

EE307 Homework 4

Name: 吉辰卿 ID: 11911303

Question 1-2:

EE 307 HW 4

Name: 吉辰卿 ID: 11911303

1. solution:

because: $A = \vec{A}_r + \vec{A}_\theta + \vec{A}_\phi = \frac{\mu I_0 e^{-jkr}}{4\pi r} \cos\theta \vec{a}_r + \left(\frac{-\mu I_0 e^{-jkr}}{4\pi r} \sin\theta \right) \vec{a}_\theta \neq$

so: for H field: $H_A = \frac{1}{\mu} \nabla \times \vec{A} = \frac{1}{\mu} \left[0 \vec{a}_r + 0 \vec{a}_\theta + \frac{\vec{a}_\phi}{r} \left[\frac{\partial(r A_\theta)}{\partial r} - \frac{\partial A_r}{\partial \theta} \right] \right]$

so: $H_A = \frac{\vec{a}_\phi}{\mu r} \left[\frac{j k \mu I_0 e^{-jkr}}{4\pi} \sin\theta + \frac{\mu I_0 e^{-jkr}}{4\pi r} \sin\theta \right]$

$= \frac{j k I_0 \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \vec{a}_\phi$

Therefore: $H_A = \frac{j k I_0 \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \vec{a}_\phi$ so, $H_r = H_\theta = 0$

$H_\phi = \frac{j k I_0 \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} \right] e^{-jkr}$

Then, For E field: $E_A = -\nabla \phi_e - j\omega A = -j\omega A - j \frac{1}{\omega \mu \epsilon} \nabla(\nabla \cdot A)$

so: $\nabla \cdot A = \frac{1}{r^2} \cdot \frac{\partial}{\partial r} \left(\frac{\mu I_0 (r \cdot e^{-jkr})}{4\pi} \cos\theta \right) + \frac{1}{r \sin\theta} \cdot \frac{\partial}{\partial \theta} \left(\frac{-\mu I_0 e^{-jkr} \sin^2\theta}{4\pi r} \right)$

$= \frac{1}{r^2} \left(\frac{\mu I_0 e^{-jkr} \cos\theta}{4\pi} + \frac{-jkr \mu I_0 e^{-jkr} \cos\theta}{4\pi} \right) + \frac{1}{r \sin\theta} \frac{\partial}{\partial \theta} \left(\frac{-\mu I_0 e^{-jkr} (1 - \cos 2\theta)}{8\pi r} \right)$

$= \frac{1}{r^2} \left(\frac{\mu I_0 e^{-jkr} \cos\theta}{4\pi} + \frac{-jkr \mu I_0 e^{-jkr} \cos\theta}{4\pi} \right) + \frac{1}{r \sin\theta} \frac{-\mu I_0 e^{-jkr} \sin 2\theta}{4\pi r}$

$= \frac{1}{r^2} \left(\frac{\mu I_0 e^{-jkr} \cos\theta}{4\pi} + \frac{-jkr \mu I_0 e^{-jkr} \cos\theta}{4\pi} \right) + \frac{-\mu I_0 e^{-jkr} \cos\theta}{2\pi r^2} = \nabla \cdot A$

so: $\nabla(\nabla \cdot A) = \vec{a}_r \frac{\partial(\nabla \cdot A)}{\partial r} + \vec{a}_\theta \cdot \frac{1}{r} \frac{\partial(\nabla \cdot A)}{\partial \theta} + \vec{a}_\phi \cdot \frac{1}{r \sin\theta} \frac{\partial(\nabla \cdot A)}{\partial \phi}$

$= \vec{a}_r \left[\frac{\mu I_0 \cos\theta}{4\pi} \left(\frac{e^{-jkr}}{r^2} + \frac{-jkr e^{-jkr}}{r^2} + \frac{-2e^{-jkr}}{r^2} \right) \right]$

