Table 19 Input data for the PANDA2 processor STAGSUNIT (allenflat.STG) for generating the STAGS input files, allenflat.bin and allenflat.inp. The same favorable circumferential variation in finite element mesh density is used as in Table 12: Finite elements are especially concentrated in the panel skin near the intersection of one of the central stringers in the 5-stringer-bay STAGS model. See Fig. 46.

```
$ Do you want a tutorial session and tutorial output?
              $ Choose type of STAGS analysis (1,3,4,5,6),INDIC
       1
              $ Restart from ISTARTth load step (0=1st nonlinear soln), ISTART
       0
              $ Local buckling load factor from PANDA2, EIGLOC
 1.000000
              $ Are the dimensions in this case in inches?
   У
              $ Nonlinear (0) or linear (1) kinematic relations?, ILIN
              $ Type 1 for closed (360-deg) cyl. shell, 0 otherwise, ITOTAL
       0
              $ X-direction length of the STAGS model of the panel: XSTAGS
9.779300
12.35250
              $ Panel length in the plane of the screen, L2
              $ Is the nodal point spacing uniform along the stringer axis?
              $ Number of nodes in the X-direction: NODEX
      61
-100.0000
              $ Resultant (e.g. lb/in) normal to the plane of screen, Nx
              $ Resultant (e.g. lb/in) in the plane of the screen,
       0
                                                                       Ny
       0
              $ In-plane shear in load set A,
       0
              $ Normal pressure in STAGS model in Load Set A, p
       0
              $ Resultant (e.g. lb/in) normal to the plane of screen, Nx0
       0
              $ Resultant (e.g. lb/in) in the plane of the screen,
                                                                       Ny0
               Normal pressure in STAGS model in Load Set B, p0
       0
              $ Starting load factor for Load System A, STLD(1)
1.000000
              $ Load factor increment for Load System A, STEP(1)
1.000000
              $ Maximum load factor for Load System A, FACM(1)
              $ Starting load factor for Load System B, STLD(2)
       0
              $ Load factor increment for Load System B, STEP(2)
       0
              $ Maximum load factor for Load System B, FACM(2)
       0
       1
              $ How many eigenvalues do you want? NEIGS
     480
              $ Choose element type: 480 or 410 or 940
              $ Have you obtained buckling modes from STAGS for this case?
   n
              $ Number of stringers in STAGS model of the flat panel
       6
       2
              $ Number of rings in the STAGS model of the panel
              $ Are there rings at the ends of the panel?
              $ Number of finite elements between adjacent stringers
       0
              $ Number of finite elements over circumference, NELCIR
      50
      30
              $ Number of finite elements between adjacent rings
       3
              $ Stringer model: 1 or 2 or 3 or 4 or 5(Type H(elp))
       3
              $ Ring model: 1 or 2 or 3 or 4 or 5 (Type H(elp))
       0
              $ Reference surface of cyl: 1=outer, 0=middle, -1=inner
              $ Do you want to use fasteners (they are like rigid links)?
   n
              $ Are the stringers to be "smeared out"?
   n
              $ Is the nodal point spacing uniform around the circumference?
    n
 4.446900
              $ Circ. callout Y(i) where the nodal point spacing changes, Y( 1)
              $ Number of nodes n(i) from Y(i-1) to Y(i) (n=odd!), n( 1)
      19
              $ Are there any more interior axial stations y where dy changes?
 4.693950
              $ Circ. callout Y(i) where the nodal point spacing changes, Y(2)
              \ Number of nodes n(i) from Y(i-1) to Y(i) (n=odd!), n(2)
       3
              $ Are there any more interior axial stations y where dy changes?
              $ Circ. callout Y(i) where the nodal point spacing changes, Y(3)
5.188050
              $ Number of nodes n(i) from Y(i-1) to Y(i) (n=odd!), n( 3)
      17
```

```
$ Are there any more interior axial stations y where dy changes?
5.435100
             $ Circ. callout Y(i) where the nodal point spacing changes, Y(4)
             $ Number of nodes n(i) from Y(i-1) to Y(i) (n=odd!), n(4)
      3
             $ Are there any more interior axial stations y where dy changes?
  У
             $ Circ. callout Y(i) where the nodal point spacing changes, Y( 5)
6.917400
             $ Number of nodes n(i) from Y(i-1) to Y(i) (n=odd!), n(5)
             $ Are there any more interior axial stations y where dy changes?
             $ Circ. callout Y(i) where the nodal point spacing changes, Y( 6)
7.905600
             $ Number of nodes n(i) from Y(i-1) to Y(i) (n=odd!), n(6)
      9
             $ Are there any more interior axial stations y where dy changes?
   n
             $ Number of nodes n(i) from last Y to y = YSTAGS, n(7)
     19
             $ Are the rings to be "smeared out"?
  n
             $ Number of nodes over height of stiffener webs, NODWEB
      5
      5
             $ Number of nodes over width of stringer flange, NDFLGS
             $ Number of nodes over width of ring flange, NDFLGR
             $ Do you want stringer(s) with a high nodal point density?
  n
             $ Do you want ring(s) with a high nodal point density?
  n
             $ Is there plasticity in this STAGS model?
  n
             $ Do you want to use the "least-squares" model for torque?
  n
             $ Is stiffener sidesway permitted at the panel edges?
  n
             $ Do you want symmetry conditions along the straight edges?
             $ Edges normal to screen (0) in-plane deformable; (1) rigid
      1
      1
             $ Edges parallel to screen (0) in-plane deformable; (1) rigid
             $ Stringer web axial displacement index, IBCX0XL=0 or 1
      1
```
