Table 1 Glossary of variables used in the generic case, "span9" (This is part of the span9.DEF file, created automatically by the GENOPT processor, GENTEXT, with use of information, variable names and one-line definitions provided by the GENOPT user.)

C C	ARRAY ?	NUMBER (ROWS,C	OF OLS)	•	PROMPT NUMBER span9.PR	•	==	DEFINITION OF VARIABLE
	======				1.0		==	
C	n	(0,	0)	2	10	WIDTH		total width of the corrugated panel
C	n	(0,	0)	2	15	LENGTH		axial length of the corrugated panel
C	n	(0,	0)	2	25	FACLEN		fraction of LENGTH for local buckling model
C	n	(0,	0)	2	30	NSEG		number of major segments in WIDTH/2
C	n	(0,	0)	2	40	EMOD		elastic modulus of the material
C	n	(0,	0)	2	45	NU		Poisson ratio of the panel material
C	n	(0,	0)	2	50	DENSTY		weight density of the panel material
C	n	(0,	0)	2	60	MLOWGS		low end of M-range: symmetric GENERAL buckling
C	n	(0,	0)	2	65	MHIGHGS		high end of M-range: symmetric GENERAL buckling
C	n	(0,	0)	2	70	MLOWGA		low end of M-range: antisymmetric GENERAL buckling
C	n	(0,	0)	2	75	MHIGHGA		high end of M-range: antisymmetric GENERAL buckling
C	n	(0,	0)	2	80	MLOWL		low end of the M-range: LOCAL buckling
C	n	(0,	0)	2	85	MHIGHL		high end of the M-range: LOCAL buckling
C	n	(0,	0)	2	95	IELMNT		finite element used in STAGS model
С	n	(0,	0)	2	105	INSUBSE		major segment number in NSUBSEG(INSUBSE)
C	У	(19,	0)	2	110	NSUBSEG		number of sub-segments in major segment
С	У	(19,	0)	2	120	UPDOWN		1 = convex surface up; 2 = convex down
С	n	(0,	0)	2	130	JUPDWNS		major segment number in UPDWNS(IUPDWNS, JUPDWNS)
С	n	(0,	0)	2	135	IUPDWNS		sub-segment number in UPDWNS(IUPDWNS, JUPDWNS)
С	У	(50,	19)	2	140	UPDWNS		1=convex up; 2=convex down (subsegments)
С	n	(0,	0)	2	150	UPDNBIG		1=convex up (hill); 2=convex down (valley)
C	n	(0,	0)	2	160	ITHICK		major segment number in THICK(ITHICK)
С	У	(19,	0)	1	165	THICK		wall thickness of the major segment
С	У	(19,	0)	1	170	SUBWID		projected width (x-width) of major segment
С	У	(19,	0)	1	175	PHISEG		half-angle (deg.) of major corrugation
С	У	(19,	0)	1	180	PHISUB		half-angle (deg.) of sub-corrugation
С	n	(0,	0)	2	190	IYPLATE		vertical displacement number in YPLATE(IYPLATE)
С	У	(20,	0)	1	195	YPLATE		vertical y above (x,y,z) origin if PHIBIG=0
С	n	(0,	0)	1	200	PHIBIG		half-angle (deg.) of overall arching
С	n	(0,	0)	2	210	NCASES	=	Number of load cases (number of environments) in
TOTLOD(NCASES)								
С	У	(20,	0)	3	215	TOTLOD		total axial load (e.g. lb) over WIDTH
С	У	(20,	0)	4	225	LOCBUK		local buckling load factor
С	У	(20,	0)	5	235	LOCBUKA		allowable for local buckling
С	У	(20,	0)	6	240	LOCBUKF		factor of safety for local buckling
С	У	(20,	0)	4	245	BUKSYM		symmetric general buckling
С	У	(20,	0)	5	250	BUKSYMA		allowable for sym. general buckling
С	У	(20,	0)	6	255	BUKSYMF		f.s. for symmetric general buckling
С	У	(20,	0)	4	260	BUKASY		antisymmetric general buckling
С	У	(20,	0)	5	265	BUKASYA	=	allowable for antisym. general buckling
С	У	(20,	0)	6	270	BUKASYF	=	f.s. for antisym. general buckling
С	n	(0,	0)	2	280	JCYLBUK		segment number in CYLBUK(NCASES,JCYLBUK)
С	У	(20,	19)	4	285	CYLBUK		classical buckling load factor
С	У	(20,	19)	5	290	CYLBUKA	=	allowable for classical buckling
С	У	(20,	19)	6	295	CYLBUKF	=	factor of safety for classical buckling
С	У	(20,	0)	4	300	STRESS	=	maximum effective stress
С	У	(20,	0)	5	305	STRESSA	=	allowable effective stress
С	У	(20,	0)	6	310	STRESSF		factor of safety for stress
C ==	n	(0,	0)	7	315	WEIGHT		weight of the corrugated panel

