

# Introduction, linear system representations

## Control Theory, Lecture 1

by Sergei Savin

Spring 2022

- Motivation
- Ordinary differential equations
  - ▶ 1st order
  - ▶ n-th order
- Linear differential equations
  - ▶ 1st order
  - ▶ n-th order
- Changing n-th order ODE to a State-Space form
- State-Space to ODE
- Read more

# WHAT IS CONTROL?

The first obvious question is, what is control theory? The easiest strategy to answer this question is to bring examples of systems that you can *learn how to control*:



Figure 1: Drone



Figure 2: Robot arms

But beware, this is not the whole answer!

# WHY CONTROL?

The second most natural question to ask is - why do we need to study Control Theory? *Why do Computer scientists need Control Theory?*

The easy answer is:

it is very useful in case you will work in robotics, industrial automation, self-driving vehicles, drones, aerospace, etc.

**But!**

this answer does not tell the main part of the story - what about people who are NOT going to work in the listed areas?

# CONTROL AS AN APPLIED PROBLEM

We propose to view Control Theory as not only yet-another-subject. Instead we can try to see Control Theory course as **an application of your combined skills as a CS student**

# CONTROL AS AN APPLIED PROBLEM

## Skills you will learn and practice

In this course we provide you with learning and practical tasks that require:

- Linear Algebra, Differential Equations, Computational methods
- Dynamical systems, Stability (concept build on top of Theory of Ordinary Differential Equations).
- Simulation of dynamical systems (closely related to computational methods in Differential Equations), as a programming problem.
- Development of experiments in Google Colab, using Python, mathematical libraries, solving concrete, real world-related math-oriented problems.
- Representation (parametrization) of equations as a tool in both mathematical analysis and simulation, software development and problem solving.
- ...and many other things.

## ...SO, WHY CONTROL?

Control Theory, as given here, is focused on:

- ① Giving you a challenge to simultaneously learn a new concepts, new general and subject-specific math, and new programming tools.
- ② Providing you with clear outcomes in terms of *understanding* and ability to *solve well-defined and meaningful real-world problems*.
- ③ Being very useful for those who will proceed to work in robotics, automation, self-driving vehicles, drones, etc.

See it as a test case for your abilities as a CS specialist.

# ENOUGH FOR THE MOTIVATION

Now that we know (kinda) why we do it:

Let's start with the content of the course!



# ORDINARY DIFFERENTIAL EQUATIONS

## 1st order

Let us remember the normal form of first-order *ordinary differential equations (ODEs)*:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, t) \quad (1)$$

where  $\mathbf{x} = \mathbf{x}(t)$  is the solution of the equation and  $t$  is a free variable.

### Definition

We can call this equation (same as any other ODE) a *dynamical system*, and  $\mathbf{x}$  is called the *state* of the dynamical system.

### Example

$$\dot{x} = -3x^3 - 7 \quad (2)$$

# ORDINARY DIFFERENTIAL EQUATIONS

## n-th order

The normal form of an *n-th order* ordinary differential equation is:

$$x^{(n)} = f(x^{(n-1)}, x^{(n-2)}, \dots, \ddot{x}, \dot{x}, x, t) \quad (3)$$

where  $x = x(t)$  is the solution of the equation. Same as before, it is a *dynamical system*, but this time the set  $\{x, \dot{x}, \dots, x^{(n-1)}\}$  is called the *state* of the dynamical system.

### Example

$$\ddot{x} = \cos(2\dot{x}) - 10x + 7 \quad (4)$$

### Example

$$\begin{cases} \ddot{x}_1 = \dot{x}_1 + x_1 + x_2^2 - 4 \\ \ddot{x}_2 = 10x_1^3 + \ddot{x}_2 \end{cases} \quad (5)$$

# LINEAR DIFFERENTIAL EQUATIONS

## 1st order

Linear ODEs of the first order have normal form:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{b} \quad (6)$$

Example

$$\begin{cases} \dot{x}_1 = -20x_1 + 7x_2 + 17 \\ \dot{x}_2 = 10.5x_1 - 3x_2 - 5 \end{cases} \quad (7)$$

Example

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -8 & 5 & 2 \\ 0.5 & -10 & -2 \\ 1 & -1 & -20 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 4 \\ 10 \\ -5 \end{bmatrix} \quad (8)$$

# LINEAR DIFFERENTIAL EQUATIONS

## n-th order

A single linear ODE of the n-th order are often written in the form:

$$a_n x^{(n)} + a_{(n-1)} x^{(n-1)} + \dots + a_2 \ddot{x} + a_1 \dot{x} + a_0 x = b \quad (9)$$

Example

$$12 \ddot{x} - 3\ddot{x} + 5.5\dot{x} + 2x = 10.5 \quad (10)$$

Example

$$5\ddot{x} - 2\dot{x} + 10x = 2 \quad (11)$$

# LINEAR DIFFERENTIAL EQUATIONS

...are what we will study

In this course we will focus entirely on linear dynamical systems. In particular, we will take a good use of the following two forms:

$$a_n x^{(n)} + a_{(n-1)} x^{(n-1)} + \dots + a_2 \ddot{x} + a_1 \dot{x} + a_0 x = b \quad (12)$$

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{b} \quad (13)$$

the last one is called *state-space representation*.

Good news:

Both of those can be used to express any linear system, hence we can change one into the other.

# CHANGING N-TH ORDER ODE TO A STATE-SPACE FORM

Consider eq.  $\ddot{x} + a_2\ddot{x} + a_1\dot{x} + a_0x = b$ .

Make a substitution:  $z_1 = x$ ,  $z_2 = \dot{x}$ ,  $z_3 = \ddot{x}$ . Therefore:

$$\begin{cases} \dot{z}_1 = \dot{x} = z_2 \\ \dot{z}_2 = \ddot{x} = z_3 \\ \dot{z}_3 = -a_2\ddot{x} - a_1\dot{x} - a_0x + b = -a_2z_3 - a_1z_2 - a_0z_1 + b \end{cases} \quad (14)$$

Which can be directly put in the state-space form:

$$\begin{bmatrix} \dot{z}_1 \\ \dot{z}_2 \\ \dot{z}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -a_0 & -a_1 & -a_2 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ b \end{bmatrix} \quad (15)$$

An example of how linear algebra serves  
to solve a seemingly difficult problem

(advanced, not going to be on the test)

# STATE SPACE TO ODE

## part 1

Consider a system in state-space form:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \iff \dot{\mathbf{x}} = \mathbf{A}\mathbf{x} \quad (16)$$

We want to find such equation

$$\ddot{y} + b_2\dot{y} + b_1y = 0 \quad (17)$$

that there exists a linear transformation of the initial conditions of (16) to the initial conditions of (17), such that the resulting solutions of the initial value problem for both (16) and (17) can be transformed into one-another via another linear transformation.



# STATE SPACE TO ODE

## part 2

We start by recognizing that differentiation is a linear operation, so  $\dot{y}(t)$  is a linear transformation of (17) of the solution  $y(t)$ .

Next, we know that  $y = \mathbf{w}^\top \mathbf{x}$  for some  $\mathbf{w} = \begin{bmatrix} w_1 \\ w_2 \end{bmatrix}$ :

$$\dot{y} = \mathbf{w}^\top \mathbf{A} \mathbf{x} \quad (18)$$

$$\dot{y} = \begin{bmatrix} (a_{11}w_1 + a_{21}w_2) & (a_{12}w_1 + a_{22}w_2) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad (19)$$

Analogous for  $\ddot{y}$ :

$$\ddot{y} = \mathbf{w}^\top \mathbf{A} \mathbf{A} \mathbf{x} \quad (20)$$

# STATE SPACE TO ODE

## part 3

Combining our results we find the linear transformation between the variables  $x_1, x_2$  and  $y, \dot{y}$ :

$$\begin{bmatrix} y \\ \dot{y} \end{bmatrix} = \begin{bmatrix} w_1 & w_2 \\ (a_{11}w_1 + a_{21}w_2) & (a_{12}w_1 + a_{22}w_2) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad (21)$$

We can choose any  $w_1, w_2$ , as long as the resulting transformation matrix  $\mathbf{T}$  is not degenerate:

$$\mathbf{T} = \begin{bmatrix} w_1 & w_2 \\ (a_{11}w_1 + a_{21}w_2) & (a_{12}w_1 + a_{22}w_2) \end{bmatrix} \quad (22)$$

# STATE SPACE TO ODE

## part 4

Remember that:

$$\ddot{y} = \mathbf{w}^\top \mathbf{A} \mathbf{A} \mathbf{x} \iff \ddot{y} = -b_1 y - b_2 \dot{y} = -\mathbf{b}^\top \begin{bmatrix} y \\ \dot{y} \end{bmatrix} \quad (23)$$

Using the map we found previously, we obtain  $\ddot{y}$  as a linear function of  $y$ ,  $\dot{y}$ , with parameters  $w_1$ ,  $w_2$ :

$$\ddot{y} = \mathbf{w}^\top \mathbf{A} \mathbf{A} \mathbf{T}^+ \begin{bmatrix} y \\ \dot{y} \end{bmatrix} \quad (24)$$

$$\mathbf{b} = -\mathbf{w}^\top \mathbf{A} \mathbf{A} \mathbf{T}^+ \quad (25)$$

From this it is clear how the same can be generalized to higher dimensions.

