac{R_1}{R_1 + R_2} \Rightarrow \beta = -\frac{V_{id}}{V_o} = \frac{R_1}{R_1 + R_2}$$

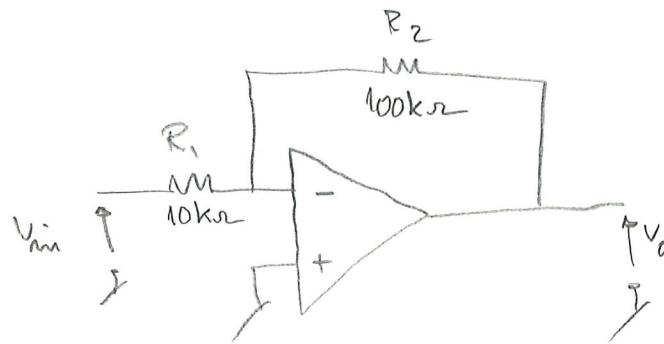
$$\alpha = \frac{V_{id}}{V_{in}} \Big|_{V_o=0}$$



$$\alpha = \frac{V_{id}}{V_{in}} = 1$$

$$\frac{\alpha}{\beta} = 1 \cdot \frac{R_1 + R_2}{R_1} = \frac{\underline{R_1 + R_2}}{\underline{R_1}} = 1 + \frac{R_2}{R_1}$$

Sp. 3 fra forberedelsen



$$A_{OL} = 10^6$$

$$A_{CL} = \frac{\beta}{\beta_0} \cdot K_f$$

$$\frac{\beta}{\beta_0} = -\frac{R_2}{R_1} \quad (\text{idetlit})$$

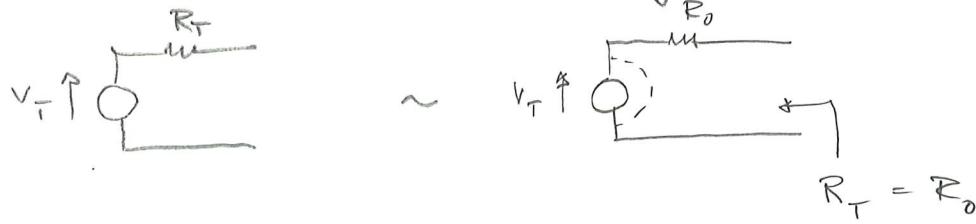
Følg 1. ligger i  $K_f$ :

$$\beta = \frac{R_2}{R_1 + R_2} = \frac{10}{10 + 100} = \frac{1}{11} \Rightarrow$$

$$K_f = \frac{1}{1 + \frac{1}{\beta A_{OL}}} = \frac{1}{1 + \frac{11}{10^6}} = 0,999989 \Rightarrow$$

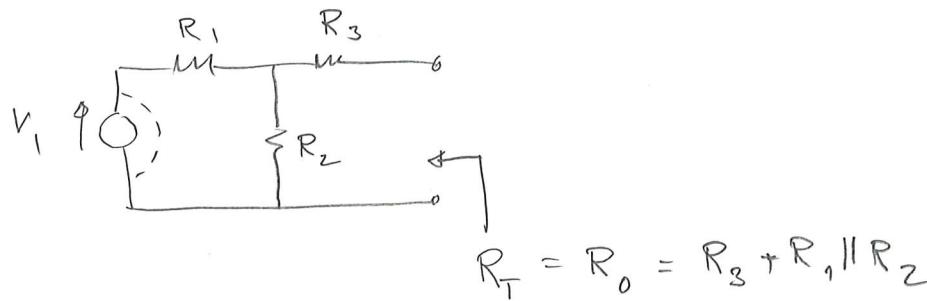
$$\text{Følg: } 1 - |K_f| = 1 - 0,999989 = 11 \cdot 10^{-6} = \underline{\underline{11 \text{ ppm}}}$$

