

# Equivalent Potential Temperature

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RAF Algorithm Review

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# What Is Equivalent Potential Temperature?

## Rossby Form

- $L_v$  and  $c_{pd}$  are kept constant.

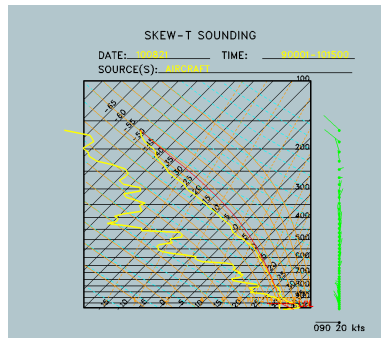
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- New: Davies-Jones, 2009

# Terminology

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“A thermodynamic quantity, with its natural logarithm proportional to the entropy of moist air, that is conserved in a reversible moist adiabatic process. “

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# Equations

$$\Theta_q = T \left( \frac{p_0}{p_d} \right)^{R_d / c_{pt}} \exp \left( \frac{L_v r}{c_{pt} T} \right) \quad (1)$$

- Quantities in red vary with temperature.
- Equation (1) is a straightforward definition if  $L_v$  and  $c_{pd}$  (entering  $c_{pt} = c_{pd} + r_t c_w$ ) are taken at the level of the LCL

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- Bolton: If  $\Theta_D$  is the dry-air potential temperature at the LCL,  $e$  the vapor pressure in mb,  $T_K$  the air temperature in kelvin,  $T_L$  the temperature at the LCL in kelvin and  $r$  the mixing ratio

$$T_L = \frac{2840}{3.5 \ln T_K - \ln e - 4.805} + 55$$

$$\Theta_p^{Bolton} = \Theta_D \exp \left\{ \left( \frac{3.376}{T_L} - 0.00254 \right) r (1 + 0.81 \times 10^{-3} r) \right\}$$

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$$\frac{dT}{dp_d} = \frac{TR_d + L_v r}{p_d} \left[ (c_{pd} + r_t c_w) + \frac{T \varepsilon}{p_d} \left( \frac{\partial \left( \frac{L_v e_s(T)}{T} \right)}{\partial T} \right)_{p_d} \right]^{-1} \quad (2)$$

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- 2 Davies-Jones repeated the analysis and obtained still better fit coefficients investigated over a wider numerical range.
- 3 If we change to the Davies-Jones formula, it may be useful to change the variable name to “pseudo-adiabatic equivalent potential temperature” at the same time to remove the conflict with the AMS definition.

# Three Associated Analyses

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  - ① Integrate the exact equation for  $dT/dp_d$  from point 1 to point 2 to find  $T_2$ .
  - ② Evaluate the equation for potential temperature at point 1, then invert it at point 2 to find  $T_2$ .

## Example: Check Davies-Jones Equation

### Method 1: Integration

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### Method 2: Inversion

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- ② Each  $\Delta p$ , calculate  
 $\Delta T = \frac{dT}{dp_d} \Delta p_d$  from (3)

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$$\Theta_p^{[DJ]} = \Theta_{DL} e^{\left\{ \frac{(L_0^* - L_1^*)(T_L - T_0) + K_2 r}{c_{pd} T_L} \right\}} \quad (4)$$

## Method 2: Inversion

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$$\Theta_{DL} = T \left( \frac{p_0}{p - e} \right)^{2/7} \left( \frac{T}{T_L} \right)^{0.28 \times 10^{-3} r}$$

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# Results

Primed quantities result from numerical integration; unprimed from formula evaluation

T [°C]	p [hPa]	final $p_2$ [hPa]	$T_q$ [K]	$T'_q$ [K]	$T_p$ [K]	$T'_p$ [K]
25	850	100	206.50	207.69	200.73	200.76
15	750	100	189.34	189.73	185.39	185.42
10	750	100	178.69	178.71	175.66	175.69
0	700	100	167.05	166.90	165.39	165.41
-10	600	100	163.54	163.44	162.68	162.70
25	850	300	222.59	222.69	222.27	222.29
10	750	300	239.43	239.46	238.52	238.51
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Example: 1.19 K error in  $\Theta_q$ , 0.03 K in  $\Theta_p$

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Largest error in  $\Theta_p$ : 0.03 K

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Error in  $\Theta_q$  larger when extended to low pressure

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NEGLIGIBLE FOR  $\Theta_p$ : Differences were typically smaller than 0.03 K for a range spanning typical conditions likely to be encountered in research flights.

POTENTIALLY WORTH ATTENTION FOR  $\Theta_q$ : Differences can exceed 1K but are more typically 0.1 K.

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FORMULA IS GOOD: Numerical tests showed that results were within about 0.05 K and in most cases were better than this limit, suggesting that little error is introduced by using the Bolton formula.



# Recommendations

1. Change to (6.5) of Davies-Jones (2009), and change the variable name to “pseudo-adiabatic equivalent potential temperature”. Continue to use (21) of Bolton (1980) to determine the saturation temperature  $T_L$ .

$$\Theta_p^{[DJ]} = \Theta_{DL} \exp \left\{ \frac{(L_0^* - L_1^*(T_L - T_0) + K_2 r) r}{c_{pd} T_L} \right\}$$

$$\Theta_{DL} = T_k \left( \frac{1000}{p_d} \right)^{0.2854} \left( \frac{T_K}{T_L} \right)^{0.28 \times 10^{-3} r}$$

$$T_L = \frac{2840}{3.5 \ln T_K - \ln e - 4.805} + 55$$

## Recommendations

2. Add a new variable “wet-equivalent potential temperature” and use the standard equation for its evaluation. .

$$\Theta_q = T \left( \frac{p_0}{p_d} \right)^{R_d/c_{pt}} \exp \left( \frac{L_v r}{c_{pt} T} \right)$$

where  $c_{pt} = c_{pd} + r_t c_w$  and  $r_{tot}$  is the total water mixing ratio,  $r_{tot} = r + r_w$  where  $r_w = \chi/\rho_d$  with  $\chi$  the liquid water content and  $\rho_d$  the density of dry air:  $\rho_d = (p - e)/(R_d T)$ .