# STATE SPACE TO ODE

## part 5

[Check out the code implementation.](#)



- State Space Representations of Linear Physical Systems  
[lpsa.swarthmore.edu/Representations/SysRepSS.html](http://lpsa.swarthmore.edu/Representations/SysRepSS.html)
- Transformation: Differential Equation to State Space  
[lpsa.swarthmore.edu/.../DE2SS.html](http://lpsa.swarthmore.edu/.../DE2SS.html)

# THANK YOU!

Lecture slides are available via Moodle.

You can help improve these slides at:

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Check Moodle for additional links, videos, textbook suggestions.



# Stability

## Control Theory, Lecture 2

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- Critical point (node)
- Stability
- Asymptotic stability
- Stability vs Asymptotic stability
- LTI and autonomous LTI
- Stability of autonomous LTI
  - ▶ Example: real eigenvalues
  - ▶ Example: complex eigenvalues
  - ▶ General case
  - ▶ Illustration
- Read more



# CRITICAL POINT (NODE)

Consider the following ODE:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, t) \quad (1)$$

Let  $\mathbf{x}_0$  be such a state that:

$$\mathbf{f}(\mathbf{x}_0, t) = 0 \quad (2)$$

Then such state  $\mathbf{x}_0$  is called a *node* or a *critical point*.

Node  $\mathbf{x}_0$  is called *stable* iff for any constant  $\delta$  there exists constant  $\varepsilon$  such that:

$$\|\mathbf{x}(0) - \mathbf{x}_0\| < \delta \longrightarrow \|\mathbf{x}(t) - \mathbf{x}_0\| < \varepsilon \quad (3)$$

Think of it as "for any initial point that lies at most  $\delta$  away from  $\mathbf{x}_0$ , the rest of the trajectory  $\mathbf{x}(t)$  will be at most  $\varepsilon$  away from  $\mathbf{x}_0$ ".

Or, more picturesque, think of it as "the solutions with different initial conditions do not diverge from the node"

Node  $\mathbf{x}_0$  is called *asymptotically stable* iff for any constant  $\delta$  it is true that:

$$||\mathbf{x}(0) - \mathbf{x}_0|| < \delta \longrightarrow \lim_{t \rightarrow \infty} \mathbf{x}(t) = \mathbf{x}_0 \quad (4)$$

Think of it as "for any initial point that lies at most  $\delta$  away from  $\mathbf{x}_0$ , the trajectory  $\mathbf{x}(t)$  will asymptotically approach the point  $\mathbf{x}_0$ ".

Or, more picturesque, think of it as "the solutions with different initial conditions converge to the node"

# STABILITY VS ASYMPTOTIC STABILITY

## Example

Consider dynamical system  $\dot{x} = 0$ , and solution  $x = 7$ . This solution is stable, but not asymptotically stable (other solutions do not diverge from  $x = 7$ , but do not converge to it either).

## Example

Consider dynamical system  $\dot{x} = -x$ , and solution  $x = 0$ . This solution is stable and asymptotically stable (other solutions converge to  $x = 0$ ).

## Example

Consider dynamical system  $\dot{x} = x$ , and solution  $x = 0$ . This solution is unstable (other solutions diverge from  $x = 0$ ).

Consider the following linear ODE:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \quad (5)$$

This is called a *linear time-invariant system*, or *LTI*.

Consider the following linear ODE:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} \quad (6)$$

This is also an LTI, but it is also called an *autonomous system*, since its evolution depends only on the state of the system.

# STABILITY OF AUTONOMOUS LTI

## Real eigenvalues

Consider autonomous LTI:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} \quad (7)$$

where  $\mathbf{A}$  can be decomposed via eigen-decomposition as  $\mathbf{A} = \mathbf{V}\mathbf{D}\mathbf{V}^{-1}$ , where  $\mathbf{D}$  is a diagonal matrix.

$$\dot{\mathbf{x}} = \mathbf{V}\mathbf{D}\mathbf{V}^{-1}\mathbf{x} \quad (8)$$

Multiply it by  $\mathbf{V}^{-1} \longrightarrow \mathbf{V}^{-1}\dot{\mathbf{x}} = \mathbf{V}^{-1}\mathbf{V}\mathbf{D}\mathbf{V}^{-1}\mathbf{x}$ .

Define  $\mathbf{z} = \mathbf{V}^{-1}\mathbf{x} \longrightarrow \dot{\mathbf{z}} = \mathbf{D}\mathbf{z}$ .

Since elements of  $\mathbf{D}$  are real, we can clearly see, that iff they are *all negative* will the system be asymptotically stable. If they are non-positive, the system is stable. And those elements are eigenvalues of  $\mathbf{A}$ .

# STABILITY OF AUTONOMOUS LTI

## Complex eigenvalues, 2-dimensional case (1)

Let us consider the following system:

$$\begin{bmatrix} \dot{\mathbf{x}}_1 \\ \dot{\mathbf{x}}_2 \end{bmatrix} = \begin{bmatrix} \alpha & -\beta \\ \beta & \alpha \end{bmatrix} \begin{bmatrix} \mathbf{x}_1 \\ \mathbf{x}_2 \end{bmatrix} \quad (9)$$

The eigenvalues of the system are  $\alpha \pm i\beta$ . We denote  $\begin{bmatrix} \mathbf{x}_1 \\ \mathbf{x}_2 \end{bmatrix} = \mathbf{x}$ .

We start by claiming that the system will be stable iff the  $\dot{\mathbf{x}}^\top \mathbf{x} < 0$ . Indeed, vector  $\dot{\mathbf{x}}$  can always be decomposed into two components,  $\dot{\mathbf{x}}_\parallel$  parallel to  $\mathbf{x}$ , and  $\dot{\mathbf{x}}_\perp$  perpendicular to  $\mathbf{x}$ . By definition  $\dot{\mathbf{x}}_\perp^\top \mathbf{x} = 0$ , and is responsible for the change in orientation of  $\mathbf{x}$ . The value of  $\dot{\mathbf{x}}_\parallel$  is responsible for the change in the length of  $\mathbf{x}$ ; the length would shrink iff  $\dot{\mathbf{x}}_\parallel$  is of opposite direction to  $\mathbf{x}$ , giving negative value of the dot product  $\dot{\mathbf{x}}^\top \mathbf{x}$ .

# STABILITY OF AUTONOMOUS LTI

## Complex eigenvalues, 2-dimensional case (2)

Let us compute  $\dot{\mathbf{x}}^\top \mathbf{x}$ :

$$\dot{\mathbf{x}}^\top \mathbf{x} = \begin{bmatrix} \mathbf{x}_1 & \mathbf{x}_2 \end{bmatrix} \begin{bmatrix} \alpha & -\beta \\ \beta & \alpha \end{bmatrix} \begin{bmatrix} \mathbf{x}_1 \\ \mathbf{x}_2 \end{bmatrix} \quad (10)$$

$$\dot{\mathbf{x}}^\top \mathbf{x} = \alpha(\mathbf{x}_1^2 + \mathbf{x}_2^2) \quad (11)$$

From this it is clear that the product  $\dot{\mathbf{x}}^\top \mathbf{x} < 0$  is negative iff  $\alpha < 0$ .

### Definition

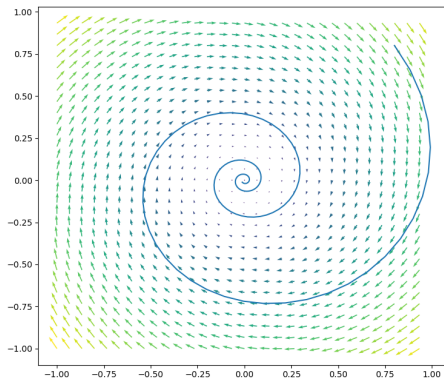
As long as the *real parts of the eigenvalues* of the system are *strictly negative*, the system is *asymptotically stable*. If the real parts of the eigenvalues of the system are zero, the system is *marginally stable*.