Table 2 Input data for the GENOPT processor, BEGIN (the file called fold98updown.BEG). These input data are provided by the End user for the specific case called "fold98updown". (See Fig. 3, middle frame.)

```
Do you want a tutorial session and tutorial output?
 100.0000
              $ total width of the corrugated plate: WIDTH
              $ axial length of the corrugated plate: LENGTH
 100.0000
0.300000
              $ fraction of LENGTH for local buckling model: FACLEN
              $ number of major segments in WIDTH/2: NSEG
0.1000000E+08 $ elastic modulus of the material: EMOD
0.3000000
              $ Poisson ratio of the plate material: NU
0.1000000
              $ weight density of the plate material: DENSTY
              $ low end of M-range: symmetric GENERAL buckling: MLOWGS
       1
              $ high end of M-range: symmetric GENERAL buckling: MHIGHGS
       1
              $ low end of M-range: antisymmetric GENERAL buckling: MLOWGA
              $ high end of M-range: antisymmetric GENERAL buckling: MHIGHGA
       5
              $ low end of the M-range: LOCAL buckling: MLOWL
       1
              $ high end of the M-range: LOCAL buckling: MHIGHL
      30
     480
              $ finite element used in STAGS model: IELMNT
       8
              $ Number INSUBSE of rows in the array NSUBSEG: INSUBSE
              $ number of sub-segments in major segment: NSUBSEG(
       0
               number of sub-segments in major segment: NSUBSEG(
       0
                                                                    2)
       0
              $ number of sub-segments in major segment: NSUBSEG(
                                                                    3)
       0
              $ number of sub-segments in major segment: NSUBSEG(
                                                                    4)
               number of sub-segments in major segment: NSUBSEG(
       0
                                                                    5)
       0
              $ number of sub-segments in major segment: NSUBSEG(
                                                                    6)
              $ number of sub-segments in major segment: NSUBSEG(
       0
       0
              $ number of sub-segments in major segment: NSUBSEG(
                                                                    8)
       1
              $ 1 = convex surface up; 2 = convex down: UPDOWN(
                                                                  1)
       2
              $ 1 = convex surface up; 2 = convex down: UPDOWN(
       1
              $ 1 = convex surface up; 2 = convex down: UPDOWN(
       2
               1 = convex surface up; 2 = convex down: UPDOWN(
       1
              $ 1 = convex surface up; 2 = convex down: UPDOWN(
              $ 1 = convex surface up; 2 = convex down: UPDOWN(
                1 = convex surface up; 2 = convex down: UPDOWN(
       1
       2
              $ 1 = convex surface up; 2 = convex down: UPDOWN(
              $ Number JUPDWNS of columns in the array, UPDWNS: JUPDWNS
       1
              $ 1=convex up (hill); 2=convex down (valley): UPDNBIG
               Number ITHICK of rows in the array
                                                      THICK: ITHICK
0.1000000
              $ wall thickness of the major segment: THICK(
0.1000000
              $ wall thickness of the major segment: THICK(
                                                              2)
0.1000000
                wall thickness of the major segment: THICK(
0.1000000
              $ wall thickness of the major segment: THICK(
                                                              4)
0.1000000
              $ wall thickness of the major segment: THICK(
                                                              5)
                wall thickness of the major segment: THICK(
0.1000000
0.1000000
              $ wall thickness of the major segment: THICK(
              $ wall thickness of the major segment: THICK(
0.1000000
              $ projected width (x-width) of sub-plate: SUBWID(
6.250000
                                                                  1)
6.250000
              $ projected width (x-width) of sub-plate: SUBWID(
              $ projected width (x-width) of sub-plate: SUBWID(
 6.250000
```

```
6.250000
              $ projected width (x-width) of sub-plate: SUBWID(
                                                                   4)
              $ projected width (x-width) of sub-plate: SUBWID(
6.250000
                                                                   5)
              $ projected width (x-width) of sub-plate: SUBWID(
6.250000
                                                                   6)
6.250000
              $ projected width (x-width) of sub-plate: SUBWID(
                                                                   7)
                projected width (x-width) of sub-plate: SUBWID(
6.250000
60.00000
              $ half-angle (deg.) of major corrugation: PHISEG(
                                                                   1)
              $ half-angle (deg.) of major corrugation: PHISEG(
60,00000
                                                                   2)
                half-angle (deg.) of major corrugation: PHISEG(
60.00000
                                                                   3)
 60.00000
              $ half-angle (deg.) of major corrugation: PHISEG(
                                                                   4)
 60.00000
