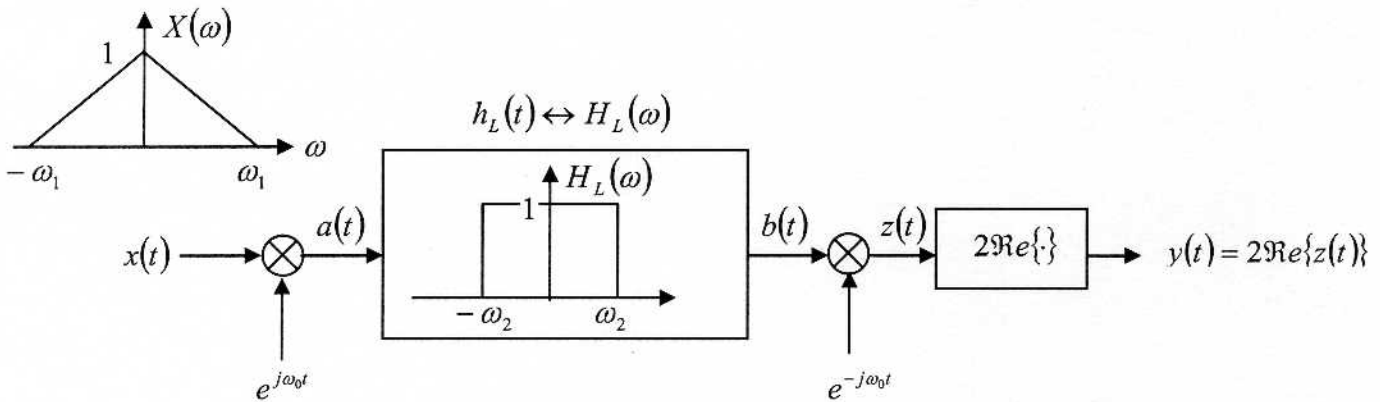


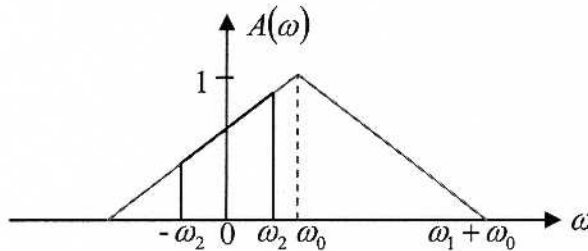
1(50). Show that the system below is basically the bandpass filter:

$$H_{BP}(\omega) = \frac{Y(\omega)}{X(\omega)} = H_L(\omega - \omega_0) + H_L(\omega + \omega_0).$$

Assume that $x(t)$ and $h(t)$ are real. Also, $y(t) = z(t) + z^*(t) \leftrightarrow Y(\omega) = Z(\omega) + Z^*(-\omega)$.



For example,



$$a(t) = x(t)e^{j\omega_0 t} \leftrightarrow A(\omega) = \frac{1}{2\pi} X(\omega) * 2\pi \delta(\omega - \omega_0) = X(\omega - \omega_0)$$

$$B(\omega) = A(\omega) H_L(\omega)$$

$$z(t) = b(t)e^{-j\omega_0 t} \leftrightarrow Z(\omega) = \frac{1}{2\pi} B(\omega) * 2\pi \delta(\omega + \omega_0) = B(\omega + \omega_0)$$

$$y(t) = 2\Re\{z(t)\} = \mathcal{Z}\left(\frac{z(t) + z^*(t)}{2}\right) \leftrightarrow Y(\omega) = Z(\omega) + Z^*(-\omega)$$

Now work backwards

1 cont.

$$\tilde{I}(\omega) = \cancel{Z(\omega)} + \cancel{Z^*(-\omega)} = \cancel{B(\omega + \omega_0)} + \cancel{B^*(-\omega + \omega_0)}$$

$$A(\omega + \omega_0) H_L(\omega + \omega_0)$$

$$A^*(\omega + \omega_0) H_L^*(-\omega + \omega_0)$$

But $h_L(t)$ is real

$$\therefore h_L(t) = h_L^*(t) \Rightarrow H_L(\omega) = H_L^*(-\omega)$$

becomes

$$H_L^*(-(\omega - \omega_0)) = H_L(\omega - \omega_0)$$

Thus

$$\tilde{I}(\omega) = A(\omega + \omega_0) H_L(\omega + \omega_0) + A^*(-\omega + \omega_0) H_L(\omega - \omega_0)$$