# STABILITY OF AUTONOMOUS LTI

## Complex eigenvalues, 2-dimensional case (3)

Vector field of  $\begin{bmatrix} \dot{\mathbf{x}}_1 \\ \dot{\mathbf{x}}_2 \end{bmatrix} = \begin{bmatrix} \alpha & -\beta \\ \beta & \alpha \end{bmatrix} \begin{bmatrix} \mathbf{x}_1 \\ \mathbf{x}_2 \end{bmatrix}$  is shown below:



# STABILITY OF AUTONOMOUS LTI

## General case (1)

Given  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x}$ , where  $\mathbf{A}$  can be decomposed via eigen-decomposition as  $\mathbf{A} = \mathbf{U}\mathbf{C}\mathbf{U}^{-1}$ , where  $\mathbf{C}$  is a complex-valued diagonal matrix and  $\mathbf{U}$  is a complex-valued invertible matrix.

We multiply both sides by  $\mathbf{U}^{-1}$ , then define  $\mathbf{z} = \mathbf{U}^{-1}\mathbf{x}$  to arrive at:

$$\dot{\mathbf{z}} = \mathbf{C}\mathbf{z} \quad (12)$$

which falls into a set of independent equations, with complex coefficients  $c_j$ :

$$\dot{z}_j = c_j z_j \quad (13)$$

# STABILITY OF AUTONOMOUS LTI

## General case (2)

Expanding  $c_j = \alpha + i\beta$ , and  $z_j = u + iv$  (we dismiss subscripts for clarity), we find that  $\dot{z}_j = c_j z_j$  can be expanded as:

$$\dot{u} + i\dot{v} = \dot{z}_j = c_j z_j = (\alpha + i\beta)(u + iv) \quad (14)$$

$$\dot{u} + i\dot{v} = \alpha u + i\beta u + i\alpha v - \beta v \quad (15)$$

$$\begin{bmatrix} \dot{u} \\ \dot{v} \end{bmatrix} = \begin{bmatrix} \alpha & -\beta \\ \beta & \alpha \end{bmatrix} \begin{bmatrix} u \\ v \end{bmatrix} \quad (16)$$

As we can see,  $\dot{z}_j = c_j z_j$  is asymptotically stable iff  $\operatorname{Re}(c_j) < 0$ , and marginally stable if  $\alpha = \operatorname{Re}(c_j) = 0$ . Same is true for  $\dot{\mathbf{z}} = \mathbf{C}\mathbf{z}$  and hence, for  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x}$ , as  $\mathbf{U}$  is invertible.

# STABILITY OF AUTONOMOUS LTI

## Condition

Consider an autonomous LTI:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} \quad (17)$$

### Definition

Eq. (17) is stable iff real parts of eigenvalues of  $\mathbf{A}$  are non-positive.

### Definition

Eq. (17) is asymptotically stable iff real parts of eigenvalues of  $\mathbf{A}$  are negative.

# STABILITY OF AUTONOMOUS LTI

## Illustration

Here is an illustration of *phase portraits* of two-dimensional LTIs with different types of stability:

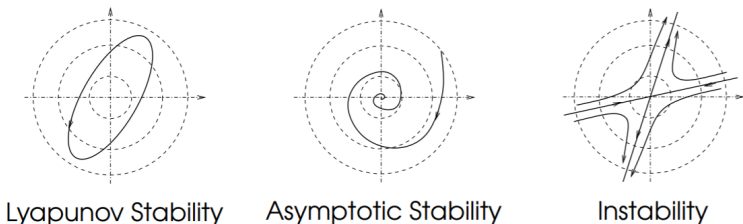
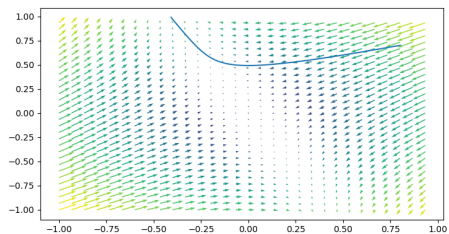
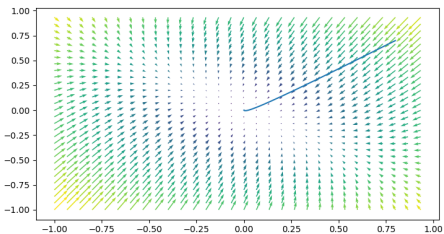
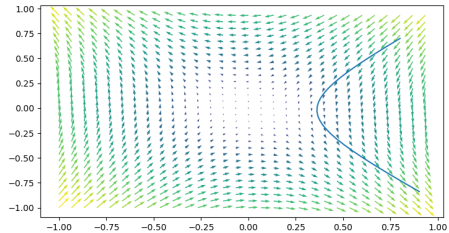
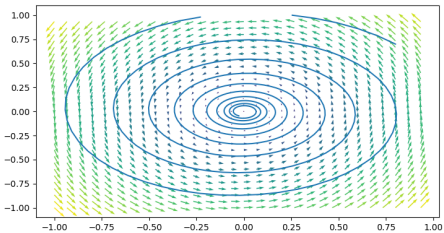


Figure 1: phase portraits for different types of stability

Credit: [staff.uz.zgora.pl/wpaszke/materialy/spc/Lec13.pdf](http://staff.uz.zgora.pl/wpaszke/materialy/spc/Lec13.pdf)



- Control Systems Design, by Julio H. Braslavsky  
[staff.uz.zgora.pl/wpaszke/materialy/spc/Lec13.pdf](http://staff.uz.zgora.pl/wpaszke/materialy/spc/Lec13.pdf)

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# Laplace Transform and Transfer Functions

## Control Theory, Lecture 3

by Sergei Savin

Spring 2022

- ODE solutions
- Laplace Transform
- Laplace Transform of a derivative
- Derivative operator
- Transfer Function
  - ▶ Example
  - ▶ Interesting things done easy
- State-Space to Transfer Function conversion
- Read more

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -5 & -10 & -10 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} u \quad (1)$$



Figure 1: Autonomous ODE ( $u = 0$ )

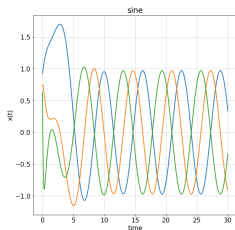


Figure 2: reaction to sine wave ( $u = \sin(t)$ )



Figure 3: Reaction to step function ( $u = 1$ )

By definition, Laplace transform of a function  $f(t)$  is given as:

$$F(s) = \int_0^{\infty} f(t)e^{-st}dt \quad (2)$$

where  $F(s)$  is called an *image* of the function.

The study of Laplace transform is a separate mathematical field with applications in solving ODEs, which we won't cover.

However, we will consider transform of one case of interest - transform of a derivative.

# LAPLACE TRANSFORM OF A DERIVATIVE

Consider a derivative  $\frac{dx}{dt}$  and its transform:

$$\mathcal{L}\left(\frac{dx}{dt}\right) = \int_0^{\infty} \frac{dx}{dt} e^{-st} dt \quad (3)$$

we will make use of the integration by parts formula:

Integration by parts

$$\int v \frac{du}{dt} dt = vu - \int \frac{dv}{dt} u dt \quad (4)$$

In our case,  $\frac{du}{dt} = \frac{dx}{dt}$ ,  $u = x$ ,  $v = e^{-st}$ ,  $\frac{dv}{dt} = -se^{-st}$ :

$$\mathcal{L}\left(\frac{dx}{dt}\right) = [xe^{-st}]_0^{\infty} - \int_0^{\infty} -se^{-st} x dt \quad (5)$$

$$\mathcal{L}\left(\frac{dx}{dt}\right) = -x(0) + s\mathcal{L}(x) \quad (6)$$

Thus, assuming that  $x(0) = 0$ , we can obtain a *derivative operator*:

$$\mathcal{L}\left(\frac{dx}{dt}\right) = s\mathcal{L}(x) \quad (7)$$

Please notice that (7) is only true when  $x(0) = 0$ ; it generally does not look very elegant either. Introducing a big-time abuse of notation, we can denote  $x(s) = \mathcal{L}(x)$  and then drop the brackets, leaving us with:

$$\frac{dx}{dt} \longrightarrow sx \quad (8)$$

This form of a derivative operator has a very strange notation in terms of the Laplace transform theory, but is very simple to use in practice.

