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Table 59a Optimized imperfect unstiffened equivalent elliposidal shell.
Design margins from Load Set 1 (+mode 1 and +mode 2 imperfection
shapes) corresponding to the design optimized with the use of only
mode 1 and mode 2 imperfection shapes. These margins are developed via
the same seven analyses of the type listed in Table 30 (which gives
results for the optimized isogrid-stiffened equivalent ellipsoidal shell)
A typical margin with the meanings of the indices, a, b, c, d, e,
 explained:
              (SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1; F.S.= 1.00
 3
    4.881E-01
                    c d e
                                c de
                                             c de
         "SKNBK" means "Local skin buckling"
    a = "A" means "Allowable value"
    b = "F" means "Factor of safety"
    c = Imperfection mode number, (1 or 2 in the cases explored here)
    d = Load set number (1 or 2 in the cases explored here)
         Load set 1 means "use +mode 1 and +mode 2 imperfection shapes"
         Load set 2 means "use -mode 1 and -mode 2 imperfection shapes"
    e = Region number:
          (1 or 2 Region 1 is from the axis of revolution to xlimit,
                           that is, 0 < x < x  xlimit.
                  Region 2 is from xlimit to the equator,
                           *** RESULTS FOR LOAD SET NO. 1 (+mode 1 and +mode 2 imperfections) ***
 MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
 MARGIN CURRENT
                         DEFINITION
 NO.
        VALUE
     -2.647E-02
  1
                  (CLAPS1(1 )/CLAPS1A(1 )) / CLAPS1F(1 )-1; F.S.=
  2
                  (GENBK1(1 )/GENBK1A(1 )) / GENBK1F(1 )-1; F.S.=
       2.456E-01
       4.881E-01
                 (SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1; F.S.= 1.00
  3
                  (SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1; F.S.= 1.00
  4
       3.092E-01
                  (STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1; F.S.= 1.00
  5
      1.795E+04
                  (STFBK1(1,2)/STFBK1A(1,2))/STFBK1F(1,2)-1; F.S.= 1.00
  6
       1.375E+04
  7
                  (SKNST1A(1,1)/SKNST1(1,1))/SKNST1F(1,1)-1; F.S.= 1.00
       4.169E-01
                  (SKNST1A(1,2)/SKNST1(1,2))/SKNST1F(1,2)-1; F.S.= 1.00
      2.184E-02
  8
  9
       6.903E-01
                 (STFST1A(1,1)/STFST1(1,1))/STFST1F(1,1)-1; F.S.= 1.00
                  (STFST1A(1,2)/STFST1(1,2))/STFST1F(1,2)-1; F.S.= 1.00
       2.948E-01
 10
 11
       1.593E+00
                 (WAPEX1A(1 )/WAPEX1(1 )) / WAPEX1F(1 )-1; F.S.=
 12
                 (CLAPS2(1 )/CLAPS2A(1 )) / CLAPS2F(1 )-1; F.S.=
      -1.309E-02
                 (GENBK2(1 )/GENBK2A(1 )) / GENBK2F(1 )-1; F.S.=
 13
       2.437E-01
                 (SKNBK2(1,1)/SKNBK2A(1,1))/SKNBK2F(1,1)-1; F.S.= 1.00
 14
       3.233E-01
                  (SKNBK2(1,2)/SKNBK2A(1,2))/SKNBK2F(1,2)-1; F.S.= 1.00
 15
       2.996E-01
                  (STFBK2(1,1)/STFBK2A(1,1))/STFBK2F(1,1)-1; F.S.= 1.00
 16
       2.713E+04
 17
                  (STFBK2(1,2)/STFBK2A(1,2))/STFBK2F(1,2)-1; F.S.= 1.00
       1.397E+04
 18
       3.307E-02
                  (SKNST2A(1,1)/SKNST2(1,1))/SKNST2F(1,1)-1; F.S.= 1.00
                  (SKNST2A(1,2)/SKNST2(1,2))/SKNST2F(1,2)-1; F.S.= 1.00
 19
      -2.605E-02
                  (STFST2A(1,1)/STFST2(1,1))/STFST2F(1,1)-1; F.S.= 1.00
 20
       1.540E+00
 21
       3.152E-01
                  (STFST2A(1,2)/STFST2(1,2))/STFST2F(1,2)-1; F.S.= 1.00
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(WAPEX2A(1)/WAPEX2(1)) / WAPEX2F(1)-1; F.S.=

22

1.316E+00