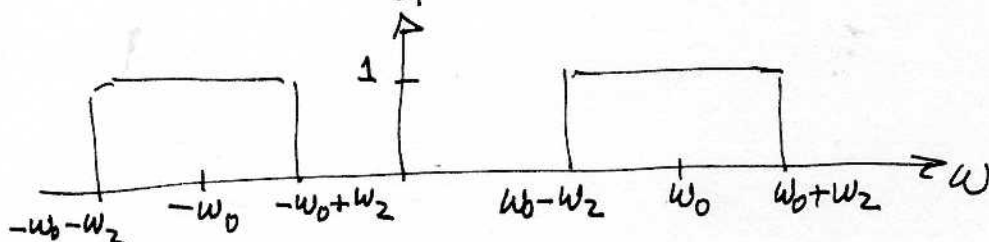
$$\text{Subs. } A(\omega) = \tilde{X}(\omega - \omega_0)$$

$$\tilde{I}(\omega) = \cancel{A(\omega + \omega_0)} \tilde{X}(\omega - \omega_0 + \omega_0) H_L(\omega + \omega_0) + \tilde{X}^*(-\omega + \omega_0 - \omega_0) H_L(\omega - \omega_0)$$

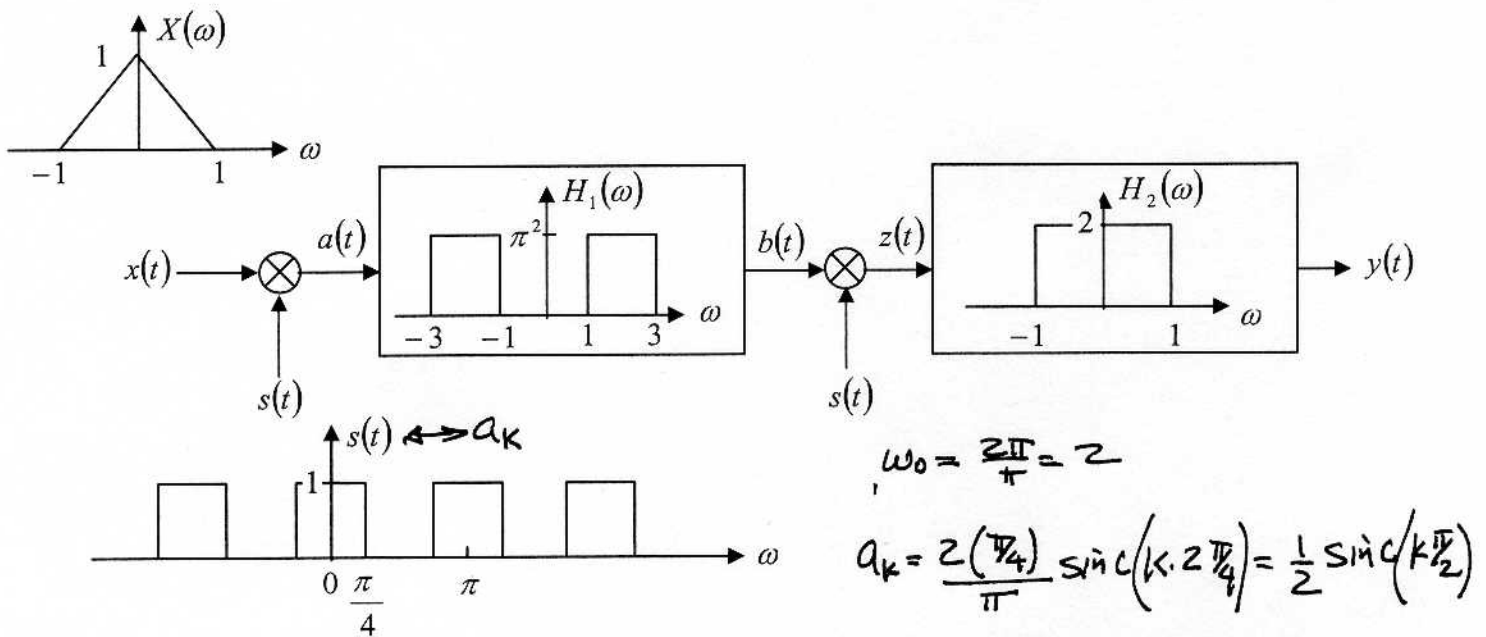
But $x(t)$ is real

$$\therefore x(t) = x^*(t) \Rightarrow \tilde{X}(\omega) = \tilde{X}^*(-\omega) \quad \text{becomes} \quad \tilde{X}(\omega)$$

$$\therefore \tilde{I}(\omega) = \tilde{X}(\omega) \underbrace{[H_L(\omega + \omega_0) + H_L(\omega - \omega_0)]}_{H_{BP}(\omega)}$$



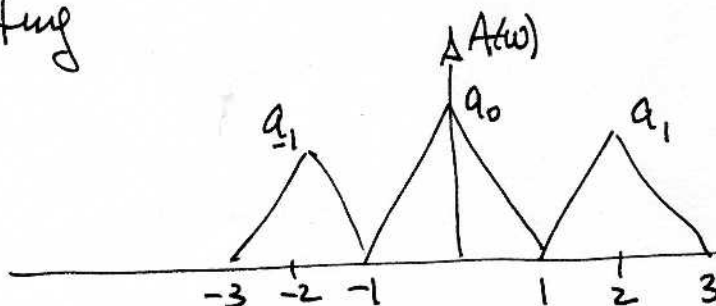
2(50). The block diagram below represents a chopper stabilized amplifier used to amplify low frequency signals such