2008 Technical Data Guide For Precast, Prestressed Concrete Hollow-core Plank



## ELEMATIC® Hollow-core Plank



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## Introduction

The purpose of this technical data is to provide assistance in selecting and detailing precast concrete hollow-core plank manufactured by Oldcastle Precast, Inc.

The load tables presented herein are intended as a guide only. Final design is determined by our engineering department based on information presented in the final plans and specifications. To ensure the optimum selection for your application, please contact us for assistance.

Although care has been taken to provide the most accurate data possible, Oldcastle Precast, Inc. does not assume responsibility for errors and omissions.

## The Manufacturing Process

Elematic® is a machine extruded, precast, prestressed hollow-core plank. The planks are manufactured on 500-foot-long beds in standard widths of 48 inches and thickness of 6, 8, 10, 12 and 16 inches. High strength prestressing strands are cast into the planks at the spacing and location required for the given span, loading and fire cover conditions. The planks are cut to length for each project using a diamond-blade saw. After the planks are cut, they are removed from the casting beds and placed into storage.

All Elematic® materials equal or exceed the requirements of applicable ASTM specifications. The concrete mix is designed to have release strength of 3,000 psi or 3,500 psi, and a 28-day compressive strength of 5,000 psi. The prestressing strands are uncoated, seven wire, low relaxation with a minimum ultimate strength of 270 ksi.

## **Load Table Design Criteria**

The tables herein list allowable live loads in pounds per square foot for uniformly distributed loading. Non-uniform loading conditions resulting from point loads, line loads, openings and cantilevers require special design consideration.

The allowable load is usually governed by the ultimate capacity of the section. As a design aid, the ultimate moment capacities in governing criterion for short spans may be the horizontal shear stress between the plank and the topping.

Allowable live loads for long-span, heavily reinforced sections are limited to loads that result in a bottom-tension stress equal to the cracking stress. Loads beyond this limit may result in deflections that exceed the allowable value set forth in the ACI code.

The load tables are based on a plank concrete strength of 5,000 psi. Tables for topped sections are based on a topping strength of 3,500 psi and minimum thickness of 2 inches.

Maximum spans and loads shown are not absolutes. Longer spans or heavier loads may be achieved under certain conditions or different criteria than assumed in the tables. Contact us if you need assistance.

## **Plank Design Considerations**

The following items will affect the selection of appropriate plank sizes and should be carefully reviewed by the Architect/Engineer while developing the plans and specifications for a project:

## Fire Rating

 The fire rating requirement should be clearly specified in the contract documents.

## Loadina Conditions

- Specify all uniform loading requirements on structural plans.
- Identify line and point loads resulting from bearing walls, masonry walls, face brick, columns, mechanical equipment, etc.
- Identify diaphragm forces and lateral loads resulting from wind or earth pressures.
- Review roof plans for vertical protrusions such as parapets, penthouses and adjacent buildings that could require designing for snow drift loads.
- Plank supporting stairs require special loading considerations.
- Large openings or closely spaced groups of smaller openings will reduce the plank load carrying capacity.

## **Topping**

- Specify whether or not concrete topping is to be composite. Composite action requires the topping to be bonded to the top surface of the plank. Topping separated by a vapor barrier or insulation is noncomposite and must be considered a superimposed load.
- Large cambers resulting from long spans and/or heavy loads will affect the quantity of topping, assuming a level floor is required. Two inches of composite topping at mid span is minimal, and additional thickness at the ends of the plank may be required to maintain level floor elevations.

## Camber

- Camber is inherent in all prestressed products. It is the result of the eccentric prestress force required to resist design loads, and cannot be designed in, out, or to an exact number. The amount of camber will depend upon the span, design loads and thickness of plank. Planks stored in the yard for more than 6 weeks, usually due to construction schedule changes, will experience more camber growth.
- Adjacent plank of dissimilar length, strand pattern or with openings will have inherent camber differences.

## Fire Rating

Fire rating specifications are as important as all other design parameters. Plank rating requirements are determined by the Architect or Engineer of Record, who is also responsible for establishing the fire rating criteria for the total project.

Three methods generally used in the Northeast for determining hollow-core plank fire-resistive ratings are:

- 1. 2006 International Building Code
- 2. Rational analysis as defined by PCI MNL 124, "Design for Fire Resistance of Precast Concrete"
- 3. Underwriters Laboratories Fire Resistive Ratings
- 4. MEA product approval (New York City only)

## International Building Code "IBC" Fire Rating

The IBC code prescribes fire ratings to any hollow-core plank section. Since 2000, the IBC code has replaced the BOCA, SBC and UBC model codes in many states. The two criteria that are measured to determine the fire rating are:

- 1. Equivalent concrete thickness 4.6" inches is required for 2 hrs
- 2. Bottom strand cover  $-\frac{3}{4}$ " cover is required for 2 hrs (restrained condition)

## **Underwriters Laboratories Fire Resistive Ratings**

Prior to codes including prescriptive fire-endurance rating methods, fire tests provided the primary source of ratings classifications. While some plank sections were fire tested, others can be evaluated by UL to qualify for existing UL numbers.

The table below lists the UL ratings available with Elematic® plank. Note that these ratings are dependent upon whether or not the ends of the planks are restrained. Determination of the restraint must be made by the Architect or the Engineer of Record, as it is primarily a function of the support structure.

UL	Ratin	g (Hour)	Plank Topping Thickness Thickness		
Number	Restrained	Unrestrained	(inch)	(inch)	
J994	1½	1½	8,10,12	0	
J994	2	1½	8,10,12	½ Gypcrete	
J994	3	11/2	8,10,12	2 <sup>1</sup> / <sub>8</sub> Topping	
J994	4	1½	8,10,12	3 <sup>1</sup> / <sub>8</sub> Topping	

## Fire Ratings by Rational Analysis

PCI MNL 124 defines the "rational analysis" method for determining the fire rating of precast, prestressed members. It is useful to use when a fire rating cannot be obtained by either of the two previous methods. Actual practice has shown that this method is very conservative and that the span of the hollow-core plank will have to be reduced (approx. 10% to 20%) to achieve the same fire rating from both IBC and UL.

In using this method, the reduced strength of the prestressed strands at elevated temperatures is determined and the resulting moment capacities are compared to that required for service loads. Strand

temperatures are based on the amount of concrete cover and the standard fire exposure as defined by the time-temperature relationship specified in ASTM E119. Fire ratings will also be improved if the plank assembly is restrained against thermal expansion. It should be noted that the only universally accepted definition of full restraint is an interior bay of a multi-bay building.

## **Sound Ratings**

The following tables contain values for the Sound Transmission Class (STC) and the Impact Insulations Class (IIC) of various floor systems utilizing Elematic® hollow-core plank.

## Sound Transmission Class (STC)

The values for the Sound Transmission Class were determined by tests which were in accordance with ASTM E90. The STC is a measure (in decibels) of the ease at which air-borne sound is transmitted through a floor system. The larger the value of the STC for a given system, the greater the sound insulation.

Sound Transmission Class (STC	
6" Elematic®	49
6" Elematic® + 2" Topping	53
8" Elematic®	51
8" Elematic® + 2" Topping	54
H8" Heavy Elematic®	51
H8" Heavy Elematic® + 2" Topping	55
10" Elematic®	52
10" Elematic® + 2" Topping	56
12" Elematic®	54
12" Elematic® + 2" Topping	57
16" Elematic®	56
16" Elematic® + 2" Topping	59

## Impact Insulation Class (IIC)

The values for the Impact Insulation Class (IIC) were determined by tests which were in accordance with ASTM ES492. The Impact Insulation Class is the resistance to impact noise transmission and is highly dependent on the floor surface and structural connection details. As with the STC, the higher IIC values are more desirable.

Impact Insulation Class (IIC)	
Types of Floor Systems	Rating
8" Hollow-core Plank	28
8" Hollow-core Plank + ½" wood block flooring adhered directly	47
8" Hollow-core Plank + 0.058" vinyl tile	50
8" Hollow-core Plank + quarry tile w/reinforced mortar bed with 0.4" nylon and carbon black spinneret matting.	54
8" Hollow-core Plank + pad & carpet	73
Add Acoustical Ceiling	+6



## SPECIFICATIONS FOR PRECAST, PRESTRESSED HOLLOW-CORE PLANK SECTION 03400

## 1. GENERAL

## 1.01 Description

В.

- A. Work Included:
  - 1. These specifications cover manufacture, transportation and erection of precast, prestressed, concrete, hollow-core plank, including grouting of joints between adjacent units.

Rela	ated Work Specified Elsewhere:
2.	Cast-in-Place Concrete: Section
3.	Architectural Precast Concrete: Section
4.	Precast Structural Concrete: Section
5.	Underlayments (Floor and/or Roof Leveling): Section
6.	Caulking and Sealants: Section
7.	Small Holes for Mechanical/Plumbing: Section
8.	Cast-in-Place Embedments: Section
9.	Steel Bearing Lintels: Section
10.	Insulation in Plank Cores: Section

## 1.02 Quality Assurance

A. Manufacturer Qualifications: The precast concrete manufacturing plant shall be certified by the Prestressed Concrete Institute (PCI) Plant Certification Program prior to the start of production. Manufacturer shall be certified in category C2.

