Case	Description of Element		Shear Lag Factor, <i>U</i>	Example
1	mitted directly to eac	where the tension load is trans- h of the cross-sectional elements s (except as in Cases 4, 5 and 6).	<i>U</i> = 1.0	-
2	tension load is trans the cross-sectional longitudinal welds ir welds. Alternatively,	s, except HSS, where the smitted to some but not all of elements by fasteners or by a combination with transverse Case 7 is permitted for W, is. (For angles, Case 8 is d.)	$U=1-\frac{\overline{x}}{l}$	\overline{x} \overline{x} \overline{x}
3		s where the tension load is transverse welds to some but sectional elements.	$U = 1.0$ and $A_n =$ area of the directly connected elements	-
4 [a]	and W-shapes with the tension load is t	nnels with welds at heels, tees, connected elements, where ransmitted by longitudinal se 2 for definition of \overline{x} .	$U = \frac{3l^2}{3l^2 + w^2} \left(1 - \frac{\overline{x}}{l} \right)$	W Plate or connected element
5	Round HSS with a single concentric gusset plate through slots in the HSS.		$l \ge 1.3D, \ U = 1.0$ $D \le l < 1.3D, \ U = 1 - \frac{\overline{x}}{l}$ $\overline{x} = \frac{D}{\pi}$	D
6	Rectangular HSS.	with a single concentric gusset plate	$l \ge H, \ U = 1 - \frac{\overline{x}}{l}$ $\overline{x} = \frac{B^2 + 2BH}{4(B+H)}$	B
		with two side gusset plates	$l \ge H, \ U = 1 - \frac{\overline{x}}{l}$ $\overline{x} = \frac{B^2}{4(B+H)}$	H B
shapes from th (If <i>U</i> is	W-, M-, S- or HP- shapes, or tees cut from these shapes. (If <i>U</i> is calculated	with flange connected with three or more fasteners per line in the direction of loading	$b_f \ge \frac{2}{3} d$, $U = 0.90$ $b_f < \frac{2}{3} d$, $U = 0.85$	_
	per Case 2, the larger value is per- mitted to be used.)	with web connected with four or more fasteners per line in the direction of loading	<i>U</i> = 0.70	-
8	Single and double angles.	with four or more fasteners per line in the direction of loading	<i>U</i> = 0.80	-

	gusset piate tirrough siots in the 155.		$D \le l < 1.3D$, $U = 1 - \frac{x}{l}$ $\overline{x} = \frac{D}{\pi}$	D
6	Rectangular HSS.	with a single concentric gusset plate	$l \ge H, \ U = 1 - \frac{\overline{x}}{l}$ $\overline{x} = \frac{B^2 + 2BH}{4(B+H)}$	H - B
		with two side gusset plates	$l \ge H, \ U = 1 - \frac{\overline{x}}{l}$ R^2	H - 1

B = overall width of rectangular HSS member, measured 90° to the plane of the connection, in. (mm); D = outside diameter of round HSS, in. (mm); H = overall height of rectangular HSS member, measured in the plane of the connection, in. (mm); d = depth of section, in. (mm); for tees, d = depth of the section from which the tee was cut, in. (mm); l = length of connection, in. (mm); w = width of plate, in. (mm); \overline{x} = eccentricity of connection, in. (mm).

U = 0.60

(If U is calculated

per Case 2, the

is permitted to

larger value

be used.)

with three fasteners per line in

fewer than three fasteners per

line in the direction of loading,

use Case 2)

 $^{[a]}$ $_l=rac{l_1+l_2}{2}$, where l_1 and l_2 shall not be less than 4 times the weld size.

the direction of loading (with