              $ half-angle (deg.) of major corrugation: PHISEG(
                                                                   5)
              $ half-angle (deg.) of major corrugation: PHISEG(
60.00000
                                                                   6)
 60.00000
               half-angle (deg.) of major corrugation: PHISEG(
                                                                   7)
 30.00000
              $ half-angle (deg.) of major corrugation: PHISEG(
                                                                   8)
70.00000
              $ half-angle (deg.) of sub-corrugation: PHISUB(
                                                                 1)
70.00000
              $ half-angle (deg.) of sub-corrugation: PHISUB(
                                                                 2)
              $ half-angle (deg.) of sub-corrugation: PHISUB(
70.00000
                                                                 3)
 70.00000
              $ half-angle (deg.) of sub-corrugation: PHISUB(
                                                                 4)
70.00000
               half-angle (deg.) of sub-corrugation: PHISUB(
                                                                 5)
 70.00000
              $ half-angle (deg.) of sub-corrugation: PHISUB(
 70.00000
              $ half-angle (deg.) of sub-corrugation: PHISUB(
                                                                 7)
               half-angle (deg.) of sub-corrugation: PHISUB(
 70.00000
                Number IYPLATE of rows in the array YPLATE: IYPLATE
30.00000
              $ vertical distance above (x,y,z) origin: YPLATE(
30.00000
              $ vertical distance above (x,y,z) origin: YPLATE(
                                                                   2)
30.00000
              $ vertical distance above (x,y,z) origin: YPLATE(
                                                                   3)
 30.00000
              $ vertical distance above (x,y,z) origin: YPLATE(
                                                                   4)
              $ vertical distance above (x,y,z) origin: YPLATE(
30.00000
                                                                   5)
              $ vertical distance above (x,y,z) origin: YPLATE(
30.00000
                                                                   6)
 30.00000
              $ vertical distance above (x,y,z) origin: YPLATE(
                                                                   7)
 30.00000
              $ vertical distance above (x,y,z) origin: YPLATE(
                                                                   8)
28.33333
              $ vertical distance above (x,y,z) origin: YPLATE(
                                                                   9)
 10.00000
              $ half-angle (deg.) of overall arching: PHIBIG
              $ Number NCASES of load cases (environments): NCASES
-200000.0
              $ total axial load (e.g. lb): TOTLOD(
 1.000000
              $ allowable for local buckling: LOCBUKA(
              $ factor of safety for local buckling: LOCBUKF(
2.000000
                                                                 1)
              $ allowable for sym. general buckling: BUKSYMA(
 1.000000
                                                                 1)
              $ f.s. for symmetric general buckling: BUKSYMF(
 1.500000
 1.000000
              $ allowable for antisym. general buckling: BUKASYA(
              $ f.s. for antisym. general buckling: BUKASYF(
1.500000
              $ Number JCYLBUK of columns in the array, CYLBUK: JCYLBUK
1.000000
               allowable for classical buckling: CYLBUKA(
                                                                  1)
               allowable for classical buckling: CYLBUKA(
 1.000000
 1.000000
              $ allowable for classical buckling: CYLBUKA(
                                                                  3)
                allowable for classical buckling: CYLBUKA(
 1.000000
                                                                  4)
              $ allowable for classical buckling: CYLBUKA(
1.000000
                                                                  5)
1.000000
               allowable for classical buckling: CYLBUKA(
                                                              1,
                                                                  6)
                allowable for classical buckling: CYLBUKA(
                                                                  7)
1.000000
1.000000
              $ allowable for classical buckling: CYLBUKA(
 1.000000
              $ factor of safety for classical buckling: CYLBUKF(
                                                                         1)
              $ factor of safety for classical buckling: CYLBUKF(
 1.000000
                                                                         2)
 1.000000
              $ factor of safety for classical buckling: CYLBUKF(
                                                                         3)
              $ factor of safety for classical buckling: CYLBUKF(
 1.000000
```

```
1.000000 $ factor of safety for classical buckling: CYLBUKF( 1, 5)
1.000000 $ factor of safety for classical buckling: CYLBUKF( 1, 6)
1.000000 $ factor of safety for classical buckling: CYLBUKF( 1, 7)
1.000000 $ factor of safety for classical buckling: CYLBUKF( 1, 8)
100000.0 $ allowable effective stress: STRESSA( 1)
1.500000 $ factor of safety for stress: STRESSF( 1)
```

