

Table 32 Optimized imperfect isogrid-stiffened equivalent ellipsoidal shell. Design margins from Load Set 2 (**-mode 1 and -mode 2 imperfection shapes**) corresponding to the design optimized with the use of only mode 1 and mode 2 imperfection shapes. These margins are developed via the seven analyses of the type listed in Table 30. Critical margins are in **bold**.

A typical margin with the meanings of the indices, a, b, c, d, e, explained:

8 4.979E-02 (SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1; F.S.= 1.00
a b
c d e c d e c d e

"SKNST" means "Skin effective stress"

a = "A" means "Allowable value"

b = "F" means "Factor of safety"

c = Imperfection mode number, (1 or 2 in the cases explored here)

d = Load set number (1 or 2 in the cases explored here)

Load set 1 means "use +mode 1 and +mode 2 imperfection shapes"

Load set 2 means "use -mode 1 and -mode 2 imperfection shapes"

e = Region number:

(1 or 2 Region 1 is from the axis of revolution to xlimit,
that is, $0 < x < x_{limit}$.)

Region 2 is from xlimit to the equator,
that is, $x_{limit} < x < \text{semi-major axis.}$)

*** RESULTS FOR LOAD SET NO. 2 (-mode 1 and -mode 2 imperfections) ***
MARGINS CORRESPONDING TO CURRENT DESIGN (F.S.= FACTOR OF SAFETY)

MARGIN CURRENT

NO.	VALUE	DEFINITION
1	2.455E-02	(CLAPS1(2)/CLAPS1A(2))/CLAPS1F(2)-1; F.S.= 1.00
2	5.860E-01	(GENBK1(2)/GENBK1A(2))/GENBK1F(2)-1; F.S.= 1.00
3	2.168E+00	(SKNBK1(2,1)/SKNBK1A(2,1))/SKNBK1F(2,1)-1; F.S.= 1.00
4	2.298E+00	(SKNBK1(2,2)/SKNBK1A(2,2))/SKNBK1F(2,2)-1; F.S.= 1.00
5	1.477E-01	(STFBK1(2,1)/STFBK1A(2,1))/STFBK1F(2,1)-1; F.S.= 1.00
6	3.683E-01	(STFBK1(2,2)/STFBK1A(2,2))/STFBK1F(2,2)-1; F.S.= 1.00
7	-4.325E-03	(SKNST1A(2,1)/SKNST1(2,1))/SKNST1F(2,1)-1; F.S.= 1.00
8	4.979E-02	(SKNST1A(2,2)/SKNST1(2,2))/SKNST1F(2,2)-1; F.S.= 1.00
9	2.005E-02	(STFST1A(2,1)/STFST1(2,1))/STFST1F(2,1)-1; F.S.= 1.00
10	-1.268E-02	(STFST1A(2,2)/STFST1(2,2))/STFST1F(2,2)-1; F.S.= 1.00
11	3.043E-01	(WAPEx1A(2)/WAPEx1(2))/WAPEx1F(2)-1; F.S.= 1.00
12	6.727E-01	(CLAPS2(2)/CLAPS2A(2))/CLAPS2F(2)-1; F.S.= 1.00
13	1.151E+00	(GENBK2(2)/GENBK2A(2))/GENBK2F(2)-1; F.S.= 1.00
14	1.790E+00	(SKNBK2(2,1)/SKNBK2A(2,1))/SKNBK2F(2,1)-1; F.S.= 1.00
15	1.791E+00	(SKNBK2(2,2)/SKNBK2A(2,2))/SKNBK2F(2,2)-1; F.S.= 1.00
16	7.854E-02	(STFBK2(2,1)/STFBK2A(2,1))/STFBK2F(2,1)-1; F.S.= 1.00
17	1.232E+00	(STFBK2(2,2)/STFBK2A(2,2))/STFBK2F(2,2)-1; F.S.= 1.00
18	1.558E-01	(SKNST2A(2,1)/SKNST2(2,1))/SKNST2F(2,1)-1; F.S.= 1.00
19	1.423E-01	(SKNST2A(2,2)/SKNST2(2,2))/SKNST2F(2,2)-1; F.S.= 1.00
20	-1.639E-02	(STFST2A(2,1)/STFST2(2,1))/STFST2F(2,1)-1; F.S.= 1.00
21	-3.856E-02	(STFST2A(2,2)/STFST2(2,2))/STFST2F(2,2)-1; F.S.= 1.00
22	5.771E-01	(WAPEx2A(2)/WAPEx2(2))/WAPEx2F(2)-1; F.S.= 1.00