Table 93 Optimum design of the unstiffened imperfect equivalent ellipsoidal shell with the thick apex (Shell Segment 1) of uniform thickness 0.61996 inch. The optimum design and margins were obtained with use of plus and minus axisymmetric modes 1 and 2 with amplitude, Wimp=0.2 inch and with the lower bound of the uniform thickness of Shell Segment 1 (the spherical cap — see Fig. 2) set equal to 0.6 inch. One execution of SUPEROPT was used to obtain the optimum design. This output is an abridged and edited version of the output file from GENOPT called "eqellipse.OPM", where "eqellipse" is the user-selected name of the specific case. Critical margins are in bold face. Note that there is no longer a local thickened band, THKSKN(3), a characteristic present in the case of the optimum design for the unstiffened imperfect shell listed in Table 33, which was found to be under-designed. This shell is not under-designed.

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STRUCTURAL ANALYSIS WITH UNPERTURBED DECISION VARIABLES
VAR.
      CURRENT
                       DEFINITION
 NO.
      VALUE
  1
     6.1996E-01
                 skin thickness at xinput: THKSKN(1)
  2
     6.1996E-01
                 skin thickness at xinput: THKSKN(2)
                 skin thickness at xinput: THKSKN(3) ←no thick band
  3
     4.1122E-01
                 skin thickness at xinput: THKSKN(4)
  4
     4.0594E-01
                 skin thickness at xinput: THKSKN(5)
  5
     3.9622E-01
     3.7653E-01
                 skin thickness at xinput: THKSKN(6)
  6
                 skin thickness at xinput: THKSKN(7 )
  7
     2.9665E-01
                 skin thickness at xinput: THKSKN(8)
  8
     2.8323E-01
                 skin thickness at xinput: THKSKN(9 )
  9
     3.0991E-01
                 skin thickness at xinput: THKSKN(10)
 10
     2.7282E-01
 11
     2.4117E-01
                 skin thickness at xinput: THKSKN(11)
                 skin thickness at xinput: THKSKN(12)
 12
     1.6825E-01
 13
     2.8315E-01
                 skin thickness at xinput: THKSKN(13)
 14
                 height of isogrid members at xinput: HIGHST(1)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(2)
 15
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(3)
 16
     1.0000E-06
 17
                 height of isogrid members at xinput: HIGHST(4)
     1.0000E-06
 18
                 height of isogrid members at xinput: HIGHST(5)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(6)
 19
     1.0000E-06
 20
                 height of isogrid members at xinput: HIGHST(7)
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(8)
 21
     1.0000E-06
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(9)
 22
                 height of isogrid members at xinput: HIGHST(10)
 23
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(11)
 24
     1.0000E-06
 25
     1.0000E-06
                 height of isogrid members at xinput: HIGHST(12)
                 height of isogrid members at xinput: HIGHST(13)
     1.0000E-06
 26
 27
                 spacing of the isogrid members: SPACNG
     3.0000E+00
                 thickness of an isogrid stiffening member: THSTIF
 28
     1.0000E-05
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************** DESTGN OBJECTIVE *************
   CURRENT VALUE OF THE OBJECTIVE FUNCTION:
VAR.
       CURRENT
NO.
        VALUE
                         DEFINITION
      1.325E+02
                 weight of the equivalent ellipsoidal head: WEIGHT
 1
                   (Compare with WEIGHT = 127.1 lb in Table 78)
**** RESULTS FOR LOAD SET NO. 1 (+mode 1 and +mode 2) *****
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
MARGIN CURRENT
NO.