The manufacturer shall retain a registered structural engineer to certify that manufacturing is in accordance with design requirements; or

The manufacturer shall, at his expense, meet the following requirements:

- 1. The basis of inspection shall be the Prestressed Concrete Institute's "Manual for Quality Control for Plants and Production of Precast and Prestressed Concrete Products", MNL-116, and the criteria for acceptance shall be the same as the Plant Certification Program.
- B. Erector Qualifications: PCI Qualified and regularly engaged for at least 5 years in the erection of precast structural concrete similar to the requirements of this project. Retain aregistered structural engineer to certify that erection is in accordance with designrequirements.
- C. Welder Qualifications: In accordance with AWS D1.1.
- D. Testing: In general compliance with applicable provisions of Prestressed Concrete Institute MNL-116, "Manual for Quality Control for Plants and Production of Precast Prestressed Concrete Products".
- E. Requirements of Regulatory Agencies: All local codes plus the following specifications, standards and codes are a part of these specifications:
  - 1. ACI 318 Building Code Requirements for Reinforced Concrete;
  - 2. AWS D1.1 Structural Welding Code-Steel;
  - 3. AWS D1.4 Structural Welding Code-Reinforcing Steel;
  - 4. ASTM Specifications As referred to in Part 2-Products, of this Specification.

## 1.03 Submittals and Design

- A. Shop Drawings:
  - 1. Erection Drawings
    - a. Plans locating and defining all hollow-core planks furnished by the manufacturer, with all major openings shown.
    - b. Sections and details showing connections, weld plates, edge conditions and support conditions of the hollowcore plank units.
    - c. All dead, live and other applicable loads used in the design.
    - d. Fire rating.
- B. Approvals:
  - 1. Submit \_\_\_\_\_ copies of erection drawings for approval prior to fabrication. Fabrication not to proceed prior to receipt of approved drawings.
- C. Product Design Criteria:
  - 1. Loadings for design
    - a. Initial handling and erection stresses.
    - b. All dead and live loads as specified on the contract documents.
    - c. All other loads specified for hollow-core plank where applicable.
  - 2. Fire rating shall be \_\_\_\_\_ hour(s).
  - 3. Design steel plank support headers when such headers are determined necessary by the manufacturer's engineer.
  - Design calculations shall be performed by an engineer, registered in the state that the project is located in, and experienced in precast prestressed concrete design. Design calculations to be submitted for approval upon request.
  - 5. Design shall be in accordance with ACI 318 and applicable codes.
- D. Permissible Design Deviations:
  - 1. Design deviations will be permitted only after the Architect/Engineer's written approval of the manufacturer's proposed design supported by complete design calculations and drawings.
  - 2. Design deviations shall provide an installation equivalent to the basic intent without incurring additional cost to the owner.
- E. Test Reports: Test reports on concrete and other materials shall be submitted upon request.

## 2. PRODUCTS

## 2.01 Materials

- A. Portland Cement:
  - 1. ASTM C150 Type I or III.
- B. Admixtures:
  - 1. Water Reducing, Retarding, Accelerating, High-Range Water Reducing Admixtures: ASTM C494
- C. Aggregates:
  - 1. ASTM C33 or C330
- D. Water: Potable or free from foreign materials in amounts harmful to concrete and embedded steel.
- E. Reinforcing Steel:
  - 1. Bars:

Deformed Billet Steel: ASTM A615 Deformed Rail Steel: ASTM A616 Deformed Axle Steel: ASTM A617 Deformed Low Alloy Steel: ASTM A706

- 2. Wire: Cold Drawn Steel: ASTM A82.
- F. Prestressing Strand:
  - 1. Uncoated, 7-Wire, Low Lax strand: ASTM A416 (including supplement) Grade 250K or 270K.

- G. Welded Studs: In accordance with AWS D1.1.
- H. Structural Steel Plates and Shapes: ASTM A36.
- I. Grout:
  - 1. Cement grout: Grout shall be a mixture of not less than one part portland cement to three parts fine sand, and the consistency shall be such that joints can be completely filled but without seepage over adjacent surfaces. The grout shall achieve a minimum 28-day compressive strength of 2,000 psi. Any grout that seeps from the joint shall be completely removed before it hardens.
- J. Bearings Strips:
  - 1. Plastic: Multi-monomer plastic strips shall be non-leaching and support construction loads with no visible overall expansion.

## 2.02 Concrete Mixes

- A. 28-day compressive strength: Minimum of 5,000 psi
- B. Release strength: Minimum of 3,000 psi
- C. Use of calcium chloride or admixtures containing chlorides is not permitted.

## 2.03 Manufacture

- A. Hollow-core plank shall be machine cast in 48-inch widths under the trade name **Elematic®** as manufactured by Oldcastle Precast Building Systems.
- B. Manufacturing procedures and tolerances shall be in general compliance with PCI MNL 116.
- C. Openings: Manufacturer shall provide for rectangular openings 10 inches or larger on all sides and as clearly shown on the architectural and structural drawings. They shall be located by the trade requiring them and then field cut. Round and small openings (less than 10 inches) shall be drilled or cut by the respective trades after grouting. Openings requiring cutting of prestressing strand shall be approved by the precast plank manufacturer before drilling or cutting.
- D. Finishes: Bottom surface shall be flat and uniform as resulting from an extrusion process, without major chips, spalls and imperfections. Top surface shall be machine troweled.
- E. Patching: Will be acceptable providing the structural adequacy of the hollow core unit is not impaired.

## 3. EXECUTION

## 3.01 Product Delivery, Storage and Handling

- A. Delivery and Handling:
  - 1. Hollow-core plank shall be lifted and supported during manufacturing, stockpiling, transporting and erection operations only at the lifting or supporting points designated by the manufacturer.
  - 2. Transportation, site handling and erection shall be performed by qualified personnel with acceptable equipment and methods.
- B. Storage:
  - 1. Store all units off ground on firm, level surfaces with dunnage placed at bearing points.
  - 2. Place stored units so that identification marks are discernible.
  - 3. Separate stacked units by dunnage across full width of each plank.

## 3.02 Erection

- A. Site Access: Erection access suitable for cranes and trucks to move unassisted from public roads to all crane working areas as required by erector, or otherwise indicated herein, will be provided and maintained by the general contractor. Obstructing wires shall be shielded or removed and, when applicable, snow removal and winter heat will be provided by the general contractor.
- B. Preparation: The general contractor shall be responsible for:
  - 1. Providing true, level, bearing surfaces on all field-placed bearing walls and other fieldplaced supporting members. Masonry wall bearing surfaces shall be bond beams with properly filled and cured concrete.
  - 2. All pipes, stacks, conduits and other such items shall be stubbed off at a level lower than the bearing plane until after the plank are set. Masonry, concrete or steel shall not be installed above plank-bearing surface until after the plank is in place.
- C. Installation: Installation of hollow-core slab units shall be performed by the manufacturer. Members shall be lifted with slings at points determined by the manufacturer. Bearing strips shall be set where required. Grout keys shall be filled. Openings shall be field cut only after grout has cured, unless authorized by the manufacturer's engineer.

D. Alignment: Members shall be properly aligned. Variations between adjacent members shall be reasonably leveled out by jacking, bolting or any other feasible method as recommended by the manufacturer.

## 3.03 Field Welding

A. Field welding is to be done by qualified welders using equipment and materials compatible to the base material.

## 3.04 Attachments and Small Holes

A. Subject to approval of the Architect/Engineer, hollow-core plank units may be drilled or "shot" provided no contact is made with the prestressing steel. Round holes and those less than 8 inches on any side shall be drilled or cut by the respective trades. Should spalling occur, it shall be repaired by the trade doing the drilling, shooting or cutting.

## 3.05 Clean up

A. Remove rubbish and debris resulting from hollow-core plank work from premises upon completion.

## 3.06 Safety

A. The general contractor will provide and maintain all safety barricades, rebar caps and opening covers required for plank in accordance with current industry safety standards.

## Production and Erection Tolerances: (Reprinted from PCI Manual for the Design of Hollow-core Slabs)

## **Product Tolerances: Hollow-core Slabs**

a =	Length	±1/2 in.
b =	Width	±1/4 in.
C =	Depth	±1/4 in.

d, = Top flange thickness

Top flange area defined by the actual measured values of average d<sub>t</sub> x b shall not be less than 85% of the nominal area calculated by d, nominal x b nominal.

d<sub>b</sub> = Bottom flange thickness

Bottom flange area defined by the actual measured values of average  $d_b x$  b shall not be less than 85% of the nominal area calculated by  $d_b$  nominal x b nominal.

e = Web thickness

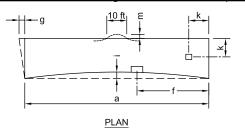
The total cumulative web thickness defined by the actual measured value of e shall not be less than 85% of the nominal cumulative width calculated by  $\Sigma$ e nominal.

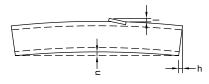
f	=	Blockout location±2 in.
g	=	Flange angle
h	=	Variation from specified end squareness or skew $\pm 1/2$ in.
i	=	Sweep (variation from straight line parallel to centerline of member) $\pm^3/8$ in.
i	=	Center of gravity of strand group

The CG of the strand group relative to the top of the plank shall be within  $\pm 1/4$  in. of the nominal strand group CG. The position of any individual strand shall be with  $\pm 1/2$  in. of nominal vertical position and  $\pm 3/4$  in. of nominal horizontal position and shall have a minimum cover of  $\pm 3/4$  in.

