Table 89 Optimum design of the unstiffened imperfect equivalent ellipsoidal shell with the thick apex (Shell Segment 1) of uniform thickness 0.47183 inch. The optimum design and margins were obtained in the presence of axisymmetric buckling modal imperfections with amplitude, Wimp = plus and minus 0.1 inch. Optimization was with the use of plus and minus axisymmetric modes 1 and 2 and one execution of SUPEROPT. During optimization the lower bound of the uniform thickness of Shell Segment 1 was 0.4 inch. Critical margins are in bold face. This table represents an abridged and edited version of the GENOPT output file, "eqellipse.OPM", in which "eqellipse" is the user-selected name of the specific case. Note that there is no longer a local thickened band, THKSKN(3), a characteristic present in the case of the optimum design for the unstiffened imperfect shell listed in Table 33, which was found to be under-designed. This shell is not under-designed.

```
STRUCTURAL ANALYSIS WITH UNPERTURBED DECISION VARIABLES
VAR.
     CURRENT
                       DEFINITION
 NO.
       VALUE
     4.7183E-01
                 skin thickness at xinput: THKSKN(1)
  1
     4.7183E-01
  2
                 skin thickness at xinput: THKSKN(2)
                 skin thickness at xinput: THKSKN(3 ) ←no thick band
  3
     3.5443E-01
                 skin thickness at xinput: THKSKN(4)
  4
     3.4638E-01
                 skin thickness at xinput: THKSKN(5)
  5
     3.3343E-01
                 skin thickness at xinput: THKSKN(6)
  6
     2.9722E-01
                 skin thickness at xinput: THKSKN(7)
  7
     2.6247E-01
                 skin thickness at xinput: THKSKN(8 )
  8
     2.5712E-01
  9
                 skin thickness at xinput: THKSKN(9)
     2.3469E-01
 10
     2.1146E-01
                 skin thickness at xinput: THKSKN(10)
 11
     2.1325E-01
                 skin thickness at xinput: THKSKN(11)
 12
     1.4812E-01
                 skin thickness at xinput: THKSKN(12)
 13
     2.3452E-01
                 skin thickness at xinput: THKSKN(13)
 14
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(1)
 15
                 height of isogrid members at xinput: HIGHST(2)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(3)
 16
     1.0000E-06
 17
                 height of isogrid members at xinput: HIGHST(4)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(5)
 18
     1.0000E-06
 19
                 height of isogrid members at xinput: HIGHST(6)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(7)
 20
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(8)
 21
     1.0000E-06
 22
                 height of isogrid members at xinput: HIGHST(9)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(10)
 23
     1.0000E-06
 24
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(11)
 25
                 height of isogrid members at xinput: HIGHST(12)
     1.0000E-06
 26
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(13)
 27 3.0000E+00
                 spacing of the isogrid members: SPACNG
```

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28
     1.0000E-05 thickness of an isogrid stiffening member: THSTIF
************ DESIGN OBJECTIVE ***********
   CURRENT VALUE OF THE OBJECTIVE FUNCTION:
VAR.
       CURRENT
NO.
        VALUE
                         DEFINITION
                weight of the equivalent ellipsoidal head: WEIGHT
 1
      1.105E+02
**** RESULTS FOR LOAD SET NO. 1 (+mode 1 and +mode 2) *****
MARGIN CURRENT
                         DEFINITION
NO.
        VALUE
 1
      1.200E-02 (CLAPS1( 1)/CLAPS1A(1 )) / CLAPS1F(1 )-1; F.S.= 1.00
 2
      7.155E-02 (GENBK1(1)/GENBK1A(1)) / GENBK1F(1)-1; F.S.= 1.00
