STAGS "crude" 180-degree "soccerball" model

8.356E-02
8.192E-03
-6.717E-02
-1.425E-01
-2.179E-01
-2.933E-01
-3.686E-01
-4.440E-01
-5.194E-01
-5.947E-01
-6.701E-01
-7.455E-01
-8.208E-01
-8.962E-01
-9.716E-01
-1.047E+00

t(apex)=0.47183; shell was optimized with imperfection amplitude, Wimp=0.1 inch; unstiff.equiv.ellipsoidal shell
PA= 0.721507; PB= 0.0; 480 finite elements are used; crude model
step 51 displacement w contours at post-collapse value of PA
nonlinear w; uniform pressure is now applied to the shell with the residual dent in the previous fig.
subroutine usrfab.soccerball.plastic.src is used with NGCP = 1

Θx   -0.00
Θy   0.00
Θz   -0.00

9.900E+00

Fig. 225 Elastic-plastic analysis of the **optimized unstiffened equivalent ellipsoidal shell with the thick apex with t(apex) = 0.47183 inch; Wimp=0.1 inch**, half the amplitude, Wimp = 0.2 inch, that pertains to the results in Figs. 145 – 200 and Tables 78 – 88**; the optimum design is listed in Table 89.** Shown here is the **post-collapse** state of the shell at the end of the STAGS run that followed Run 9 (Fig. 216). In that following run, Load Set A (uniform external pressure) is applied to the shell with the residual dent displayed in Fig. 224. The seventh trace in Fig. 217 shows results from this STAGS run. Compare this figure with Fig. 222, also with Fig. 183, which is for a different optimum design, that listed in Table 78, for which Wimp = 0.2 inch.