# Thevenin modstand $\sim$ Udgangsmodstand

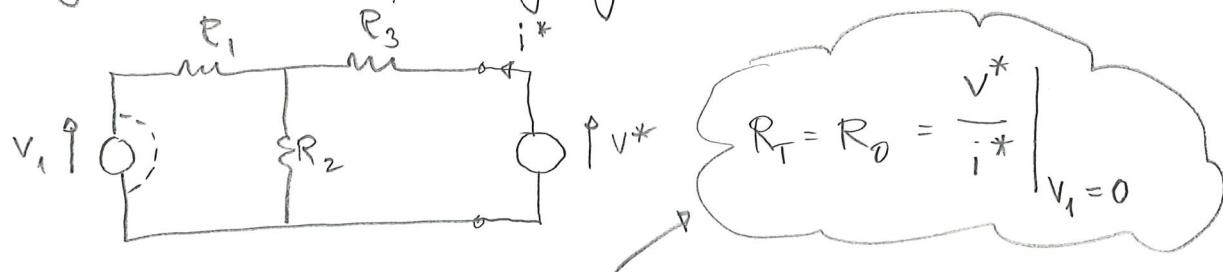


Princip : Væghængige kilder mulstilles, og man "set ind i den økv. Thevenin modstand".

Ex



Denne modstand findes egentlig som et "v/i - forhold" for en generator sat på udgangen:



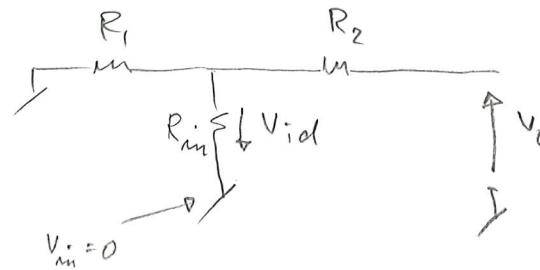
Metode til at finde  $R_o$  med

# Effekt af negativ feedback på $Z_0$ , $Z_{in}$ og $A_{ce}$

(se diagram på PPS)

Vi starter med at finde  $\beta$  (god idé til senere 😊)

$$\beta = - \frac{V_{id}}{V_o} \Big|_{V_{in}=0}$$

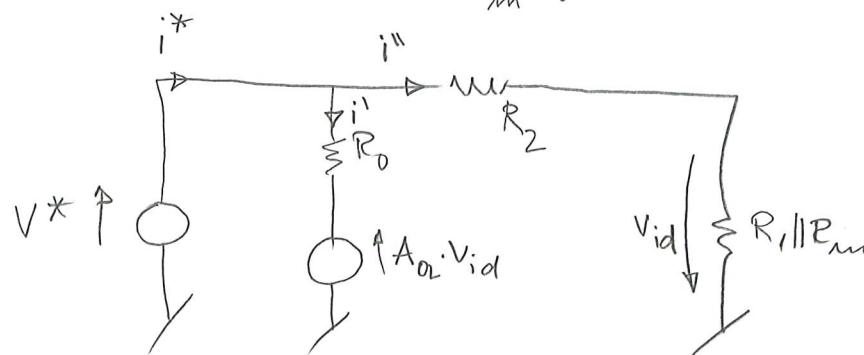


$$V_{id} = - \frac{R_1 \parallel R_{in}}{R_2 + R_1 \parallel R_{in}} \Rightarrow \beta = \frac{R_1 \parallel R_{in}}{R_2 + R_1 \parallel R_{in}}$$


---

## Vælgangsmodstand $Z_0$ ( $= R_T$ )

$$Z_0 = \frac{V^*}{I^*} \Big|_{V_{in}=0}$$



$$\textcircled{1} \quad i^* = i' + i''$$

$$\textcircled{2} \quad i' = \frac{V^* - A_{OL} \cdot V_{id}}{R_0} \quad \Rightarrow \quad i' = \frac{V^* + \beta A_{OL} \cdot V^*}{R_0}$$