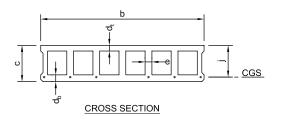
(does not apply to top deck surface left rough to receive a topping or to visually concealed surfaces) Plank weight: Excess concrete material in the plank internal features is within tolerance as long as the measured weight of the individual plank does not exceed 110% of the nominal published unit weight used in the load capacity calucation.

 n = Applications requiring close control of differential camber between adjacent membes of the same design should be discussed in detail withthe producer to determine applicable tolerances.





**ELEVATION** 



## **Erection Tolerances: Hollow-core Floor & Roof Members**

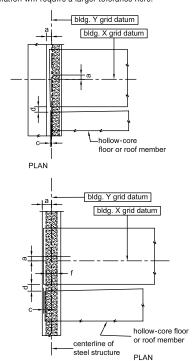
a =	Plan location from building grid datum	±1 in.
a. =	Plan location from centerline of steel <sup>1</sup>	±1 in.
b' =	Top elevation from nonminal elevation at member ends	
	Covered with topping	±3/4 in.
	Untopped floor	±1/4 in.
	Untopped roof	
C =	Maximum jog in alighment of matching edges	
	(both topped and untopped construction)	±1 in.
d =	Joint width	
	0 to 40 ft. member length	±1/2 in.
	41 to 60 ft. member length	±3/4 in.
	61 ft. plus	±1 in.
e =	Differential top elevation as erected	
	Covered with topping	<sup>3</sup> /4 in.
	Untopped floor	
	Untopped roof <sup>2</sup>	<sup>3</sup> /4 in.
f =	Bearing length <sup>3</sup> (span direction)	±3/4 in.
g =	Differential bottom elevation of exposed hollow-core slabs <sup>4</sup> .	<sup>1</sup> /4 in.

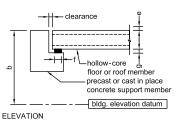
<sup>1</sup>For precast concrete erected on a steel frame building, this tolerance takes takes precedence over tolerance on dimension "a".

 $^2$ lt may be necessary to father the edges to  $\pm^1/4$  in. to properly apply some roof membranes.

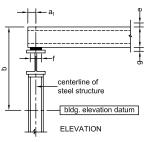
<sup>3</sup>This is a setting tolerance and should not be confused with structural performance requirements set by the architect/engineer.

<sup>4</sup>Untopped installation will require a larger tolerance here.





Precast element to precast or cast-in-place concrete or masonry



Precast element to structural steel

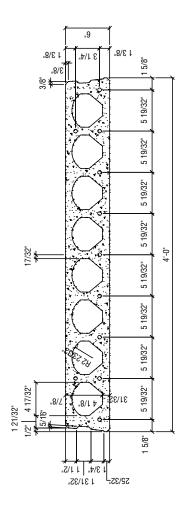


## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

φ Vcw in Kips per	Onit	8.58	8.58	8.58	8.58		
	33						
	10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32						
	30						
	29						l
	28						ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS IN PLACE
	27						N N
	26						ANKS
	25						D PL
_	24			77	84		
SIMPLE SPAN IN FEET	23		74	85	92		E GR(
Z Z	22	89	84	94	101		BAR
PAN	21	79	94	103	112		뿔
E S	20		104	114	124		부
MPI	19	104	116	127	138		VEIGH
SI	18	116	129	142	154		HEV
	17	130	145	159	172		101
	16	147	164	180	190		ONAL
	15	167	186	199	206		E
	14	191	210	217	224		IS AL
	13	219	229	237	244		HAT
	12	245	253	261	269		AD
	=	271	280	289	298		AD LC
	10	304 271 245 219 191 167 147 130 116 104 91	314 280 253 229 210 186 164 145 129 116 104 94	324 289 261 237 217 199 180 159 142 127 114 103 94	334 298 269 244 224 206 190 172 154 138 124 112 101 92		Y DE
Ultimate Bending Moment, ¢ Mn	Kip-Ft. per Unit	39.96	48.76	57.12	64.64		
P/S Strand Area	Sq. In.	0.460	0.575	0.690	0.805		THE LIVE LO
7-Wire 270 Lolax P/S Strand	Combination	4-7/16"¢	6-7/16"¢	6-7/16"≬	7-7/16"♠		* INCLUDES THE LIVE LOAD PLUS
Standard Designation		20_06704	20_06705	20_06706	20_06707		

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- 4. The table indicates maximum safe loads. Camber and deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span so that these factors are compatible with the contiguous materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank is 45 lbs. per sq. ft.

f'c = 5,000 psi f'ci = 3,000 psi

Area =  $173 \text{ in}^2$ 

bw = 10.0 in.

 $I = 719 \text{ in}^4$ 

f'pu = 270,000 psi

E6" x 48" SECTION WITH NO TOPPING



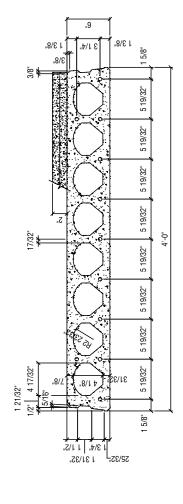
WITH 2" TOPPING (3500 PSI) E6" x 48" SECTION

## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

sw ips r	<u>=</u>	0	0	0	0		
<ul><li>Vcw</li><li>in Kips</li><li>per</li></ul>	.5	12.30	12.30	12.30	12.30		
	33						
	32						
	30 31						
	29						
	28						PPIN
	27						& TO
	26						NKS
	25			69	87		PLA
	24			84	103		UTED
EET	23		78	100	120		GRO
2	22	89	92	119	134		3ARE
PAN	21	82	114	136	150		뿔
E SI	20	105	136	153	168		P
MPL	19	128	155	172	189		HBI
SII	8	155	175	195	207		IE WE
	17	176	199	218	222		흐
	16	201	228	235	240		NAL -
	15	232	250	255	260		OITIO
	4	267	273	278	284		3 ADE
	13	293	599	305	311		AT IS
	12	323	330	336	343		
	=	360	367	374	381		707 C
	10	404 360 323 293 267 232 201 176 155 128	412 367 330 299 273 250 228 199 175 155 136 114	420 374 336 305 278 255 235 218 195 172 153 136 119 100 84	428 381 343 311 284 260 240 222 207 189 168 150 134 120 103		DEAL
Ultimate Bending Moment,	Kip-Ft. per Unit	57.36	70.00	82.16	91.84		D PLUS ANY
P/S Strand Area		0.460	0.575	0.690	0.805		INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS & TOPPING
7-Wire 270 Lolax P/S Strand	Combination	4-7/16"ø	5-7/16"♠	6-7/16"ф	7-7/16"♠		* INCLUDES 1
Standard Designation		20_06704T	20_06705T	20_06706T	20_06707T		

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous and/or engineer for the contemplated loading and span deflection must always be investigated by the architect, 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank & 2" topping is 45+25 = 70 lbs. per sq. ft.

f'c = 5,000 psi

f'ci = 3,000 psi

Area =  $173 \text{ in.}^2$ 

 $lc = 1,580 in.^4$ 

f'pu = 270,000 psi

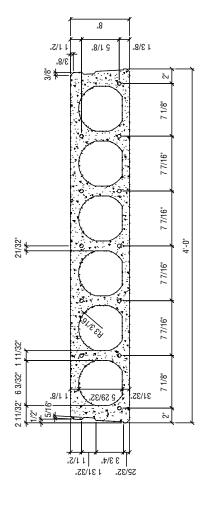
bw = 10.0 in.



## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

<ul><li>Vcw</li><li>in Kips</li><li>per</li></ul>	Onit	12.30	12.30	12.30	12.30	12.30	
	33						
	32						
	31				72	81	
	1 8			69	80	88	
	29			77	88	92	
	28		71	98	96	103	LACE
	27		81	96	104	111	IN P
	26	89	91		112	121	ANKS
	25	77	103	113	122	131	D PL
	24	87	112	123	133	143	
ΉĒΤ	23	163 143 126 112 99 87	398 359 326 298 275 254 226 202 182 164 148 135 123 112 103	460 411 370 337 308 283 262 243 221 199 179 163 148 135 123 113 104	423 381 347 317 292 270 251 234 215 194 176 160 146 133 122 112 104	473 423 381 347 317 292 270 251 234 219 205 188 171 156 143 131 121 111 103	E GR(
<u>Z</u>	22	112	135	148	160	171	BAR
SIMPLE SPAN IN FEET	10 11 12 13 14 15 16 17 18 19 20 21 22 23	126	148	163	176	188	置
E SI	20	143	164	179	194	205	IT OF
MPL	19	163	182	199	215	219	FIG
S	18	182	202	221	234	234	N H.
	17	204	226	243	251	251	101
	16	230	254	262	270	270	DNAL
	15	386 348 316 289 260 230 204 182	275	283	292	292	TIC
	14	289	298	308	317	317	IS AL
	13	316	326	337	347	347	'HAT
	12	348	329	370	381	381	JAD T
	=	386	398	411	423	423	N C
	10	196	446	460	473	473	Y DE/
Ultimate Bending Moment, \$ Mn	Kip-Ft. per Unit	58.88	72.52	85.44	98.04	109.96	AD PLUS AN
P/S Strand Area	Sq. In.	0.460	0.575	069.0	0.805	0.918	* INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS IN PLACE
7-Wire 270 Lolax P/S Strand	Combination	4-7/16"¢	5-7/16"¢	6-7/16"ф	7-7/16"φ	6-1/2"¢	* INCLUDES
Standard Designation	,	20_08704	20_08705	20_08706	20_08707	20_08806	

