

ContCarSim: Continuous Carousel Simulator documentation

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To accompany the manuscript:

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The simulator has been developed on MATLAB R2019a for Windows.

1. Process description

The carousel reproduced by the simulator is sketched in Figure 1. A schematic P&ID of the process is provided in Figure 2, with the legend of the equipment reported in Table 1. Figures 1-2 and Table 1 also report the sensors and controllers network implemented in the carousel simulator.

The unit can continuously process an inlet slurry stream into a dry crystals cake. The slurry system considered in the simulator is composed by pure paracetamol crystals in a mother liquor composed by pure ethanol. The carousel features five cylindrical ports, each one of 15 mm diameter, which allow a maximum hold-up of 10 mL. The ports are embedded in a main cylindrical body, aligned to five processing stations (Stations 1-5). For illustrative purposes, in Figure 2 the stations are represented as vessels in series (V-101-V-105), although the actual layout of the carousel is as in Figure 1. Stations 1-4 present a filter mesh at the bottom (F101-F104). Station 5 is, instead, open at the bottom for cake discharge, which is enabled by the action of a pneumatic piston (not shown). The pressure gradient for filtration and drying is provided by a compressor (P101), connected to the top section of all the stations, whereas all stations are maintained at atmospheric pressure on the bottom section.

The carousel operates in cyclic mode: processing cycles, during which every port processes batch-wise the material therein contained, are alternated to carousel rotations, during which the ports containing the material being processed are moved to the following station. Carousel rotations are logically represented in the P&ID as material streams, whose flows are controlled by FC-101. The alternating processing cycles and carousels rotations are interrupted when significant mesh fouling is

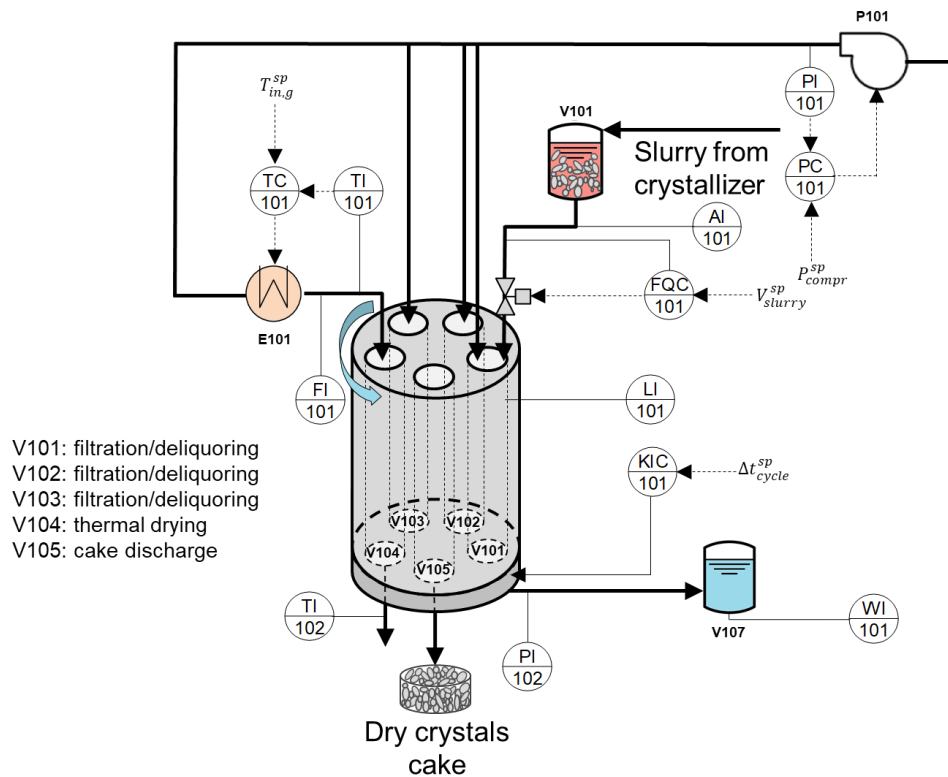


Figure 1. Schematic drawing of the carousel for continuous integrated filtration-drying of crystallization slurries mimicked by the simulator. Filter meshes are placed at the bottom of V-101-V04 (i.e., processing stations 1–4). Station 5, instead, is open for cake discharge. In physical carousels, controllers FQC-101 and KIC-101 are routines of the programmable logic controllers of the unit.

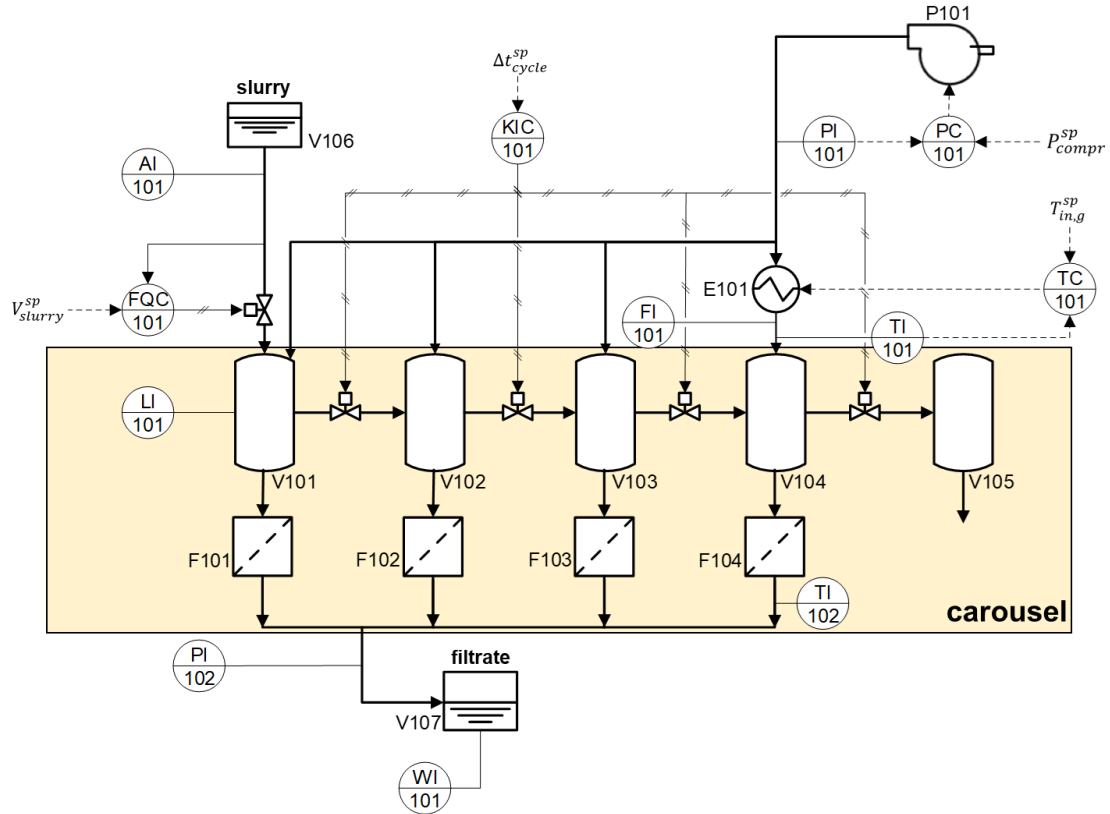


Figure 2. Logical P&ID of the carousel illustrated in Figure 1. The equipment legend is reported in Table 1.

detected: a cleaning-in-place cycle is then triggered. In this case, the material already loaded in the carousel ports is regularly processed during the following cycles, but no more slurry is loaded into the first station. Hence, at every cycle following cleaning-in-place initiation, an increasing number of ports will be empty. When all ports are empty, all meshes are automatically cleaned by sending a cleaning solvent into the carousel. The idle time for mesh cleaning is an input of the simulator, set to zero by default. The idle time at the end of every cycle (to sum up with the idle time for mesh cleaning when occurring), accounting for the carousel rotation and piston movement for cake discharge, is an additional input of the simulator, by default set to zero.

Stations 1-3 are dedicated to filtration and deliquoring, while in Station 4 thermal drying is carried out. In Station 5, only cake discharge occurs. Slurry processing occurs as follows. The crystallization slurry is fed to Station 1 at the beginning of every cycle, by keeping the valve between the slurry tank (V-106) and Station 1 open. After slurry feeding, a subsequent filtration step starts in Station 1, and it continues until filtration ends. If a carousel rotation is triggered before filtration finishes, filtration will continue in Station 2 (and, possibly, in Stations 3 and 4). During filtration, the liquid contained in the slurry is filtered out of the port by the action of the pressure gradient generated by P101, and stored in filtrate collector V-106, while the crystals are retained on top of the filter mesh, leading to cake formation. We distinguish between actual filtration, when there is a slurry hold-up on top of the cake being formed, and the subsequent deliquoring, during which the sole remaining liquid is the one retained inside the cake pores. Upon deliquoring, the liquid in the cake pores is mechanically displaced out of the cake by the action of the pressure gradient, until a certain pore saturation equilibrium is achieved. Filtration duration depends on the cake properties and on the pressure gradient itself. Depending on filtration duration, the cake can be partially deliquored in Stations 1-3, or it might even enter Station 4 with some slurry hold-up (drying cannot be properly conducted in

this situation, which should be avoided). Thermal drying is performed in Station 4 by flowing a hot air stream through the cake.

Table 1. Legend of Figures 1-2, including unit operations and ancillary equipment.

