Table 27 allenflat54.diff file obtained from the following command:

## diff allenflat5.inp allenflat4.inp > allenflat54.diff

> 8.009E-02, \$ TL =layer thickness. Wall type: 4, Layer: 1

Difference between the \*.inp files for the 2-bay flat panel without edge stiffeners (case=allenflat5) and the 2-bay flat panel with edge stiffeners (case=allenflat4). The panel without edge stiffeners actually has edge stiffeners but they are very, very tiny, have very, very small moduli, and have very, very small prebuckling loads. The allenflat5.inp file is obtained starting from the allenflat4.inp file and changing the appropriate GCP records pertaining to edge stiffeners only. See Fig. 73.

```
1591c1591
< 5.050E+01, $ Matl 2: E1=Modulus along fibers.
                                                    BEGIN I-2 rec.
> 5.050E+06, $ Matl 2: E1=Modulus along fibers.
                                                    BEGIN I-2 rec.
1593c1593
< 1.942E+01, $ Matl 2: G = In-plane shear modulus
> 1.942E+06, $ Matl 2: G = In-plane shear modulus
1596c1596
< 5.050E+01, $ Matl 2: E2 = Modulus normal to fibers (normal to PHI1)
> 5.050E+06, $ Matl 2: E2 = Modulus normal to fibers (normal to PHI1)
1688,1693c1688,1693
< 5.050E+01, $Matl 2 : E1=modulus along fibers.
                                                   BEGIN I-7a rec.
< 5.050E+01, $Matl 2 : E2=modulus normal to fibers. I-7a rec.
< 5.050E+01, $Matl 2 : E3=modulus normal to fibers. I-7a rec.
< 1.942E+01, $Matl 2:G12=in-plane shear modulus. I-7a rec.
< 1.942E+01, $Matl 2:G13=x-z shear modulus.
                                                  I-7a rec.
< 1.942E+01, $Matl 2:G23=y-z shear modulus.
                                                  I-7a rec.
> 5.050E+06, $Matl 2 : E1=modulus along fibers.
                                                   BEGIN I-7a rec.
> 5.050E+06, $Matl 2 : E2=modulus normal to fibers. I-7a rec.
> 5.050E+06, $Matl 2 : E3=modulus normal to fibers. I-7a rec.
> 1.942E+06, $Matl 2:G12=in-plane shear modulus. I-7a rec.
> 1.942E+06, $Matl 2:G13=x-z shear modulus.
                                                  I-7a rec.
> 1.942E+06, $Matl 2:G23=y-z shear modulus.
                                                  I-7a rec.
1812c1812
< 8.009E-03 $ I-21c TL=layer thickness. Wall type: 4, Layer: 1
> 8.009E-02 $ I-21c TL=layer thickness. Wall type: 4, Layer: 1
1818c1818
< 6.006E-03 $ I-21c TL=layer thickness. Wall type: 5, Layer: 1
> 6.006E-02 $ I-21c TL=layer thickness. Wall type: 5, Layer: 1
1930c1930
< 8.009E-03, $ TL =layer thickness. Wall type: 4, Layer: 1
```

```
1941c1941
< 6.006E-03, $ TL =layer thickness. Wall type: 5, Layer: 1
> 6.006E-02, $ TL = layer thickness. Wall type: 5, Layer: 1
2174c2174
< 0.0 9.77930E+00 0.000000E+00 8.592105E-03 $ m-2 X1,X4,Y1,Y2; stringer 1
> 0.0 9.77930E+00 0.000000E+00 8.592105E-01 $ m-2 X1,X4,Y1,Y2; stringer 1
2176.2177c2176.2177
< 0.000000E+00 0.000000E+00 8.592105E-03 $ m-4b XGC2,YGC2,ZGC2 corner 2 of stringer web
< 9.779300E+00 0.000000E+00 8.592105E-03 $ m-4c XGC3, YGC3, ZGC3 corner 3 of stringer web
> 0.000000E+00 0.000000E+00 8.592105E-01 $ m-4b XGC2,YGC2,ZGC2 corner 2 of stringer web
> 9.779300E+00 0.000000E+00 8.592105E-01 $ m-4c XGC3,YGC3,ZGC3 corner 3 of stringer web
2187,2188c2187,2188
< 7.701489E-08 2 1 1 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row 1)
< -7.701489E-08 2 1 81 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row(81))
> 7.701489E+01 2 1 1 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row 1)
> -7.701489E+01 2 1 81 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row(81))
2248c2248
< 0.0 9.77930E+00 0.000000E+00 8.592105E-03 $ m-2 X1,X4,Y1,Y2; stringer 3
> 0.0 9.77930E+00 0.000000E+00 8.592105E-01 $ m-2 X1,X4,Y1,Y2; stringer 3
2250,2251c2250,2251
< 0.000000E+00 4.941000E+00 8.592105E-03 $ m-4b XGC2,YGC2,ZGC2 corner 2 of stringer web
< 9.779300E+00 4.941000E+00 8.592105E-03 $ m-4c XGC3, YGC3, ZGC3 corner 3 of stringer web
> 0.000000E+00 4.941000E+00 8.592105E-01 $ m-4b XGC2,YGC2,ZGC2 corner 2 of stringer web
> 9.779300E+00 4.941000E+00 8.592105E-01 $ m-4c XGC3, YGC3, ZGC3 corner 3 of stringer web
2261,2262c2261,2262
< 7.701489E-08 2 1 1 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row 1)
< -7.701489E-08 2 1 81 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row(81))
> 7.701489E+01 2 1 1 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row 1)
> -7.701489E+01 2 1 81 0 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Nx, row(81))
2285c2285
< 0.000000E+00 8.592105E-03 0.000000E+00 4.941000E+00 $ m-2 X1,X4,Y1,Y2;rectplate,ring no. 1
> 0.000000E+00 8.592105E-01 0.000000E+00 4.941000E+00 $ m-2 X1,X4,Y1,Y2;rectplate,ring no. 1
2288c2288
< 0.000000E+00 4.941000E+00 8.592105E-03 $ m-4c XGC3,YGC3,ZGC3 corner 3 of subring
> 0.000000E+00 4.941000E+00 8.592105E-01 $ m-4c XGC3,YGC3,ZGC3 corner 3 of subring
2298,2299c2298,2299
< -1.448589E-08 3 2 0 1 0 0 $ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col 1)
```

- 1.448589E-08 3 2 0 81 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col( 81))
  -1.448589E+01 3 2 0 1 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col 1)
  1.448589E+01 3 2 0 81 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col( 81))
  2322c2322
  0.000000E+00 8.592105E-03 0.000000E+00 4.941000E+00 \$ m-2 X1,X4,Y1,Y2;rectplate,ring no. 2
  0.000000E+00 8.592105E-01 0.000000E+00 4.941000E+00 \$ m-2 X1,X4,Y1,Y2;rectplate,ring no. 2
  2325c2325
  9.779300E+00 4.941000E+00 8.592105E-03 \$ m-4c XGC3,YGC3,ZGC3 corner 3 of subring
- > 9.779300E+00 4.941000E+00 8.592105E-01 \$ m-4c XGC3,YGC3,ZGC3 corner 3 of subring 2335,2336c2335,2336
- < -1.448589E-08 3 2 0 1 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col 1)
- < 1.448589E-08 3 2 0 81 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col(81))

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- > -1.448589E+01 3 2 0 1 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col 1)
- > 1.448589E+01 3 2 0 81 0 0 \$ q-3 P,LT,LD,LI,LJ,LAX,NX (Ny, col(81))

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