Table 3 Optimized design of the specific case called "fold98updown" (with "corners" between adjacent segments, that is, no "smoothing" as described in Section 14). This optimized design was obtained with the use of the "OLD" boundary conditions: u, v, w held and rotation free along the left-hand longitudinal edge and symmetry or anti-symmetry along the right-hand longitudinal edge. (See Section 4, Fig. 2 and Figs. 6-8.) The thicknesses, THICK(i), i=1,2,...8, are the same for all eight major segments because THICK(j), j=2,3,...8 are all linked to THICK(1). This linking of thicknesses is used for all of the cases explored in this paper: all the panels are of uniform thickness.

```
VALUES OF DESIGN VARIABLES CORRESPONDING TO BEST FEASIBLE DESIGN
VAR.
       CURRENT
NO.
                          DEFINITION
        VALUE
       6.918E-02
                  wall thickness of the major segment: THICK(1)
  1
  2
                  wall thickness of the major segment: THICK(2)
       6.918E-02
                  wall thickness of the major segment: THICK(3)
  3
       6.918E-02
  4
       6.918E-02
                  wall thickness of the major segment: THICK(4)
                  wall thickness of the major segment: THICK(5)
  5
       6.918E-02
  6
       6.918E-02
                  wall thickness of the major segment: THICK(6)
  7
       6.918E-02
                  wall thickness of the major segment: THICK(7
  8
       6.918E-02
                  wall thickness of the major segment: THICK(8)
                  projected width (x-width) of major segment: SUBWID(1)
  9
       1.118E+01
 10
       4.790E+00
                  projected width (x-width) of major segment: SUBWID(2)
 11
       7.133E+00
                  projected width (x-width) of major segment: SUBWID(3
12
       3.683E+00
                  projected width (x-width) of major segment: SUBWID(4
13
       7.242E+00
                  projected width (x-width) of major segment: SUBWID(5
 14
       9.932E+00
                  projected width (x-width) of major segment: SUBWID(6)
15
       2.809E+00
                  projected width (x-width) of major segment: SUBWID(7
       2.716E+00
                  projected width (x-width) of major segment: SUBWID(8)
 16
17
       5.693E+01
                  half-angle (deg.) of major corrugation: PHISEG(1)
                  half-angle (deg.) of major corrugation: PHISEG(2)
18
       6.220E+01
19
       2.826E+01
                  half-angle (deg.) of major corrugation: PHISEG(3)
20
       5.502E+01
                  half-angle (deg.) of major corrugation: PHISEG(4)
21
       4.902E+01
                  half-angle (deg.) of major corrugation: PHISEG(5)
                  half-angle (deg.) of major corrugation: PHISEG(6)
22
       6.522E+01
23
       3.970E+01
                  half-angle (deg.) of major corrugation: PHISEG(7)
24
       2.394E+01
                  half-angle (deg.) of major corrugation: PHISEG(8)
25
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(1)
26
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(2)
27
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(3)
28
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(4)
 29
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(5)
 30
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(6)
```

```
31
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(7)
 32
       7.000E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(8)
 33
       3.000E+01
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(1)
 34
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(2)
       1.312E+01
 35
       1.463E+01
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(3)
 36
       1.046E+01
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(4)
 37
       6.295E+00
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(5)
 38
       9.305E+00
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(6)
 39
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(7)
       5.000E+00
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(8)
 40
       8.789E+00
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(9)
 41
       7.235E+00
                  half-angle (deg.) of overall arching: PHIBIG
 42
       5.807E+01
MARGINS CORRESPONDING TO THE DESIGN (F.S. = FACTOR OF SAFETY)
(critical and nearly critical margins are in bold face.)
MAR.
       CURRENT
NO.
        VALUE
                       DEFINITION
      1.016E-01
                6.05-0.10*V(9)-0.10*V(10)-0.10*V(11)-0.10*V(12)-0.10*V(13)-0
 1
 2
     -1.622E-03
                -3.95+0.10*V(9)+0.10*V(10)+0.10*V(11)+0.10*V(12)+0.10*V(13)+
 3
      1.838E-03
                (LOCBUK(1)/LOCBUKA(1)) / LOCBUKF(1)-1; F.S.= 2.00
 4
     -2.035E-03
                (BUKSYM(1)/BUKSYMA(1)) / BUKSYMF(1)-1; F.S.=
 5
                (BUKASY(1)/BUKASYA(1)) / BUKASYF(1)-1; F.S.= 1.50
     -6.481E-04
                (CYLBUK(1,1)/CYLBUKA(1,1)) / CYLBUKF(1,1)-1; F.S.=
 6
      9.946E-02
                (CYLBUK(1 ,2 )/CYLBUKA(1 ,2 )) / CYLBUKF(1 ,2 )-1; F.S.=
 7
      1.326E+00
                                                                     1.
 8
      7.281E-03
                (CYLBUK(1,3)/CYLBUKA(1,3)) / CYLBUKF(1,3)-1; F.S.=
 9
      2.600E+00
                (CYLBUK(1,4)/CYLBUKA(1,4)) / CYLBUKF(1,4)-1; F.S.=
                                                                     1.
 10
      3.630E-01
                (CYLBUK(1 ,5 )/CYLBUKA(1 ,5 )) / CYLBUKF(1 ,5 )-1; F.S.=
                                                                     1.
                (CYLBUK(1,6)/CYLBUKA(1,6))/CYLBUKF(1,6)-1; F.S.=
 11
      5.077E-01
                                                                     1.
12
      1.476E+00
                (CYLBUK(1 ,7 )/CYLBUKA(1 ,7 )) / CYLBUKF(1 ,7 )-1; F.S.=
                                                                     1.
                (CYLBUK(1 ,8 )/CYLBUKA(1 ,8 )) / CYLBUKF(1 ,8 )-1; F.S.=
 13
      1.500E+00
                (STRESSA(1 )/STRESS(1 )) / STRESSF(1 )-1; F.S.= 1.50
14
      2.090E+00
 ************ DESIGN OBJECTIVE ************
 ******
                                           ******
 CORRESPONDING VALUE OF THE OBJECTIVE FUNCTION:
VAR.
       CURRENT
 NO.
         VALUE
                          DEFINITION
       9.269E+01 weight of the corrugated panel: WEIGHT
 ******
                                        *****
 ************* DESTGN OBJECTIVE ************
 ****************
NOTE on Table 3: The optimized weight of this complexly corrugated panel
```