Name	Description
<i>Unit ID</i>	
F101-F104	Filter mesh below Stations 1-4 (respectively)
P101	Compressor
E101	Drying air electrical heater
V101	Carousel Station 1
V102	Carousel Station 2
V103	Carousel Station 3
V104	Carousel Station 4
V105	Carousel Station 5
V106	Filtrate collector
V107	Slurry tank
<i>Controllers and sensors</i>	
AI-101	Slurry concentration indicator
FC-101	Fed slurry volume controller
FI-101	Flowmeter for drying air entering carousel ports
KIC-101	Carousel rotation controller
LI-101	Camera system measuring volume of fed slurry and cake height
PC-101	Air pressure controller
PI-101	Compressor delivery pressure indicator
PI-102	Filtrate pressure indicator
TC-101	Drying air inlet temperature controller
TI-101	Thermocouple for drying air inlet temperature
TI-102	Thermocouple for drying air outlet temperature
WI-101	Scale for inferring filtrate flowrate

Table 2. Simulator inputs.

Variable name in run_carousel.m	Variable	UOM	Admissible values
control_mode	Flag for selecting control strategy: 0: open-loop 1: closed-loop controller of sample case study (Section 4) Other modes can be set up by the user	-	0, 1, other values set up by user
disturbance_scenario	Flag for selecting disturbance scenario: (see Section 2.4) 0: normal operating conditions 1: slurry concentration ramp change 2: specific cake resistance step change	-	0, 1, 2
total_duration	Simulation duration	s	[0, +∞)
u_nominal.t_rot	Nominal set-point cycle duration	s	[5, +∞)*
u_nominal.V_slurry	Nominal set-point fed slurry volume	m ³	[5×10 ⁻⁷ , 1×10 ⁻⁶]
u_nominal.P_compr	Nominal set-point compressor delivery pressure (gauge)	Pa _g	[1×10 ⁴ , 2×10 ⁵]
u_nominal.Tinlet_drying	Nominal set-point drying air inlet temperature	K	[293, 353]
cryst_output.conc_slurry	Nominal slurry concentration	kg/ m ³	[50, 500]
control_interval	Time interval at which run_carousel.m is called	s	Multiples of 1
sampling_interval	Sampling interval for measurements and states in simulation output	s	Submultiples of 1
inter_cycle_Dt	Idle time at the end of every cycle	s	[0, +∞)*; default: 0
mesh_clean_Dt	Idle time at mesh cleaning	s	[0, +∞)*; default: 0

***MUST BE AN INTEGER**

2 How to use the simulator

2.1 Inputs

The simulator inputs are reported in Table 2, and have to be set up in the script `run_carousel.m`.

2.2 Simulation execution

Figure 3 shows the logical structure of the simulator, while Figure 4 elucidates the set of scripts and functions that make up the simulator, together with the order and the logics with which they are called. The simulation is initialized by running the script `run_carousel.m`, after having set up the desired inputs. The simulation is carried out as shown in Figure 4. Function `run_simulation.m`, handling the simulation routine, is automatically called. The parameters of the model are automatically retrieved from function `carousel_parameters.m`, and the resistances of the filter meshes for the first 1200 processing cycles are loaded from `resistances.m` (for simulating more than 1200 processing cycles, the relevant number of additional values of filter mesh resistances have to be added to `resistances.m`).

Then, the simulation of the first processing cycle begins. The `carousel_simulator.m` function is called for simulating 1 s of carousel operation. The `estimator_online.m` function is then executed. By default, `estimator_online.m` is an empty function, but it can be modified by the user for setting up parameter and state estimation routines.

Afterwards, carousel operation is simulated again for a duration of 1 s with `carousel_simulator.m`, or, if the control interval specified by the user has been achieved, the `controller_online.m` function is called. Function `controller_online.m` is the high-level controller that updates the value of the set-points of the operating variables at every control interval and, together with function `controller_switch.m` (called at every cycle switch), forms the “High-level controller” block of Figure 3.

The set-point of the low-level controllers of the operating variables are (Figures 1-2):

- The set-point of the inlet drying air temperature $T_{in,g}^{sp}$;
- The set-point of the slurry volume fed to the carousel at every cycle V_{slurry}^{sp} ;
- The set-point of the cycle duration Δt_{cycle}^{sp} ;
- The set-point of the pressure provided by the compressor P_{compr}^{sp} .

Within the default control mode 0, the process is operated at open-loop. Therefore, the set-points of the lower-layer controllers (FQC-101, PC-101, TC-101, and KIC-101) coincide with the nominal values set by the user (Table 2). If closed-loop routines are implemented, the lower-layer controllers set-points are instead adjusted during carousel operation, based on the control laws implemented in `controller_online.m`.

The drying air inlet temperature ($T_{in,g}$), the pressure provided by the compressor (P_{compr}), and the cycle duration (Δt_{cycle}) are assumed to be perfectly controlled, namely the actual responses perfectly track the relevant setpoints. The fed slurry volume (V_{slurry}) is instead subject to Gaussian fluctuations around the set-point, to reflect the behavior of real life carousels, as outlined in Section 2.4. Moreover, for cycles during which V-101 is empty due to the cleaning-in-place routine, V_{slurry} is automatically set equal to zero. Function `controller_online.m` also contains a sample closed-loop control routine (control mode 1), illustrated in the sample case study (Section 5).

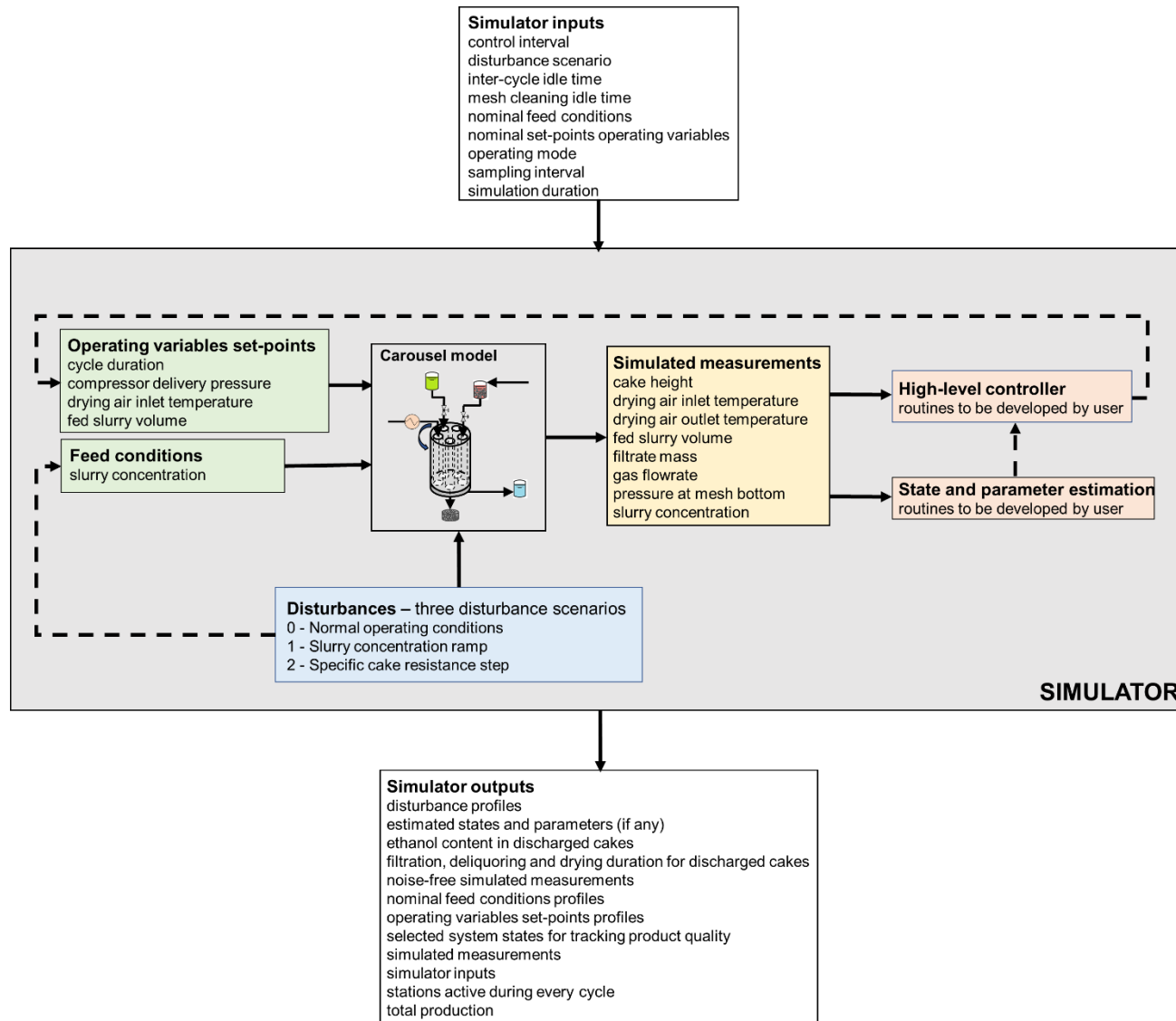


Figure 3. ContCarSim: schematic elucidating the simulator structure. The “Carousel model” block contains the low-level controllers of the operating variables, whose set-points are fixed at open-loop, while they are adjusted by the “High-level controller” block at closed-loop.