# TRANSFER FUNCTION

Consider the following ODE, where  $u$  is an input (function of time that influences the solution of the ODE):

$$\ddot{x} + a\dot{x} + bx = u \quad (9)$$

We can rewrite it using the derivative operator:

$$s^2x + asx + bx = u \quad (10)$$

and then collect  $x$  on the left-hand-side:

$$x = \frac{1}{s^2 + as + b}u \quad (11)$$

At this point the mathematical meaning of this expression as an ODE is very vague, but it has a different direct use; this form is called a *transfer function*.

# TRANSFER FUNCTION

## Examples

### Example

Given ODE:  $2\ddot{x} + 5\dot{x} - 40x = 10u$

The transfer function for it looks:  $x = \frac{10}{2s^3 + 5s - 40}u$

### Example

Given ODE:  $2\dot{x} - 4x = u$

The transfer function for it looks:  $x = \frac{1}{2s - 4}u$

### Example

Given ODE:  $3\ddot{x} + 4x = u$

The transfer function for it looks:  $x = \frac{1}{2s^3 + 4}u$



# TRANSFER FUNCTION

Interesting things done easy

Consider the following (strange) ODE:

$$2\ddot{x} + 3\dot{x} + 2x = 10\dot{u} - u \quad (12)$$

Using the differential equation:

$$2s^2x + 3sx + 2x = 10su - u \quad (13)$$

...which is the same as:

$$(2s^2 + 3s + 2)x = (10s - 1)u \quad (14)$$

The transfer function for it looks:

$$x = \frac{10s - 1}{2s^2 + 3s + 2}u \quad (15)$$

# STATE-SPACE TO TRANSFER FUNCTION CONVERSION

Transfer functions are being used to study the relation between the input and the output of the dynamical system.

Consider standard form state-space dynamical system:

$$\begin{cases} \dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u} \end{cases} \quad (16)$$

We can rewrite it using the derivative operator:

$$\begin{cases} s\mathbf{I}\mathbf{x} - \mathbf{A}\mathbf{x} = \mathbf{B}\mathbf{u} \\ \mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u} \end{cases} \quad (17)$$

and then collect  $\mathbf{x}$  on the left-hand-side:  $\mathbf{x} = (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}\mathbf{u}$   
and finally, express  $\mathbf{y}$  out:

$$\mathbf{y} = (\mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}) \mathbf{u} \quad (18)$$

Let the dynamic system be described as a transfer function:

$$y = G(s)x \quad (19)$$

We can try to modify the input based on how the output looks-like. Since we always do it in a linear way, we can write it as:

$$y = G(s)(x - H(s)y) \quad (20)$$

where  $H(s)y$  is called *feedback*.

How would the transfer function from  $x$  to  $y$  look like?

# TRANSFER FUNCTION AND CONTROL (1)

From  $y = G(s)(x - H(s)y)$  we go:

$$y = G(s)x - G(s)H(s)y \quad (21)$$

$$y + G(s)H(s)y = G(s)x \quad (22)$$

$$y = \frac{G(s)}{1 + G(s)H(s)}x \quad (23)$$

Thus, we found *closed-loop* transfer function:

$$W(s) = \frac{G(s)}{1 + G(s)H(s)} \quad (24)$$

- Chapter 6 Transfer Functions
- Control Systems Lectures - Transfer Functions, by Brian Douglas
- The Laplace Transform - A Graphical Approach, by Brian Douglas

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# Frequency response, Bode

## Control Theory, Lecture 4

by Sergei Savin

Spring 2022

- Laplace and Fourier transforms
- Laplace and steady state solution
- Bode plot
- Bode plot - example
- Stability margins
- Code example



# LAPLACE AND FOURIER TRANSFORMS

- *Fourier series* can be seen as representing a periodic function as a sum of harmonics (sines and cosines). These sines and cosines can be thought of as forming a basis in a linear space. The coefficients of the series can be thought of as a discrete spectrum of the function.
- *Fourier transform* gives a continuous spectrum of the function. The "basis" is still made of harmonic functions.
- *Laplace transform* also gives a continuous spectrum of the function, but in a different basis: the basis is given by complex exponentials. I like to think of this basis as solutions of second order ODEs.

# LAPLACE AND FOURIER TRANSFORMS

Let's compare. Fourier transform:

$$F(\omega) = \int_{-\infty}^{\infty} f(t)e^{-2\pi j t \omega} dt, \quad \omega \in \mathbb{R} \quad (1)$$

Laplace transform:

$$F(s) = \int_0^{\infty} f(t)e^{-st} dt, \quad s \in \mathbb{C} \quad (2)$$

We can see that Fourier looks like Laplace with purely imaginary number in the exponent.

# LAPLACE AND STEADY STATE SOLUTION

From analysing solutions of linear ODEs we know that, given harmonic input (sine, cosine, their combination) "after the transient process is over, the solution approaches a harmonic with the same frequency", but possibly different amplitude and phase.

Intuitively we can think of the imaginary part of  $s$  as having to do with this frequency response.

The kernel function of the Laplace transform is  $e^{-st}$  with  $s = \sigma + j\omega$  being a complex variable. If  $\sigma = 0$ , the kernel becomes  $e^{-j\omega t} = \cos(\omega t) - j\sin(\omega t)$ . You can see the similarity with Fourier transform kernel.

# BODE PLOT

The first key idea of a Bode plot is substitution of purely complex variable  $j\omega$  in place of Laplace variable  $s$ , which can have non-zero real part.

Given a transfer function  $W(s)$ ,  $s = \sigma + j\omega$  we can analyse its behaviour when  $\sigma = 0$ . We can plot its amplitude

$a(\omega) = |W(j\omega)|$  and its phase

$\varphi(\omega) = \text{atan2}(\text{im}(W(j\omega)), \text{real}(W(j\omega)))$ .

Bode plot is actually two plots, 1)  $20 \cdot \log(a(\omega))$  and 2)  $\frac{180}{\pi}\varphi(\omega)$ . The 20 and log has to do with the vertical axis being in decibels.

## BODE PLOT - EXAMPLE

Consider  $W(s) = \frac{1}{1+s}$ . Then  $W(j\omega) = \frac{1}{1+j\omega}$ . We can transform it as:

$$W(j\omega) = \frac{1 - j\omega}{(1 + j\omega)(1 - j\omega)} = \frac{1 - j\omega}{1 + \omega^2} \quad (3)$$

We that we know that  $\text{real}(W(j\omega)) = \frac{1}{1+\omega^2}$  and  $\text{im}(W(j\omega)) = -\frac{\omega}{1+\omega^2}$ .

Bode plot is then given as:

$$a(\omega) = \sqrt{\frac{1 - \omega^2}{(1 + \omega^2)^2}} \quad (4)$$

$$\varphi(\omega) = \text{atan2} \left( -\frac{\omega}{1 + \omega^2}, \frac{1}{1 + \omega^2} \right) \quad (5)$$

## BODE PLOT - STABILITY MARGINS

Before we discuss the use of Bode plot, let us remember that closed-loop transfer function has form (when simple feedback is used):

$$W(s) = \frac{G(s)}{1 + G(s)} \quad (6)$$

Substituting  $s \rightarrow j\omega$  we get:

$$W(\omega) = \frac{G(j\omega)}{1 + G(j\omega)} \quad (7)$$

From this we can see that  $W(\omega)$  becomes ill-defined if  $G(j\omega) = -1$ . Meaning, we want to avoid two things happening simultaneously: the amplitude of  $G(j\omega)$  being equal to 1, and its phase (argument) being equal to  $180^\circ$  (remember, phase of  $0^\circ$  is pure positive real number, phase of  $90^\circ$  is pure positive imaginary number,  $180^\circ$  is pure negative real number, etc.).

# STABILITY MARGINS - GRAPHICAL EXAMPLE

Let's check an illustration:



Check the colab notebook based on the example above for an illustration of how the Bode plot can be made by hand or via scipy signal library.





## ■ Control System Lectures - Bode Plots, Introduction

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# Stabilizing Control

## Control Theory, Lecture 5

by Sergei Savin

Spring 2022

- Changing stability
- Stabilizing control
- Linear control: Closed-loop system,
- Affine control
- Error dynamics
- Affine trajectory tracking
- Point-to-point control
- Pure state feedback
- Read more

# CHANGING STABILITY

Here are two LTIs:

$$\dot{x} = 2x \quad (1)$$

$$\dot{x} = 2x + u \quad (2)$$

First one is autonomous and unstable. Second one is not autonomous, and we won't know whether or not it is stable, until we know what  $u$  is.