NOTE on Table 3: The optimized weight of this complexly corrugated panel with NSEG=8 major segments over WIDTH/2 = 50 inches is significantly less than the smallest weight plotted at NSEG=8 in Fig. 43 because the "OLD" boundary conditions along the left-hand longitudinal edge, used for generation of this table, are more restrictive than the "NEW" boundary conditions from which Fig. 43 was generated. (See Section 4 for definition of the "OLD" and "NEW" boundary conditions.)

Table 4 Optimized design of the specific case called "narw96updown" ("narrow" panel) with "corners" between adjacent segments (no smoothing) and factor of safety for local buckling = 1.5. The width, WIDTH, of the panel that is optimized is 50 inches, and there are 6 segments per WIDTH/2 = 25 inches, that is, 12 segments per 50 inches. Compare with Table 5.

VALUES OF DESIGN VARIABLES CORRESPONDING TO BEST FEASIBLE DESIGN

```
VAR.
       CURRENT
NO.
        VALUE
                         DEFINITION
                 wall thickness of the major segment: THICK(1)
 1
      6.016E-02
                 wall thickness of the major segment: THICK(2)
 2
      6.016E-02
 3
                 wall thickness of the major segment: THICK(3)
      6.016E-02
                 wall thickness of the major segment: THICK(4)
 4
      6.016E-02
 5
                 wall thickness of the major segment: THICK(5)
      6.016E-02
                 wall thickness of the major segment: THICK(6)
 6
      6.016E-02
 7
      7.185E+00
                 projected width (x-width) of major segment: SUBWID(1)
                 projected width (x-width) of major segment: SUBWID(2)
 8
      7.484E+00
                 projected width (x-width) of major segment: SUBWID(3)
 9
      1.368E+00
                 projected width (x-width) of major segment: SUBWID(4
10
      1.192E+00
                 projected width (x-width) of major segment: SUBWID(5)
11
      2.138E+00
                 projected width (x-width) of major segment: SUBWID(6)
12
      5.191E+00
                 half-angle (deg.) of major corrugation: PHISEG(1)
13
      5.557E+01
                 half-angle (deg.) of major corrugation: PHISEG(2)
14
      7.596E+01
                 half-angle (deg.) of major corrugation: PHISEG(3)
15
      3.037E+01
                 half-angle (deg.) of major corrugation: PHISEG(4)
16
      1.216E+01
17
      7.712E+01
                 half-angle (deg.) of major corrugation: PHISEG(5)
                 half-angle (deg.) of major corrugation: PHISEG(6)
18
      4.415E+01
                 half-angle (deg.) of sub-corrugation: PHISUB(1)
19
      7.000E+01
                 half-angle (deg.) of sub-corrugation: PHISUB(2)
20
      7.000E+01
                 half-angle (deg.) of sub-corrugation: PHISUB(3)
21
      7.000E+01
                 half-angle (deg.) of sub-corrugation: PHISUB(4)
22
      7.000E+01
2.3
      7.000E+01
                 half-angle (deg.) of sub-corrugation: PHISUB(5)
24
      7.000E+01
                 half-angle (deg.) of sub-corrugation: PHISUB(6)
25
      3.000E+01
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(1)
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(2
2.6
      2.005E+01
27
      9.076E+00
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(3)
2.8
      1.154E+01
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(4
29
      1.104E+01
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(5)
30
      1.015E+01
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(6)
                 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(7)
31
      5.196E+00
32
      8.095E+01
                 half-angle (deg.) of overall arching: PHIBIG
```