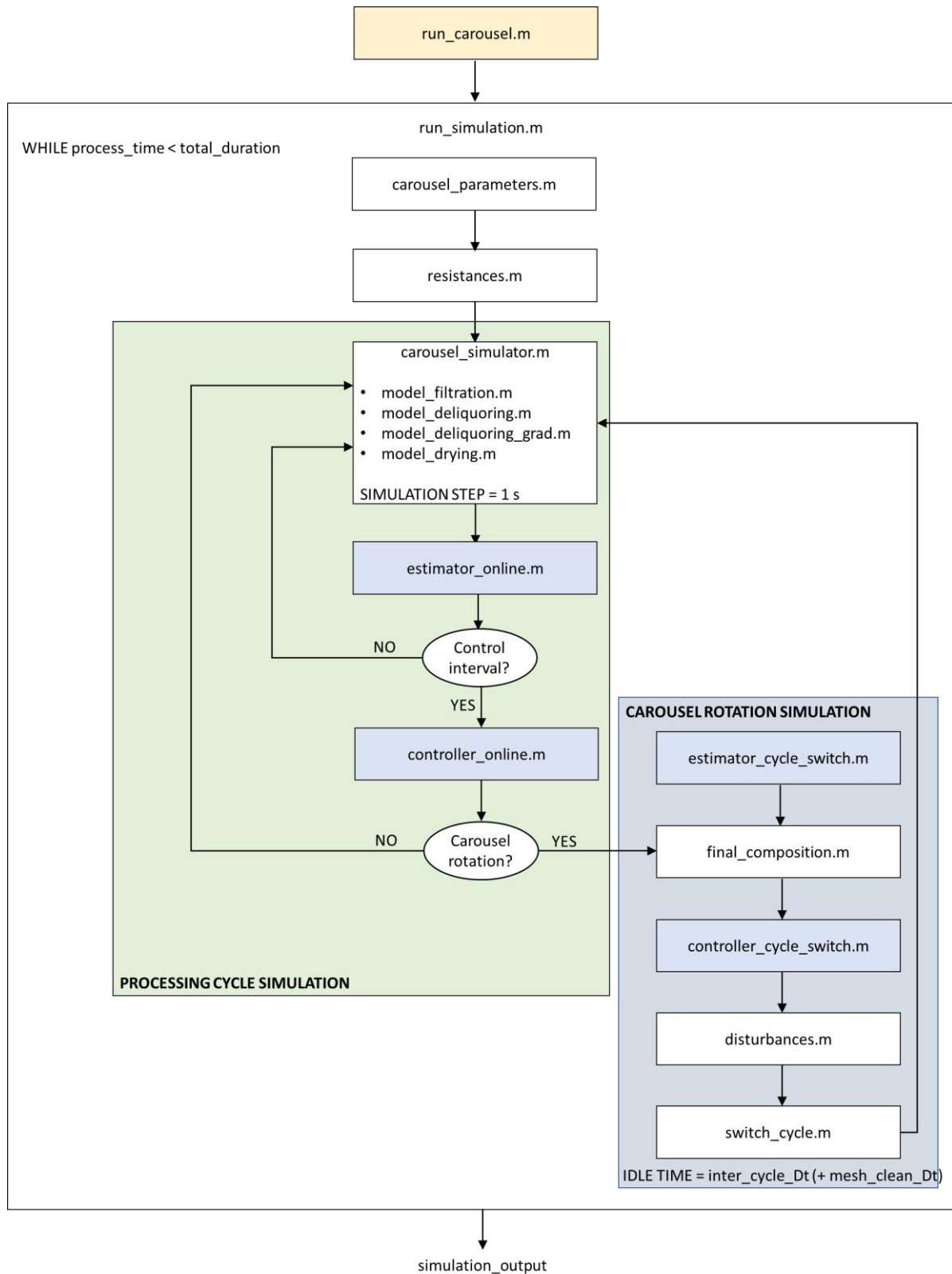


Figure 4. ContCarSim: computational structure of the simulator, showing the logics and the order with which the functions and scripts of the simulator are called. Yellow: script to be (optionally) edited with desired operating settings and then run. Blue: functions that can be edited for modifying the control strategy. At the end of the simulation of a carousel rotation, the process time (`process_time`) is increased of an idle time corresponding to `inter_cycle_Dt` when no mesh cleaning occurs, and of `inter_cycle_Dt+mesh_clean_Dt` when mesh cleaning occurs. Default settings: `inter_cycle_Dt=mesh_clean_Dt=0`.

Functions `carousel_simulator.m`, `estimator_online.m`, and `controller_online.m` are subsequently called until the cycle time reaches the current cycle duration Δt_{cycle} . At that point, the following functions are called:

- `estimator_cycle_switch.m`: by default an empty function, that can be modified by the user for setting up parameter and state estimation routines;
- `final_composition.m`: calculates the composition of the discharged cake, if there is any, and stores other variables that are outputs of the simulator;
- `controller_cycle_switch.m`: high level controller updating the set-points of the operating variables, following the control laws set up by user. The default implementation acts only on V_{slurry}^{sp} , setting it to zero for cycles in which V-101 is empty, and to the nominal set-point of fed slurry volume specified in `run_carousel.m` in all the other cases;
- `disturbances.m`: updates the value of the disturbances for the following cycle;
- `switch_cycle.m`: handles the carousel rotation routine.

The process time (`process_time`) is then increased of an idle time corresponding to `inter_cycle_Dt` when no mesh cleaning occurs, and of `inter_cycle_Dt+mesh_clean_Dt` when mesh cleaning occurs. Simulation of a new processing cycle is then initiated. Note that, unless otherwise specified in `run_carousel.m`, `inter_cycle_Dt` and `mesh_clean_Dt` are, by default, both set to zero.

Subsequent processing cycles and carousel rotation routines are simulated, until the set total process duration is reached. At that point, the simulation is terminated, and the simulation output object (`simulation_output.mat`) is generated.

2.3 Outputs

The structure of `simulation_output.mat` is elucidated in Table 3. Note that `simulation_output.mat` is generated only if at least one cake has been discharged by the carousel, namely if a large enough total process duration has been specified, compared to the set cycle duration.

The fields of `simulation_output.mat` correspond to the simulator outputs in Figure 3:

- `states`, storing the value assumed by selected system states during the simulation;
- `measurements`, storing the process measurements collected from the sensors reported in Figures 1-2 and Table 1;
- `measurements_nf`, storing the noise-free values of the process measurements;
- `disturbances`, containing the values assumed by the disturbances during the simulation (Section 2.4);
- `operating_vars`, storing the profiles of the set-points of the operating variables;
- `x_estim`, containing the states and parameters estimated through `estimator_online.m` and `estimator_cycle_switch.m`;
- `feed`, storing the nominal slurry concentration profile during the simulation;
- `cakes_proc_times`, reporting the filtration, deliquoring and drying duration undergone by all the cakes discharged from the carousel;
- `final_content`, listing the ethanol mass fraction in all the discharged cakes;

Table 3. Structure of `simulation_output.mat`. `n_cycles` = total number of initiated carousel cycles.

Field	Sub-field	Sub-sub-field	Variable	Description	UOM
states	station1 station2 station3	cake_x	t	Readings of timer reinitialized at every carousel rotation – vector, step: <code>sampling_interval</code>	s
			S	Average cake saturation time profile for <code>cake_x</code> in Station 1/2/3 – vector [1×length(t)]	-
			w_EtOH_cake	Time profile of average ethanol mass fraction in cake for <code>cake_x</code> in Station 1/2/3 – vector [1×length(t)]	-
	station4	cake_x	t	Readings of timer reinitialized at every carousel rotation – vector – step: <code>sampling_interval</code>	s
			S	Average cake saturation time profile for <code>cake_x</code> in Station 2/3/4 – vector [1×length(t)]	-
			w_EtOH_cake	Time profile of average ethanol mass fraction in cake for <code>cake_x</code> in Station 2/3/4 – vector [1×length(t)]	-
			Tg_top	Temperature of drying air at top of cake in Station 4 – vector [1 × length(t)]	K
	measurements		t_meas	Readings of timer initialized at process onset - vector: step = <code>sampling_interval</code>	s
			m_filt_WI101	Readings of WI101 – vector [1 × length(t_meas)]	kg
			P_PI101	Readings of PI101– vector [1 × length(t_meas)]	Pa _g
			P_PI102	Readings of PI102– vector [1 × length(t_meas)]	Pa _g
			c_slurry_AI101	Readings of AI101– vector [1 × length(t_meas)]	kg/m ³
			L_cake_LI101	Readings of LI101– vector [1 × length(t_meas)]	m
			V_slurry_LI101	Readings of LI101– vector [1 × length(t_meas)]	m ³
			Tg_in_TI101	Readings of TI101– vector [1 × length(t_meas)]	K
measurements_nf	same structure of measurements		Tg_out_TI102	Readings of TI102– vector [1 × length(t_meas)]	K
			Vdryer_FI101	Readings of FI101– vector [1 × length(t_meas)]	L/min
disturbances			resistances	Vector [<code>n_cycles</code> × 4] – element (<i>i</i> , <i>j</i>) = resistance of mesh in position <i>j</i> during processing cycle <i>i</i> , for <i>i</i> = 1, 2, ..., <code>n_cycles</code> (= total number of simulated cycles)	1/m
			c_slurry	Multiplicative coefficients to nominal slurry concentration – vector [1 × <code>n_cycles</code>]	-
			V_slurry	Multiplicative coefficients to current fed slurry set-point – vector [1 × <code>n_cycles</code>]	-
			E	Multiplicative coefficients to nominal cake porosity – vector [1 × <code>n_cycles</code>]	-
			alpha	Multiplicative coefficients to nominal specific cake resistance – vector [1 × <code>n_cycles</code>]	-
			hM	Multiplicative coefficients to nominal mass transfer parameter – vector [1 × <code>n_cycles</code>]	-
			hT	Multiplicative coefficient to nominal heat transfer parameter – vector [1 × <code>n_cycles</code>]	-
			t_vector	Readings of timer initialized at process onset – vector: step = <code>control_interval</code>	s
			P_compr_vector	Profile of set-points of compressor delivery pressure (gauge)– vector [1 × length(t_vector)]	Pa _g

