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Table 59b Optimized **imperfect unstiffened** equivalent elliposidal shell.
Design margins from Load Set 2 (-mode 1 and -mode 2 imperfection
shapes) corresponding to the design optimized with the use of only
mode 1 and mode 2 imperfection shapes. These margins are developed via
the same seven analyses of the type listed in Table 30 (which gives
results for the optimized isogrid-stiffened equivalent ellipsoidal shell)
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 A typical margin with the meanings of the indices, a, b, c, d, e,
 explained:
                         a                              b
 8  4.121E-02  (SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1; F.S.= 1.00
                      c  d e         c d e         c  d e

          "SKNST" means "Skin effective stress"
      a = "A" means "Allowable value"
      b = "F" means "Factor of safety"
      c = Imperfection mode number, (1 or 2 in the cases explored here)
      d = Load set number (1 or 2 in the cases explored here)
          Load set 1 means "use +mode 1 and +mode 2 imperfection shapes"
          Load set 2 means "use -mode 1 and -mode 2 imperfection shapes"
      e = Region number:
            (1 or 2 Region 1 is from the axis of revolution to xlimit,
                              that is, 0 < x < xlimit.
                    Region 2 is from xlimit to the equator,
                              that is, xlimit < x < semi-major axis.)
 *** RESULTS FOR LOAD SET NO. 2 (-mode 1 and -mode 2 imperfections) ***
 MARGINS CORRESPONDING TO CURRENT DESIGN (F.S.= FACTOR OF SAFETY)
 MARGIN CURRENT
 NO.     VALUE              DEFINITION
  1    -4.738E-02   (CLAPS1(2 )/CLAPS1A(2 )) / CLAPS1F(2 )-1; F.S.=  1.00
  2     1.056E-01   (GENBK1(2 )/GENBK1A(2 )) / GENBK1F(2 )-1; F.S.=  1.00
  3     1.401E+00   (SKNBK1(2,1)/SKNBK1A(2,1))/SKNBK1F(2,1)-1; F.S.= 1.00
  4     3.010E-01   (SKNBK1(2,2)/SKNBK1A(2,2))/SKNBK1F(2,2)-1; F.S.= 1.00
  5     1.559E+04   (STFBK1(2,1)/STFBK1A(2,1))/STFBK1F(2,1)-1; F.S.= 1.00
  6     1.548E+04   (STFBK1(2,2)/STFBK1A(2,2))/STFBK1F(2,2)-1; F.S.= 1.00
  7    -2.310E-02   (SKNST1A(2,1)/SKNST1(2,1))/SKNST1F(2,1)-1; F.S.= 1.00
  8     4.121E-02   (SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1; F.S.= 1.00
  9     4.675E-01   (STFST1A(2,1)/STFST1(2,1))/STFST1F(2,1)-1; F.S.= 1.00
 10     4.572E-01   (STFST1A(2,2)/STFST1(2,2))/STFST1F(2,2)-1; F.S.= 1.00
 11    -2.238E-02   (WAPEX1A(2 )/WAPEX1(2 )) / WAPEX1F(2 )-1; F.S.=  1.00

 12    -2.396E-02   (CLAPS2(2 )/CLAPS2A(2 )) / CLAPS2F(2 )-1; F.S.=  1.00
 13     2.160E-01   (GENBK2(2 )/GENBK2A(2 )) / GENBK2F(2 )-1; F.S.=  1.00
 14     7.498E-01   (SKNBK2(2,1)/SKNBK2A(2,1))/SKNBK2F(2,1)-1; F.S.= 1.00
 15     3.103E-01   (SKNBK2(2,2)/SKNBK2A(2,2))/SKNBK2F(2,2)-1; F.S.= 1.00
 16     2.042E+04   (STFBK2(2,1)/STFBK2A(2,1))/STFBK2F(2,1)-1; F.S.= 1.00
 17     1.234E+04   (STFBK2(2,2)/STFBK2A(2,2))/STFBK2F(2,2)-1; F.S.= 1.00
 18     7.760E-02   (SKNST2A(2,1)/SKNST2(2,1))/SKNST2F(2,1)-1; F.S.= 1.00
 19    -2.056E-02   (SKNST2A(2,2)/SKNST2(2,2))/SKNST2F(2,2)-1; F.S.= 1.00
 20     5.434E-01   (STFST2A(2,1)/STFST2(2,1))/STFST2F(2,1)-1; F.S.= 1.00
 21     1.618E-01   (STFST2A(2,2)/STFST2(2,2))/STFST2F(2,2)-1; F.S.= 1.00
 22     1.252E-01   (WAPEX2A(2 )/WAPEX2(2 )) / WAPEX2F(2 )-1; F.S.=  1.00
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