$+ \frac{1}{r} \left[\frac{1}{r^2} \frac{-\mu I_0 e^{-jkr} \sin\theta}{4\pi} + \frac{1+jkr}{r^2} \frac{\mu I_0 e^{-jkr} \sin\theta}{4\pi} + \frac{\mu I_0 e^{-jkr} \sin\theta}{2\pi r^2} \right] \vec{a}_\theta$

$$= \frac{\mu_0 I_0 \cos \theta}{4\pi} \left(\frac{-jke^{-jkr}}{r^2} - \frac{2e^{-jkr}}{r^3} + \frac{jke^{-jkr}}{r} - \frac{k^2 e^{-jkr}}{r} \right) + \frac{jk2e^{-jkr}}{r^2} + \frac{4\pi e^{-jkr}}{r} \Bigg) \vec{a}_r$$

$$+ \frac{1}{r^3} \frac{\mu_0 I_0 e^{-jkr} \sin \theta}{4\pi} \left[jkr - 1 + \frac{r}{2} \right] \vec{a}_\theta \quad \text{and } \eta = \frac{\omega \mu}{k} = \sqrt{\frac{\mu}{\epsilon}}$$

$$S_0: \vec{E}_\theta = -j\omega A - j\frac{1}{\omega \mu \epsilon} \nabla(\nabla \cdot \vec{A}) = -j\omega \left[\frac{\mu_0 I_0 e^{-jkr}}{4\pi r} \cos \theta \vec{a}_r - \frac{\mu_0 I_0 e^{-jkr}}{4\pi r} \sin \theta \vec{a}_\theta \right]$$

$$- j\frac{1}{\omega \mu \epsilon} \left[\frac{\mu_0 I_0 \cos \theta}{4\pi} \left(\frac{-jke^{-jkr}}{r^2} - \frac{2e^{-jkr}}{r^3} + \frac{jke^{-jkr}}{r} - \frac{k^2 e^{-jkr}}{r} + \frac{jk2e^{-jkr}}{r^2} + \frac{4\pi e^{-jkr}}{r} \right) \vec{a}_r \right.$$

$$\left. + \frac{1}{r^3} \frac{\mu_0 I_0 e^{-jkr} \sin \theta}{4\pi} [jkr + 1] \vec{a}_\theta \right]$$

$$= \frac{\omega \mu_0 I_0 \cos \theta}{2\pi r^2 \cdot k} \left[\frac{1}{jkr} + 1 \right] e^{-jkr} \vec{a}_r + \frac{j\omega \mu_0 I_0 \sin \theta}{4\pi kr} \left[1 - \frac{1}{(kr)^2} + \frac{1}{jkr} \right] e^{-jkr}$$

$$S_0: \vec{E}_A = \frac{\eta I_0 \cos \theta}{2\pi r^2} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \vec{a}_r + \frac{j\eta k I_0 \sin \theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{-jkr} \vec{a}_\theta$$

$$\text{and: } \vec{E}_r = \frac{\eta I_0 \cos \theta}{2\pi r^2} \left[1 + \frac{1}{jkr} \right] e^{-jkr} \quad \text{and } \vec{E}_\theta = j\eta \frac{k I_0 \sin \theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{-jkr}$$

$$\vec{E}_\phi = 0$$

2. solution

because: $f = 10^6 \text{ Hz}$ so: $\lambda = \frac{c}{f} = \frac{3 \times 10^8}{10^6} = 300 \text{ m}$

so: $l = 1 \text{ m} = \frac{\lambda}{300}$ and because $l = \frac{\lambda}{300} < \frac{\lambda}{50}$

Therefore, we can assume that this antenna is an Infinite small dipole antenna

so, the average power density: $W_{av} = \frac{1}{2} \text{Re} (\vec{E} \times \vec{H}^*) = \vec{a}_r \cdot \frac{\eta}{2} \left| \frac{k I_0 l}{4\pi} \right|^2 \frac{\sin^2 \theta}{r^2}$

In this problem: $I_0 = 12 \text{ A}$, $r = 5 \times 10^3 \text{ m}$, $\theta = 45^\circ$ and $\eta = \sqrt{\frac{\mu}{\epsilon}} = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377$

so: $W_{av} = \frac{377}{2} \cdot k = \frac{2\pi}{\lambda} = \frac{\pi}{150}$

so: $W_{av} = \frac{377}{2} \times \left| \frac{\frac{\pi}{150} \cdot 12 \text{ A} \times 1 \text{ m}}{4\pi} \right|^2 \times \frac{\left(\frac{\sqrt{2}}{2} \right)^2}{25 \times 10^6} \approx 1.508 \times 10^{-9} \text{ W/m}^2$

so, the average power density is $1.508 \times 10^{-9} \text{ W/m}^2$.