        VALUE
                         DEFINITION
 1
      1.124E-01 (CLAPS1(1 )/CLAPS1A(1 )) / CLAPS1F(1 )-1; F.S.=1.00
 2
      1.638E-01 (GENBK1(1 )/GENBK1A(1 )) / GENBK1F(1 )-1; F.S.=1.00
 3
      7.183E+01 (SKNBK1(1,1)/SKNBK1A(1,1))/SKNBK1F(1,1)-1;F.S.=1.00
 4
      1.761E+01 (SKNBK1(1,2)/SKNBK1A(1,2))/SKNBK1F(1,2)-1;F.S.=1.00
 5
      4.160E+04 (STFBK1(1,1)/STFBK1A(1,1))/STFBK1F(1,1)-1;F.S.=1.00
      1.073E+04 (STFBK1(1,2)/STFBK1A(1,2))/STFBK1F(1,2)-1;F.S.=1.00
 6
 7
      3.940E-01 (SKNST1A(1,1)/SKNST1(1,1))/SKNST1F(1,1)-1;F.S.=1.00
 8
     -3.545E-02 (SKNST1A(1,2)/SKNST1(1,2))/SKNST1F(1,2)-1;F.S.=1.00
 9
      1.960E+00 (STFST1A(1,1)/STFST1(1,1))/STFST1F(1,1)-1;F.S.=1.00
      1.062E-02 (STFST1A(1,2)/STFST1(1,2))/STFST1F(1,2)-1;F.S.=1.00
10
11
      1.828E+00 (WAPEX1A(1 )/WAPEX1(1 )) / WAPEX1F(1 )-1; F.S.=1.00
12
      5.309E-03 (CLAPS2(1 )/CLAPS2A(1 )) / CLAPS2F(1 )-1; F.S.=1.00
13
      8.763E-02 (GENBK2(1 )/GENBK2A(1 )) / GENBK2F(1 )-1; F.S.=1.00
14
      6.998E+01 (SKNBK2(1,1)/SKNBK2A(1,1))/SKNBK2F(1,1)-1;F.S.=1.00
15
      1.802E+01 (SKNBK2(1,2)/SKNBK2A(1,2))/SKNBK2F(1,2)-1;F.S.=1.00
16
      1.738E+04 (STFBK2(1,1)/STFBK2A(1,1))/STFBK2F(1,1)-1;F.S.=1.00
17
      1.070E+04 (STFBK2(1,2)/STFBK2A(1,2))/STFBK2F(1,2)-1;F.S.=1.00
      2.446E-01 (SKNST2A(1,1)/SKNST2(1,1))/SKNST2F(1,1)-1;F.S.=1.00
18
19
     -1.350E-02 (SKNST2A(1,2)/SKNST2(1,2))/SKNST2F(1,2)-1;F.S.=1.00
20
      6.359E-01 (STFST2A(1,1)/STFST2(1,1))/STFST2F(1,1)-1;F.S.=1.00
21
      6.960E-03 (STFST2A(1,2)/STFST2(1,2))/STFST2F(1,2)-1;F.S.=1.00
2.2
      1.391E+00 (WAPEX2A(1 )/WAPEX2(1 )) / WAPEX2F(1 )-1; F.S.=1.00
***** RESULTS FOR LOAD SET NO.
                                2 (-mode 1 and -mode 2) *****
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S. = FACTOR OF SAFETY)
MARGIN CURRENT
NO.
        VALUE
                         DEFINITION
 1
     -3.891E-03 (CLAPS1(2 )/CLAPS1A(2 )) / CLAPS1F(2 )-1; F.S.=1.00
      1.818E-01 (GENBK1(2 )/GENBK1A(2 )) / GENBK1F(2 )-1; F.S.=1.00
 2
 3
      1.022E+02 (SKNBK1(2,1)/SKNBK1A(2,1))/SKNBK1F(2,1)-1;F.S.=1.00
 4
      1.818E+01 (SKNBK1(2,2)/SKNBK1A(2,2))/SKNBK1F(2,2)-1;F.S.=1.00
 5
      1.564E+04 (STFBK1(2,1)/STFBK1A(2,1))/STFBK1F(2,1)-1;F.S.=1.00
 6
      1.294E+04 (STFBK1(2,2)/STFBK1A(2,2))/STFBK1F(2,2)-1;F.S.=1.00
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7
      4.300E-01 (SKNST1A(2,1)/SKNST1(2,1))/SKNST1F(2,1)-1;F.S.=1.00
 8
      1.524E-02 (SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1;F.S.=1.00
 9
      4.726E-01 (STFST1A(2,1)/STFST1(2,1))/STFST1F(2,1)-1;F.S.=1.00
      2.181E-01 (STFST1A(2,2)/STFST1(2,2))/STFST1F(2,2)-1;F.S.=1.00
10
11
      9.265E-01 (WAPEX1A(2 )/WAPEX1(2 )) / WAPEX1F(2 )-1; F.S.=1.00
      1.284E-02 (CLAPS2(2 )/CLAPS2A(2 )) / CLAPS2F(2 )-1; F.S.=1.00
12
      7.084E-02 (GENBK2(2 )/GENBK2A(2 )) / GENBK2F(2 )-1; F.S.=1.00
13
14
      7.807E+01 (SKNBK2(2,1)/SKNBK2A(2,1))/SKNBK2F(2,1)-1;F.S.=1.00
      1.787E+01 (SKNBK2(2,2)/SKNBK2A(2,2))/SKNBK2F(2,2)-1;F.S.=1.00
15
      1.670E+04 (STFBK2(2,1)/STFBK2A(2,1))/STFBK2F(2,1)-1;F.S.=1.00
16
17
      1.084E+04 (STFBK2(2,2)/STFBK2A(2,2))/STFBK2F(2,2)-1;F.S.=1.00
      4.498E-01 (SKNST2A(2,1)/SKNST2(2,1))/SKNST2F(2,1)-1;F.S.=1.00
18
19
     -2.353E-02 (SKNST2A(2,2)/SKNST2(2,2))/SKNST2F(2,2)-1;F.S.=1.00
      5.721E-01 (STFST2A(2,1)/STFST2(2,1))/STFST2F(2,1)-1;F.S.=1.00
20
21
      2.093E-02 (STFST2A(2,2)/STFST2(2,2))/STFST2F(2,2)-1;F.S.=1.00
      7.158E-01 (WAPEX2A(2 )/WAPEX2(2 )) / WAPEX2F(2 )-1; F.S.=1.00
22
      5.927E-01 (WAPEX2A(2 )/WAPEX2(2 )) / WAPEX2F(2 )-1; F.S.=1.00
22
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NOTE: The design margins listed above are divided into two groups of 11 margins each: Margins 1-11 and Margins 12-22. The first group of 11 margins are obtained with use of the axisymmetric mode 1 imperfection, and the second group of 11 margins are obtained with use of the axisymmetric mode 2 imperfection.