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank is 54 lbs. per sq. ft.

f'c = 5,000 psi

f'pu = 270,000 psi

f'ci = 3,000 psi

Area =  $207 \text{ in.}^2$ 

bw = 10.0 in. $l = 1,580 \text{ in.}^4$ 

WITH NO TOPPING E8" x 48" SECTION



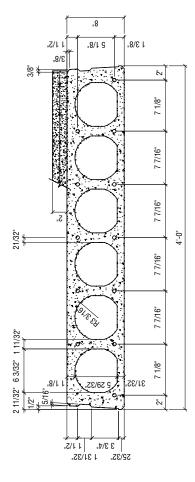
WITH 2" TOPPING (3500 PSI) E8" x 48" SECTION

## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

¢ Vcw in Kips per	Onit	16.01	16.01	16.01	16.01	16.01	
	33						
	32					74	
	31				71	98	
	30				82	86	
	29			9/	92	112	G
	28 29		29	06	109	125	PPIN
	27		80		125	137	& T0
	26	89	96	121	139	150	NKS
	25	83	112	139	152	165	PLA
	24	100	131 112	153	168	182	
SIMPLE SPAN IN FEET	10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	243 213 436 395 361 331 301 265 234 205 179 157 138 119 100	495 445 403 368 338 312 289 263 234 209 188 170 152	504 453 411 375 345 318 295 274 256 232 208 187 169 153 139 121 104	577 514 462 419 383 352 325 301 280 261 245 227 205 185 168 152 139 125 109	577 514 462 419 383 351 324 301 280 261 245 230 216 200 182 165 150 137 125 112	GRO
<b>Z</b>	22	138	170	187	205	216	3ARE
PAN	21	157	188	208	227	230	뿔
IS	20	179	209	232	245	245	든
MPL	19	205	234	256	261	261	EIGH.
S	8	234	263	274	280	280	F W
	17	265	289	295	301	301	2
	16	301	312	318	325	324	MAL
	15	331	338	345	352	351	을
	14	361	368	375	383	383	SADE
	13	395	403	411	419	419	AT !!
	12	436	445	453	462	462	₽ T
	=	213	495	504	514	514	0 [0
	10	243	248	999	277	277	DEA
Ultimate Bending Moment, Moment,	Kip-Ft. per Unit	76.28	93.72	110.36	126.48	141.92	D PLUS ANY
P/S Strand Area	Sq. In.	0.460	0.575	0.690	0.805	0.918	THE LIVE LOA
7-Wire 270 Lolax P/S Strand	Combination	4-7/16"ø	5-7/16"≬	6-7/16"≬	7-7/16"≬	6-1/2"♠	* INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS & TOPPING
Standard Designation		20_08704T	20_08705T	20_08706T	20_08707T	20_08806T	

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous and/or engineer for the contemplated loading and span deflection must always be investigated by the architect, 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank & 2" topping is 54+25 = 79 lbs. per sq. ft.

f'c = 5,000 psi

f'ci = 3,000 psi

 $lc = 3,072 in.^4$ 

f'pu = 270,000 psi

Area =  $207 \text{ in.}^2$ 

bw = 10.0 in.



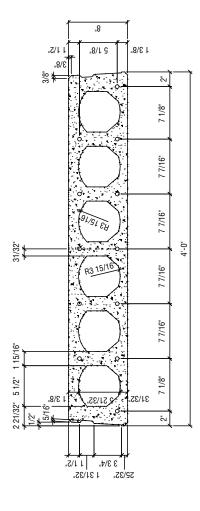
## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT. WITH NO TOPPING

H8" x 48" SECTION

Standard 270 Lolax Strand Moment, Area Moment, P/S Strand Combination P/S Strand O.690 58.88 222 421 367 224 228 259 234 210 182 169 139 122 107 94 83 73 500 8706 6-7/16" 0.690 85.44 633 566 511 456 384 200 8806 6-1/2" 0.9806 6-1/2" 0.9918 110.12 649 581 525 478 438 400 354 316 284 285 231 193 177 163 148 132 177 163 148 132 177 163 148 132 177 163 148 132 177 163 148 148 132 177 163 148 148 148 148 148 148 148 148 148 148	φ Vcw in Kips per	28 29 30 31 32 33	16.93	16.93	81 72 16.93	95 85 76 68 16.93	108 97 87 78 16.93	
7-Wire P/S Bending 270 Lolax Strand Area \$\text{Moment,}\$ P/S Strand Area \$\text{Moment,}\$ P/S Strand Area \$\text{Min-Ft.}\$ P/S Strand Area \$\text{Min-Ft.}\$ P/S Combination Sq. In. \$\text{Pi.Pt.}\$ per Unit 10 11 4-7/16"\$\phi\$ 0.460 58.88 222 421 5-7/16"\$\phi\$ 0.690 85.44 633 566 7-7/16"\$\phi\$ 0.805 98.04 650 581 6-1/2"\$\phi\$ 0.918 110.12 649 581	EET	25 26	83	98 86		166 148 132 118 100	177 163 148 133 120	
7-Wire P/S Bending 270 Lolax Strand Area \$\text{Moment,}\$ P/S	IMPLE SPAN IN FI	19 20 21 22	159 139 122 107	206 181 160 142	225 204 186 165	7 241 219 199 182	256 232 211 193	
7-Wire P/S Bending 270 Lolax Strand Area \$\text{Moment,}\$ P/S Strand Area \$\text{Moment,}\$ P/M P/S Strand Area \$\text{Moment,}\$ P/M P/S Strand Area \$\text{Moment,}\$ P/M P/S Strand Area \$\text{Moment,}\$ P/S Strand Area \$Moment	03	14 15 16 17 18	89 259 234 210 182	64   323   287   257   230	98 350 310 277 249	27 376 333 297 267	38 400 354 316 284	
7-Wire P/S Bending 270 Lolax Strand Moment, P/S Strand Area \$\theta\$ Mn Kip-Ft. Combination Sq. In. Per Unit 4-7/16"\$\phi\$ 0.460 58.88 5-7/16"\$\phi\$ 0.690 85.44 7-7/16"\$\phi\$ 0.805 98.04 6-1/2"\$\phi\$ 0.918 110.12		10 11 12 13	222 421 367 324 2	609 526 461 408 3	633 566 511 456 3	581	581	
7-Wire 270 Lolax P/S Strand Combination 4-7/16"\$\phi\$ 6-7/16"\$\phi\$ 6-1/2"\$\phi\$ 0			58.88	72.52	85.44	98.04	110.12	
1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2			30_08704 4-7/16"(	30_08705 5-7/16"(	30_08706 6-7/16"0	30_08707 7-7/16"(	30_08806   6-1/2"\$	

## NOTES

- 1. Design Standard: ACI 318-2005
- For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- 4. The table indicates maximum safe loads. Camber and deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span so that these factors are compatible with the contiguous materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank is 60 lbs. per sq. ft.

f'c = 5,000 psi f'ci = 3,000 psi

Area =  $230 \text{ in.}^2$ 

bw = 13.77 in.

 $I = 1,667 \text{ in.}^4$ 

f'pu = 270,000 psi



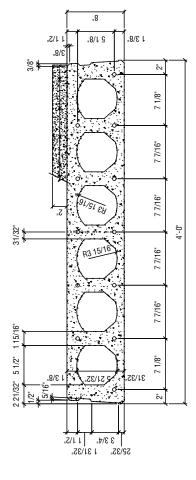
WITH 2" TOPPING (3500 PSI) H8" x 48" SECTION

## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

<ul><li>Vcw</li><li>in Kips</li><li>per</li></ul>	Unit	22.04	22.04	22.04	22.04	22.04	
⊕ .⊑		22	22	22	22	22	
	2 33						
	1 32					0	
	31					8	
	30				75	3 92	
	59			89	3 86	100	NG
	28			82	103	122	OPPI
	27		72	1 97	116	136	% T
	26		88	114	137	158	ANKS
	25	9/	105	133	157	180	D PL
	24	93	678 593 524 467 420 379 337 298 261 229 199 171 146 124	789 704 635 577 528 469 413 367 327 294 265 234 204 177 153 133 114 97	802 716 646 587 538 495 446 396 353 317 285 258 234 205 180 157 137 119 103 89	802   716   646   587   538   495   458   423   377   339   305   276   251   228   204   180   158   139   122   106	JUE
SIMPLE SPAN IN FEET	23	112	146	177	205	228	E GR(
2	22	133	171	204	234	251	BARE
PAN	21	152	199	234	258	276	뿔
LE S	20	175	229	265	285	305	T OF
MP	19	200	261	294	317	339	EIGH
S	18	231	298	327	353	377	씨
	17	266	337	367	396	423	T0T
	16	299	379	413	446	458	NAL
	15	331	420	469	495	495	
	10 11 12 13 14 15 16 17 18 19 20 21	472 416 370 331 299 266 231 200 175 152	467	528	538	538	S ADI
	13	416	524	277	287	287	1AT
	12	472	593	635	646	646	4D T
	=		8/9	704	716	716	0 [0
	10	283 239	356	789	802	802	DEA
Ultimate Bending Moment, \$ Mn	Kip-Ft. per Unit	76.28	93.76	110.36	126.52	141.92	D PLUS ANY
P/S Strand Area	Sq. In.	0.460	0.575	0.690	0.805	0.918	INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS & TOPPING
7-Wire 270 Lolax P/S Strand	Combination	4-7/16"φ	5-7/16"¢	6-7/16"φ	7-7/16"φ	6-1/2"¢	* INCLUDES T
Standard Designation		30_08704T	30_08705T	30_08706T	30_08707T	30_0880GT	

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous and/or engineer for the contemplated loading and span deflection must always be investigated by the architect, 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank & 2" topping is 60+25 = 85 lbs. per sq. ft.

f'c = 5,000 psi

f'ci = 3,000 psi

Area =  $230 \text{ in.}^2$ 

bw = 13.77 in.