 3
      5.177E+01 (SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1; F.S.=1.00
      1.196E+01 (SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1; F.S.=1.00
 4
 5
      2.369E+04 (STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1; F.S.=1.00
 6
      1.232E+04 (STFBK1(1,2)/STFBK1A(1,2))/STFBK1F(1,2)-1; F.S.=1.00
 7
      4.728E-01 (SKNST1A(1,1)/SKNST1(1,1))/SKNST1F(1,1)-1; F.S.=1.00
     -4.803E-02 (SKNST1A(1,2)/SKNST1(1,2))/SKNST1F(1,2)-1; F.S.=1.00
 8
 9
      1.231E+00 (STFST1A(1,1)/STFST1(1,1))/STFST1F(1,1)-1; F.S.=1.00
10
      1.602E-01 (STFST1A(1,2)/STFST1(1,2))/STFST1F(1,2)-1; F.S.=1.00
11
      1.863E+00 (WAPEX1A(1 )/WAPEX1(1 )) / WAPEX1F(1 )-1; F.S.= 1.00
12
      1.367E-02 (CLAPS2( 1)/CLAPS2A(1 )) / CLAPS2F(1 )-1; F.S.= 1.00
     -4.165E-02 (GENBK2(1)/GENBK2A(1)) / GENBK2F(1)-1; F.S.= 1.00
13
14
      3.937E+01 (SKNBK2(1,1)/SKNBK2A(1,1))/SKNBK2F(1,1)-1; F.S.=1.00
15
      1.178E+01 (SKNBK2(1,2)/SKNBK2A(1,2))/SKNBK2F(1,2)-1; F.S.=1.00
      2.578E+04 (STFBK2(1,1)/STFBK2A(1,1))/STFBK2F(1,1)-1; F.S.=1.00
16
17
      1.060E+04 (STFBK2(1,2)/STFBK2A(1,2))/STFBK2F(1,2)-1; F.S.=1.00
18
      1.483E-01 (SKNST2A(1,1)/SKNST2(1,1))/SKNST2F(1,1)-1; F.S.=1.00
19
     -4.159E-02 (SKNST2A(1,2)/SKNST2(1,2))/SKNST2F(1,2)-1; F.S.=1.00
20
      1.356E+00 (STFST2A(1,1)/STFST2(1,1))/STFST2F(1,1)-1; F.S.=1.00
21
     -2.192E-03 (STFST2A(1,2)/STFST2(1,2))/STFST2F(1,2)-1; F.S.=1.00
22
      1.321E+00 (WAPEX2A(1 )/WAPEX2(1 )) / WAPEX2F(1 )-1; F.S.= 1.00
***** RESULTS FOR LOAD SET NO. 2 (-mode 1 and -mode 2) *****
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
MARGIN CURRENT
NO.
        VALUE
                         DEFINITION
     -1.727E-02 (CLAPS1(2 )/CLAPS1A(2 )) / CLAPS1F(2 )-1; F.S.= 1.00
 1
 2
     -8.594E-03 (GENBK1(2 )/GENBK1A(2 )) / GENBK1F(2 )-1; F.S.= 1.00
 3
      4.772E+01 (SKNBK1(2,1)/SKNBK1A(2,1))/SKNBK1F(2,1)-1; F.S.=1.00
 4
      1.182E+01 (SKNBK1(2,2)/SKNBK1A(2,2))/SKNBK1F(2,2)-1; F.S.=1.00
 5
      1.806E+04 (STFBK1(2,1)/STFBK1A(2,1))/STFBK1F(2,1)-1; F.S.=1.00
      1.112E+04 (STFBK1(2,2)/STFBK1A(2,2))/STFBK1F(2,2)-1; F.S.=1.00
 6
 7
      6.212E-01 (SKNST1A(2,1)/SKNST1(2,1))/SKNST1F(2,1)-1; F.S.=1.00
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8
     -3.045E-02 (SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1; F.S.=1.00
 9
      7.006E-01 (STFST1A(2,1)/STFST1(2,1))/STFST1F(2,1)-1; F.S.=1.00
      4.729E-02 (STFST1A(2,2)/STFST1(2,2))/STFST1F(2,2)-1; F.S.=1.00
10
      1.017E+00 (WAPEX1A(2 )/WAPEX1(2 )) / WAPEX1F(2 )-1; F.S.= 1.00
11
12
     -3.065E-02 (CLAPS2(2 )/CLAPS2A(2 )) / CLAPS2F(2 )-1; F.S.= 1.00
13
      1.441E-01 (GENBK2(2 )/GENBK2A(2 )) / GENBK2F(2 )-1; F.S.= 1.00
14
      5.792E+01 (SKNBK2(2,1)/SKNBK2A(2,1))/SKNBK2F(2,1)-1; F.S.=1.00
15
      1.200E+01 (SKNBK2(2,2)/SKNBK2A(2,2))/SKNBK2F(2,2)-1; F.S.=1.00
      1.378E+04 (STFBK2(2,1)/STFBK2A(2,1))/STFBK2F(2,1)-1; F.S.=1.00
16
      1.212E+04 (STFBK2(2,2)/STFBK2A(2,2))/STFBK2F(2,2)-1; F.S.=1.00
17
18
      3.137E-01 (SKNST2A(2,1)/SKNST2(2,1))/SKNST2F(2,1)-1; F.S.=1.00
     -2.544E-02 (SKNST2A(2,2)/SKNST2(2,2))/SKNST2F(2,2)-1; F.S.=1.00
19
20
      2.971E-01 (STFST2A(2,1)/STFST2(2,1))/STFST2F(2,1)-1; F.S.=1.00
      1.409E-01 (STFST2A(2,2)/STFST2(2,2))/STFST2F(2,2)-1; F.S.=1.00
21
      1.414E+00 (WAPEX2A(2)/WAPEX2(2)) / WAPEX2F(2)-1; F.S.= 1.00
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NOTE: The design margins listed above are divided into two groups of 11 margins each: Margins 1-11 and Margins 12-22. The first group of 11 margins are obtained with use of the axisymmetric mode 1 imperfection, and the second group of 11 margins are obtained with use of the axisymmetric mode 2 imperfection.