		Tin_drying_vector	Profile of set-points of drying gas temperature – vector [1 × length(t_vector)]	K
		n_cycle_vector	Initiated cycles counter - vector [1 × n_cycles]	-
		t_rot_vector	Completed cycles duration – vector [1 × number of completed cycles]	
		V_slurry_vector	Set-point of fed slurry volume – vector [1 × n_cycles]	m ³
x_estim	structure depends on routines set up in estimator_online.m and estimator_cycle_switch.m			
feed		c_slurry_nom_vector	Profile of nominal slurry concentration – vector [1 × n_cycles]	kg/m ³
cakes_proc_times		cake_x	Duration of filtration undergone by cake_x during carousel processing	s
			Duration of deliquoring undergone by cake_x during carousel processing	S
		drying_duration	Duration of drying undergone by cake_x during carousel processing	s
final_content			Mass fraction of ethanol content in discharged cakes [1 x number discharged cakes]	-
active_stations			Vector [n_cycles x 4] – if port j processes material during cycle i, active_stations(i, j) = 1. Otherwise, active_stations(i, j) = 0.	-
total_production			cumulative mass of cakes of acceptable quality obtained during the simulation	kg
settings		control_mode	Scalar	-
		disturbance_scenario	Scalar	-
		control_interval	Time interval at which control routines are called - scalar	s
		sampling_interval	Sampling interval for all sensors – scalar	s
		total_duration	Simulation duration – scalar	s
		inter_cycle_Dt	Idle time at the end of every cycle	s
		mesh_clean_Dt	Idle time at mesh cleaning	s
	cryst_out_nom	conc_slurry	Nominal slurry concentration in feed – scalar	kg/m ³
		x	Crystal size distribution – particles diameters	m
		CSD_perc	Volumetric crystal size distribution	%
		T	Inlet slurry temperature (equal to room temperature)	K
	u_nom	t_rot	Nominal set-point cycle duration – scalar	s
		V_slurry	Nominal set-point fed slurry volume - scalar	m ³
		P_compr	Nominal set-point pressure provided by compressor (gauge) – scalar	Pa _g
		Tinlet_drying	Nominal set-point inlet drying gas temperature - scalar	K

- `active_stations`, summarizing which stations were active during which carousel cycle (as outlined in Sections 1, 2.4 and 4, certain stations are alternatively empty during carousel operation, due to the cleaning-in-place routine);
- `settings`, containing the settings that were specified in `run_carousel.m` before initiating the simulation.
- `total_production`, cumulative mass of cakes of acceptable quality obtained during the simulation

Of all the simulation outputs, the only ones available in physical carousels are those contained in the `measurements` field.

To retrieve the actual value of the variables affected by disturbances from the simulation output:

- **fed slurry concentration:** the actual concentrations of the slurries fed to the carousel in all cycles are obtained from the product of:
`simulation_output.disturbances.c_slurry` with
`simulation_output.feed.c_slurry_nom_vector`;
- **drying kinetic parameter and heat transfer coefficient** between cake and air during drying: the nominal values of the parameters vary during every cycle, following the drying model presented in the companion paper, and are not provided in the simulation output. The multiplicative coefficients acting as disturbance, varying at each cycle, are accessible from `simulation_output.disturbances`;
- **fed slurry volume:** the actual slurry volumes fed to the carousel in all cycles are obtained from the product of `simulation_output.operating_vars.V_slurry_vector` with `simulation_output.disturbances.V_slurry`;
- **specific cake resistance:** the actual resistances of all the processed cakes are calculated as:
`simulation_output.disturbances.alpha` $\times 2.7 \times 10^9$ (m/kg)
- **cake porosity:** the actual porosities of all the processed cakes are calculated as:
`simulation_output.disturbances.E` $\times 0.35$

2.4 Disturbances and disturbance scenarios

A set of disturbances is implemented in the simulator. All disturbances assume a given value of the relevant variable at the beginning of every carousel cycle, but do not vary within the same cycle. Two different types of disturbances are present in the simulator: a fouling disturbance and parametric disturbances. The simulator automatically reproduces the same disturbance pattern for every simulation, for benchmarking purposes.

A **realistic routine simulating filter mesh fouling and cleaning-in-place** is implemented in the simulator (Figure 5). The filter mesh resistances of V-101-V-104 ($R_{m,1}$, $R_{m,2}$, $R_{m,3}$, and $R_{m,4}$) are first initialized, sampling each one from $N(3 \times 10^9, 1 \times 10^{18})$ 1/m. At the end of each cycle during which some material is processed in Station i (i.e., when the station is not empty due to the triggering of the cleaning-in-place routine, described in Section 2.1), the corresponding filter mesh resistance $R_{m,i}$ increases by 2×10^9 1/m. During the first cycle of carousel operation, only the first processing station works, as no material has reached the subsequent stations, yet. It is just from the fourth cycle on that all stations V-101-V-104 will be fully operational. When the filter mesh resistance reaches a threshold value (set to 1.2×10^{10} 1/m), the mesh cleaning-in-place procedure is triggered. No additional material is loaded into the carousel for the following three cycles, which are required to complete the processing and discharge of the batches of slurry trapped into the carousel ports. Then, the filter mesh

resistances are re-initialized, sampling again from $N(3 \times 10^9, 1 \times 10^{18})$ 1/m, and the feeding and fouling routines are repeated again. In practice, the described routine yields to triggering a cleaning-in-place routine every six processing cycles (Figure 5).

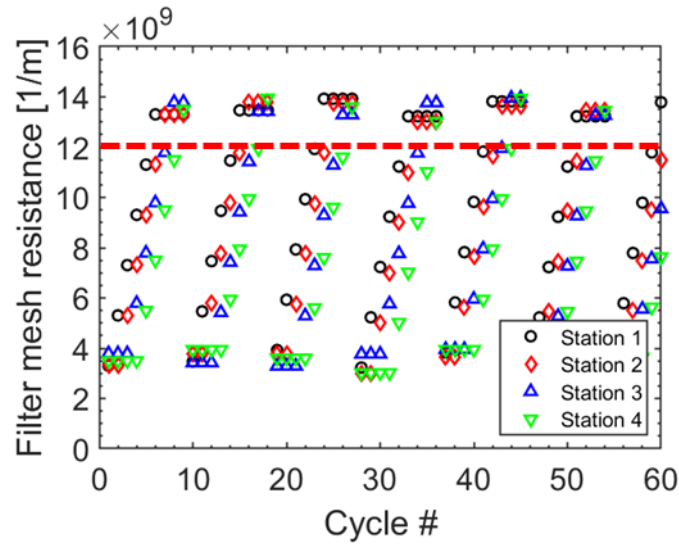


Figure 5. Filter mesh resistances profile implemented in the simulator for the first 60 carousel cycles. The red dashed line marks the threshold filter resistance that, when crossed by any mesh of the stations, triggers the onset of the cleaning-in-place routine.

Table 4 summarizes which stations are active and the identifying numbers of the cakes being processed by the carousel for the first 18 cycles from the process onset.

Table 4. List of carousel stations active for each of the first 18 cycles of carousel operation. The identifying number of cakes being processed in every station for each of the considered cycle is also reported. The information reported in this table is valid for all simulations, independently from the input settings.

Cycle #	Stations active	Cake processed in Station:			
		1	2	3	4
1	1	1	-	-	-
2	1,2	2	1	-	-
3	1,2,3	3	2	1	-
4	1,2,3,4	4	3	2	1
5	1,2,3,4	5	4	3	2
6	1,2,3,4	6	5	4	3
7	2,3,4	-	6	5	4
8	3,4	-	-	6	5
9	4	-	-	-	6
10	1	7	-	-	-
11	1,2	8	7	-	-
12	1,2,3	9	8	7	-
13	1,2,3,4	10	9	8	7
14	1,2,3,4	11	10	9	8
15	1,2,3,4	12	11	10	9
16	2,3,4	-	12	11	10
17	3,4	-	-	12	11
18	4	-	-	-	12

Parametric disturbances with respect to the nominal values are set for the following variables:

- the fed slurry concentration
- the drying kinetic parameter

- the heat transfer coefficient between cake and air during drying
- the fed slurry volume
- the specific cake resistance
- the cake porosity

The parametric disturbances are implemented in the simulator as multiplicative coefficients, **which vary at every cycle, but not during a cycle**, according to:

$$\gamma = \bar{\gamma} \gamma^{dist}, \quad (1)$$

where γ is the actual value of the parameter or variable used in the model equations, $\bar{\gamma}$ is its nominal value, while γ^{dist} is the parametric disturbance.

Three different disturbance scenarios are available in the simulator, presenting different disturbance profiles. Note that the simulator is implemented so that the disturbances profiles are consistent across simulations in the same disturbance scenario, for reproducibility purposes. The fouling disturbance always occurs as aforementioned, while parametric disturbances follow different patterns based on the disturbance scenario:

- Disturbance scenario #0 (normal operating conditions). All parametric disturbances are normally distributed;
- Disturbance scenario #1 (slurry concentration ramp change). All parametric disturbances are as in normal operating conditions, except for an increase of the nominal slurry concentration by 2% per minute, starting from 5 min after the process onset and up to 25 min from the process onset;
- Disturbance scenario #2 (specific cake resistance step). All disturbances profiles are as in normal operating conditions, except for a 100% step increase of the nominal specific cake resistance value, starting from 5 min after the process onset, and continuing up to the end of the process.

More information about disturbances is provided in Section 2.4 of the companion manuscript. Additional disturbance scenarios can be implemented by modifying function `disturbances.m` and/or the filter mesh resistances profiles in `resistances.mat`.

2.5 Setting up a control strategy

Control strategies can be set up by the user modifying one or more of the following functions:

- `controller_cycle_switch.m`
- `controller_online.m`
- `estimator_cycle_switch.m`
- `estimator_online.m`

The input/output structure is thoroughly documented in each function. Although the functions can be freely modified, the bottom part of `controller_cycle_switch.m` and `controller_online.m`, where the updated values of the set-points of the operating variables are stored and a null slurry volume for cycles in which Station 1 is empty, should not be edited.

Note that, among all the simulation outputs, **only the process measurements are available for state and parameter estimation routines** implemented in `estimator_cycle_switch.m` and `estimator_online.m`. At the same time, **only the process measurements and potential estimated states and parameters for control routines** implemented in `controller_cycle_switch.m` and `controller_online.m`.

