Table 70 Optimized "perfect" isogrid-stiffened equivalent elliposidal shell. Design margins from Load Set 1 (+mode 1 and +mode 2 imperfection shapes) corresponding to the design optimized with the use of only mode 1 and mode 2 imperfection shapes. These margins are developed via the seven analyses of the type listed in Table 30. Wimp = 0.0001 inch.

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A typical margin with the meanings of the indices, a, b, c, d, e,
explained:
                                а
   3.895E-03
             (STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1; F.S.= 1.00
                   c d e
                               c de
                                             c de
        "STFBK" means "Stiffener buckling"
   a = "A" means "Allowable value"
   b = "F" means "Factor of safety"
   c = Imperfection mode number, (1 or 2 in the cases explored here)
   d = Load set number (1 or 2 in the cases explored here)
        Load set 1 means "use +mode 1 and +mode 2 imperfection shapes"
        Load set 2 means "use -mode 1 and -mode 2 imperfection shapes"
   e = Region number:
          (1 or 2 Region 1 is from the axis of revolution to xlimit,
                          that is, 0 < x < x  xlimit.
                 Region 2 is from xlimit to the equator,
                          that is, x = x < x < x < x.
*** RESULTS FOR LOAD SET NO. 1 (+mode 1 and +mode 2 imperfections) ***
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
MARGIN CURRENT
NO.
       VALUE
                        DEFINITION
     -5.564E-03
 1
                (CLAPS1(1 )/CLAPS1A(1 )) / CLAPS1F(1 )-1; F.S.=
 2
                (GENBK1(1 )/GENBK1A(1 )) / GENBK1F(1 )-1; F.S.=
     2.324E-01
                (SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1; F.S.= 1.00
 3
     1.510E+00
                (SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1; F.S.= 1.00
 4
     1.726E+00
                (STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1; F.S.= 1.00
 5
     3.895E-03
                (STFBK1(1,2)/STFBK1A(1,2))/STFBK1F(1,2)-1; F.S.= 1.00
 6
     4.329E-01
 7
                (SKNST1A(1,1)/SKNST1(1,1))/SKNST1F(1,1)-1; F.S.= 1.00
     1.821E-01
                (SKNST1A(1,2)/SKNST1(1,2))/SKNST1F(1,2)-1; F.S.= 1.00
 8
     -1.323E-02
 9
     5.500E-03
                (STFST1A(1,1)/STFST1(1,1))/STFST1F(1,1)-1; F.S.= 1.00
                (STFST1A(1,2)/STFST1(1,2))/STFST1F(1,2)-1; F.S.= 1.00
10
     -2.193E-02
      6.640E-01
                (WAPEX1A(1 )/WAPEX1(1 )) / WAPEX1F(1 )-1; F.S.= 1.00
11
12
                (CLAPS2(1 )/CLAPS2A(1 )) / CLAPS2F(1 )-1; F.S.=
     -5.564E-03
13
      2.326E-01
                (GENBK2(1)/GENBK2A(1)) / GENBK2F(1)-1; F.S.=
                (SKNBK2(1,1)/SKNBK2A(1,1))/SKNBK2F(1,1)-1; F.S.= 1.00
14
     1.510E+00
                (SKNBK2(1,2)/SKNBK2A(1,2))/SKNBK2F(1,2)-1; F.S.= 1.00
15
     1.726E+00
                (STFBK2(1,1)/STFBK2A(1,1))/STFBK2F(1,1)-1; F.S.= 1.00
16
     4.598E-04
                (STFBK2(1,2)/STFBK2A(1,2))/STFBK2F(1,2)-1; F.S.= 1.00
17
     4.367E-01
18
     1.824E-01
                (SKNST2A(1,1)/SKNST2(1,1))/SKNST2F(1,1)-1; F.S.= 1.00
                (SKNST2A(1,2)/SKNST2(1,2))/SKNST2F(1,2)-1; F.S.= 1.00
19
     -1.567E-02
20
      2.061E-03
                (STFST2A(1,1)/STFST2(1,1))/STFST2F(1,1)-1; F.S.= 1.00
```

(STFST2A(1,2)/STFST2(1,2))/STFST2F(1,2)-1; F.S.= 1.00

(WAPEX2A(1)/WAPEX2(1)) / WAPEX2F(1)-1; F.S.=

21

22

-2.219E-02

6.645E-01