

# 1 Introduction

This document presets the mathematical model used to implement the ship-in-transit-simulator".

## 2 Ship dynamics

The ship is modelled in three degrees of freedom (surge, sway and yaw) according to the following equations:

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{R}_z(\psi)\mathbf{v} \\ \mathbf{M}\dot{\mathbf{v}} &= -\mathbf{C}_{RB}(\mathbf{v})\mathbf{v} - \mathbf{C}_A(\mathbf{v}_R)\mathbf{v}_R - \mathbf{D}_L\mathbf{v}_R - \mathbf{D}_{NL}(\mathbf{v}_R)\mathbf{v}_R + \boldsymbol{\tau}_w + \boldsymbol{\tau}_r + \boldsymbol{\tau}_p\end{aligned}\tag{1}$$

where:

- $\mathbf{x} = [N, E, psi]^T$  is the north and east position, and the yaw angle.
- $\mathbf{x} = [u, v, r]^T$  is the velocity vector representing the forward and sideways speed, and the yaw rate.
- $\mathbf{R}_z(\psi)$  is the rotation matrix about the vertical axis, used to express the velocity vector in terms of a reference frame oriented north-east-down.
- $\mathbf{M} = \mathbf{M}_{RB} + \mathbf{M}_A$  is the ship's mass matrix including the rigid body mass and added mass.
- $\mathbf{C}_{RB}(\mathbf{v})\mathbf{c}$  is the centripetal and Coriolis forces.
- $\mathbf{C}_A(\mathbf{v}_R)\mathbf{v}_R$  are the centripetal and Coriolis forces due to the added mass.
- $\mathbf{D}_L\mathbf{v}_R$  is the linear damping forces. Only the diagonal of the linear damping matrix is non-zero.
- $\mathbf{D}_{NL}(\mathbf{v}_R)\mathbf{v}_R$  is the non-linear damping forces. Only the diagonal of the non-linear damping matrix is non-zero.
- $\boldsymbol{\tau}_w$  is the forces acting on the ship from the wind. The wind forces are calculated based on the relative wind speed, based on the ship's projected area towards the wind, according to  $F = 0.5\rho_a v_w^2 c_d A_p$  where  $F$  is the force in some direction,  $\rho_a$  is the density of the air,  $v_w$  is the relative wind speed in the direction of  $F$ ,  $c_d$  is the drag coefficient in air and  $A_p$  is the projected area of the ship in the same direction.
- $\boldsymbol{\tau}_r = [0, F_v, F_r]^T$  is the rudder force where  $F_v = c_v \cdot \delta(u - u_c)$  and  $F_r = c_r \cdot \delta(u - u_c)$  where  $c_v$  and  $c_r$  are coefficients,  $u - u_c$  is the velocity of a water particle in the direction of the ship's longitudinal axis relative to the ship's surge speed, and  $\delta$  is the rudder angle.

- $\tau_p = [F_p, 0, 0]^T$  is the propulsion force. The provided classes gives at least two ways of generating the propulsion force.

### 3 Machinery system

The machinery system can be modelled either using a model that includes shaft dynamics, or as a simplified model where the the dynamics between engine load and propulsion force is modelled as a transfer function. In either case the engine load is the input which determines the propulsion force (output).

#### 3.1 Model with shaft dynamics

The shaft dynamics is described as:

$$J_p \dot{\omega}_p = \frac{1}{r_{ME}} (\tau_{ME} - d_{ME} \omega_p) + \frac{1}{r_{HSG}} (\tau_{HSG} - d_{HSG} \omega_p) - k_p \omega_p^2 \quad (2)$$

where...

The thrust force  $F_p$  is given as

$$F_p = D_p^4 K_T \omega_p |\omega_p| \quad (3)$$

where  $D_p$  is the diameter of the propeller,  $K_T$  is a constant, and  $\omega_p$  is the rotation speed of the propeller.

#### 3.2 Simplified model

The simplified propeller force dynamics is described as

$$\dot{F}_p = -\frac{P_{max}}{T \cdot F_{max}} F_p + \frac{1}{T} P \quad (4)$$

where  $F_p$  is the propeller force in the surge direction,  $P_{max}$  is the maximum continuous rated power of the main engine (or the set of engines used to generate propulsion force),  $F_{max}$  is the maximal propulsion force,  $T$  is a time constant, and  $u$  is the engine load in kW.