

Table a46 STAGS input file, **soccerball.bin**, corresponding to the input file, \*.inp, listed in Table a40, that is, loading is by an **imposed normal displacement** that varies as **cos(theta)** from 0 to 90 degrees and that is imposed along a circumferential line at the junction between shell segments 3 and 4 in Figs. 2, a1-a3. In this STAGS run the imposed normal displacement continues to increase above 1.3 inches, the maximum value in Load Set B listed in Table a41. We want to produce a residual dent with a depth of close to 0.2 inch, and we need to increase the maximum applied normal displacement to a greater value than 1.3 in order to do this. The results from this run are shown as Run 5 in Table 88 and in Fig. 193.

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optimized imperfect shell, nonlinear theory (INDIC=3)
3, $ INDIC=1 is bifur.buckling; INDIC=3 is nonlinear BEGIN B-1
1, $ IPOST=1 means save displacements every IPOSTth step
0, $ ILIST =0 means normal batch-oriented output
0, $ ICOR  =0 means projection in; 1 means not in.
1, $ IMPTHE=index for imperfection theory.
0, $ IOPTIM=0 means bandwidth optimization will be performed
0, $ IFLU  =0 means no fluid interaction.
-1 $ ISOLVR= 0 means original solver; -1 new solver.END B-1 rec
0.0, $ STLD(1) = starting load factor, System A. BEGIN C-1 rec.
0.0, $ STEP(1) = load factor increment, System A
0.0, $ FACM(1) = maximum load factor, System A
1.3, $ STLD(2) = starting load factor, System B
1.0, $ STEP(2) = load factor increment, System B
2.0, $ FACM(2) = maximum load factor, System B
0 $ ITEMP =0 means no thermal loads. END C-1 rec.
37, $ ISTART=restart from ISTARTth load step. BEGIN D-1 rec.
0,$ NSEC= number of CPU seconds before run termination
10,$ NCUT = number of times step size may be cut
-20, $ NEWT = number of refactorings allowed
-1,$ NSTRAT=-1 means path length used as independent parameter
0.00010,$ DELX=convergence tolerance
0. $ WUND = 0 means initial relaxation factor =1.END D-1 rec.
0, 0, 0 $ NPATH=0: Riks, NEIGS=no.of eigs, NSOL=1=discontin.ET-1
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