If we pick  $u = 0$ , the result is an unstable equation. But we can also pick  $u$  such that the resulting dynamics is stable, such as  $u = -3x$ :

$$\dot{x} = 2x + u = 2x - 3x = -x \quad (3)$$

So, we can use *control input*  $u$  to change stability of the system!

## Definition

The problem of finding control law  $\mathbf{u}$  that make a certain solution  $\mathbf{x}^*$  of dynamical system  $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u})$  stable is called *stabilizing control problem*

This is true for both linear and non-linear systems. But for linear systems we can get a lot more details about this problem, if we restrict our choice of control law.

# LINEAR CONTROL

## Closed-loop system

Consider an LTI system:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \quad (4)$$

and let us chose *control as a linear function of the state  $x$* :

$$\mathbf{u} = -\mathbf{K}\mathbf{x} \quad (5)$$

Thus, we know how the system is going to look when the control is applied:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} - \mathbf{B}\mathbf{K}\mathbf{x} \quad (6)$$

$$\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{B}\mathbf{K})\mathbf{x} \quad (7)$$

Note that (7) is an autonomous system. We call this a *closed loop* system.

Observing the system  $\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{BK})\mathbf{x}$  we obtained, we can notice that we already have the tools to analyse its stability:

## Stability condition for LTI closed-loop system

The real parts of the eigenvalues of the matrix  $(\mathbf{A} - \mathbf{BK})$  should be negative for asymptotic stability, or non-positive for stability in the sense of Lyapunov.

## Hurwitz matrix

If square matrix  $\mathbf{M}$  has eigenvalues with strictly negative real parts, it is called Hurwitz. We will denote it as  $\mathbf{M} \in \mathcal{H}$ .

So, all you need to do is to find such  $\mathbf{K}$  that  $(\mathbf{A} - \mathbf{BK})$  is Hurwitz, and you made a an asymptotically stable closed-loop system!



# AFFINE CONTROL

## Part 1

We don't have to limit ourselves to just this  $\dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}$  and  $\mathbf{u} = -\mathbf{Kx}$  pair.

In fact, this pair mostly works for the simple case when the solution we want to stabilize is trivial  $\mathbf{x}^*(t) = 0$ .

Let us consider a slightly more complicated system:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} + \mathbf{c} \quad (8)$$

This is called *affine system*, because of the constant term  $\mathbf{c}$ .

What is the control that stabilizes this system? Let us propose an *affine control law*:

$$\mathbf{u} = -\mathbf{K}\mathbf{x} + \mathbf{u}^* \quad (9)$$

where  $\mathbf{u}^*$  is a constant term.

Thus, from  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} + \mathbf{c}$  and  $\mathbf{u} = -\mathbf{K}\mathbf{x} + \mathbf{u}^*$  we get the following closed-loop system:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} - \mathbf{B}\mathbf{K}\mathbf{x} + \mathbf{B}\mathbf{u}^* + \mathbf{c} \quad (10)$$

And as long as we can choose such  $\mathbf{u}^*$  that  $\mathbf{B}\mathbf{u}^* = -\mathbf{c}$ , we will get back to the previously seen form  $\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{B}\mathbf{K})\mathbf{x}$ .

### Existence of the stabilizing control

Same as it is possible that there exists no such  $\mathbf{K}$  that  $\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{B}\mathbf{K})\mathbf{x}$  is stable, there might exist no such  $\mathbf{u}^*$  that  $\mathbf{B}\mathbf{u}^* = -\mathbf{c}$

Let us now consider an arbitrary solution  $\mathbf{x}^* = \mathbf{x}^*(t)$  for the linear system

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \quad (11)$$

and try to find a stabilizing control for it.

Our first step is to notice that, if  $\mathbf{x}^* = \mathbf{x}^*(t)$  is a solution, that means that it satisfies the ODE (11):

$$\dot{\mathbf{x}}^* = \mathbf{A}\mathbf{x}^* + \mathbf{B}\mathbf{u}^* \quad (12)$$

where  $\mathbf{u}^* = \mathbf{u}^*(t)$  is some control law, for which the solution  $\mathbf{x}^* = \mathbf{x}^*(t)$  is obtained.

If we are not given  $\mathbf{u}^* = \mathbf{u}^*(t)$ , we can compute it as:

$$\mathbf{u}^* = \mathbf{B}^+(\dot{\mathbf{x}}^* - \mathbf{A}\mathbf{x}^*) \quad (13)$$

where  $\mathbf{B}^+$  is a pseudo-inverse, and the solution to this least-squared problem will have to have no residual (since  $\mathbf{x}^* = \mathbf{x}^*(t)$  is a solution).

$$\|\dot{\mathbf{x}}^* - \mathbf{A}\mathbf{x}^* - \mathbf{B}\mathbf{B}^+(\dot{\mathbf{x}}^* - \mathbf{A}\mathbf{x}^*)\| = 0 \quad (14)$$

Now, let us introduce the concept of *control error*  $\mathbf{e}$ :

$$\mathbf{e} = \mathbf{x} - \mathbf{x}^* \quad (15)$$

### Control error and stability

If control error goes to zero asymptotically, every solution goes to  $\mathbf{x}^*$ .

Remember that we have two simultaneous equations:

$\dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}$  and  $\dot{\mathbf{x}}^* = \mathbf{Ax}^* + \mathbf{Bu}^*$ . We can now subtract one from the other to get:

$$\dot{\mathbf{x}} - \dot{\mathbf{x}}^* = \mathbf{Ax} - \mathbf{Ax}^* + \mathbf{Bu} - \mathbf{Bu}^* \quad (16)$$

in other words:

$$\dot{\mathbf{e}} = \mathbf{Ae} + \mathbf{Bv} \quad (17)$$

where  $\mathbf{v} = \mathbf{u} - \mathbf{u}^*$

We arrived at a new dynamical system  $\dot{\mathbf{e}} = \mathbf{A}\mathbf{e} + \mathbf{B}\mathbf{v}$ , which is an LTI, and we are interested in stabilizing the solution  $\mathbf{e}^* = 0$ . We know how to do it with a linear control law:

$$\mathbf{v} = -\mathbf{K}\mathbf{e} \quad (18)$$

Now remember that  $\mathbf{v} = \mathbf{u} - \mathbf{u}^*$  and  $\mathbf{e} = \mathbf{x} - \mathbf{x}^*$ , this will become:

$$\mathbf{u} = -\mathbf{K}(\mathbf{x} - \mathbf{x}^*) + \mathbf{u}^* \quad (19)$$



This control law  $\mathbf{u} = -\mathbf{K}(\mathbf{x} - \mathbf{x}^*) + \mathbf{u}^*$  can be thought of as consisting of two parts:

- Feedback control  $\mathbf{u}_{FB} = -\mathbf{K}(\mathbf{x} - \mathbf{x}^*)$ , which depends on the control error (which requires a feedback about the current state of your system)
- Feed-forward control  $\mathbf{u}_{FF} = \mathbf{u}^*$ , which depends only on the trajectory and the equations of dynamics of your system, but not on your current state

# AFFINE TRAJECTORY TRACKING

## Part 1

What we just did - stabilization of the arbitrary trajectory  $\mathbf{x}^* = \mathbf{x}^*(t)$  - is also called *trajectory tracking control*, or *trajectory stabilization*. The solution we stabilized is called *trajectory*.

Just for completeness, let's consider the system:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} + \mathbf{c} \quad (20)$$

and stabilize trajectory  $\mathbf{x}^* = \mathbf{x}^*(t)$ .

# AFFINE TRAJECTORY TRACKING

## Part 2

We start by observing that, as before, our solution gives us equality:

$$\dot{\mathbf{x}}^* = \mathbf{A}\mathbf{x}^* + \mathbf{B}\mathbf{u}^* + \mathbf{c} \quad (21)$$

and after introducing control error and subtracting (21) from the original dynamics (20), we get:

$$\dot{\mathbf{e}} = \mathbf{A}\mathbf{e} + \mathbf{B}\mathbf{v} \quad (22)$$

where  $\mathbf{v} = \mathbf{u} - \mathbf{u}^*$ , which we already saw before. The only difference is that now  $\mathbf{u}^*$  is found as:

$$\mathbf{u}^* = \mathbf{B}^+(\dot{\mathbf{x}}^* - \mathbf{A}\mathbf{x}^* - \mathbf{c}) \quad (23)$$

What if we want to move our system  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$  from initial condition to some desired state  $\mathbf{x}^*$ . This can be called *point-to-point control*.