The default control strategies implemented in the simulator are:

- control mode = 0: open-loop operation, no estimated parameters/states;
- control mode = 1: automatic adjustment of the cycle duration (Section 2.4), no estimated parameters/states;

2.6 Simulator scripts and functions:

2.6.1 Summary

<code>run_carousel.m</code>	Script for initiating carousel simulation
<code>run_simulation.m</code>	Function handling carousel simulation schedule
<code>carousel_parameters.m</code>	Function containing simulation and model parameters
<code>resistances.mat</code>	Matrix containing the values of the filter mesh resistances for the first 1200 processing cycles (size = 1200×4).
<code>carousel_simulator.m</code>	Function simulating carousel operation using filtration, deliquoring and drying models
<code>estimator_online.m</code>	Function that can be written by the user for online state/parameter estimation
<code>controller_online.m</code>	Function that can be written by the user, containing online control routines. Together with <code>controller_switch.m</code> , forms the “High-level controller” block of Figure 3.
<code>estimator_cycle_switch.m</code>	Function that can be written by the user for state/parameter estimation routines to be executed at every carousel rotation
<code>final_composition.m</code>	Function executed at the end of every cycle to calculate the composition of the discharged cake, if there is any, and for storing the value of other variables contained in the simulation output
<code>controller_cycle_switch.m</code>	Function that can be written by the user, containing control routines to be executed at every carousel rotation. Together with <code>controller_online.m</code> , forms the “High-level controller” block of Figure 3.
<code>disturbances.m</code>	Function that sets the value of the disturbances for the following cycle (e.g., filter mesh resistance, Gaussian fluctuations, ...)
<code>switch_cycle.m</code>	Function containing carousel rotation simulation routines, such as material transfer from one port to the following one

<code>model_filtration.m</code>	Function simulating filtration (ODE model)
<code>model_deliquoring.m</code>	Function simulating deliquoring with design charts (approximate method called when cake is very small, i.e. with height below 0.3 mm)
<code>model_deliquoring_grad.m</code>	Function simulating deliquoring (PDE model)
<code>model_drying.m</code>	Function simulating drying (PDE model)

2.6.2 Which scripts and functions can be edited?

In principle, all the functions and scripts in the simulator are openly accessible and can be edited, including all the models and the routine calling the models and the sub-functions for handling the carousel simulation (`run_simulation.m`). However, numerical stability and physical consistency are guaranteed only when properly editing the following files, which have been conceived and thoroughly commented for this purpose:

- Script to edit and run for starting the simulation with the desired settings:

`run_carousel.m`

- Functions to edit for changing the control strategy:

`controller_cycle_switch.m`, `controller_online.m`

`estimator_cycle_switch.m`, `estimator_online.m`

- Function to edit for modifying the physical properties of the system:

`carousel_parameters.m`

- Files to edit for implementing additional disturbance scenarios or to modify the existing ones:

`disturbances.m` and `resistances.m`

3 Quality-by-design and quality-by-control challenges

The simulator proposed in this study can be used for testing different control strategies within the QbD and QbC frameworks.

The general objective of the process is delivering dry cakes meeting the target quality, namely a residual ethanol content (critical quality attribute) below 0.5% w. This is achieved by setting suitable values for the operating variables, for a given inlet slurry concentration (critical material attribute of the process). Following the QbD jargon, the critical process parameters are identified as V_{slurry}^{sp} and Δt_{cycle}^{sp} , since they significantly impact the residual ethanol in the discharged cake. $T_{in,g}^{sp}$ and P_{compr}^{sp} , instead, are identified as the control variables, which affect the product quality to a smaller extent, compared to the critical process parameters. High-level control routines can be implemented in the simulator for adjusting the set-points of the operating variables used by the low-level controllers. The simulator also features blocks specifically dedicated to the implementation of state and parameter

estimation routines. Note that, although the simulator makes the values of multiple outputs available, only the simulated measurements can be used by the developed control and estimation routines (Figure 3), as in real life carousels.

The following specific challenges are envisioned for the simulator:

1. Open-loop operation. Determination of operating points delivering the target product quality and description of the design space of the unit.
2. State estimation and soft-sensing. Implementation of state estimators, soft sensors, and real time parameter estimation routines for monitoring key process variables, such as the ethanol content in the cake being dried and the resistance of the filter meshes.
3. Closed-loop control by manipulation of $T_{in,g}^{sp}$ and P_{compr}^{sp} . Implementation of (model-free and model-based) control routines for automatic adjustment of the control variables (i.e., $T_{in,g}^{sp}$ and P_{compr}^{sp}) to meet the target product quality in the face of disturbances (disturbance scenarios 0-2) and/or changes in the inlet slurry concentration. Description of the design space of the unit with such closed-loop routines in place.
4. Closed-loop control by manipulation of V_{slurry}^{sp} and Δt_{cycle}^{sp} . Implementation of (model-free and model-based) control routines for automatic adjustment of the critical process parameters (i.e., V_{slurry}^{sp} and Δt_{cycle}^{sp}), to meet the target product quality in the face of disturbances (disturbance scenarios 0-2) and/or changes in the inlet slurry concentration.
5. Throughput maximization under a reference scenario. We define the specific objective of implementing closed-loop control routines acting on V_{slurry}^{sp} and Δt_{cycle}^{sp} to maximize the cumulative mass of the cakes (meeting the target quality) discharged by the carousel during a simulation of 1 h duration, with $\bar{c}_{slurry} = 250 \text{ kg/m}^3$, $\bar{T}_{in,g}^{sp} = 323 \text{ K}$, and $\bar{P}_{compr}^{sp} = 10^5 \text{ Pa}_g$, and with the inter-cycle and mesh cleaning idle times set to zero. The maximum throughput that can be achieved in these conditions should be assessed under disturbance scenarios 0-2.
6. Throughput maximization under a general scenario. Implementing closed-loop control routines acting on P_{compr}^{sp} , $T_{in,g}^{sp}$, V_{slurry}^{sp} , and Δt_{cycle}^{sp} , to maximize the cumulative mass of the cakes (meeting the target quality) discharged by the carousel in a given timeframe, under disturbance scenarios 0-2, for different \bar{c}_{slurry} and inter-cycle and mesh cleaning idle times.

In addition to the listed tasks, the simulator can also be used for generating data for data analytics studies, or for benchmarking fault detection, identification and diagnosis methodologies.

4 Sample case study

This is the same case study reported in the paper:

Destro, F., Nagy, Z. K. and M. Barolo (2022). A benchmark simulator for quality-by-design and quality-by-control studies in continuous pharmaceutical manufacturing – Intensified filtration-drying of paracetamol/ethanol slurries. *Comput. Chem. Eng.*

We consider a sample case study with the objective of designing a control strategy to assign or adjust

Δt_{cycle}^{sp} , following the operating conditions proposed in challenge #5 (Section 3). We investigate three control strategies (#1-3). The only difference between them is the way in which Δt_{cycle}^{sp} is adjusted; all the other operating variables are always kept at their nominal values, which are the same in all cases (Table 5). Control strategies #1 and #2 keep Δt_{cycle}^{sp} constant at an assigned nominal value; therefore, the operation is entirely open loop for these strategies. Instead, control strategy #3 features a closed-loop control system that automatically adjusts Δt_{cycle}^{sp} based on the attainment of an assigned quality target. For each disturbance scenario described in Section 2.4, all three control strategies are tested, resulting in nine simulations of carousel operation, each one of 30 min duration. The simulator inputs are summarized in Table 5. The implemented control strategies are coded in the default `controller_cycle_switch.m` and `controller_online.m` functions of the simulator.

Table 5. Case study: simulator inputs set in `run_carousel.m`.

Variable name in <code>run_carousel.m</code>	Value	UOM
<code>control_mode</code>	Control strategies #1,2: 0 Control strategy #3: 1	-
<code>disturbance_scenario</code>	0, 1, 2 (every control strategy tested in every disturbance scenario)	-
<code>total_duration</code>	1800	s
<code>u_nominal.t_rot</code>	Control strategies #1,3: 30 Control strategy #2: 45	s
<code>u_nominal.V_slurry</code>	3.0×10^{-6}	m ³
<code>u_nominal.P_compr</code>	1.0×10^5	Pa _g
<code>u_nominal.Tinlet_drying</code>	323.0	K
<code>cryst_output.conc_slurry</code>	250.0	kg/ m ³
<code>control_interval</code>	1	s
<code>sampling_interval</code>	0.1	s
<code>inter_cycle_Dt</code>	0	s
<code>mesh_clean_Dt</code>	0	s

Let us first consider the two open-loop control strategies (control strategies #1 and #2):

- control strategy #1: open-loop control, with $\Delta t_{cycle}^{sp} = 30$ s;
- control strategy #2: open-loop control, with $\Delta t_{cycle}^{sp} = 45$ s.

Figure 6 shows the ethanol content in the discharged cakes for the simulation conditions of Table 5, with control strategies #1 and #2 under normal operating conditions (disturbance scenario 0); results are also plotted for control strategy #3 (to be discussed later). While with control strategy #2 all the discharged cakes meet the target quality, with control strategy #1 several cakes contain more ethanol than can be accepted. The improved performance of control strategy #2 is due to the larger cycle duration, that allows for longer cake drying.

