Table 92 Optimum design of the unstiffened imperfect equivalent ellipsoidal shell with the thick apex (Shell Segment 1) of uniform thickness 0.6 inch. The design in this table is the same as that in Table 78 except that the thickness of the spherical apex (cap = Shell Segment no. 1 in Fig. 2) is t(apex) = 0.6 inch instead of t(apex) = 0.4 inch, as is the case in Table 78. This output is an abridged and edited version of the output file from GENOPT called "eqellipse.OPM", where "eqellipse" is the user-selected name of the specific case. The critical margins are in bold face.

```
STRUCTURAL ANALYSIS WITH UNPERTURBED DECISION VARIABLES
VAR.
     CURRENT
                       DEFINITION
NO.
       VALUE
  1
     6.0000E-01
                 skin thickness at xinput: THKSKN(1)
                 skin thickness at xinput: THKSKN(2)
  2
     6.0000E-01
                 skin thickness at xinput: THKSKN(3)
  3
     6.0418E-01
  4
     3.1405E-01
                 skin thickness at xinput: THKSKN(4)
  5
     3.6261E-01
                 skin thickness at xinput: THKSKN(5)
  6
     3.6471E-01
                 skin thickness at xinput: THKSKN(6)
  7
     3.0622E-01
                 skin thickness at xinput: THKSKN(7)
  8
     3.1319E-01
                 skin thickness at xinput: THKSKN(8)
  9
     2.8240E-01
                 skin thickness at xinput: THKSKN(9)
                 skin thickness at xinput: THKSKN(10)
 10
     2.4984E-01
    2.0428E-01
                 skin thickness at xinput: THKSKN(11)
 11
                 skin thickness at xinput: THKSKN(12)
 12
     1.7857E-01
     2.4628E-01
 13
                 skin thickness at xinput: THKSKN(13)
 14
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(1)
 15
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(2)
                 height of isogrid members at xinput: HIGHST(3)
 16
     1.0000E-06
 17
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(4)
                 height of isogrid members at xinput: HIGHST(5)
 18
     1.0000E-06
 19
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(6)
                 height of isogrid members at xinput: HIGHST(7)
 20
     1.0000E-06
 21
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(8)
                 height of isogrid members at xinput: HIGHST(9)
 2.2
     1.0000E-06
 23
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(10)
                 height of isogrid members at xinput: HIGHST(11)
 2.4
     1.0000E-06
 25
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(12)
 26
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(13)
 27
     3.0000E+00
                 spacing of the isogrid members: SPACNG
                thickness of an isogrid stiffening member: THSTIF
 28
     1.0000E-05
```

```
CURRENT VALUE OF THE OBJECTIVE FUNCTION:
VAR.
       CURRENT
NO.
        VALUE
                         DEFINITION
 1
      1.289E+02
                 weight of the equivalent ellipsoidal head: WEIGHT
              (Compare with WEIGHT = 127.1 lb in Table 78)
***** RESULTS FOR LOAD SET NO.
                                1 (+mode 1 and +mode 2) *****
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
MARGIN CURRENT
NO.