This is the same as trajectory control with  $\mathbf{x}^* = \text{const}$  and  $\dot{\mathbf{x}}^* = 0$ .

- Richard M. Murray Control and Dynamical Systems  
California Institute of Technology [Optimization-Based Control](#)
- [Dynamic Simulation in Python](#)

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# Discrete Dynamics

## Control Theory, Lecture 6

by Sergei Savin

Spring 2022

- Discrete Dynamics
- Stability of the Discrete Dynamics
- Discretization
  - ▶ Finite difference
  - ▶ Finite difference in an autonomous LTI
- Zero order hold
- ZOH and other types of discretization
  - ▶ Zero order hold vs First order hold
  - ▶ Exact discretization
- Read more



The following dynamical system is called *discrete*:

$$\mathbf{x}_{i+1} = \mathbf{A}\mathbf{x}_i + \mathbf{B}\mathbf{u}_i \quad (1)$$

Note that those:

- have no derivatives in the equation;
- are easily simulated.

The affine control for this system can be given as:

$$\mathbf{u}_i = -\mathbf{K}\mathbf{x}_i + \mathbf{u}_i^* \quad (2)$$

# STABILITY OF THE DISCRETE DYNAMICS

## Real eigenvalues

Let us consider stability of the discrete dynamical system where matrix  $\mathbf{A}$  has purely real eigenvalues:

$$\mathbf{x}_{i+1} = \mathbf{A}\mathbf{x}_i \quad (3)$$

With eigendecomposition  $\mathbf{A} = \mathbf{V}^{-1}\mathbf{D}\mathbf{V}$  (where  $\mathbf{D}$  is a diagonal matrix with eigenvalues  $\lambda_j$  of  $\mathbf{A}$  on its diagonal) and introducing notation  $\mathbf{z}_i = \mathbf{V}\mathbf{x}_i$  we get:

$$\mathbf{x}_{i+1} = \mathbf{V}^{-1}\mathbf{D}\mathbf{V}\mathbf{x}_i \quad (4)$$

$$\mathbf{z}_{i+1} = \mathbf{D}\mathbf{z}_i \quad (5)$$

Meaning that the dynamics became a system of independent scalar equations  $z_{j,i+1} = \lambda_j z_{j,i}$ .

# STABILITY OF THE DISCRETE DYNAMICS

## Real eigenvalues

Thus, with  $z_{j,i+1} = \lambda_j z_{j,i}$  we can find now the absolute value of the scalars  $z_j$  will dwindle with time iff  $|\lambda_j| < 1$ :

$$\left| \frac{z_{j,i+1}}{z_{j,i}} \right| = |\lambda_j| \tag{6}$$

# STABILITY OF THE DISCRETE DYNAMICS

## 2x2 system

Let us consider stability of the discrete dynamical system with a 2-by-2 matrix  $\mathbf{A}$ :

$$\begin{bmatrix} x_{1,i+1} \\ x_{2,i+1} \end{bmatrix} = \begin{bmatrix} \alpha & -\beta \\ \beta & \alpha \end{bmatrix} \begin{bmatrix} x_{1,i} \\ x_{2,i} \end{bmatrix} \quad (7)$$

Let us find norms of  $\begin{bmatrix} x_{1,i+1} \\ x_{2,i+1} \end{bmatrix}$  and  $\begin{bmatrix} x_{1,i} \\ x_{2,i} \end{bmatrix}$ :

$$\left\| \begin{bmatrix} x_{1,i} \\ x_{2,i} \end{bmatrix} \right\|^2 = x_{1,i}^2 + x_{2,i}^2 \quad (8)$$

$$\left\| \begin{bmatrix} x_{1,i+1} \\ x_{2,i+1} \end{bmatrix} \right\|^2 = (\alpha^2 + \beta^2)(x_{1,i}^2 + x_{2,i}^2) \quad (9)$$

# STABILITY OF THE DISCRETE DYNAMICS

## 2x2 system

We can find the ratio of the norms of  $\begin{bmatrix} x_{1,i+1} \\ x_{2,i+1} \end{bmatrix}$  and  $\begin{bmatrix} x_{1,i} \\ x_{2,i} \end{bmatrix}$ :

$$\left\| \begin{bmatrix} x_{1,i+1} \\ x_{2,i+1} \end{bmatrix} \right\|^2 / \left\| \begin{bmatrix} x_{1,i} \\ x_{2,i} \end{bmatrix} \right\|^2 = \alpha^2 + \beta^2 \quad (10)$$

Remembering that eigenvalues of the system are  $\lambda = \alpha \pm j\beta$ , we can rewrite the expression above as:

$$\left\| \begin{bmatrix} x_{1,i+1} \\ x_{2,i+1} \end{bmatrix} \right\|^2 / \left\| \begin{bmatrix} x_{1,i} \\ x_{2,i} \end{bmatrix} \right\|^2 = |\lambda| \quad (11)$$

We can see that the norm of the variable  $\mathbf{x}$  will dwindle with time iff  $|\lambda| < 1$ .

# STABILITY OF THE DISCRETE DYNAMICS

General stability criterion is given below:

## Stability criterion

In general, discrete systems  $\mathbf{x}_{i+1} = \mathbf{A}\mathbf{x}_i$  are stable as long as the eigenvalues of  $\mathbf{A}$  are smaller than 1 by absolute value:  $|\lambda_i(\mathbf{A})| \leq 1, \forall i$ . This is true for complex eigenvalues as well.

# DISCRETIZATION

## Finite difference

Consider linear time-invariant autonomous system:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} \quad (12)$$

The time derivative  $\dot{\mathbf{x}}$  can be replaced with a finite difference:

$$\dot{\mathbf{x}} \approx \frac{1}{\Delta t}(\mathbf{x}(t + \Delta t) - \mathbf{x}(t)) \quad (13)$$

Note that we could have also used other definitions of a finite difference:

$$\dot{\mathbf{x}} \approx \frac{1}{\Delta t}(\mathbf{x}(t + 0.5\Delta t) - \mathbf{x}(t - 0.5\Delta t)) \quad (14)$$

or

$$\dot{\mathbf{x}} \approx \frac{1}{\Delta t}(\mathbf{x}(t) - \mathbf{x}(t - \Delta t)) \quad (15)$$

# DISCRETIZATION

## Finite difference notation

We can introduce notation:

$$\begin{cases} \mathbf{x}_0 = \mathbf{x}(0) \\ \mathbf{x}_1 = \mathbf{x}(\Delta t) \\ \mathbf{x}_2 = \mathbf{x}(2\Delta t) \\ \dots \\ \mathbf{x}_n = \mathbf{x}(n\Delta t) \end{cases} \quad (16)$$

We say that  $\mathbf{x}_i$  is the value of  $\mathbf{x}$  at the time step  $i$ . Then the finite difference can be written, for example, as follows:

$$\dot{\mathbf{x}} \approx \frac{1}{\Delta t} (\mathbf{x}_{i+1} - \mathbf{x}_i) \quad (17)$$



# DISCRETIZATION

## Finite difference in an autonomous LTI

We can rewrite our original autonomous LTI as follows:

$$\frac{1}{\Delta t}(\mathbf{x}_{i+1} - \mathbf{x}_i) = \mathbf{A}\mathbf{x}_i \quad (18)$$

Isolating  $\mathbf{x}_{i+1}$  on the left hand side, we get:

$$\mathbf{x}_{i+1} = (\mathbf{A}\Delta t + \mathbf{I})\mathbf{x}_i \quad (19)$$

---

Or alternatively:

$$\frac{1}{\Delta t}(\mathbf{x}_{i+1} - \mathbf{x}_i) = \mathbf{A}\mathbf{x}_{i+1} \quad (20)$$

Isolating  $\mathbf{x}_{i+1}$  on the left hand side, we get:

$$\mathbf{x}_{i+1} = (\mathbf{I} - \mathbf{A}\Delta t)^{-1}\mathbf{x}_i \quad (21)$$

# DISCRETIZATION

## Zero order hold

Defining *discrete state space matrix*  $\bar{\mathbf{A}}$  and *discrete control matrix*  $\bar{\mathbf{B}}$  as follows:

$$\bar{\mathbf{A}} = \mathbf{A}\Delta t + \mathbf{I} \quad (22)$$

$$\bar{\mathbf{B}} = \mathbf{B}\Delta t \quad (23)$$

We get discrete dynamics:

$$\mathbf{x}_{i+1} = \bar{\mathbf{A}}\mathbf{x}_i + \bar{\mathbf{B}}\mathbf{u}_i \quad (24)$$

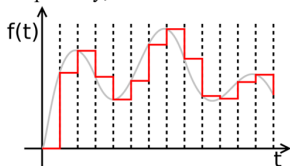
This way of defining discrete dynamics is called *zero order hold (ZOH)*.