Table 6 clarifies the correspondence between the process time and the number of processing cycle under control strategy #2 in normal operating conditions. The stations active during each cycle are also listed (note that this piece of information is available from the simulation output; Table 3). For a given cycle, two additional pieces of information are also reported: the progressive count of cakes that will form from the slurry loaded in Station 1, and the progressive count of cakes dried in Station 4 and discharged at the cycle end. Note that the numbers of the discharged cakes correspond to those in Figure 6 for control strategy #2. During the first cycle after carousel start-up, only Station 1 is active. From the slurry loaded into this station, cake #1 forms, but it will be discharged from the

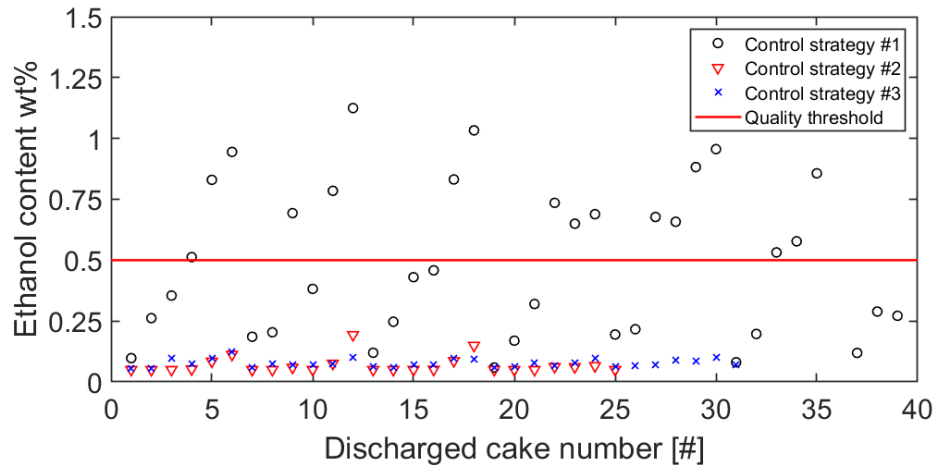


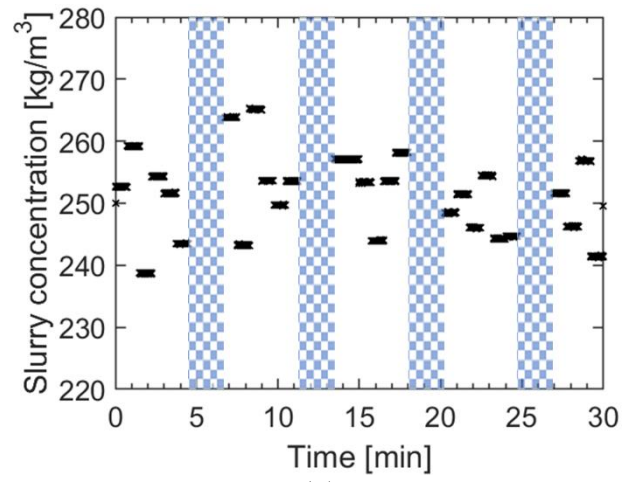
Figure 6. Case study: ethanol content in discharged cakes under control strategy #1-3 in disturbance scenario 0 (normal operating conditions).

carousel only at the end of the fourth cycle, after having being processed in Station 2, 3 and 4 during, respectively, cycles 2, 3 and 4.

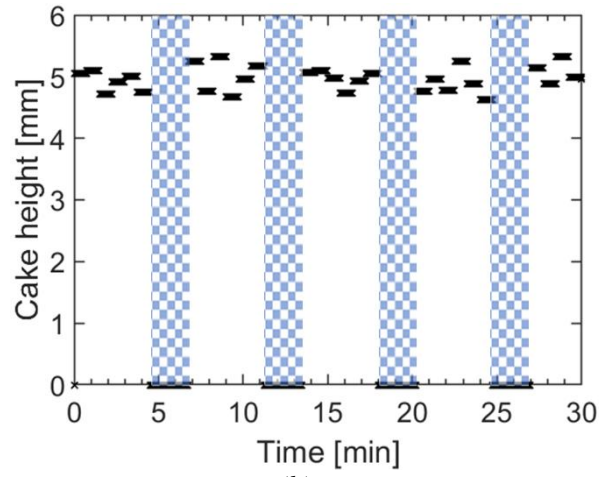
From the process onset, cycle 4 is the first one during which all the stations of the carousel are filled and operate simultaneously. At the end of cycle 6, the resistance of the filter mesh of Station 1 crosses the threshold value (Figure 5), and this triggers the cleaning-in-place procedure. Hence, during cycle 7, no slurry is fed to Station 1, and this station remains inactive. During cycle 8, the ports corresponding to both Stations 1 and 2 are empty, while during cycle 9 only Station 4 is active. At the end of cycle 9, the cake just dried in Station 4 is discharged, and all ports remain empty. The filter meshes are cleaned (instantaneously, as set in the inputs; Table 5), and from cycle 10 the carousel is

Table 6. Case study: control strategy #2 in disturbance scenario 0. Correspondence among process time, cycle number, and stations active during every cycle. For every cycle, the following information is also reported; progressive count of cakes formed from the slurry fed to Station 1, and progressive count of cakes dried in Station 4 and discharged at the cycle end.

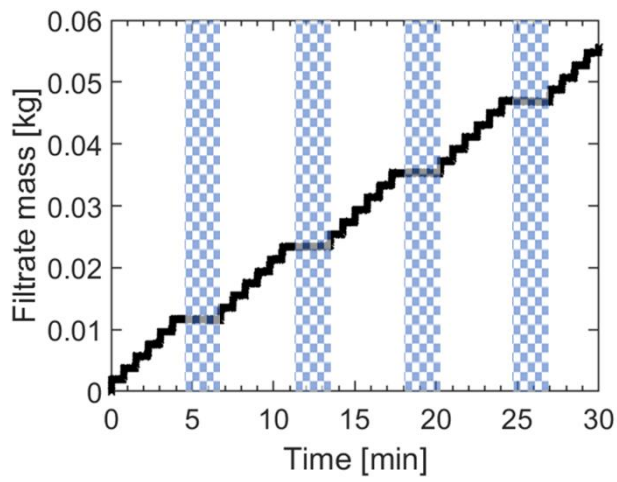
Process time [min]	Cycle #	Stations active	Loaded cake #	Discharged cake #
0.00-0.75	1	1	1	-
0.75-1.50	2	1,2	2	-
1.50-2.25	3	1,2,3	3	-
2.25-3.00	4	1,2,3,4	4	1
3.00-3.75	5	1,2,3,4	5	2
3.75-4.50	6	1,2,3,4	6	3
4.50-5.25	7	2,3,4	-	4
5.25-6.00	8	3,4	-	5
6.00-6.75	9	4	-	6
6.75-7.50	10	1	7	-
7.50-8.25	11	1,2	8	-
8.25-9.00	12	1,2,3	9	-
9.00-9.75	13	1,2,3,4	10	7
9.75-10.50	14	1,2,3,4	11	8
10.50-11.25	15	1,2,3,4	12	9
11.25-12.00	16	2,3,4	-	10
12.00-12.75	17	3,4	-	11
12.75-13.50	18	4	-	12
...
28.50-29.25	39	1,2,3	27	-
29.25-30.00	40	1,2,3,4	28	25



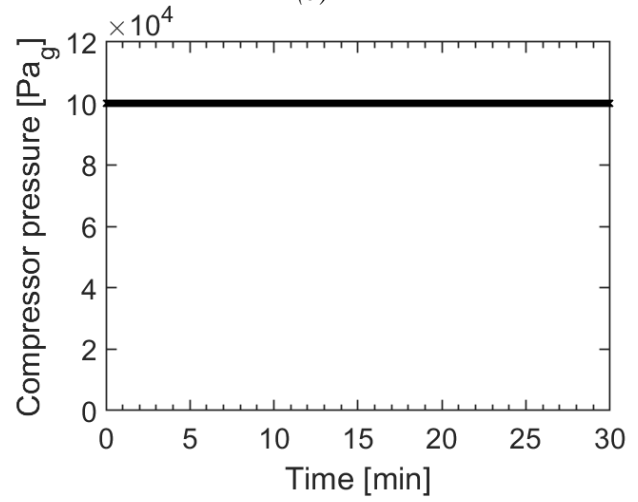
(a)



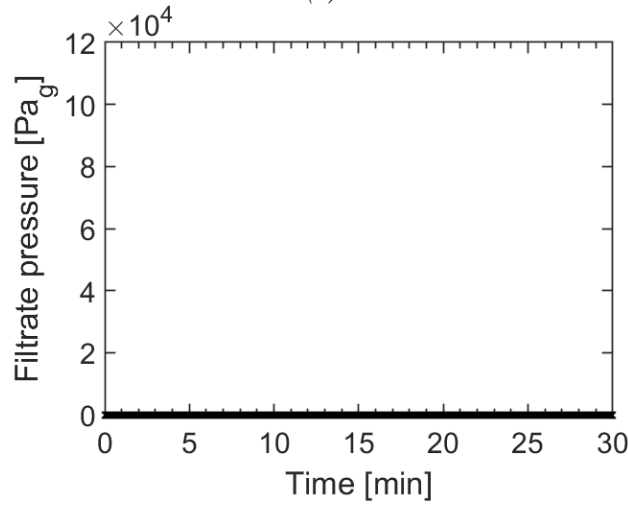
(b)



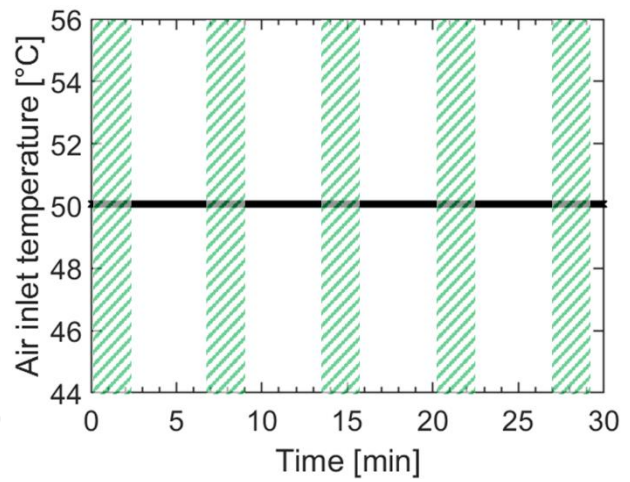
(c)