        VALUE
                         DEFINITION
 1
     -1.310E-01 (CLAPS1(1 )/CLAPS1A(1 )) / CLAPS1F(1 )-1; F.S.=1.00
 2
     -1.928E-02 (GENBK1(1 )/GENBK1A(1 )) / GENBK1F(1 )-1; F.S.=1.00
 3
      3.344E+01 (SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1;F.S.=1.00
 4
      2.205E+01 (SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1;F.S.=1.00
 5
      1.087E+04 (STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1;F.S.=1.00
 6
      6.322E+03 (STFBK1(1,2)/STFBK1A(1,2))/STFBK1F(1,2)-1;F.S.=1.00
 7
     -2.456E-01 (SKNST1A(1,1)/SKNST1(1,1))/SKNST1F(1,1)-1;F.S.=1.00
     -4.762E-01 (SKNST1A(1,2)/SKNST1(1,2))/SKNST1F(1,2)-1;F.S.=1.00
 8
 9
      2.373E-02 (STFST1A(1,1)/STFST1(1,1))/STFST1F(1,1)-1;F.S.=1.00
     -4.048E-01 (STFST1A(1,2)/STFST1(1,2))/STFST1F(1,2)-1;F.S.=1.00
10
11
      5.572E-01 (WAPEX1A(1 )/WAPEX1(1 )) / WAPEX1F(1 )-1; F.S.=1.00
12
     -8.753E-02 (CLAPS2(1 )/CLAPS2A(1 )) / CLAPS2F(1 )-1; F.S.=1.00
     -1.560E-01 (GENBK2(1 )/GENBK2A(1 )) / GENBK2F(1 )-1; F.S.=1.00
13
14
      3.763E+01 (SKNBK2(1,1)/SKNBK2A(1,1))/SKNBK2F(1,1)-1;F.S.=1.00
15
      2.127E+01 (SKNBK2(1,2)/SKNBK2A(1,2))/SKNBK2F(1,2)-1;F.S.=1.00
16
      2.808E+04 (STFBK2(1,1)/STFBK2A(1,1))/STFBK2F(1,1)-1;F.S.=1.00
17
      8.418E+03 (STFBK2(1,2)/STFBK2A(1,2))/STFBK2F(1,2)-1;F.S.=1.00
18
     -7.025E-02 (SKNST2A(1,1)/SKNST2(1,1))/SKNST2F(1,1)-1;F.S.=1.00
19
     -2.398E-01 (SKNST2A(1,2)/SKNST2(1,2))/SKNST2F(1,2)-1;F.S.=1.00
20
      5.055E-01 (STFST2A(1,1)/STFST2(1,1))/STFST2F(1,1)-1;F.S.=1.00
21
     -2.075E-01 (STFST2A(1,2)/STFST2(1,2))/STFST2F(1,2)-1;F.S.=1.00
22
      9.693E-01 (WAPEX2A(1 )/WAPEX2(1 )) / WAPEX2F(1 )-1; F.S.=1.00
***** RESULTS FOR LOAD SET NO.
                                2 (-mode 1 and -mode 2) *****
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
MARGIN CURRENT
NO.
        VALUE
                         DEFINITION
 1
      2.462E-01 (CLAPS1(2 )/CLAPS1A(2 )) / CLAPS1F(2 )-1; F.S.=1.00
      2.182E-01 (GENBK1(2 )/GENBK1A(2 )) / GENBK1F(2 )-1; F.S.=1.00
 2
 3
      6.408E+01 (SKNBK1(2,1)/SKNBK1A(2,1))/SKNBK1F(2,1)-1;F.S.=1.00
 4
      2.061E+01 (SKNBK1(2,2)/SKNBK1A(2,2))/SKNBK1F(2,2)-1;F.S.=1.00
 5
      2.835E+04 (STFBK1(2,1)/STFBK1A(2,1))/STFBK1F(2,1)-1;F.S.=1.00
 6
      7.589E+03 (STFBK1(2,2)/STFBK1A(2,2))/STFBK1F(2,2)-1;F.S.=1.00
 7
      8.319E-01 (SKNST1A(2,1)/SKNST1(2,1))/SKNST1F(2,1)-1;F.S.=1.00
 8
     -4.132E-01 (SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1;F.S.=1.00
```

************ DESIGN OBJECTIVE ************

```
9
      1.669E+00 (STFST1A(2,1)/STFST1(2,1))/STFST1F(2,1)-1;F.S.=1.00
10
     -2.855E-01 (STFST1A(2,2)/STFST1(2,2))/STFST1F(2,2)-1;F.S.=1.00
11
      1.227E+00 (WAPEX1A(2 )/WAPEX1(2 )) / WAPEX1F(2 )-1; F.S.=1.00
12
     -7.665E-02 (CLAPS2(2 )/CLAPS2A(2 )) / CLAPS2F(2 )-1; F.S.=1.00
13
      1.543E-01 (GENBK2(2 )/GENBK2A(2 )) / GENBK2F(2 )-1; F.S.=1.00
14
      4.927E+01 (SKNBK2(2,1)/SKNBK2A(2,1))/SKNBK2F(2,1)-1;F.S.=1.00
15
      2.193E+01 (SKNBK2(2,2)/SKNBK2A(2,2))/SKNBK2F(2,2)-1;F.S.=1.00
      9.984E+03 (STFBK2(2,1)/STFBK2A(2,1))/STFBK2F(2,1)-1;F.S.=1.00
16
      1.113E+04 (STFBK2(2,2)/STFBK2A(2,2))/STFBK2F(2,2)-1;F.S.=1.00
17
     -2.740E-01 (SKNST2A(2,1)/SKNST2(2,1))/SKNST2F(2,1)-1;F.S.=1.00
18
     -9.780E-02 (SKNST2A(2,2)/SKNST2(2,2))/SKNST2F(2,2)-1;F.S.=1.00
19
20
     -6.002E-02 (STFST2A(2,1)/STFST2(2,1))/STFST2F(2,1)-1;F.S.=1.00
21
      4.794E-02 (STFST2A(2,2)/STFST2(2,2))/STFST2F(2,2)-1; F.S.=1.00
      5.927E-01 (WAPEX2A(2 )/WAPEX2(2 )) / WAPEX2F(2 )-1; F.S.=1.00
22
______
```

NOTE: The design margins listed above are divided into two groups of 11 margins each: Margins 1-11 and Margins 12-22. The first group of 11 margins are obtained with use of the axisymmetric mode 1 imperfection, and the second group of 11 margins are obtained with use of the axisymmetric mode 2 imperfection.