Question 3

The radiation pattern for :

- half wavelength dipole

1. result figure

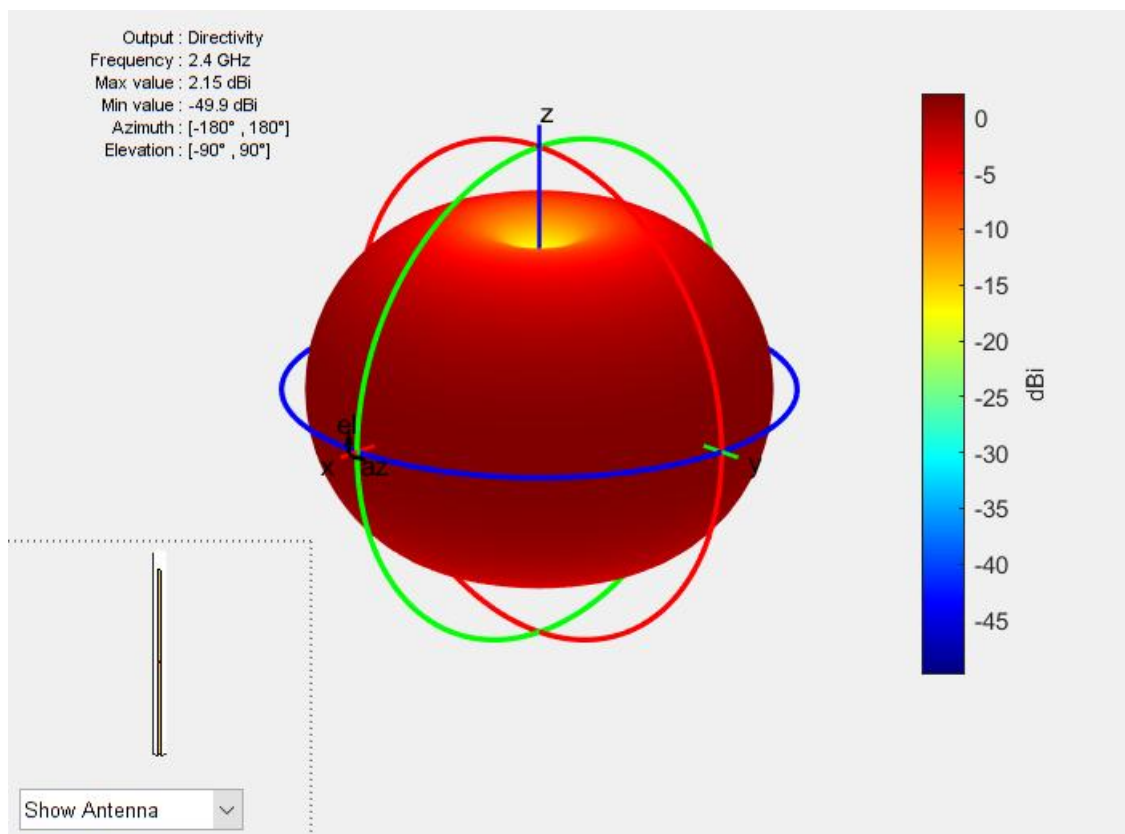


Figure 1 3D radiation pattern for half wavelength dipole

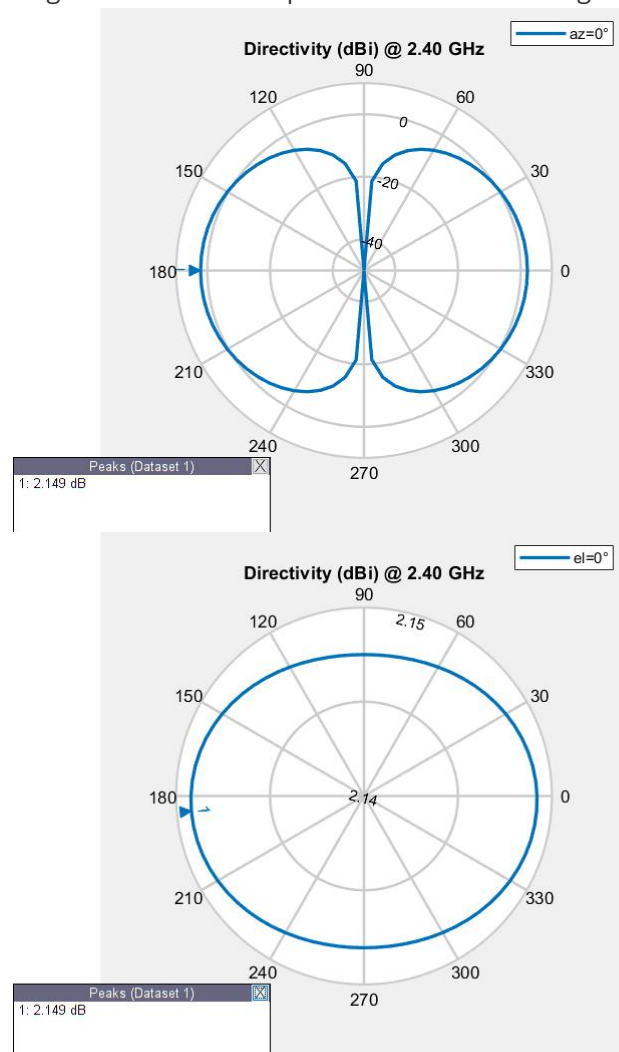


Figure 2 2D radiation pattern for half wavelength dipole

2. MATLAB codes

```

1 % Create a dipole antenna
2 % Generated by MATLAB(R) 9.10 and Antenna Toolbox 5.0.
3 % Generated on: 12-Mar-2022 00:56:42
4
5 %% Antenna Properties
6
7 antennaObject = design(dipole, 2400*1e6);
8 antennaObject.Length = 0.062;
9 % Show
10 figure;
11 show(antennaObject)
12
13 %% Antenna Analysis
14 % Define plot frequency
15 plotFrequency = 2400*1e6;
16 % Define frequency range
17 freqRange = (2160:24:2640)*1e6;
18 % sparameter
19 figure;
20 s = sparameters(antennaObject, freqRange);
21 rfplot(s)
22 % pattern
23 figure;
24 pattern(antennaObject, plotFrequency)
25 % azimuth
26 figure;
27 patternAzimuth(antennaObject, plotFrequency, 0, 'Azimuth', 0:5:360)
28 % elevation
29 figure;
30 patternElevation(antennaObject, plotFrequency, 0, 'Elevation', 0:5:360)

```

- quarter wavelength monopole (infinite ground)