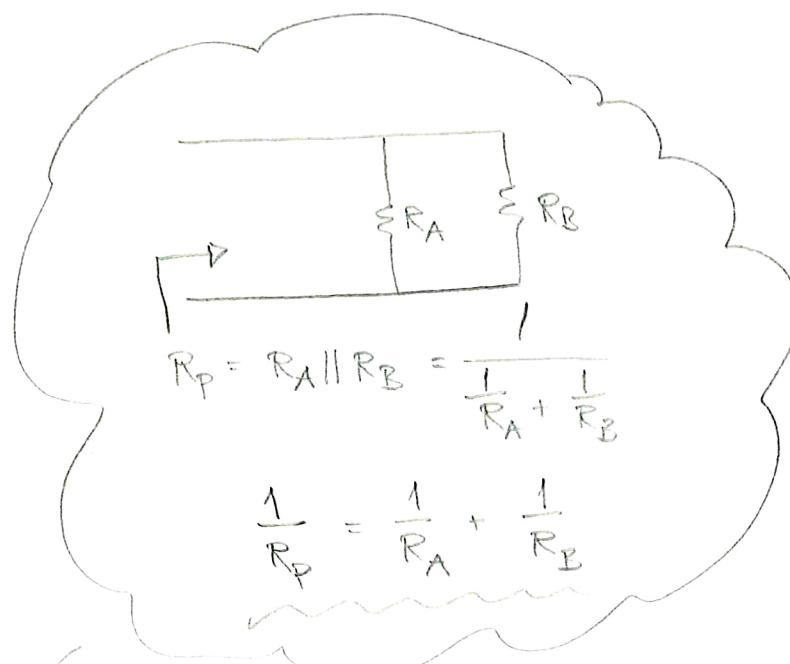
$$V_{id} = -V^* \cdot \frac{R_1 \parallel R_{in}}{R_2 + R_1 \parallel R_{in}} = -\beta \cdot V^*$$

$$\textcircled{3} \quad i'' = \frac{V^*}{R_2 + R_1 \parallel R_{in}}$$

$$\textcircled{2} + \textcircled{3} \rightarrow \textcircled{1} \quad \Rightarrow$$

$$i^* = \frac{V^* + \beta A_{OL} \cdot V^*}{R_0} + \frac{V^*}{R_2 + R_1 \parallel R_{in}} \quad \Rightarrow$$

$$\frac{i^*}{V^*} = \frac{1}{Z_0} = \frac{1 + \beta A_{OL}}{R_0} + \frac{1}{R_2 + R_1 \parallel R_{in}}$$



$$Z_0 = \frac{R_0}{1 + \beta A_{OL}} \parallel (R_2 + R_1 \parallel R_{in}) \approx \frac{R_0}{1 + \beta \cdot A_{OL}}$$

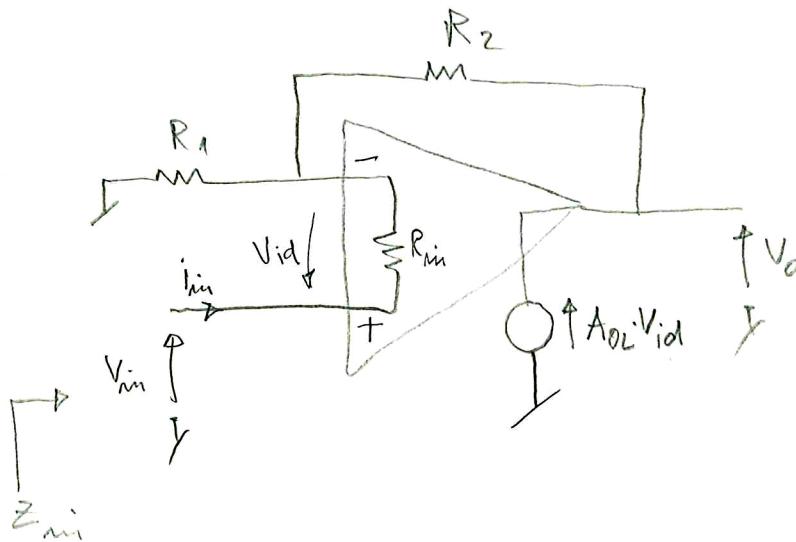
$$[\mu_2] \rightarrow [m_2] \quad [k_2]$$

NB:  $A_{OL} \rightarrow \infty \Rightarrow Z_0 \rightarrow 0 \Omega$

Sämtliche negativen  $R_0$  in der folgenden Berechnung.