MARGINS CORRESPONDING TO THE DESIGN (F.S.= FACTOR OF SAFETY) (critical margins are in bold face.)

```
MAR.
      CURRENT
NO.
       VALUE
                       DEFINITION
               3.55-0.10*V(7)-0.10*V(8)-0.10*V(9)-0.10*V(10)-0.10*V(11)-0.1
 1
     9.421E-02
 2
     5.794E-03
               -1.45+0.10*V(7)+0.10*V(8)+0.10*V(9)+0.10*V(10)+0.10*V(11)+0.
                (LOCBUK(1)/LOCBUKA(1)) / LOCBUKF(1)-1; F.S.=
 3
     8.471E-02
 4
                (BUKSYM(1)/BUKSYMA(1)) / BUKSYMF(1)-1; F.S.=
    -7.064E-03
                (BUKASY(1)/BUKASYA(1)) / BUKASYF(1)-1; F.S.=
 5
    -9.445E-03
                (CYLBUK(1 ,1 )/CYLBUKA(1 ,1 )) / CYLBUKF(1 ,1 )-1; F.S.=
 6
     4.371E-01
                                                                      1.
 7
     4.799E-01
                (CYLBUK(1 ,2 )/CYLBUKA(1 ,2 )) / CYLBUKF(1 ,2 )-1; F.S.=
                                                                      1.
 8
     1.473E+00
                (CYLBUK(1,3)/CYLBUKA(1,3)) / CYLBUKF(1,3)-1; F.S.=
                (CYLBUK(1 ,4 )/CYLBUKA(1 ,4 )) / CYLBUKF(1 ,4 )-1; F.S.=
 9
     1.922E+00
10
     6.479E+00
                (CYLBUK(1 ,5 )/CYLBUKA(1 ,5 )) / CYLBUKF(1 ,5 )-1; F.S.=
                                                                      1.
11
     5.013E-01
                (CYLBUK(1,6)/CYLBUKA(1,6)) / CYLBUKF(1,6)-1; F.S.=
                                                                     1.
12
     2.035E+00
                (STRESSA(1 )/STRESS(1 )) / STRESSF(1 )-1; F.S.= 1.50
************ DESIGN OBJECTIVE ***********
*****
                                            ******
 CORRESPONDING VALUE OF THE OBJECTIVE FUNCTION:
VAR.
       CURRENT
NO.
        VALUE
                          DEFINITION
 1
      4.552E+01 weight of the corrugated panel: WEIGHT
*****
                                        *****
************* DESIGN OBJECTIVE ************
```

NOTE: The objective, 45.52 lb, is the weight of the panel of LENGTH = 100 inches and WIDTH = 50 inches. **The optimized weight, 2 x 45.52 = 91.04 lb, of the corresponding 100 x 100 inch complexly corrugated panel** is slightly smaller than the smallest weight among all of the data points plotted in Fig. 46 (See Table 5.) The weight, 91.04 lb, is about 14 per cent lower than the minimum weight, 106.5 lb, plotted for the optimized uniformly corrugated panel. (See the open square data point in Fig. 46 plotted for the "Number of major segments spanning 50 inches" = 10.)

Table 5 Optimized design of the specific case called "narw96updown" ("narrow" panel) with smoothing between adjacent segments as described in Section 14 and factor of safety for local buckling = 1.5. The width, WIDTH, of the panel that is optimized is 50 inches, and there are 6 segments per WIDTH/2 = 25 inches, that is, 12 segments per 50 inches.