1. Result figure

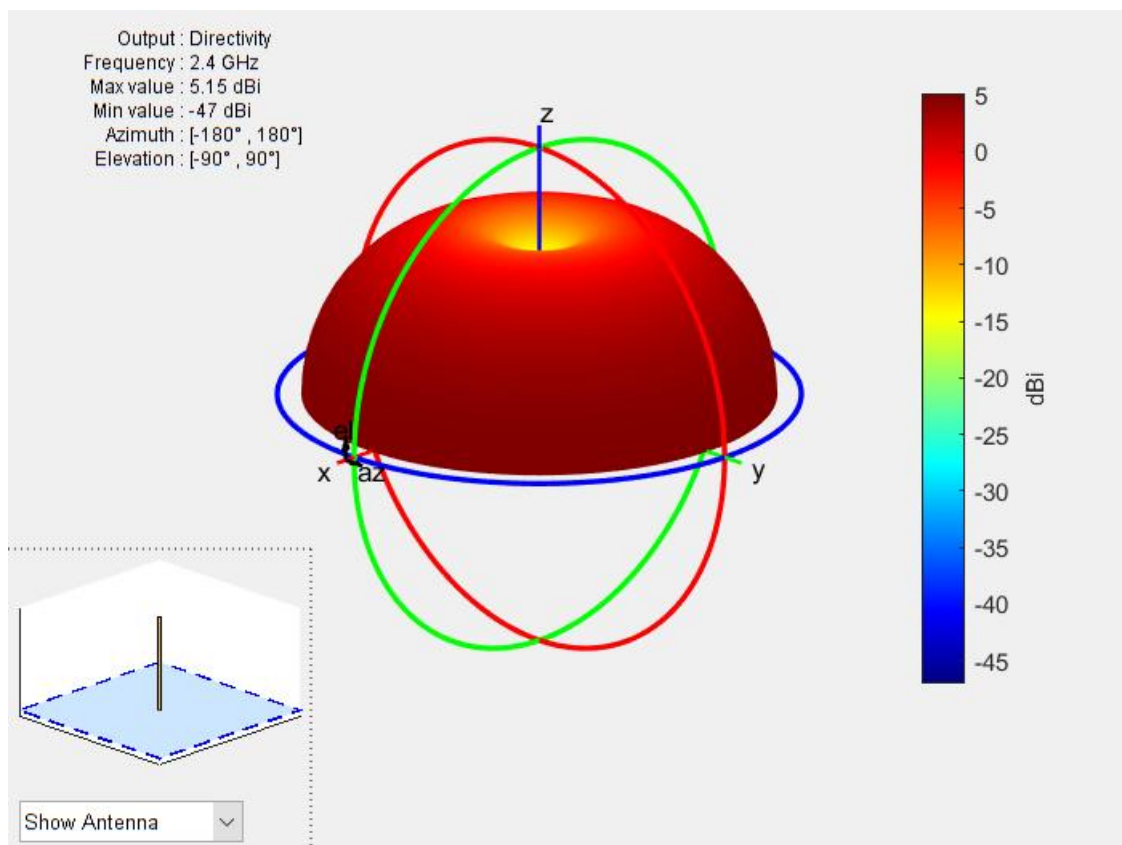


Figure 3 3D radiation pattern for quarter wavelength monopole

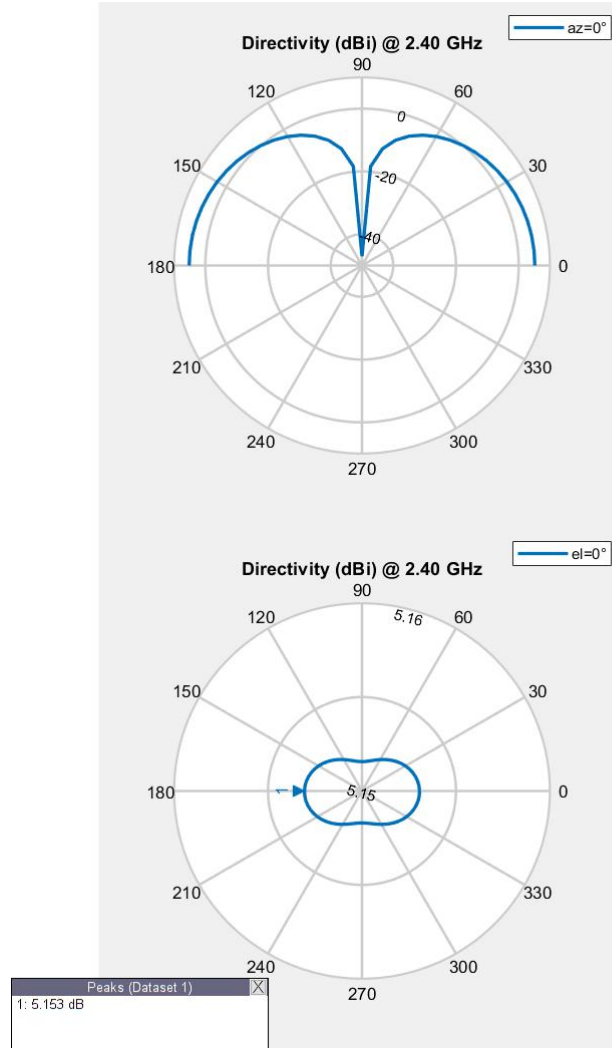


Figure 4 2D radiation pattern for quarter wavelength monopole

2. MATLAB codes

```

1 % Create a monopole antenna
2 % Generated by MATLAB(R) 9.10 and Antenna Toolbox 5.0.
3 % Generated on: 12-Mar-2022 01:15:12
4
5 %% Antenna Properties
6
7 antennaObject = design(monopole, 2400*1e6);
8 antennaObject.Height = 0.0307;
9 antennaObject.GroundPlaneLength = inf;
10 antennaObject.GroundPlaneWidth = inf;
11 % Show
12 figure;
13 show(antennaObject)
14
15 %% Antenna Analysis
16 % Define plot frequency
17 plotFrequency = 2400*1e6;
18 % Define frequency range
19 freqRange = (2160:24:2640)*1e6;
20 % pattern
21 figure;
22 pattern(antennaObject, plotFrequency)
23 % azimuth
24 figure;
25 patternAzimuth(antennaObject, plotFrequency, 0, 'Azimuth', 0:5:360)
26 % elevation
27 figure;
28 patternElevation(antennaObject, plotFrequency, 0, 'Elevation', 0:5:360)

```

Theoretical Calculation (Calculate Directivity and HPBW for each antenna)

See the next two page below :

3. solution

calculate the directivity and HPBW for each antenna.