# Indgangsmønststand $Z_{in}$

9



$$Z_{in} = \frac{V_{in}}{i_{in}}$$

$$V_{id} = e^+ - e^- = V_{in} - \beta \cdot V_o = V_{in} - \beta (A_{OL} \cdot V_{id}) \Rightarrow$$

$$V_{id} + \beta A_{OL} \cdot V_{id} = V_{in}$$

$$\downarrow V_{id} (1 + \beta A_{OL}) = V_{in}$$

$$\uparrow V_{id} = i_{in} \cdot R_{in} \Rightarrow$$

$$i_{in} \cdot R_{in} (1 + \beta A_{OL}) = V_{in} \Rightarrow$$

$$Z_{in} = \frac{V_{in}}{i_{in}} = \underline{\underline{R_{in} (1 + \beta A_{OL})}}$$

$$NB : A_{OL} \rightarrow \infty \Rightarrow Z_{in} \rightarrow \infty$$

## Lukkets sløjfe for styrkevingen $A_{CL}$

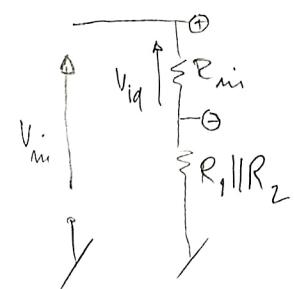
$$A_u = \frac{\alpha}{\beta} \cdot k_f$$

$k_f = \frac{1}{1 + \frac{1}{\beta A_{OL}}}$

Vi har:

$$\beta = \frac{R_1 \parallel R_{in}}{R_2 + R_1 \parallel R_{in}}$$

$$\alpha = \frac{V_{id}}{V_{in}} \Big|_{V_{id}=0} \rightarrow \alpha = \frac{R_{in}}{R_{in} + R_1 \parallel R_2}$$



$$\begin{aligned} \frac{\alpha}{\beta} &= \frac{R_{in}}{R_{in} + R_1 \parallel R_2} \cdot \frac{R_2 + R_1 \parallel R_{in}}{R_1 \parallel R_{in}} = \frac{R_{in}}{R_{in} + \frac{R_1 \cdot R_2}{R_1 + R_2}} \cdot \frac{R_2 + \frac{R_1 \cdot R_{in}}{R_1 + R_{in}}}{\frac{R_1 \cdot R_{in}}{R_1 + R_{in}}} \\ &= \frac{R_{in} (R_1 + R_2)}{R_1 R_{in} + R_2 R_{in} + R_1 R_2} \cdot \frac{R_1 R_{in} + R_2 R_{in} + R_1 R_2}{R_1 \cdot R_{in}} = \frac{R_1 + R_2}{R_1} = 1 + \frac{R_2}{R_1} \end{aligned}$$

$A_{u \text{ ideal}}$

NB: Bemerk at  $R_{in}$  ikke indgår.

$A_{OL} \rightarrow \infty \Rightarrow V_{id} = 0 \Rightarrow$  ingen strøm i  $R_{in}$

Således after:

$$A_{OL} \rightarrow \infty \Rightarrow A_{CL} \rightarrow \underline{\underline{A_{CL \text{ ideal}}}}$$

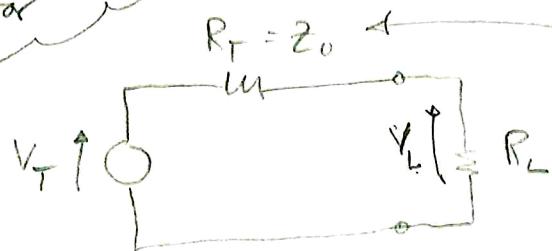
Evt. fyl/gfugelse (hvis  $A_{OL}$  ikke er uendelig) ligger i  $k_f$ .

# Feedback dumper

Hvor dan skal kredsløbet se ud som kilde?