# ZOH AND OTHER TYPES OF DISCRETIZATION

## Zero order hold vs First order hold

Graphically, we can understand what zero order hold is, by comparing it to the first order hold:

Graphically, zero order hold is this:



First order hold is this:

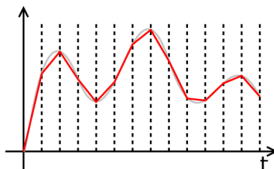


Figure 1: Different types of discretization

# ZOH AND OTHER TYPES OF DISCRETIZATION

## Exact discretization

Let the discrete state  $\mathbf{x}_i$  correspond to continuous state  $\mathbf{x}$  at the moment of time  $t_i$ . Then, we can say that the discretization is *exact* the following holds for any solution  $\mathbf{x}(t)$

$$\mathbf{x}_0 = \mathbf{x}(t_0) \rightarrow \mathbf{x}_i = \mathbf{x}(t_i), \quad \forall i \quad (25)$$

We can compute the exact discretization as follows:

$$\bar{\mathbf{A}} = e^{\mathbf{A}\Delta t} \quad (26)$$

$$\bar{\mathbf{B}} = \mathbf{B} \int_{t_0}^{t_0+\Delta t} e^{\mathbf{A}s} ds \quad (27)$$

- [Automatic Control 1 Discrete-time linear systems](#), Prof. Alberto Bemporad, University of Trento

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# Lyapunov Theory, Lyapunov equations

## Control Theory, Lecture 7

by Sergei Savin

Spring 2022

- Lyapunov method: stability criteria
- Lyapunov method: examples
- Linear case
- Discrete case
- Lyapunov equations
- Read more



# LYAPUNOV METHOD: STABILITY CRITERIA

## Asymptotic stability criteria

Autonomous dynamic system  $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$  is asymptotically stable, if there exists a scalar function  $V = V(\mathbf{x}) > 0$ , whose time derivative is negative  $\dot{V}(\mathbf{x}) < 0$ , except  $V(\mathbf{0}) = 0$ ,  $\dot{V}(\mathbf{0}) = 0$ .

## Marginal stability criteria

$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$  is stable in the sense of Lyapunov,  $\exists V(\mathbf{x}) > 0$ ,  $\dot{V}(\mathbf{x}) \leq 0$ .

## Definition

Function  $V(\mathbf{x}) > 0$  in this case is called *Lyapunov function*.

This is not the only type of stability as you remember, you are invited to study criteria for other stability types on your own.

# LYAPUNOV METHOD: EXAMPLES

## Example 1

Take dynamical system  $\dot{x} = -x$ .

We propose a *Lyapunov function candidate*  $V(x) = x^2 \geq 0$ .

Let's find its derivative:

$$\dot{V}(x) = \frac{\partial V}{\partial x}(-x) = 2x(-x) = -x^2 \leq 0 \quad (1)$$

This satisfies the Lyapunov criteria, so the system is stable. It is in fact asymptotically stable, because  $\dot{V}(x) \neq 0$  if  $x \neq 0$ .

# LYAPUNOV METHOD: EXAMPLES

## Example 2

Consider oscillator  $\ddot{q} = f(q, \dot{q}) = -\dot{q}$ .

We propose a *Lyapunov function candidate*

$V(q, \dot{q}) = T(q, \dot{q}) = \frac{1}{2}\dot{q}^2 \geq 0$ , where  $T(q, \dot{q})$  is kinetic energy of the system. Let's find its derivative:

$$\dot{V}(q, \dot{q}) = \frac{\partial V}{\partial q}\dot{q} + \frac{\partial V}{\partial \dot{q}}f(q, \dot{q}) = \dot{q}(-\dot{q}) = -\dot{q}^2 \leq 0 \quad (2)$$

This satisfies the Lyapunov criteria, so the system is stable.

But it is not proven to be asymptotically stable, because

$\dot{V}(q, \dot{q}) = 0$  for any  $q$  as long as  $\dot{q} = 0$ .

# LYAPUNOV METHOD: EXAMPLES

## Example 3

Consider pendulum  $\ddot{q} = f(q, \dot{q}) = -\dot{q} - \sin(q)$ .

We propose a *Lyapunov function candidate*

$V(q, \dot{q}) = E(q, \dot{q}) = \frac{1}{2}\dot{q}^2 + 1 - \cos(q) \geq 0$ , where  $E(q, \dot{q})$  is total energy of the system. Let's find its derivative:

$$\dot{V}(q, \dot{q}) = \frac{\partial V}{\partial q} \dot{q} + \frac{\partial V}{\partial \dot{q}} f(q, \dot{q}) = \dot{q} \sin(q) + \dot{q}(-\dot{q} - \sin(q)) = -\dot{q}^2 \leq 0 \quad (3)$$

This satisfies the Lyapunov criteria, so the system is stable. It is not proven to be asymptotically stable, because  $\dot{V}(q, \dot{q}) = 0$  for any  $q$ , as long as  $\dot{q} = 0$ .

# LINEAR CASE

## Part 1

As you saw, Lyapunov method allows you to deal with nonlinear systems, as well as linear ones. But for linear ones there are additional properties we can use.

### Observation 1

For a linear system  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x}$  we can always pick Lyapunov function candidate in the form  $V = \mathbf{x}^\top \mathbf{S}\mathbf{x} \geq 0$ , where  $\mathbf{S}$  is a positive semidefinite matrix.

Next slides will show where this leads us.

# LINEAR CASE

## Part 2

Given  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x}$  and  $V = \mathbf{x}^\top \mathbf{S}\mathbf{x} \geq 0$ , let's find its derivative:

$$\dot{V}(\mathbf{x}) = \dot{\mathbf{x}}^\top \mathbf{S}\mathbf{x} + \mathbf{x}^\top \mathbf{S}\dot{\mathbf{x}} \quad (4)$$

$$\dot{V}(\mathbf{x}) = (\mathbf{A}\mathbf{x})^\top \mathbf{S}\mathbf{x} + \mathbf{x}^\top \mathbf{S}\mathbf{A}\mathbf{x} = \mathbf{x}^\top (\mathbf{A}^\top \mathbf{S} + \mathbf{S}\mathbf{A})\mathbf{x} \quad (5)$$

Notice that  $\dot{V}(x)$  should be negative for all  $\mathbf{x}$  for the system to be stable, meaning that  $\mathbf{A}^\top \mathbf{S} + \mathbf{S}\mathbf{A}$  should be negative semidefinite. A more strict form of this requirement is *Lyapunov equation*:

$$\mathbf{A}^\top \mathbf{S} + \mathbf{S}\mathbf{A} = -\mathbf{Q} \quad (6)$$

where  $\mathbf{Q}$  is a positive-definite matrix.

# DISCRETE CASE

## Part 1

### Marginal stability criteria, discrete case

Given  $\mathbf{x}_{i+1} = \mathbf{f}(\mathbf{x}_i)$ , if  $V(\mathbf{x}_i) > 0$ , and  $V(\mathbf{x}_{i+1}) - V(\mathbf{x}_i) \leq 0$ , the system is stable.

Same as before, for linear systems we will be choosing *positive semidefinite quadratic forms* as Lyapunov function candidates.

# DISCRETE CASE

## Part 2

Consider dynamics  $\mathbf{x}_{i+1} = \mathbf{A}\mathbf{x}_i$  and  $V = \mathbf{x}_i^\top \mathbf{S}\mathbf{x}_i \geq 0$ , let's find  $V(\mathbf{x}_{i+1}) - V(\mathbf{x}_i)$ :

$$V(\mathbf{x}_{i+1}) - V(\mathbf{x}_i) = (\mathbf{A}\mathbf{x}_i)^\top \mathbf{S}\mathbf{A}\mathbf{x}_i - \mathbf{x}_i^\top \mathbf{S}\mathbf{x}_i \quad (7)$$

$$V(\mathbf{x}_{i+1}) - V(\mathbf{x}_i) = \mathbf{x}_i^\top (\mathbf{A}^\top \mathbf{S}\mathbf{A} - \mathbf{S})\mathbf{x}_i \quad (8)$$

Notice that  $V(\mathbf{x}_{i+1}) - V(\mathbf{x}_i)$  should be negative for all  $\mathbf{x}_i$  for the system to be stable, meaning that  $\mathbf{A}^\top \mathbf{S}\mathbf{A} - \mathbf{S}$  should be negative semidefinite. A more strict form of this requirement is *Discrete Lyapunov equation*:

$$\mathbf{A}^\top \mathbf{S}\mathbf{A} - \mathbf{S} = -\mathbf{Q} \quad (9)$$

where  $\mathbf{Q}$  is a positive-definite matrix.