 $lc = 3,143 in.^4$ 

f'pu = 270,000 psi

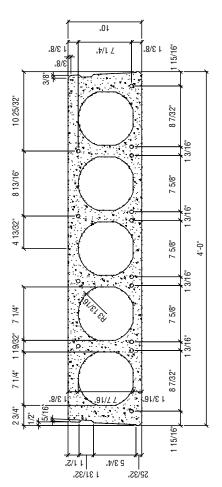


## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

φ Vcw in Kips per	Unit	16.01	16.01	16.01		
	38			82		
	37		70	87		
	36		77	66		
	35		85	66		
	4			413 383 355 332 310 291 274 259 245 225 207 191 177 164 152 141 131 122 114 106 99		
	33	92	363 337 314 294 276 259 240 219 201 185 170 157 145 134 125 116 108 100 93	114		2
	32	85	108	122		2
	31	98	116	131		NINO
	30	105	125	141		2
	29 30	115 105	134	152		H
SIMPLE SPAN IN FEET	28	189 173 159 146 135 124	145	164		00
2	27	135	157	177		0 4 0
PAN		146	170	191		H
E SI	24 25 26	159	185	207		12
MPL	24	173	201	225		2
S	23	189	219	245		1
	22	207	240	259		5
	21	228	259	274		
	16 17 18 19 20 21 22	343 318 297 277 251 228 207	276	291		Ė
	19	277	294	310		2
	18	297	314	332		į
	17	318	337	355		2
	16	343	363	383		2
	15	371	392	413		2
Ultimate Bending Moment,	•	1		180.08		ואי טון ומ טיי
P/S Strand Area	Sq. In.	0.690	0.920	1.150		TUELIVELO
7-Wire 270 Lolax P/S Strand	Combination	6-7/16"¢	8-7/16"φ	10-7/16"φ		* INICI INEC THE LIVE LOAD HE ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE DADE CODITED BLANKE IN BLACE
Standard Designation	)	20_10706	20_10708			-

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- Shaded region indicates expected camber greater than 1".



Grouted weight of plank is 67 lbs. per sq. ft.

f'c = 5,000 psi

f'ci = 3,000 psi

 $I = 3,080 \text{ in.}^4$ 

f'pu = 270,000 psi

Area =  $257 \text{ in.}^2$ 

bw = 10.0 in.

E10" x 48" SECTION WITH NO TOPPING



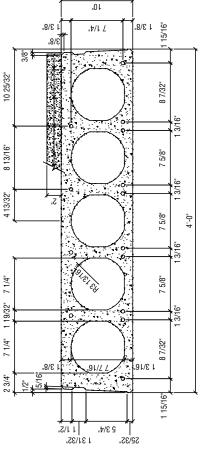
WITH 2" TOPPING (3500 PSI) E10" x 48" SECTION

## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

ø Vcw in Kips per	Unit	19.72	19.72	19.72		
	38			80		
	37			90		
	36		72	101		
	35		83	112		
	34		95	122		] ر
	33	29	107	132		NIda
	32	79	120	143		Z Z
	31	93	134	154		NKO
	30	107	145	167		۵
	29	123	158	181		
Ë	28	141	172	197		S PO
<u> </u>	27	158	187	214		A B F
PAN	26	172	204	231		불
E SI	25	189	223	243		2
SIMPLE SPAN IN FEET	24	208	245	256		I H
S	23	228	260	271		×
	22	252	276	287		
	21	279	293	305		
	15     16     17     18     19     20     21     22     23     24     25     26     27     28     29     30     31     32     33     34     35     36     37	431 398 369 343 320 300 279 252 228 208 189 172 158 141 123 107 93 79	448 414 384 357 333 312 293 276 260 245 223 204 187 172 158 145 134 120 107 95 83	465 429 398 371 346 324 305 287 271 256 243 231 214 197 181 167 154 143 132 122 112 101 90		Ę
	19	320	333	346		עע עע
	18	343	357	371		¥
	17	369	384	398		
	16	398	414	429		
	15	431	448	465		1
Ultimate Bending Moment, \$ Mn	Kip-Ft. per Unit	138.96	179.64	218.44		TO DITIS ANY DEAD I DAD THAT IS ADDITIONAL TO THE WEIGHT OF THE RABE GROUTED BLANKS & TODDING
P/S Strand Area		0.690	0.920	1.150		INCLLINES THE LIVE LOAD PLII
7-Wire 270 Lolax P/S Strand	Combination	6-7/16"♠	8-7/16"♠	10-7/16"ø		* INCLINES
Standard Designation		20_10706T	20_10708T	20_10710T		

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous and/or engineer for the contemplated loading and span deflection must always be investigated by the architect, 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are
- 6. Shaded region indicates expected camber greater than 1".



Grouted weight of plank & 2" topping is 67+25 = 92 lbs. per sq. ft.

f'c = 5,000 psi

f'ci = 3,000 psi

Area =  $257 \text{ in.}^2$ 

bw = 10.0 in.

 $lc = 5,238 in.^4$ 

f'pu = 270,000 psi

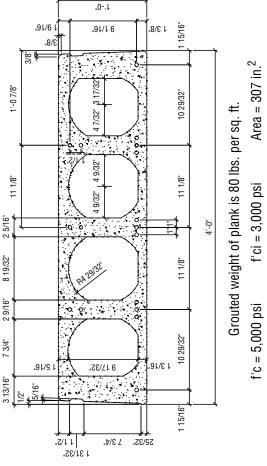


## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

Sq. In. Mip-Ft. Sq. In. Ber Unit 2	٠, ۵	7-Wire 270 Lolax P/S Strand	P/S Strand	Ultimate Bending Moment,										SII	/IPLE	SIMPLE SPAN IN FEET	N N	出っ	Ь											<ul><li>Vcw</li><li>in Kips</li></ul>
0.805	- ర	ombination	Sq. In.	Kip-Ft. per Unit		21		23	24	25			78	29	30	3	3	3	33	36	3 37	38	39	40	4	42	43		45	Unit
0.805 164.52 403 367 337 311 286 266 244 222 202 183 166 151 183 125 113 102 92 83 75 9 81 73 7 9 9 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	ė	-7/16"♠	0.690	142.08	377	343	307	276	248	224 (	203	184	167	51	37 1	25 1-	13 10	33		_										28.10
0.920 186.08 427 390 357 328 303 281 260 243 224 186 170 155 142 129 118 108 98 89 81 73 7 7 7 7 7 7 7 8 8 8 8 8 8 8 8 8 8 8	7.	-7/16"φ	0.805		403	367	337	311	286	7997	244 ;	222	202	83	1 99	51 13	38 12	25 11	3 10	2 92	83	_								28.10
1.035 206.92 451 412 377 346 320 295 274 256 238 223 205 187 142 157 144 132 121 111 102 93 85 78 78 70 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	œ	-7/16"φ	0.920		427	390	357	328	303	281	7 097	243 2	224 2	1 40	86 1	70 15	55 14	12 12	1	8 10	86 8	_	_							28.10
1.071 213.36 459 419 384 353 326 301 279 259 242 226 211 193 177 163 149 137 126 115 106 97 89 81 74 7 80 73 76 346 320 297 276 257 240 224 211 197 182 168 155 143 131 121 112 103 95 87 80 73 78 73 74 75 75 75 75 75 75 75 75 75 75 75 75 75	6	-7/16"¢	1.035		451	412	377	346	320	295 ;	274 ;	256	238 2	23 2	105	87 17	72 15	57 14	13	2 12	+	1 102	93			70				28.10
1.224 240.36 489 446 409 376 346 320 297 276 257 240 224 211 197 182 168 155 143 131 121 112 103 95 87 80 73	7	'-1/2"φ	1.071		459	419	384	353	326	301	279	259 2	242 2	26 2	111	93 17	77 16	33 17	13	7 12	6 11	2 106	97		_	74				28.10
	8	3-1/2"φ	1.224	240.36	489	446	409	376	346	320 2	297	3 9 2 3	257 2	40 2	24 2	11 19	97 18	32 16	15	5 14	3 13	1 12	1112	103	92	87	80	73		28.10

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- 6. Shaded region indicates expected camber greater than 1".



 $I = 5,246 \text{ in.}^4$ 

f'pu = 270,000 psi

bw = 14.25 in.