Set fra  $R_L$

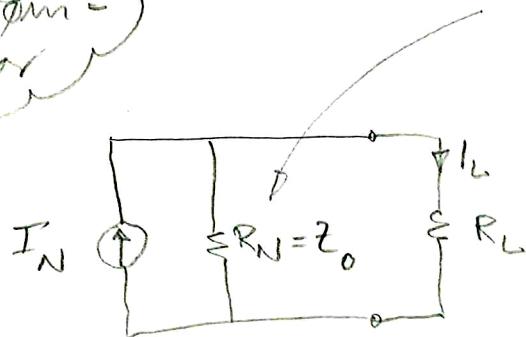
Ideal strømgeneratør



Værdi af  $R_0$  hvis  $V_L$  skal være konstant, selv om  $R_L$  varierer?

$$R_0 = 0 \cdot R_L \Rightarrow V_L = V_T$$

Ideal strømgeneratør



Værdi af  $R_0$  hvis  $I_L$  skal være konstant, selv om  $R_L$  varierer?

$$R_0 \rightarrow \infty \Rightarrow I_L = I_N$$

Hvor dan skal kredsløbet se ud som belastning?

Set fra  $V_s$

Husk her at fejlstørrelsen på figur 9.14:

$V_f$  for spændingsfeedback

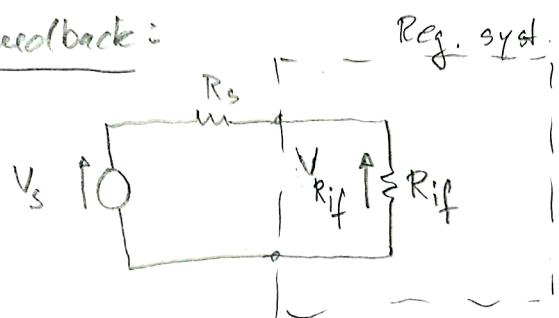
$i_f$  for strømfedback

skal regulere mod 0.

Teknisk set (se figur 9.14), skal man altså opnå, at

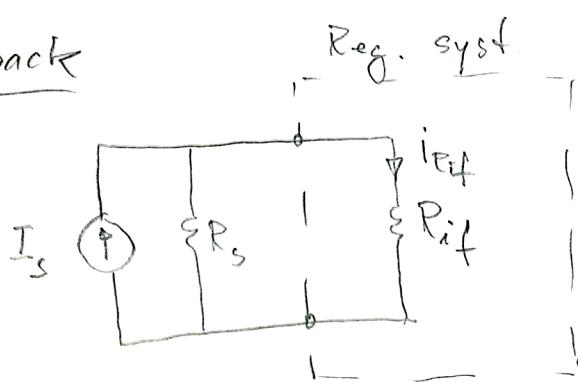
$$\boxed{\begin{aligned} V_f &= V_s \Rightarrow V_i = 0 \\ i_f &= I_s \Rightarrow i_i = 0 \end{aligned}}$$

Spændingsfeedback:



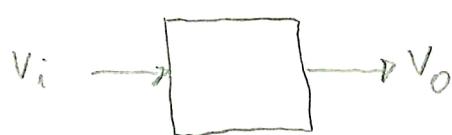
R<sub>if</sub> → ∞ ⇒  $V_{R_if} = V_s$  uanset værdien af R<sub>s</sub>

Strømfedback



R<sub>if</sub> = 0 Ω ⇒  $i_{R_if} = I_s$  uanset værdien af R<sub>s</sub>

# Forstärkertyper i styrelssloffen



$$\frac{v_o}{v_i} \left[ \frac{V}{V} \right] \rightarrow A_v$$

Spanningsförstärker



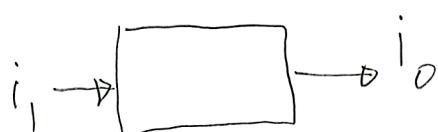
$$\frac{i_o}{i_i} \left[ \frac{A}{V} \right] \rightarrow G_m$$