as those found in transducer outputs. Assume the frequency range of $x(t)$ is given by the Fourier transform $X(\omega)$ shown. Find the overall gain of the amplifier over the frequency range of interest.



$$\text{Now } s(t) = \sum_{k=-\infty}^{\infty} a_k e^{jk2t} \leftrightarrow S(\omega) = \sum_{k=-\infty}^{\infty} a_k 2\pi \delta(\omega - 2k)$$

$$\begin{aligned} \text{Then } a(t) &= x(t) s(t) \leftrightarrow A(\omega) = \frac{1}{2\pi} X(\omega) * S(\omega) \\ &= \frac{1}{2\pi} X(\omega) * \sum_{k=-\infty}^{\infty} a_k 2\pi \delta(\omega - 2k) \\ &= \sum_{k=-\infty}^{\infty} a_k X(\omega - 2k) \end{aligned}$$

Plotting

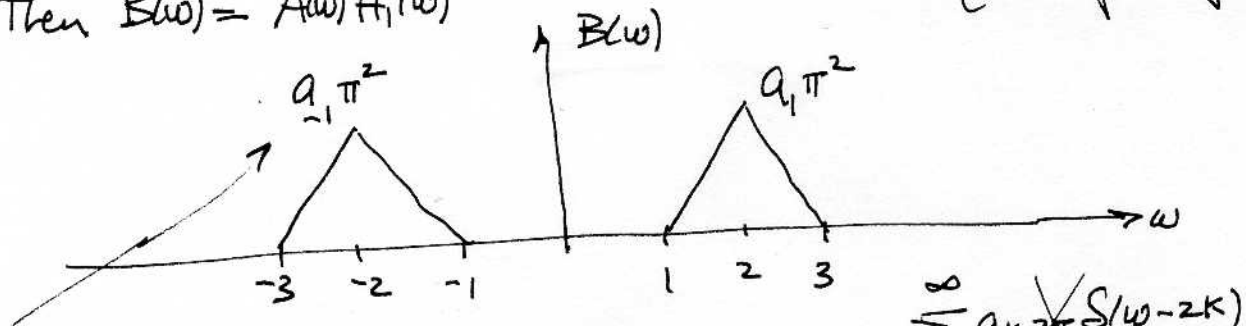


No need to plot other terms because $H_1(\omega)$ filters them out, along with $X(\omega)$.