① half-wavelength dipole

because we know: for linear Antenna:

$$W_{av} = \vec{a}_r \cdot W_{av} = \vec{a}_r \cdot \gamma \frac{I_0^2}{8\pi^2 r^2} \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2$$

$$\text{and } U = r^2 W_{av} = \gamma \frac{I_0^2}{8\pi^2} \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2$$

$$\text{so: } D_0 = D_{max} = P(\theta, \phi)_{max} = \frac{U(\theta, \phi)_{max}}{U_0} = \frac{4\pi U(\theta, \phi)_{max}}{P_{rad}}$$

$$\text{and: } P_{rad} = \int_0^{2\pi} \int_0^\pi \vec{a}_r \cdot W_{av} \cdot \vec{a}_r \cdot r^2 \sin\theta d\theta d\phi = \gamma \frac{I_0^2}{4\pi^2} \int_0^{2\pi} \int_0^\pi \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2 \sin\theta d\theta d\phi$$

$$\therefore P_{rad} = \gamma \frac{I_0^2}{4\pi^2} \left\{ C + \ln(kl) - Ci(kl) + \frac{1}{2} \sin(kl) [Si(2kl) - 2Si(kl)] + \frac{1}{2} \cos(kl) [C + \ln(kl/2) + Ci(2kl) - 2Ci(kl)] \right\} \quad \text{where } C = 0.5772$$

and $Ci(x)$ and $Si(x)$ are the cosine and sine integrals.

$$\text{so: } D_0 = \frac{2F(\theta)_{max}}{Q}, \quad \text{and } F(\theta) = \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2$$

$$Q = \left\{ C + \ln(kl) - Ci(kl) + \frac{1}{2} \sin(kl) [Si(2kl) - 2Si(kl)] + \frac{1}{2} \cos(kl) [C + \ln(kl/2) + Ci(2kl) - 2Ci(kl)] \right\}$$

so, by calculator, we easily know that $Q \approx 1.2195$

because $(\frac{k}{2})$ in this problem, $k = \frac{2\pi}{\lambda}$ so: $kl = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{2} = \pi \Rightarrow \frac{kl}{2} = \frac{\pi}{2}$

$$\text{so: } F(\theta) = \left[\frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{\sin\theta} \right]^2, \quad \text{it means that } \text{when: } \theta = \frac{\pi}{2},$$

$$F(\theta)_{max} = 1 \quad \text{Therefore: } D_0 = \frac{2F(\theta)_{max}}{Q} = \frac{2}{1.2195} \approx 1.64 = D_{max}$$

$$\text{so: } P_{max} = D_0 = 1.64 = 2.15 \text{ dBi}$$

so, the directivity of $\frac{\lambda}{2}$ dipole is 2.15 dBi.

$$\text{Then: because: } D_0 = \frac{2F(\theta)_{max}}{Q} \quad \text{and } F(\theta) = \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2 = \left[\frac{\cos(\frac{\pi}{2} \cos\theta)}{\sin\theta} \right]^2$$

because when: $\theta = \frac{\pi}{2}$ or $\frac{3\pi}{2}$, we can get $F(\theta)_{max} = 1$

$$\text{and when: } F(\theta) = \frac{1}{2} \Rightarrow \text{That means: } \frac{\cos(\frac{\pi}{2} \cos\theta)}{\sin\theta} = \frac{1}{\sqrt{2}} = \frac{\sqrt{2}}{2} \quad \text{--- (1)}$$

so, by solving equation 1, we can get: $\theta = 51^\circ$ or 129° (in $\frac{\pi}{2}$ range)

$$\text{so: because } \theta = 51^\circ \text{ or } 129^\circ, \quad \text{HPBW} = (129^\circ - 51^\circ) = 78^\circ$$

∴ Therefore, for $\frac{1}{2}$ dipole, the directivity is 2.15 dBi and the HPBW for this antenna is 78° .