Trans-konduktans



$$\frac{v_o}{i_i} \left[ \frac{V}{A} \right] \rightarrow R_m$$

Trans-impedans

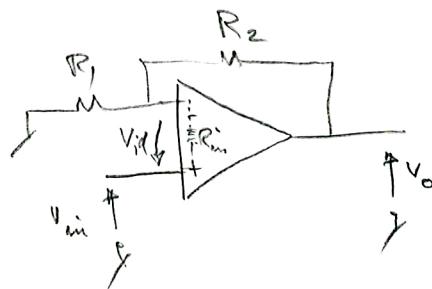


$$\frac{i_o}{i_i} \left[ \frac{A}{A} \right] \rightarrow A_i$$

Strömförstärker

Således i tabell 9.1 uppfatt följer:

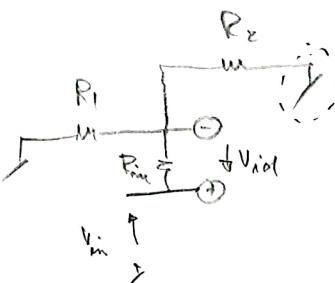
$$A_v = G_m = R_m = A_i = A_{OL}$$

Sp. 5 fra forberedelsen

$$R_1 = 10k\Omega; R_2 = 90k\Omega; R_{in} = 1M\Omega$$

Max. fylg. pga. ikke ideal AOL  $\approx 100$ ppm

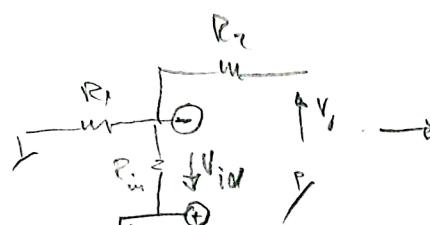
$$\alpha = \frac{V_{id}}{V_{in}} \Big|_{V_o=0}$$



$$\frac{V_{id}}{V_{in}} = \frac{R_{in}}{R_{in} + R_1 \parallel R_2} \cdot V_{in} \Rightarrow \alpha = \frac{R_{in}}{R_{in} + R_1 \parallel R_2}$$

$$= 0,991083$$

$$\beta = -\frac{V_{id}}{V_o} \Big|_{V_{in}=0}$$



$$\frac{V_{id}}{V_o} = -\frac{R_1 \parallel R_{in}}{R_2 + R_1 \parallel R_{in}} \cdot V_o \Rightarrow \beta = \frac{R_1 \parallel R_{in}}{R_2 + R_1 \parallel R_{in}}$$

$$= 0,0991080$$

$$\frac{\alpha}{\beta} = \frac{R_{in}}{R_{in} + \frac{R_1 \cdot R_{in}}{R_1 + R_2}} \cdot \frac{R_2 + \frac{R_1 \cdot R_{in}}{R_1 + R_{in}}}{\frac{R_1 \cdot R_{in}}{R_1 + R_{in}}} =$$

$$= \frac{\cancel{R_{in}(R_1 + R_2)}}{\cancel{R_{in}P_1 + R_{in}R_2 + R_1R_2}} \cdot \frac{\cancel{R_2 \cdot P_1 + P_2 R_{in} + R_1 \cdot R_{in}}}{\cancel{R_1 \cdot R_{in}}} = \frac{\cancel{R_1 + R_2}}{\cancel{R_1}} = \underline{\underline{10}}$$

NB!  
Vegle. av  $R_{in}$  ...  
hvordan?

$$f_l = 100 \text{ ppm} \Rightarrow 1 - k_f = 100 \cdot 10^{-6} \Rightarrow k_f = 999,900 \cdot 10^{-3}$$

$$k_f = \frac{1}{1 - \frac{1}{\beta \cdot A_{OL}}} \Rightarrow \frac{1}{\beta \cdot A_{OL}} = \frac{1}{k_f} - 1 \Rightarrow A_{OL} = \frac{1}{\frac{1}{k_f} - 1} \cdot \frac{1}{\beta} \Rightarrow$$

$$A_{OL} = \frac{1}{\frac{1}{999,900 \cdot 10^{-3}} - 1} \cdot \frac{1}{0,0991080} = 100,89 \cdot 10^3 = \underline{\underline{101 \cdot 10^3 = 100dB}}$$

Dette er en minimumsværdi for  $A_{OL}$ !