E12" x 48" SECTION WITH NO TOPPING



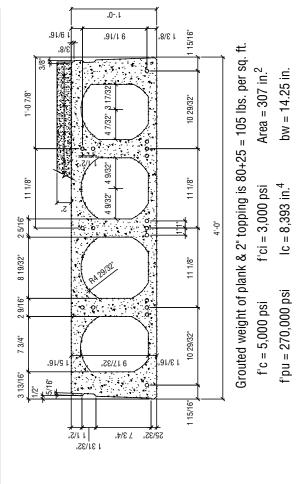
WITH 2" TOPPING (3500 PSI) E12" x 48" SECTION

## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

cw r	<u></u>	69	39	69	33	39	60	
<ul><li>Vcw</li><li>in Kips</li><li>per</li></ul>	Ď	33.39	33.39	33.39	33.39	33.39	33.39	
	45							
	44							
	43						2/3	
	42						83	
	40 41 42					23	66	
					8/	84	104	<u>ن</u>
	39			72	88	92	115	PPIN
	38			83	101	107	127	8 TO
	37		22	92	114	119	141	NKS
	36		87	108	127	133	155	) PLA
_	35	78	100	122	141	147	170	
	34	90	114	137	156	163	188	GRC
	33	104	129	153	173	180	206	BARE
PAN	32	120	146	170	192	190	226	뿔
SIMPLE SPAN IN FEET	31	208 188 170 154 136 120	444 404 371 340 307 278 252 229 206 184 164 146 129 114 100	<i>472 431</i> 395 362 334 310 286 259 233 210 189 170 153 137 122 108 95 83	500 456 418 384 354 327 302 281 259 234 212 192 173 156 141 127 114 101	309 286 266 243 220 190 180 163 147 133 119	533 497 455 418 385 356 329 306 285 265 248 226 206 188 170 155 141 127 115 104 93	T OF
IMPI	99	154	184	210	234	243	265	(EIGH
S	29	170	206	233	259	266	285	HE W
	28	188	229	259	281	286	306	101
	27	208	252	286	302	309	329	JNAL
	26	284 256 231	278	310	327	333	356	Ĭ
	25	256	307	334	354	391 361 333	385	IS AD
	24	284	340	362	384	391	418	HAT
	23	395 353 317	371	395	418	465 426	455	JAD 1
	22	353	404	431	456	465	497	\D [C
	21	395	444	472	200	510	533	Y DE
	20	444	487	519	550	260	268	SAN
Ultimate Bending Moment, \$ Mn	Kip-Ft. per Unit	167.28	192.96	217.56	241.64	249.08	280.20	E LOAD PLU
P/S Strand Area	Sq. In.	0.690	908.0	0.920	1.035	1.071	1.224	* INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS & TOPPING
7-Wire 270 Lolax P/S Strand	Combination	6-7/16"♠	7-7/16"♠	8-7/16"₽	9-7/16"♠	7-1/2"♠	8-1/2"¢	* INCLU
Standard Designation		20_12706T	20_12707T	20_12708T	20_12709T	20_12807T	20_12808T	

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- Shaded region indicates expected camber greater than 1".





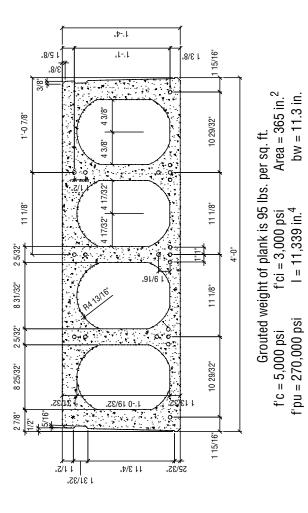
## E16" x 48" SECTION WITH NO TOPPING

# UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

¢ Vcw in Kips per	Unit	30.67	30.67	30.67	30.67	30.67	30.67	
	22					75	84	
	54					80	06	
	53				22	98	96	
	52				81	95	103	
	21			73	87	66	312 293 276 260 245 232 219 207 196 186 176 167 159 151 144 136 130 124 117 110 103 96	
	20			80	94	106	117	
	49 50			87	101	121 113 106	124	
	48		74	96	108	121	130	ACF
	47		8		150 142 134 125 116 108	298 280 263 248 234 221 209 197 187 177 168 159 151 143 136 129	136	N N
	9	75	89	156 148 138 128 119 110 102	125	136	144	ANKS
	1 45 4	82	26	119	134	143	151	l l
	4	91	106	128	142	151	159	
SIMPLE SPAN IN FEET	43	66	115 106	138	150	159	167	F GR(
<u>=</u>	42 ,	9	125	148	158	168	176	BAR
PAN	41	119 10	135	156	167	177	186	불
E S	40 41	141 130	229 215 202 190 180 169 158 146 135 125	175 165	176 167	187	196	늘
MPI	39	141	158	175	186	197	207	VFIG
S	38		169	185	197	209	219	IHE V
	37	179 166 153	180	196	209	221	232	Ė
	36	179	190	208	221	234	245	OAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED PLANKS IN PLACE
	35	191	202	266 250 235 221 208 196 185	235 221 209 197	248	260	I
	34	230 216 203	215	235	266 250	263	276	S A
	33	216	229	250	266	280	293	THAT
	32	230	244	266	283	298	312	J. OAD
	31	246	260	284	302	318	333	AD
	29 30 31	263	298 279 260	304	345 322 302	363 339 318	355	N PF
	29	281 263 246	298	325 304 284	345	363	380 355 333	IS AN
Ultimate Bending Moment, \$ Mn	Kip-Ft. per Unit	261.12	292.16	341.84	379.44	416.12	452.04	/F I OAD PI I
P/S Strand Area	Sq. In.	0.920	1.035	1.224	1.377	1.530	1.683	* INCLUDES THE LIVE LOAD PLUS ANY DEAD I
7-Wire 270 Lolax P/S Strand	Combination	8-7/16"♠	9-7/16"♠	8-1/2"¢	9-1/2"¢	10-1/2"¢	11-1/2"¢	* INCL
Standard Designation		20_16708	20_16709	20_16808	20_16809	20_16810	20_16811	

## NOTES

- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- Shaded region indicates expected camber greater than 1".



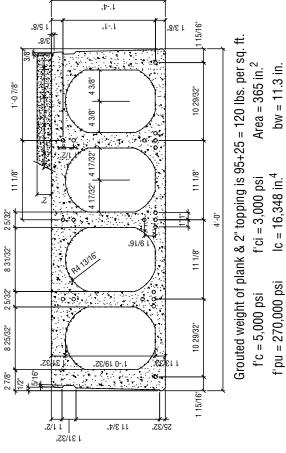


WITH 2" TOPPING (3500 PSI) E16" x 48" SECTION

## UNIFORMLY DISTRIBUTED SUPERIMPOSED\* LOAD IN LBS. PER SQ. FT.

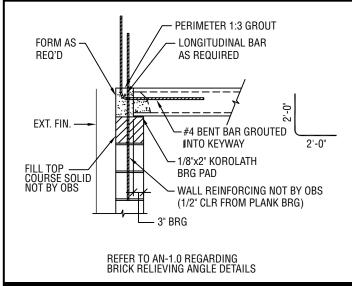
φ Vcw in Kips per	49 50 51 52 53 54 55	34.87	34.87	76 34.87	96 86 77 34.87	111 102 94 86 78 34.87	356 334 313 294 276 260 245 231 218 205 194 183 173 164 155 146 136 126 116 107 99 91 83 76 34.87	
	44 45 46 47 48			95 85	263 247 232 218 205 193 182 172 160 147 136 125 114 105	339 317 297 279 262 247 232 218 206 194 183 173 163 154 142 131 121	146 136	
	45 46	70	77   78	166 152 140 128 117 106	136 125	154 142	164 155	
EI	3 44	80	86	.0 128 ·	147	73 163	3 173	1
SIMPLE SPAN IN FEET	40 41 42 43	101 90	209 196 179 164 149 135 122 110	152 14	172 16	183 17	194 18	0 1 0 1
: SPAN	10 41	27 114	49 135	80 166	93 182	06 194	18 205	1
IMPLE	39	173 156 141 127 114 101	164 1	300 281 263 246 231 217 203 192 180	205 1	218 2	231 2	!
05	37 38	73 156	179   179	217 203	232 218	247 232	260 245	
	36	191	4 209 1	3 231 2	3 247 2	9 262 2	4 276 2	
	34 35	256 240 224 209	255 238 224	263 246	281 26	297 279	313 294	1
	33	6 240	3 255 3	0 281	320 300	9 317	6 334 3	
	31 32	275 250	293 273	322 30	343 320	362 33	381 35	
	30	318 295 2	338 314 2	370 345	394 367	408 388 3	418 400	
ate ng int,	t. nit 29							
Ultimate Bending Moment, \$ Mn	Kip-F per U	293.52	327.52	380.72	422.84	464.12	504.56	
P/S Strand Area		0.920	1.035	1.224	1.377	1.530	1.683	
7-Wire 270 Lolax P/S Strand	Combination	8-7/16"♠	0-7/16"₽	8-1/2"≬	9-1/2"¢	10-1/2"ø	11-1/2"ø	*
Standard Designation	1	20_16708T	20_16709T	20_16808T	20-16809T	20_16810T	20_16811T	

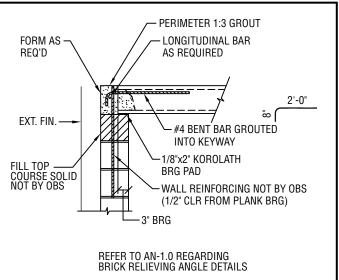
- 1. Design Standard: ACI 318-2005
- 2. For complete and detailed calculations consult Oldcastle Precast.
- 3. For longer spans, heavier loads, or special conditions, consult Oldcastle Precast.
- so that these factors are compatible with the contiguous deflection must always be investigated by the architect, and/or engineer for the contemplated loading and span 4. The table indicates maximum safe loads. Camber and materials in the proposed structure.
  - 5. Values to the left and below the heavy stepped line are controlled by shear.
- 6. Shaded region indicates expected camber greater than 1".