2. Continued.

$$\text{Then } B(\omega) = A(\omega) H_1(\omega)$$

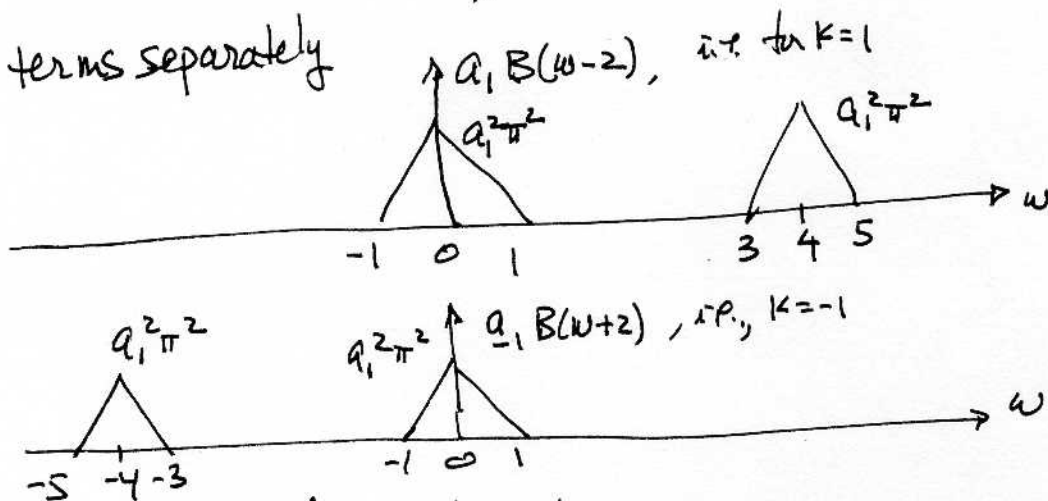
(π^2 is filter gain)



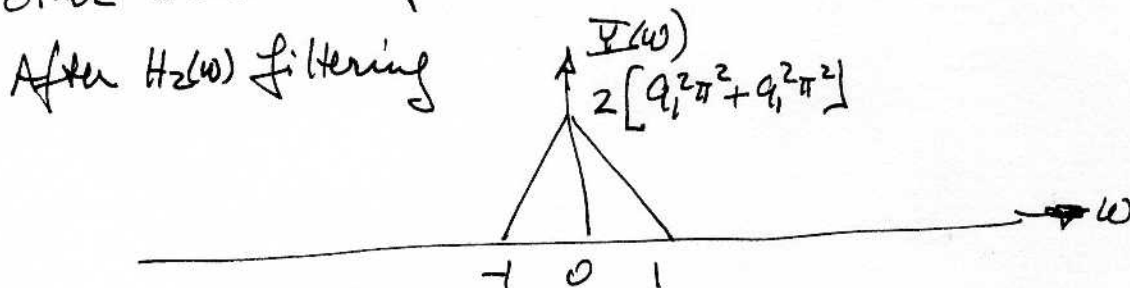
note $x(t)$ real & even $\therefore a_{-1} = a_1$

$$\begin{aligned} \text{Now } Z(t) = x(t) S(t) &\leftrightarrow Z(\omega) = \frac{1}{2\pi} B(\omega) * S(\omega) \\ &= \sum_{k=-\infty}^{\infty} a_k B(\omega - 2k) \end{aligned}$$

Plot terms separately



other terms are filtered out



$$\text{But } a_1 = \frac{1}{2} \text{sinc}\left(\frac{\pi}{2}\right) = \frac{1}{2} \frac{\sin(\pi/2)}{\pi/2} = \frac{1}{\pi}$$

$$\therefore \text{Gain} = 2 \left[\frac{1}{\pi^2} \pi^2 + \frac{1}{\pi^2} \pi^2 \right] = \boxed{4}$$