

Fig. 194 Elastic-plastic analysis of the **optimized unstiffened equivalent ellipsoidal shell with the thick apex with t(apex) = 0.4 inch; Wimp=0.2 inch; the optimum design is listed in Table 78.** State of the shell at load set B (PB) step no. 37 at the end of Run 1. (See Fig. 193). Load set B consists of a number of concentrated normal inward-directed imposed **displacements** applied along the junction of Shell segments 3 and 4 (Figs. 2, 169, 181, 190, 191) distributed as  $\cos(\text{theta})$  from theta = 0 to 90 degrees in the circumferential coordinate along Row no. 5 in Shell Units 11 and 12. (See Table a40). This imposed normal displacement distribution is used because it generates a dent that **locally** resembles the deformation in Figs. 190 and 191, that is, the linear buckling modal imperfection with n = 1 circumferential wave. Compare with Fig. 181, for which a  $\cos(\text{theta})$  distribution of concentrated normal inward-directed loads generates the dent rather than normal inward-directed imposed displacements.