 $lc = 16,348 in.^4$ 

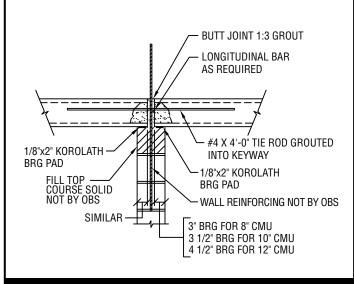
bw = 11.3 in.

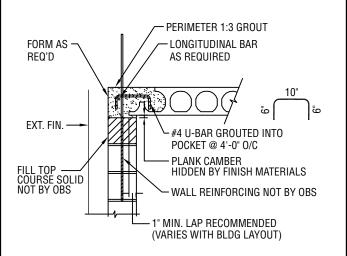




## E1.0 Exterior Bearing (Typ. Flr.)

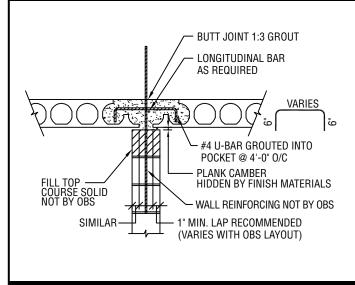
## E2.0 Exterior Bearing (Roof)

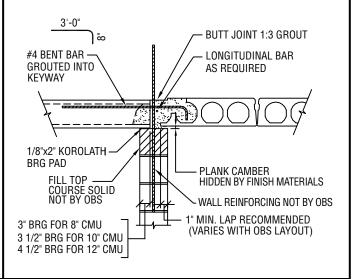




## E3.0 Interior Bearing

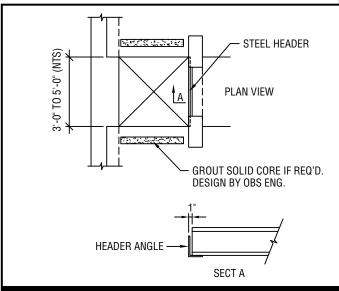
## E4.0 Exterior Side Lap

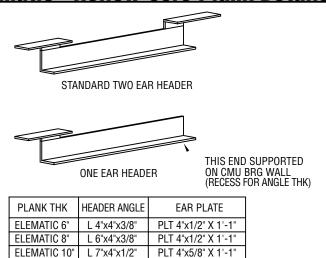




E5.0 Interior Shear Wall

E6.0 Interior Change of Direction



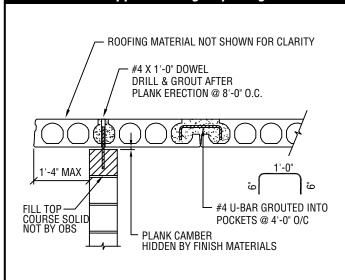


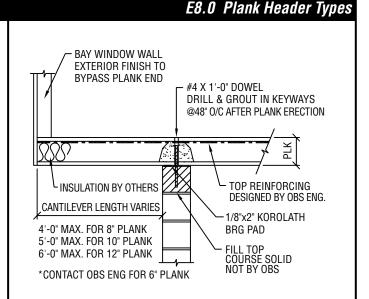
PLT 4"x3/4" X 1'-1"

ELEMATIC 12"

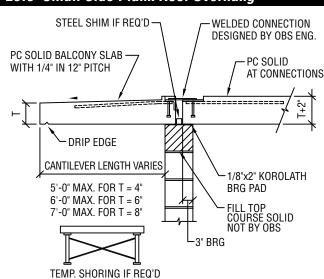
L 8"x4"x1/2"

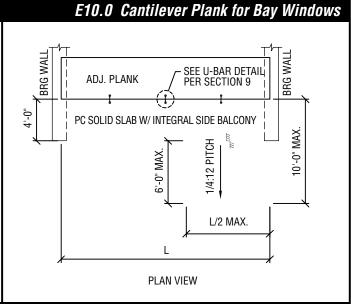
## E7.0 Header Support at Large Opening





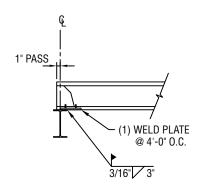
## E9.0 Small Side Plank Roof Overhang



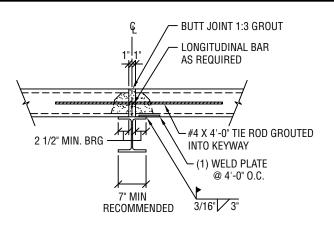


## E11.0 Cantilever Solid Slab Balconies

E12.0 Side Cantilever Balconies



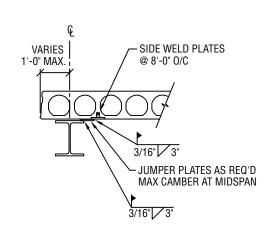
IOTE: DO NOT WELD BOTH ENDS OF THE SAME PLANK
IF RESTRAINT IS EXCESSIVE. WELDING ALTERNATING
PLANKS WILL STILL PROVIDE LATERAL BEAM BRACING.

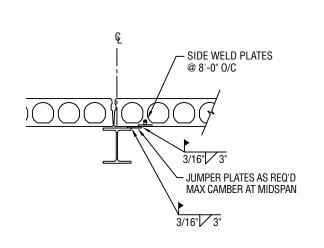


NOTE: DO NOT WELD BOTH ENDS OF THE SAME PLANK
IF RESTRAINT IS EXCESSIVE. WELDING ALTERNATING
PLANKS WILL STILL PROVIDE LATERAL BEAM BRACING.

## E13.0 End Bearing on Steel

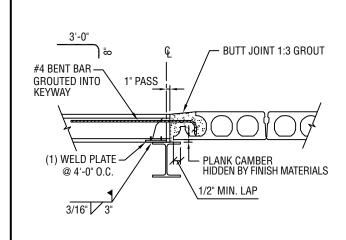
## E14.0 Interior Bearing on Steel

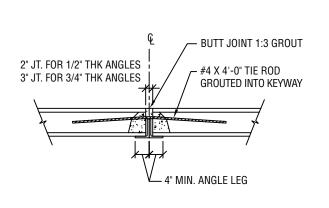




## E15.0 Exterior Side Lap on Steel

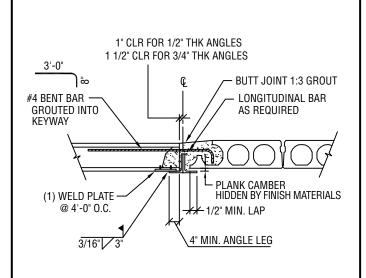
## E16.0 Interior Side Lap on Steel

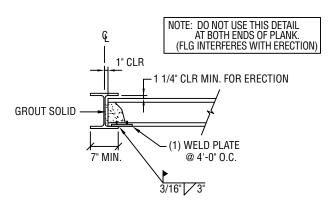




E17.0 Interior Change of Direction

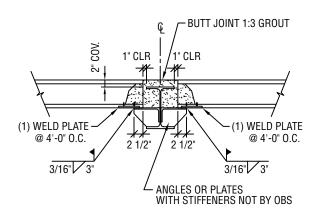
E18.0 Angle Support at Corridors





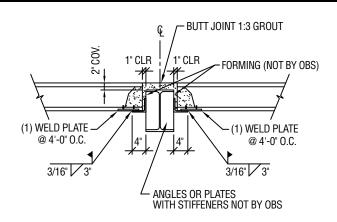
NOTE: DO NOT WELD BOTH ENDS OF THE SAME PLANK IF RESTRAINT IS EXCESSIVE. WELDING ALTERNATING PLANKS WILL STILL PROVIDE LATERAL BEAM BRACING.

## E19.0 Change of Direction on Angles



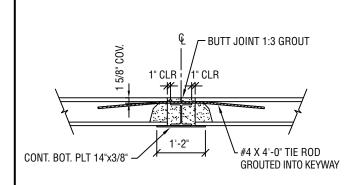
NOTE: DO NOT WELD BOTH ENDS OF THE SAME PLANK IF RESTRAINT IS EXCESSIVE. WELDING ALTERNATING PLANKS WILL STILL PROVIDE LATERAL BEAM BRACING.

## E20.0 End Bearing on Upset Steel

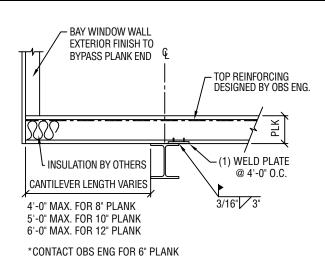


NOTE: DO NOT WELD BOTH ENDS OF THE SAME PLANK IF RESTRAINT IS EXCESSIVE. WELDING ALTERNATING PLANKS WILL STILL PROVIDE LATERAL BEAM BRACING.

