

# NE585 – Nuclear fuel cycle analysis

## Project 4 – Nuclear reactor theory

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# 1 Neutron multiplication factor

(25)

Find the neutron multiplication factor for a fuel of (1) 90%  $^{235}\text{U}$  and 10%  $^{238}\text{U}$ , (2) pure  $^{239}\text{Pu}$ , and (3) pure  $^{233}\text{U}$  for thermal neutrons. Do the same for fast neutrons ( $\sim 2 \text{ MeV}$ ). Calculate  $\eta$ ; don't just look it up in the book. Assume  $\epsilon p$  is approximately unity

*Comment on any major characteristics of these results in terms of fast v thermal reactors.*

## 2 Enrichment

(30)

What is the minimum  $^{235}\text{U}$  enrichment needed for a critical assembly of a homogenous core of  $^{235}\text{U}$  and  $^{238}\text{U}$ ? Assume  $\epsilon p$  is approximately unity and a thermal core. Comment on the results.

*This is kind of a trick question.*

### 3 Fissioning your electricity bill

(25)

What is the fission rate, in fissions per day, for a 1000 MWe reactor? Assume 200 MeV is released per fission and 35% reactor efficiency. If 1.16 atoms of  $^{235}\text{U}$  are consumed per fission, then how many atoms are consumed per day due to fission? How many grams of  $^{235}\text{U}$  per day is this? Given how much your last monthly electric bill was, how much  $^{235}\text{U}$  did you consume per day? Assume uranium costs (\$100/kg.)

*Comment on the results.*

## 4 Neutron flux and current density

(25)

Derive the expression for neutron flux and current density for a point source [ $S$  n/s] in an infinite vacuum [ $D = 0$ ]. Think physically about what is going on.

## 5 Neutron flux and geometry I

(30)

If three isotropic point sources of equal strength in an infinite *medium* are located at three corners of an equilateral triangle with sides of length  $a$ , what is the flux and current at the midpoint of one side of the triangle? The center of the triangle?

*D does not equal zero here.*

## 6 Maximum flux

(30)

For the infinite, bare slab geometry of thickness  $[2a]$  with source  $S$   $n/cm^2/s$ , *derive* the flux and the maximum flux. In the 2nd edition, it's on p203, eq. 5.41, but should be just around there in the other editions. Neglect the extrapolated distance.

## 7 Two group theory

(25)

For the infinite bare slab geometry again, assume a fast, constant *point source*  $s \text{ n/cm}^2/\text{s}$ , derive explicit expressions for the fast and the thermal flux using two group diffusion theory as follows –

$$D_1 \nabla^2 \phi_1 - \Sigma_A^1 \phi_1 - \Sigma_{1 \rightarrow 2} \phi_1 + \Sigma_{2 \rightarrow 1} \phi_2 + s = 0 \quad (1)$$

$$D_2 \nabla^2 \phi_2 - \Sigma_A^2 \phi_2 - \Sigma_{2 \rightarrow 1} \phi_2 + \Sigma_{1 \rightarrow 2} \phi_1 = 0 \quad (2)$$

Hints and tips –

- (a) There is only a fast source. Leave it as  $s$ .
- (b) Don't worry about boundary conditions. Leave in the constants and just get the general solution.
- (c) Don't assume either absorption cross section is zero.

*This differential equation system is very common to many engineering problems. There is a standard solution approach that can be found with some research. The solution procedure is not tricky, but it can be tedious.*



## 8 Neutron flux and geometry II

(30)

Derive the flux for a rectangular parallelepiped. See the section on the slab reactor, 6.2 in the second edition and assume a separable solution. Show the buckling. Compute maximum to average flux.

## 9 Critical geometry

(25)

What is the critical size of the previous parallelepiped reactor for a homogeneous mixture of  $^{239}\text{Pu}$  and  $\text{Na}$ , with atom densities of  $0.00395 \times 10^{24}$  and  $0.0234 \times 10^{24}$ , respectively. Make assumptions on the relationship between the x, y, z dimensions. Neglect extrapolation distance.

## 10 Critical mass

(25)

A spherical thermal reactor of  $R = 50$  cm contains a homogenous core of  $^{235}\text{U}$  and water. Find the mass of  $^{235}\text{U}$ . It is reflected by graphite. Find the new critical mass. Use room temperature; i.e., standard cross sections.

## 11 Reactivity equation

(30)

Derive the reactivity equation. Work through the derivation in the book (or wherever) and explain the steps sufficiently in terms of the physics of what is going on.

$$\rho = \frac{\omega l_P}{1 + \omega l_P} + \frac{\omega}{1 + \omega l_P} \cdot \frac{\beta}{\omega + \lambda} \quad (3)$$

Prove that  $\omega$  is the reciprocal of the stable period with math. Why is there an asymptote at  $\rho = 1$ ? What does that mean physically?

## 12 Reactor period

(25)

Plot reactor period versus absolute value of reactivity for  $l_P = 10^{-6}, 10^{-5}, \dots, 10^{-1}$  seconds for the six groups of delayed neutrons for fast fission in  $^{235}\text{U}$ . What observations can be drawn regarding *reactor operation*? Compare to the figure at the beginning of chapter 7 (The Time-Dependent Reactor). It's 7.2 in the 2nd edition.

## 13 Delayed neutrons

(30)

Using the six group reactivity equation for  $^{235}\text{U}$ , show with math that for increasingly negative reactivity, the period is limited (controlled) by the decay of the longest lived precursor. At about what reactivity does this occur? What is the period (*the actual number*)?

## 14 Neutron poison production

(30)

Solve for the  $^{135}\text{Xe}$  and  $^{135}\text{I}$  concentrations *analytically*, assuming a constant, average thermal flux of  $10^{14} \text{ n/cm}^2/\text{s}$ . Plot the concentration as a function of time and note any important trends from  $t = 0$  to 500 h. From  $t = 0$  to 200 h, the reactor operates at full power. The reactor is instantaneously scrammed at  $t = 200$  h. Assume a reactor with solely  $^{235}\text{U}$  with no resonance absorbers or fissionable material. (Just solve the two equations and make whatever simplifying assumptions).

## 15 Reactor operation

(15)

What is the period for a critical reactor?



## 16 BONUS – Xenon equilibrium time

(50)

What is the equilibrium time for  $^{135}\text{Xe}$ ?

*Show with math.*

## Tables

## Figures