VALUES OF DESIGN VARIABLES CORRESPONDING TO BEST FEASIBLE DESIGN VAR. CURRENT DEFINITION NO. VALUE 1 6.252E-02 wall thickness of the major segment: THICK(1) 2 6.252E-02 wall thickness of the major segment: THICK(2) 3 6.252E-02 wall thickness of the major segment: THICK(3) 6.252E-02 wall thickness of the major segment: THICK(4) 4 5 6.252E-02 wall thickness of the major segment: THICK(5) 6 6.252E-02 wall thickness of the major segment: THICK(6) 7 6.850E+00 projected width (x-width) of major segment: SUBWID(1) projected width (x-width) of major segment: SUBWID(2) 8 7.722E+00 9 1.693E+00 projected width (x-width) of major segment: SUBWID(3) projected width (x-width) of major segment: SUBWID(4) 10 1.434E+00 11 1.478E+00 projected width (x-width) of major segment: SUBWID(5) projected width (x-width) of major segment: SUBWID(6) 12 5.390E+00 half-angle (deg.) of major corrugation: PHISEG(1) 13 6.679E+01 14 7.381E+01 half-angle (deg.) of major corrugation: PHISEG(2) 15 half-angle (deg.) of major corrugation: PHISEG(3) 2.340E+01 1.394E+01 half-angle (deg.) of major corrugation: PHISEG(4) 16 half-angle (deg.) of major corrugation: PHISEG(5) 17 7.042E+01 18 4.489E+01 half-angle (deg.) of major corrugation: PHISEG(6) 19 half-angle (deg.) of sub-corrugation: PHISUB(1) 7.000E+01 20 7.000E+01 half-angle (deg.) of sub-corrugation: PHISUB(2) half-angle (deg.) of sub-corrugation: PHISUB(3) 21 7.000E+01 22 7.000E+01 half-angle (deg.) of sub-corrugation: PHISUB(4) half-angle (deg.) of sub-corrugation: PHISUB(5) 23 7.000E+01 half-angle (deg.) of sub-corrugation: PHISUB(6) 24 7.000E+01 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(1) 25 3.000E+01 1.954E+01 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(2 26 27 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(3 9.471E+00 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(4) 28 1.241E+01 29 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(5) 1.157E+01 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(6) 30 1.115E+01 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(7) 31 5.938E+00 half-angle (deg.) of overall arching: PHIBIG 7.566E+01 32 MARGINS CORRESPONDING TO THE DESIGN (F.S. = FACTOR OF SAFETY) (Critical and near-critical margins are in **bold face.**) MAR. CURRENT

DEFINITION

NO.

VALUE

```
9.332E-02
               3.55-0.10*V(7)-0.10*V(8)-0.10*V(9)-0.10*V(10)-0.10*V(11)-0.1
1
               -1.45+0.10*V(7)+0.10*V(8)+0.10*V(9)+0.10*V(10)+0.10*V(11)+0.
2
     6.678E-03
               (LOCBUK(1)/LOCBUKA(1)) / LOCBUKF(1)-1; F.S.=
3
     1.171E-01
4
    -2.984E-03
               (BUKSYM(1)/BUKSYMA(1)) / BUKSYMF(1)-1; F.S.=
               (BUKASY(1)/BUKASYA(1)) / BUKASYF(1)-1; F.S.=
5
    -7.739E-03
6
     1.162E+00
               (CYLBUK(1 ,1 )/CYLBUKA(1 ,1 )) / CYLBUKF(1 ,1 )-1; F.S.=
                                                                   1.
               (CYLBUK(1 ,2 )/CYLBUKA(1 ,2 )) / CYLBUKF(1 ,2 )-1; F.S.=
7
     6.333E-01
                                                                   1.
               (CYLBUK(1,3)/CYLBUKA(1,3)) / CYLBUKF(1,3)-1; F.S.=
     5.056E-01
8
9
     1.803E+00
               (CYLBUK(1 ,4 )/CYLBUKA(1 ,4 )) / CYLBUKF(1 ,4 )-1; F.S.=
                                                                   1.
10
     9.992E+00
               (CYLBUK(1,5)/CYLBUKA(1,5)) / CYLBUKF(1,5)-1; F.S.=
                                                                   1.
               (CYLBUK(1 ,6 )/CYLBUKA(1 ,6 )) / CYLBUKF(1 ,6 )-1; F.S.=
     5.194E-01
                                                                   1.
11
     2.039E+00
               (STRESSA(1 )/STRESS(1 )) / STRESSF(1 )-1; F.S.= 1.50
12
***************
************** DESIGN OBJECTIVE *************
******
                                          *****
 CORRESPONDING VALUE OF THE OBJECTIVE FUNCTION:
VAR.
       CURRENT
NO.
        VALUE
                         DEFINITION
 1
      4.558E+01 weight of the corrugated panel: WEIGHT
*****
                                       *****
************** DESTGN OBJECTIVE ************
```