## E21.0 Interior Bearing on Upset Steel (1)

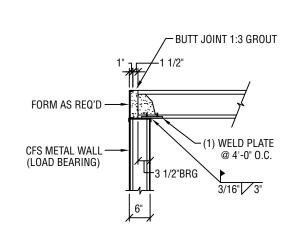


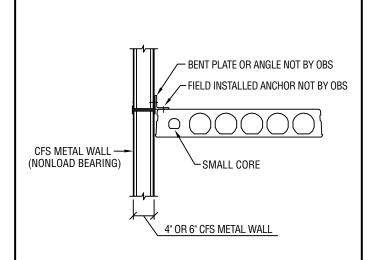
## E22.0 Interior Bearing on Upset Steel (2)



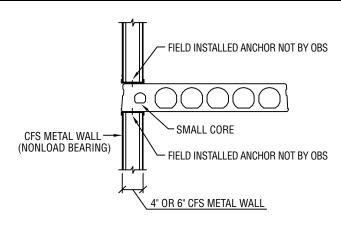
E23.0 Interior Bearing on Upset Steel (3)

E24.0 Cantilever Plank for Bay Windows



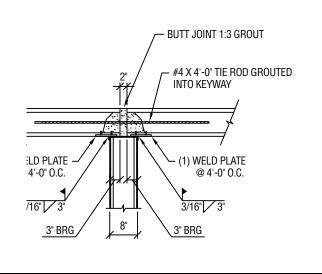


## E25.0 Exterior Bearing on Metal Stud

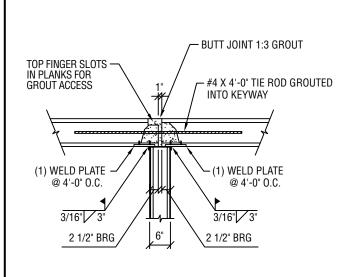


SHIMMING OF METAL STUDS REQ'D TO ADJUST FOR PLANK CAMBER

## E26.0 Exterior Bypass Side on Metal Stud

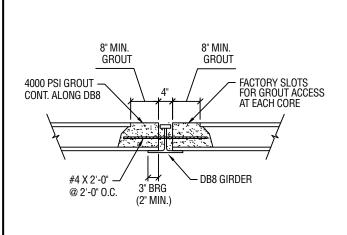


## E27.0 Exterior Side Lap on Metal Stud

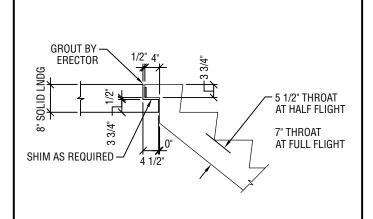


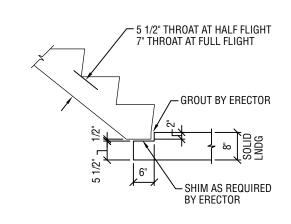
E29.0 Interior Bearing on 6" Metal Wall

## E28.0 Interior Bearing on 8" Metal Wall



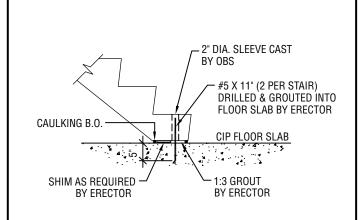
E30.0 Typ. Girder-Slab System

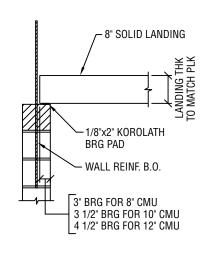




## E31.0 Precast Stair Landing & Stair Down

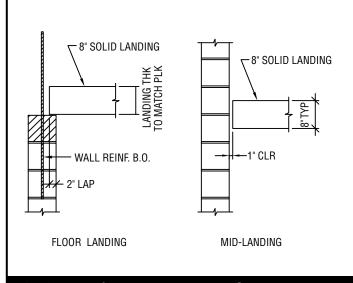
E32.0 Precast Stair Landing & Stair Up

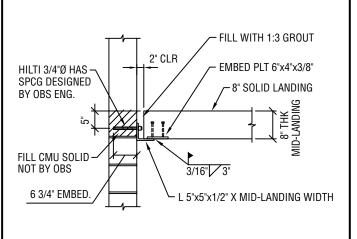




## E33.0 Precast Stair at Ground Slab

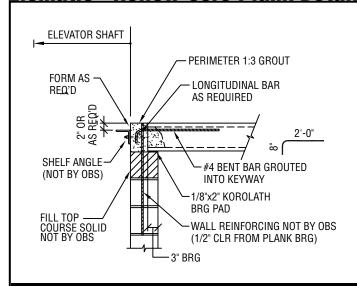
E34.0 Floor Landing End Bearing

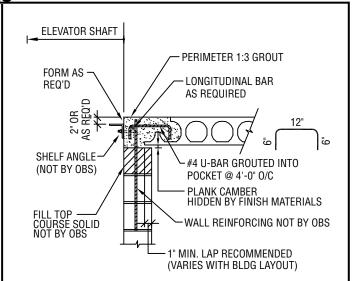




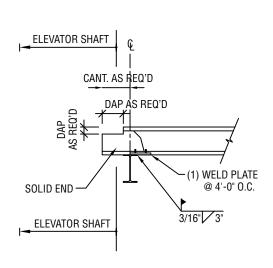
E35.0 Floor & Mid-Landing Back Side Lap

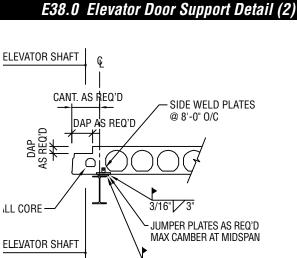
E36.0 Mid-Landing Support Angle





E37.0 Elevator Door Support Detail (1)

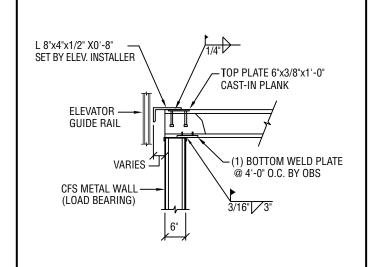




3/16" 3"

E40.0 Elevator Door Support Detail (4)

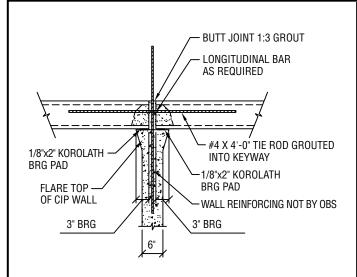
E39.0 Elevator Door Support Detail (3)



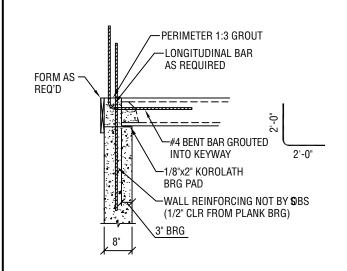
E41.0 Elevator Stud & Plank at Elevator Wall

## PERIMETER 1:3 GROUT LONGITUDINAL BAR AS REQUIRED #4 BENT BAR GROUTED INTO KEYWAY 2'-0" 1/8"x2" KOROLATH BRG PAD WALL REINFORCING NOT BY OBS (1/2" CLR FROM PLANK BRG) 3" BRG

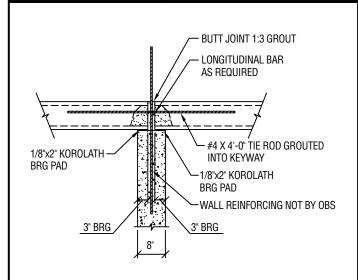
E42.0 Exterior Bearing on 6" ICF Wall



## E43.0 Interior Bearing on 6" ICF Wall



## E44.0 Exterior Bearing on 8" ICF Wall

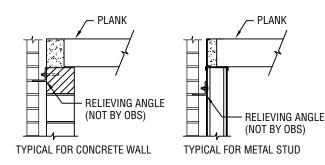


OLDCASTLE BUILDING SYSTEMS (OBS) DOES NOT SUPPLY OR INSTALL BRICK RELIEVING ANGLES.

IF GROUT AND INSTALLION OF PLANK IS TO BE PERFORMED BY OBS THEN THE CONTRACTOR IS TO REFRAIN FROM INSTALLING BRICK RELIEVING ANGLES UNTILL THE WORK HAS BEEN COMPLETED. ESPECIALLY IN SITUATIONS WHERE THE ANGLE WOULD HINDER OBS FROM PERFORMING THE AGREED UPON SCOPE OF WORK.

ALL BRICK RELIEVING ANGLES SHOULD BE ANCHORED INTO THE WALL SYSTEM (SEE SECTIONS BELOW), WHICH HAS BEEN DESIGNED TO ACCOUNT FOR SUCH LOADING. DO NOT INSTALL RELIEVING ANGLES INTO GROUT OR ATTACH DIRECTLY TO THE HOLLOW-CORE (PLANK).

IF YOU NEED ADDITIONAL INFORMATION OR ASSISTANCE PLEASE CONTACT THE OLDCASTLE BUILDING SYSTEMS ENGINEERING DEPARTMENT.



E45.0 Interior Bearing on 8" ICF Wall

AN-1.0 Brick Relieving Angle

oldcastleprecast.com/buildingsystems

Phone: (800) 523-3747