② for $\frac{1}{4}$ monopole (infinite ground)

Solution:

由镜像原理, 该 $\frac{1}{4}$ 单极子天线和其镜像构成了一个偶极子。

在地面上方, 该单极子天线和偶极子天线是完全相同的。

但 P_{rad} 只包围了上半空间的半球面。因此, 单极子的辐射功率 (P_{rad}) 是偶极子相应值的一半。

so: for monopole antenna: $P_{rad}/_{mono} = \frac{1}{2} P_{rad}/_{dipole}$

Therefore: for monopole antenna: $P_0 = \frac{4\pi U(\theta, \phi)_{max}}{P_{rad}/_{mono}} = \frac{4\pi U(\theta, \phi)_{max}}{\frac{1}{2} P_{rad}/_{dipole}}$

so: 相同长度的单极子天线的 D_0 为相同长度偶极子天线的 D_0 的 2 倍。
(单极子等效)

so, for dipole: $D_0 = \frac{2F(\theta)_{max}}{\Omega}$ and $\Omega \approx 1.2195$

$$F(\theta) = \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2 \quad \text{when } l = \frac{1}{2} \lambda \quad \text{so } kl = \pi \quad \text{and } \frac{kl}{2} = \frac{\pi}{2}$$

$$so: F(\theta) = \left[\frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{\sin\theta} \right]^2 \quad \text{因为这个 monopole 可以建模为: } \begin{array}{c} \frac{1}{4} \lambda \uparrow \\ \frac{1}{4} \lambda \uparrow (\text{镜像}) \end{array}$$

∴ 该 $\frac{1}{4}$ monopole antenna 相当于总长为 $\frac{1}{2}$ 的 dipole。

∴ 该 $\frac{1}{4}$ monopole antenna 的 D_0 为 $\frac{1}{2}$ 的 dipole 的 D_0 的 2 倍。

so, in the last problem: for $\frac{1}{2}$ dipole: $D_0 = 1.64 = 2.15 \text{ dBi} = D_0 / \frac{1}{2} \text{ dipole}$

so: for $\frac{1}{4}$ monopole antenna: $D_0 = \frac{4\pi U(\theta, \phi)_{max}}{P_{rad}/_{mono}} = \frac{4\pi U(\theta, \phi)_{max}}{\frac{1}{2} P_{rad}/_{dipole}} = 2D_0 / \frac{1}{2} \text{ dipole}$

so: $P_0 = 2D_0 / \frac{1}{2} \text{ dipole} = 3.28 \approx 5.15 \text{ dBi}$

Thom. for HPBW: $F(\theta) = \left[\frac{\cos(\frac{kl}{2} \cos\theta) - \cos(\frac{kl}{2})}{\sin\theta} \right]^2$ 因为 $\frac{1}{4}$ monopole antenna 可等效为 $\frac{1}{2}$ dipole.

so, as the same in problem (1), when: $F(\theta) = \frac{1}{2} F(\theta)_{max}$

we get: $\frac{\cos(\frac{\pi}{2} \cos\theta)}{\sin\theta} = \frac{\sqrt{2}}{2} \dots (1) \Rightarrow \theta = 51^\circ \text{ or } 129^\circ$ and when $\theta = \frac{\pi}{2} \text{ or } \frac{3\pi}{2}$, $F(\theta)$

but θ is for the dipole antenna, so, for monopole antenna,

we can get: $2 = \frac{\theta}{\frac{\pi}{2}} \dots (2)$ so, when $F(\theta)$ is max: $\theta = \frac{\pi}{2} \text{ or } \frac{3\pi}{2} \Rightarrow 2 = \frac{\theta}{\frac{\pi}{2}} \text{ or } \frac{3\pi}{2}$

when $F(\theta)$ is half the $F(\theta)_{max} = \theta = 51^\circ \text{ or } 129^\circ \Rightarrow 2 = \frac{\theta}{\frac{\pi}{2}} = 25.5^\circ \text{ or } 64.5^\circ$

so: HPBW = $64.5^\circ - 25.5^\circ = 39^\circ$ Therefore: for monopole antenna: The directivity is 3.28 (5.15 dBi) and the HPBW is 39° .