Table 75 Optimized "**perfect**" **unstiffened** equivalent elliposidal shell. Design margins from Load Set 1 (+mode 1 and +mode 2 imperfection shapes) corresponding to the design optimized with the use of only mode 1 and mode 2 imperfection shapes. These margins are developed via the seven analyses of the type listed in Table 30. Wimp = 0.0001 inch.

A typical margin with the meanings of the indices, a, b, c, d, e, explained:

```
                                    a            b
4  1.752E-01  (SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1; F.S.= 1.00
                    c d e       c  d e        c  d e
```

"SKNBK" means "local skin buckling"
a = "A" means "Allowable value"
b = "F" means "Factor of safety"
c = Imperfection mode number, (1 or 2 in the cases explored here)
d = Load set number (1 or 2 in the cases explored here)
Load set 1 means "use +mode 1 and +mode 2 imperfection shapes"
Load set 2 means "use -mode 1 and -mode 2 imperfection shapes"
e = Region number:
(1 or 2 Region 1 is from the axis of revolution to xlimit, that is, 0 < x < xlimit.
Region 2 is from xlimit to the equator, that is, xlimit < x < semi-major axis.)

*** RESULTS FOR LOAD SET NO. 1 (+mode 1 and +mode 2 imperfections) ***
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S.= FACTOR OF SAFETY)

MARGIN NO.	CURRENT VALUE	DEFINITION
1	**-4.320E-02**	**(CLAPS1(1)/CLAPS1A(1)) / CLAPS1F(1)-1; F.S.= 1.00**
2	**-4.354E-02**	**(GENBK1(1)/GENBK1A(1)) / GENBK1F(1)-1; F.S.= 1.00**
3	1.103E+00	(SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1; F.S.= 1.00
4	**1.752E-01**	**(SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1; F.S.= 1.00**
5	2.131E+04	(STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1; F.S.= 1.00
6	1.623E+04	(STFBK1(1,2)/STFBK1A(1,2))/STFBK1F(1,2)-1; F.S.= 1.00
7	2.410E-01	(SKNST1A(1,1)/SKNST1(1,1))/SKNST1F(1,1)-1; F.S.= 1.00
8	**1.357E-02**	**(SKNST1A(1,2)/SKNST1(1,2))/SKNST1F(1,2)-1; F.S.= 1.00**
9	1.006E+00	(STFST1A(1,1)/STFST1(1,1))/STFST1F(1,1)-1; F.S.= 1.00
10	5.281E-01	(STFST1A(1,2)/STFST1(1,2))/STFST1F(1,2)-1; F.S.= 1.00
11	1.739E+00	(WAPEX1A(1)/WAPEX1(1)) / WAPEX1F(1)-1; F.S.= 1.00
12	**-4.236E-02**	**(CLAPS2(1)/CLAPS2A(1)) / CLAPS2F(1)-1; F.S.= 1.00**
13	**-4.107E-02**	**(GENBK2(1)/GENBK2A(1)) / GENBK2F(1)-1; F.S.= 1.00**
14	1.103E+00	(SKNBK2(1,1)/SKNBK2A(1,1))/SKNBK2F(1,1)-1; F.S.= 1.00
15	**1.752E-01**	**(SKNBK2(1,2)/SKNBK2A(1,2))/SKNBK2F(1,2)-1; F.S.= 1.00**
16	2.133E+04	(STFBK2(1,1)/STFBK2A(1,1))/STFBK2F(1,1)-1; F.S.= 1.00
17	1.627E+04	(STFBK2(1,2)/STFBK2A(1,2))/STFBK2F(1,2)-1; F.S.= 1.00
18	2.463E-01	(SKNST2A(1,1)/SKNST2(1,1))/SKNST2F(1,1)-1; F.S.= 1.00
19	**1.134E-02**	**(SKNST2A(1,2)/SKNST2(1,2))/SKNST2F(1,2)-1; F.S.= 1.00**
20	1.008E+00	(STFST2A(1,1)/STFST2(1,1))/STFST2F(1,1)-1; F.S.= 1.00
21	5.314E-01	(STFST2A(1,2)/STFST2(1,2))/STFST2F(1,2)-1; F.S.= 1.00
22	1.736E+00	(WAPEX2A(1)/WAPEX2(1)) / WAPEX2F(1)-1; F.S.= 1.00