In practice, you can easily use Lyapunov equations for stability verification. Python and MATLAB have built-in functionality to solve it:

- `scipy: linalg.solve_continuous_lyapunov(A, Q)`
- `MATLAB: lyap(A,Q)`

- 3.9 Liapunov's direct method
- Università degli studi di Padova Dipartimento di Ingegneria dell'Informazione, Nicoletta Bof, Ruggero Carli, Luca Schenato, Technical Report, Lyapunov Theory for Discrete Time Systems

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# Hamilton-Jacobi-Bellman eq., Riccati eq., Linear Quadratic Regulator

Control Theory, Lecture 9

by Sergei Savin

Spring 2022

## ■ Hamilton-Jacobi-Bellman equation

- ▶ Definitions
- ▶ Cost, optimal cost
- ▶ Differentiating optimal cost

## ■ Algebraic Riccati equation

- ▶ HJB for LTI
- ▶ Linear Quadratic Regulator
- ▶ Numerical methods

# HAMILTON-JACOBI-BELLMAN EQUATION

## Definitions

Let us define dynamics:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}) \quad (1)$$

with initial conditions  $\mathbf{x}(0)$ .

Additionally we define *control policy* as:

$$\mathbf{u} = \pi(\mathbf{x}, t) \quad (2)$$

To connect with the previous ways we talked about control, we can say that choosing different control gains and different feed-forward control amounts to choosing a different control policy.

# HAMILTON-JACOBI-BELLMAN EQUATION

## Cost, optimal cost

Let  $J$  be an additive cost function:

$$J(\mathbf{x}_0, \pi(\mathbf{x}, t)) = \int_0^\infty g(\mathbf{x}, \mathbf{u}) dt \quad (3)$$

where  $g(\mathbf{x}, \mathbf{u})$  is instantaneous cost and  $\mathbf{x}_0 = \mathbf{x}(0)$  is the initial conditions. Notice that  $J$  depends on  $\mathbf{x}_0$  rather than  $\mathbf{x}(t)$ , since initial conditions and control policy completely define the trajectory of the system  $\mathbf{x}(t)$ .

Let  $J^*$  be the optimal (lowest possible) cost. In other words:

$$J^*(\mathbf{x}_0) = \inf_{\pi} J(\mathbf{x}_0, \pi(\mathbf{x}, t)) \quad (4)$$

Optimal cost is attained when optimal policy is attained:

$$\pi = \pi^*(\mathbf{x}, t)$$

With this, we can formulate *Hamilton-Jacobi-Bellman equation* (HJB):

$$\min_{\mathbf{u}} \left[ g(\mathbf{x}, \mathbf{u}) + \frac{\partial J^*}{\partial \mathbf{x}} \mathbf{f}(\mathbf{x}, \mathbf{u}) \right] = 0 \quad (5)$$

This can be loosely interpreted as follows: the value in square brackets is  $\dot{J}(\mathbf{x}_0, \pi)$ , which is equal to 0 when  $\pi = \pi^*(\mathbf{x}, t)$ , and is positive otherwise (in the small vicinity of  $\pi^*$ ), as  $J(\mathbf{x}_0, \pi^*)$  is smaller than any  $J(\mathbf{x}_0, \pi)$ ,  $\pi^* \neq \pi$ .

We can find control that delivers minimum to the function (5):

$$u^* = \arg \min_{\mathbf{u}} \left[ g(\mathbf{x}, \mathbf{u}) + \frac{\partial J^*}{\partial \mathbf{x}} \mathbf{f}(\mathbf{x}, \mathbf{u}) \right] \quad (6)$$



For LTI, dynamics is:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \quad (7)$$

We can choose quadratic cost:

$$g(\mathbf{x}, \mathbf{u}) = \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^\top \mathbf{R}\mathbf{u} \quad (8)$$

Then HJB becomes:

$$\min_{\mathbf{u}} [\mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^\top \mathbf{R}\mathbf{u} + \frac{\partial J^*}{\partial \mathbf{x}}(\mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u})] = 0 \quad (9)$$

where  $\mathbf{Q} = \mathbf{Q}^\top \geq 0$  and  $\mathbf{R} = \mathbf{R}^\top > 0$ .

There is a theorem that says that for LTI with quadratic cost,  $J^*$  has the form:

$$J^* = \mathbf{x}^\top \mathbf{S} \mathbf{x} \quad (10)$$

where  $\mathbf{S} = \mathbf{S}^\top \geq 0$ .

Then HJB becomes:

$$\min_{\mathbf{u}} \left[ \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^\top \mathbf{R} \mathbf{u} + \mathbf{x}^\top \mathbf{S} (\mathbf{A} \mathbf{x} + \mathbf{B} \mathbf{u}) + (\mathbf{A} \mathbf{x} + \mathbf{B} \mathbf{u})^\top \mathbf{S} \mathbf{x} \right] = 0$$

Simplifying, we get:

$$\min_{\mathbf{u}} \left[ \mathbf{u}^\top \mathbf{R} \mathbf{u} + \mathbf{x}^\top (\mathbf{Q} + \mathbf{S} \mathbf{A} + \mathbf{A}^\top \mathbf{S}) \mathbf{x} + \mathbf{x}^\top \mathbf{S} \mathbf{B} \mathbf{u} + \mathbf{u}^\top \mathbf{B}^\top \mathbf{S} \mathbf{x} \right] = 0$$

# ALGEBRAIC RICCATI

## Linear Quadratic Regulator

Finding partial derivative of the HJB with respect to  $\mathbf{u}$  and setting it to zero (as it is an extreme point) we get:

$$2\mathbf{u}^\top \mathbf{R} + 2\mathbf{x}^\top \mathbf{S}\mathbf{B} = 0 \quad (11)$$

This expression can be transposed and  $\mathbf{u}$  separated:

$$\mathbf{u} = -\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S}\mathbf{x} \quad (12)$$

This is the desired control law. We can see that it is *proportional*. We can re-write it as:

$$\mathbf{u} = -\mathbf{K}\mathbf{x} \quad (13)$$

where  $\mathbf{K} = \mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S}$  is the controller gain. This control law is called Linear Quadratic Regulator (LQR).

Substituting found control law into the HJB, we find:

$$\min_{\mathbf{u}} [\mathbf{x}^\top (\mathbf{Q} + \mathbf{S}\mathbf{A} + \mathbf{A}^\top \mathbf{S})\mathbf{x} + \mathbf{x}^\top \mathbf{S}\mathbf{B}\mathbf{R}^{-1}\mathbf{R}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S}\mathbf{x} - \mathbf{x}^\top \mathbf{S}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S}\mathbf{x} - \mathbf{x}^\top \mathbf{S}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S}\mathbf{x}] = 0 \quad (14)$$

Simplifying, we get:

$$\mathbf{x}^\top (\mathbf{Q} + \mathbf{S}\mathbf{A} + \mathbf{A}^\top \mathbf{S} - \mathbf{S}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S})\mathbf{x} = 0 \quad (15)$$

which would hold for all  $\mathbf{x}$  iff:

$$\mathbf{Q} - \mathbf{S}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{S} + \mathbf{S}\mathbf{A} + \mathbf{A}^\top \mathbf{S} = 0 \quad (16)$$

This is the *Algebraic Riccati equation*.

# ALGEBRAIC RICCATI

## Numerical methods

There are a number of ways to solve LQR:

- In MATLAB there is a function  $[K, S, P] = \text{lqr}(A, B, Q, R)$ , where  $P = \text{eig}(A - B * K)$
- In Python, there is  $S = \text{scipy.linalg.solve\_continuous\_are}(A, B, Q, R)$
- In Drake (by MIT and Toyota Research) there is a function  $(K, S) = \text{LinearQuadraticRegulator}(A, B, Q, R)$

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