(d)



(e)



(f)

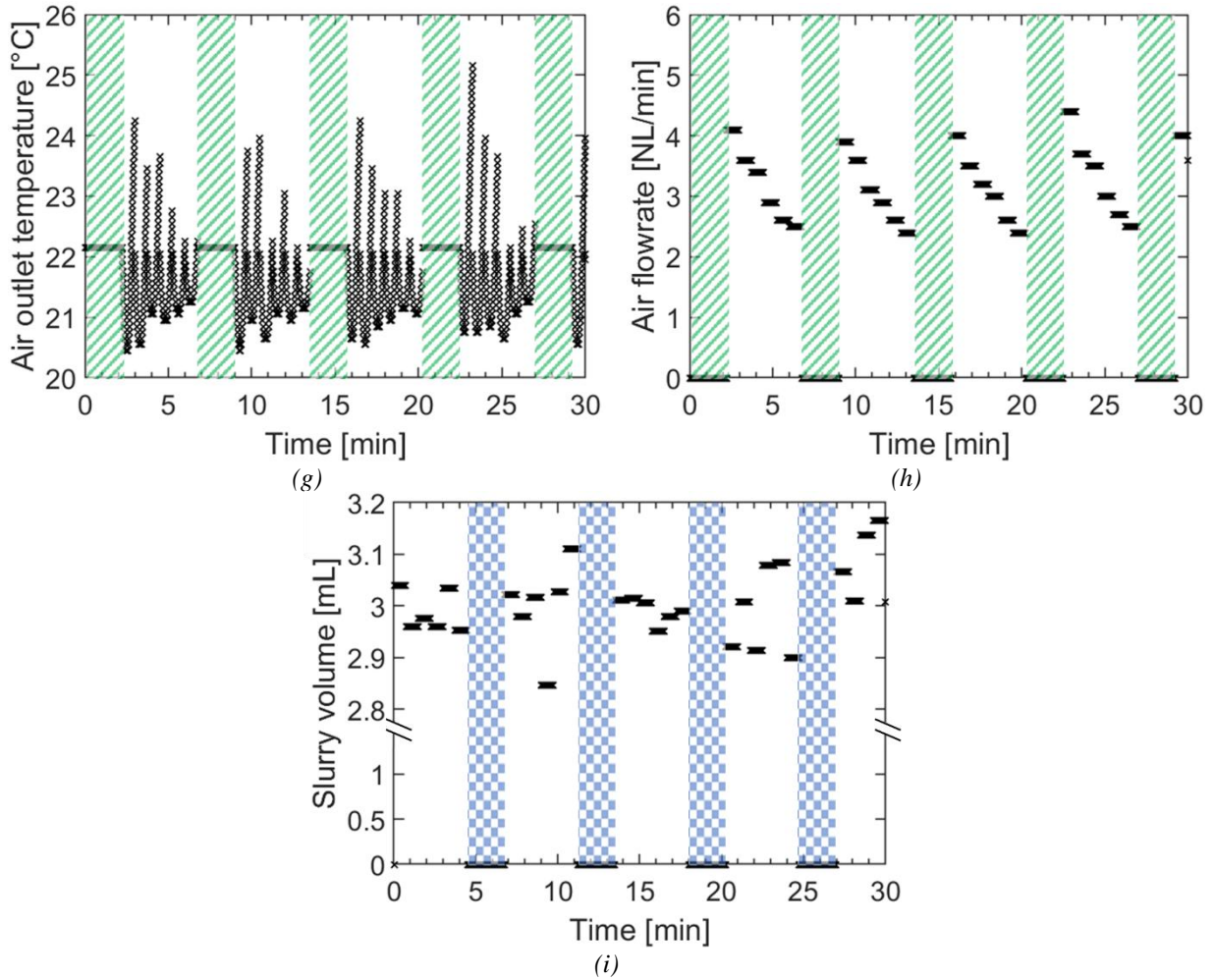


Figure 7. Case study: simulated measurements (Table 3) under control strategy #2 in disturbance scenario 0 (normal operating conditions). (a) slurry concentration, (b) cake height, (c) filtrate mass, (d) compressor delivery pressure, (e) filtrate pressure, (f) drying air inlet temperature, (g) drying air outlet temperature, (h) air flowrate, and (i) fed slurry volume. The shaded areas in the figures indicate the time windows during which the station relevant to each measurement is inactive: blue squares= Station 1, green diagonal stripes= Station 4.

started-up again, with the same schedule followed at the process onset. The same processing-cleaning routine is followed until the process finishes.

The plots of selected simulated variables under control strategy #2 in normal operating conditions are shown in Figure 7. The step variations seen in most plots (e.g., in the measured slurry concentration, Figure 7a), are due to the onset of new cycles, when the carousel rotates and a new slurry load is fed to V101. Time intervals during which no slurry concentration is plotted in Figure 7a correspond to those periods when V101 is empty due to the cleaning-in-place routine. Null values during the cleaning-in-place routines are also registered for the measured cake height (Figure 7b) and fed slurry volume (Figure 7i). While (small) intra-cycle variations of the measured slurry concentration are due to noise (not visible in Figure 7a), inter-cycle fluctuations around the nominal slurry concentration ($\bar{c}_{slurry} = 250 \text{ kg/m}^3$) are a consequence of disturbance c_{slurry}^{dist} . The same applies to the fed slurry volume, whose inter-cycle fluctuations (Figure 7h) around $V_{slurry}^{sp} (= 3 \text{ mL})$ are due to V_{slurry}^{dist} . Inter-cycle variations of the cake height (Figure 7b) are, instead, due to the combined effect of c_{slurry}^{dist} , V_{slurry}^{dist} , and ϵ^{dist} .

The filtrate mass (Figure 7c) presents a growing profile, as during the process the filtrate keeps accumulating in the filtrate receiver under which scale WI-101 is installed. Since there is only one filtrate collector for all ports, the signal read in Figure 7c is the cumulative filtrate from filtration and deliquoring coming from all ports. However, since the weight of the filtrate collected from filtration is orders of magnitudes greater than the one from deliquoring and, for the given disturbance scenario with the operating variables set as in control strategy #2, cake filtration ends while the cake is still in V101, most (>99%) of the filtrate collected in the receiver comes from V101. Sharp increases in the filtrate mass are due to the onset of a new cycle, when new slurry is loaded into V101 and starts being filtered. When filtration finishes, the filtrate mass remains almost constant, except for small changes due to deliquoring, until a new cycle is initiated. The longer periods of time during which the filtrate mass does not increase (e.g., about 4.5 to 6.75 min from the process onset) correspond to the time window during which V101 is empty, due to the cleaning-in-place routine.

The measured inlet drying air temperature (Figure 7f) is constant during the simulation, because $T_{in,g}^{sp}$ is operated at open-loop, fixed at its nominal value in control strategy #2. At the drying onset, the outlet air temperature (Figure 7g) drops, because of the large amount of heat spent for ethanol vaporization. When the ethanol content in the cake becomes lower, the drying rate decreases, and the outlet air temperature starts rising. The periods of time during which the measured air temperature is at the room value (22.1 °C) are the cycles in which no cake is being dried in V104. These cycles are the first three ones after the process onset or mesh cleaning, and are also identified in Figure 7h as those time windows in which the air flowrate is null. The benefits of mesh cleaning are also highlighted in Figure 7h, which shows how the air flowrate decreases cycle-after-cycle after that the cleaning routine is carried out.

The plots of the ethanol content during carousel processing for the first discharged cake (Figure 8) under control strategy #2 in disturbance scenario 0 provide additional information on the process. Note that even though the ethanol content is an output of the simulator, it is not a measurement available in real carousels. During processing in the first station (Figure 8a), the ethanol content decreases from the initial value of about 26 wt% to slightly below 5 wt%. The trait in Figure 8a at constant ethanol content (up to about 30 s from the process onset) corresponds to filtration. When filtration ends, deliquoring starts, and the liquid starts exiting the cake pores. The ethanol content in the cake quickly approaches the equilibrium value for deliquoring, and the further reduction in Stations 2-3 (Figure 8b-c, respectively) is modest. Only by thermal drying (Station 4; Figure 8d) can the ethanol content significantly decrease, eventually dropping below the acceptable quality threshold. As shown in Figure 8d, the drying duration needed for reaching the target quality is about 20 s for this cake. However, simulations show that for cakes processed in presence of more severe fouling conditions, a larger drying duration is needed: this is the reason why control strategy #2 leads to obtain product of satisfying quality in Figure 6, while control strategy #1 does not.