NOTE: The objective, 45.58 lb, is the weight of the panel of LENGTH = 100 inches and WIDTH = 50 inches. **The value plotted in Fig. 46 equals 2 x 45.58 = 91.16 lb, corresponding to a panel of width = 100 inches.** (See the solid circular data point in Fig. 46 plotted for the "Number of major segments spanning 50 inches" = 12.) The optimized weight, 91.16 lb, of this 100 x 100 inch complexly corrugated panel is the smallest weight among all of the data points plotted in Fig. 46. The weight, 91.16 lb, is about 14 per cent lower than the minimum weight, 106.5 lb, plotted for the optimized uniformly corrugated panel. (See the open square data point in Fig. 46 plotted for the "Number of major segments spanning 50 inches" = 10.)

Table 6 Optimized design of the specific case called "narw91updown" ("narrow" panel) with smoothing between adjacent segments as described in Section 14 and factor of safety for local buckling = 1.5. The width, WIDTH, of the panel that is optimized is 11.11111 inches, and there is only one segment per WIDTH/2 = 5.555556 inches, that is, 9 segments per 50 inches.

```
VALUES OF DESIGN VARIABLES CORRESPONDING TO BEST FEASIBLE DESIGN
        CURRENT
 VAR.
 NO.
         VALUE
                          DEFINITION
       6.461E-02
                  wall thickness of the major segment: THICK(1)
  1
                  projected width (x-width) of major segment: SUBWID(1)
  2
       5.556E+00
                  half-angle (deg.) of major corrugation: PHISEG(1)
  3
       4.527E+01
                  half-angle (deg.) of sub-corrugation: PHISUB(1)
  4
       7.000E+01
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(1)
  5
       3.000E+01
                  vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(2)
  6
       3.449E+01
                  half-angle (deg.) of overall arching: PHIBIG
  7
       1.000E-01
MARGINS CORRESPONDING TO THE DESIGN (F.S. = FACTOR OF SAFETY)
(Critical margins are in bold face.)
MAR.
       CURRENT
NO.
        VALUE
                        DEFINITION
                (LOCBUK(1)/LOCBUKA(1)) / LOCBUKF(1)-1; F.S.=
 1
      6.732E-03
                (BUKSYM(1)/BUKSYMA(1)) / BUKSYMF(1)-1; F.S.=
     -3.979E-04
                (BUKASY(1)/BUKASYA(1)) / BUKASYF(1)-1; F.S.=
 3
     -1.521E-03
      5.963E-01
                (CYLBUK(1 ,1 )/CYLBUKA(1 ,1 )) / CYLBUKF(1 ,1 )-1; F.S.=
                (STRESSA(1 )/STRESS(1 )) / STRESSF(1 )-1; F.S.= 1.50
      2.081E+00
************ DESIGN OBJECTIVE ************
CORRESPONDING VALUE OF THE OBJECTIVE FUNCTION:
 VAR.
        CURRENT
NO.
         VALUE
                          DEFINITION
                  weight of the corrugated panel: WEIGHT
  1
       1.027E+01
************ DESIGN OBJECTIVE ************
```

NOTE: The objective, 10.27 lb, is the weight of the panel of LENGTH = 100 inches and WIDTH = 11.11111 inches. The value plotted in Fig. 46 equals 9 x 10.27 = 92.43 lb, corresponding to a panel of width = 100 inches. (See the solid square data point in Fig. 46 plotted for the "Number of major segments spanning 50 inches" = 9.) The optimized weight, 92.43 lb, of this 100×100 inch corrugated panel is the smallest weight among all of the solid square data points plotted in Fig. 46 for which optimization was performed with use of a one-segment model. See Fig. 54. There are only 3 decision variables in the specific case, narw91updown:

```
1 6.461E-02 wall thickness of the major segment: THICK(1)
3 4.527E+01 half-angle (deg.) of major corrugation: PHISEG(1)
6 3.449E+01 vertical y above (x,y,z) origin if PHIBIG=0: YPLATE(2)
```