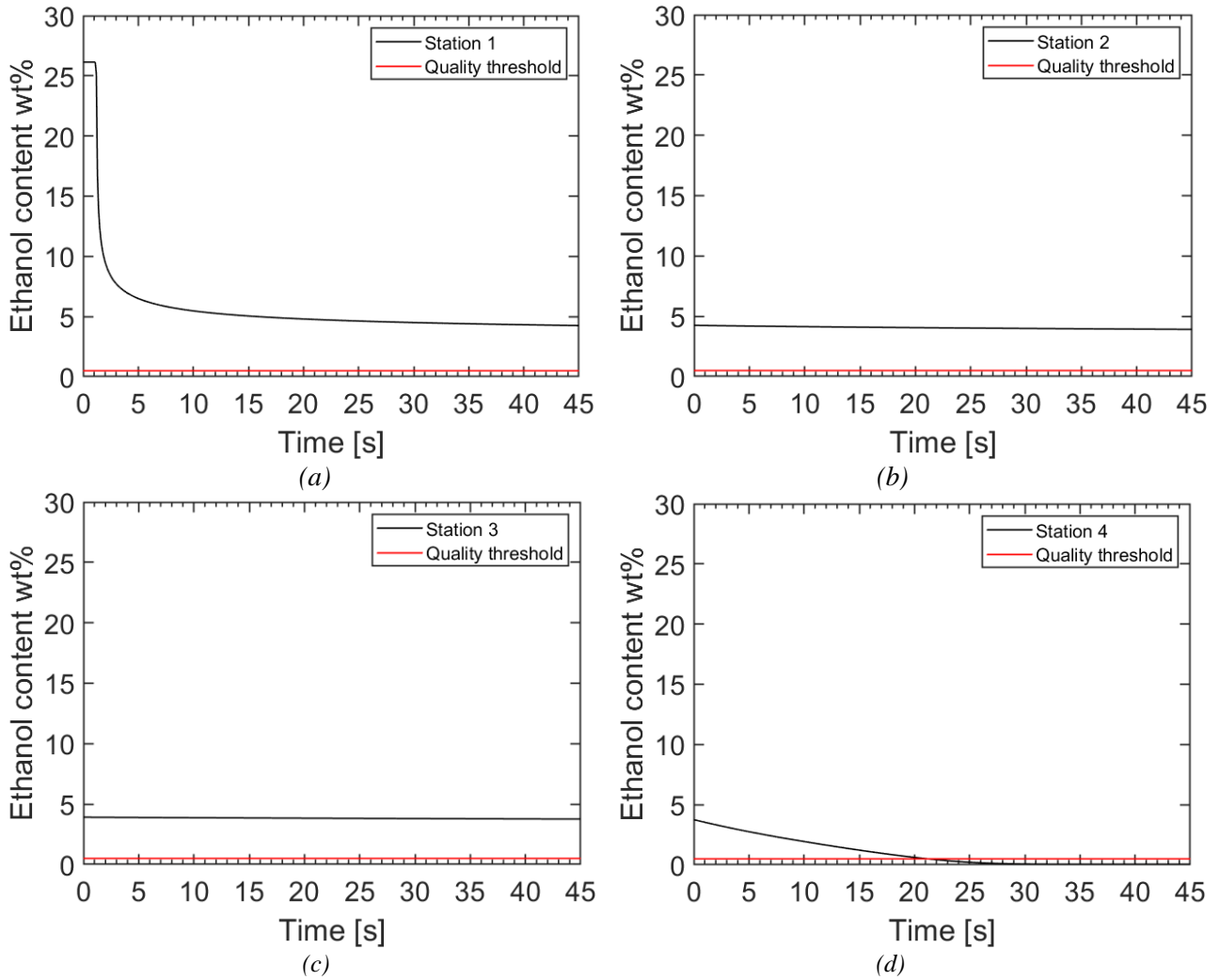


Figure 8. Case study: ethanol content in the first discharged cake across whole carousel processing (control strategy #2, disturbance scenario 0). (a) Station 1, (b) Station 2, (c) Station 3, and (d) Station 4.

We now consider a third control strategy (control strategy #3), which manipulates Δt_{cycle} to terminate every cycle when the target product quality is estimated to have been achieved. Under control strategy #3:

- i) For cycles in which no cake is being dried in Station 4 (V104), $\Delta t_{cycle}^{sp} = 30$ s;
- ii) For cycles in which a cake is being dried in Station 4 (V104), the cycle is terminated when the drying air outlet temperature measurement reaches room temperature (after the temperature inversion). In practice, the drying air outlet temperature measurement is used as a surrogate measurement to infer the cycle end-point at which the target ethanol content in the cake being dried is reached.

Note that, although drying is almost complete after the temperature inversion, generally speaking there is no guarantee that waiting for outlet air temperature to reach room temperature is always enough to guarantee the product quality for all process and operating conditions. In this study, condition ii) has been designed and validated with simulations for the case study under investigation. control strategy #3 allows meeting the target quality for all the discharged cakes in normal operating conditions, and yields to obtaining six more cakes than with control strategy #2 in the same processing time (Figure 6). control strategy #3 leads to an improved performance also under abnormal operating conditions. When the slurry concentration is subject to a ramp increase (disturbance scenario 1; Figure

9a), control strategy #2 allows meeting the product quality specification, but under control strategy #3 two cakes more are produced in the same processing time. However, under a step increase of the specific cake resistance (disturbance scenario 2; Figure 9b), control strategy #2 does not even allow meeting the target quality in most cakes, whereas control strategy #3 always lead to satisfying the target product quality.

The profiles of cycle duration under control strategy #3 in disturbance scenarios 0-2 are reported in Figure 10. Following Condition #1 of control strategy #3, cycles during which the dryer is empty (e.g., cycle #0-3) always present Δt_{cycle} equal to 30 s. However, when drying occurs, the cycle duration is adapted by the controller system, based on the drying air outlet temperature measurement. The effect is, as expected, that a larger cycle duration is selected for increasing mesh fouling conditions, as particularly evident in normal operating conditions (disturbance scenario 0). The significantly larger cycle duration needed for obtaining a cake meeting the target quality under the specific cake step disturbance (disturbance scenario 2) can be clearly assessed in Figure 10, explaining why control strategy #2 fails to deliver the target product quality in this situation (Figure 9b).

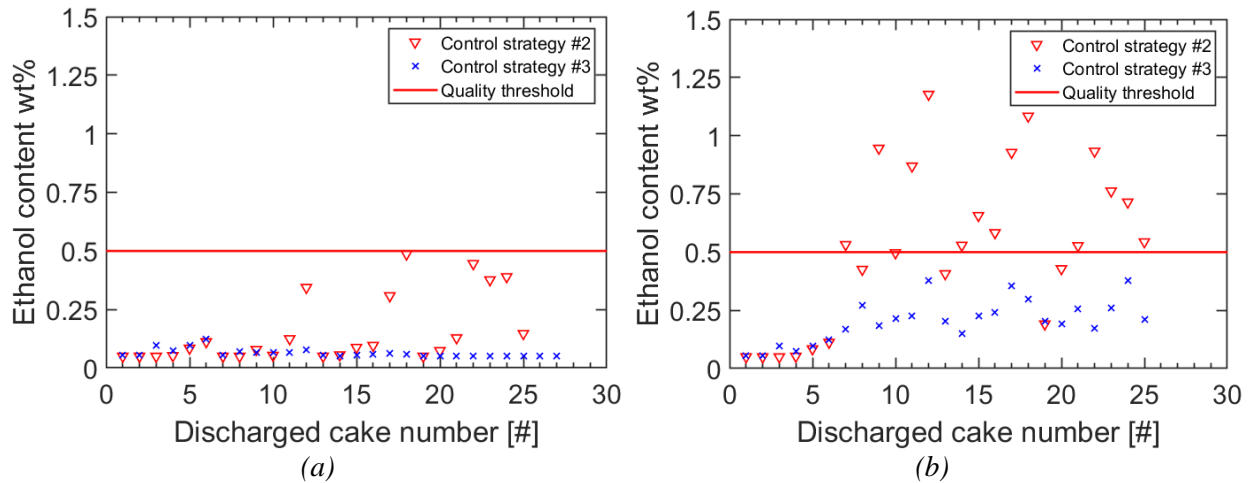


Figure 9. Case study: ethanol content in discharged cakes under control strategies #2-3 (a) in disturbance scenario 1 (slurry concentration ramp change), and (b) in disturbance scenario 2 (specific cake resistance step change).

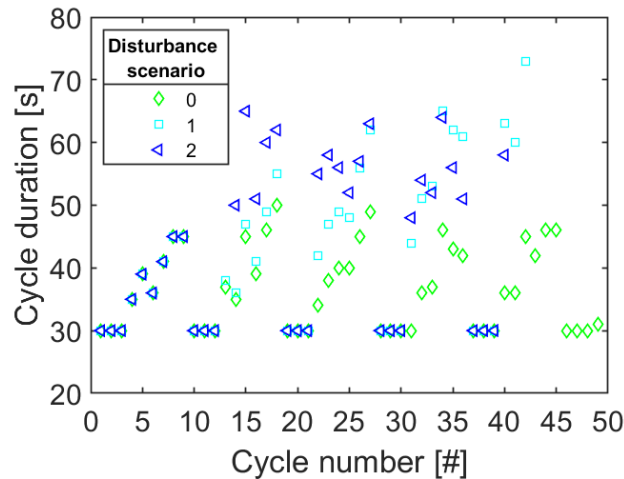


Figure 10. Case study: cycle duration under control strategy #3 in disturbance scenarios 0-2.

Additional details on processing and cleaning cycles

Table 7 provides clarification on which stations are active during which cycle of carousel operation, for the first 18 cycles of carousel operation. For each cycle, the identifying number of the cake being processed in each station is also reported. Note that Table 7 is valid for all the simulations generated with *ContCarSim*. Since the fouling schedule of Figure 5 is always reproduced in all simulations according to the same pattern, the cycles at which the cleaning-in-place routine is triggered are always the same, and the number of the cake processed in a particular station in a given cycle is always the same. However, the time at which a particular cycle is initiated depends on the specific simulation settings.

Table 7. List of carousel stations active for each of the first 18 cycles of carousel operation. The identifying number of cakes being processed in every station for each of the considered cycle is also reported. The information reported in this table is valid for all simulations, independently from the input settings.

Cycle #	Stations active	Cake processed in Station:			
		1	2	3	4
1	1	1	-	-	-
2	1,2	2	1	-	-
3	1,2,3	3	2	1	-
4	1,2,3,4	4	3	2	1
5	1,2,3,4	5	4	3	2
6	1,2,3,4	6	5	4	3
7	2,3,4	-	6	5	4
8	3,4	-	-	6	5
9	4	-	-	-	6
10	1	7	-	-	-
11	1,2	8	7	-	-
12	1,2,3	9	8	7	-
13	1,2,3,4	10	9	8	7
14	1,2,3,4	11	10	9	8
15	1,2,3,4	12	11	10	9
16	2,3,4	-	12	11	10
17	3,4	-	-	12	11
18	4	-	-	-	12