

# NE585 – Nuclear fuel cycle analysis

## Project 4a – Burnup & Depletion

Name

University of Idaho • Idaho Falls Center for Higher Education

Nuclear Engineering and Industrial Management Department

email

2023.08.08

# 1 Plutonium production

(100)

Solve the Pu-239 production equation. See Appendix I and Table 1 for guidance.

## 2 Fission product production I

(100)

Solve for fission product production for U-235 and Pu-239.

### 3 Burnup

(100)

Plot  $NvB$  for U-235, U-238, Pu-239, and the fission products all together. Compare to Fig. 3.29 from Benedict in Appendix II. Don't worry that the graph is  $B$  v  $w$ ; the shape of the curves should be similar.

## 4 Fission product production II

(100)

Compute and plot the production and decay of Cs-137 and Sr-90 for an irradiation time of 24 months and a cooling time of 25 years.

## Tables

Table 1	Burnup & depletion data . . . . .	6
---------	-----------------------------------	---

**Table 1.** Burnup & depletion data

initial fuel mass	99.2 MTU
enrichment	3.2%
$\bar{\phi}$	$3.5 \times 10^{13} \frac{n}{cm^2 \cdot s}$
$\epsilon$	1.0476
$P_F$	0.9889
$p$	0.772
$\sigma_{25}$	555.6 b
$\sigma_{28}$	2.23 b
$\sigma_{49}$	1618.2 b
$\sigma_{40}$	2616.8 b
$\sigma_{41}$	1567.3 b
$\sigma_{42}$	381 b
$\eta_{25}$	1.96
$\eta_{28}$	2.3432
$\eta_{49}$	1.86
$\eta_{41}$	3.06
$\alpha_{25}$	0.2398
$\alpha_{28}$	0.1907
$\alpha_{49}$	0.5430
$\alpha_{41}$	0.3765

## Figures



## Appendix I: Equations

$$\begin{aligned}
\frac{dN_{49}}{d\theta} &= N_{28}^0 \sigma_{28} + \kappa_{25} N_{25} \sigma_{25} - \gamma_{49} N_{49} \sigma_{49} \\
N_{49}(0) &= 0 \\
\kappa_m &= \eta_m \epsilon P_F (1 - p) + \eta_m \frac{\alpha_{28}}{1 + \alpha_{28}} \cdot \frac{\epsilon - 1}{\eta_{28} - 1} \\
\gamma_m &= 1 - \kappa_m \\
N_{49}(\theta) &= C_1 (1 - e^{-\sigma_{49} \gamma_{49} \theta}) + C_2 (e^{-\sigma_{25} \theta} - e^{-\sigma_{49} \gamma_{49} \theta}) \\
C_1 &= \frac{N_{28}^0 \sigma_{28}}{\sigma_{49} \gamma_{49}} \\
C_2 &= \frac{\kappa_{25} N_{25}^0 \sigma_{25}}{\sigma_{49} \gamma_{49} - \sigma_{25}}
\end{aligned} \tag{1}$$

$$\begin{aligned}
\frac{dN_{25}^F}{d\theta} &= \frac{1}{1 + \alpha_{25}} N_{25} \sigma_{25} \\
N_m^F(0) &= 0
\end{aligned} \tag{2}$$

$$\begin{aligned}
\frac{dN_{49}^F}{d\theta} &= \frac{1}{1 + \alpha_{49}} N_{49} \sigma_{49} \\
N_m^F(0) &= 0
\end{aligned} \tag{3}$$

$$\begin{aligned}
B &= 9.5 \times 10^5 \cdot w \\
w &= \frac{235N_{25}^F + 238N_{28}^F + 239N_{49}^F + 241N_{41}^F}{235N_{25}^0 + 238N_{28}^0}
\end{aligned} \tag{4}$$

$$\begin{aligned}
N_i(T + C) &= e^{-\lambda_i C} [Y_{25}^i N_{25}^F(T) + Y_{49}^i N_{49}^F(T)] \\
N_i(0) &= 0
\end{aligned} \tag{5}$$

## **Appendix II: Burnup graph**

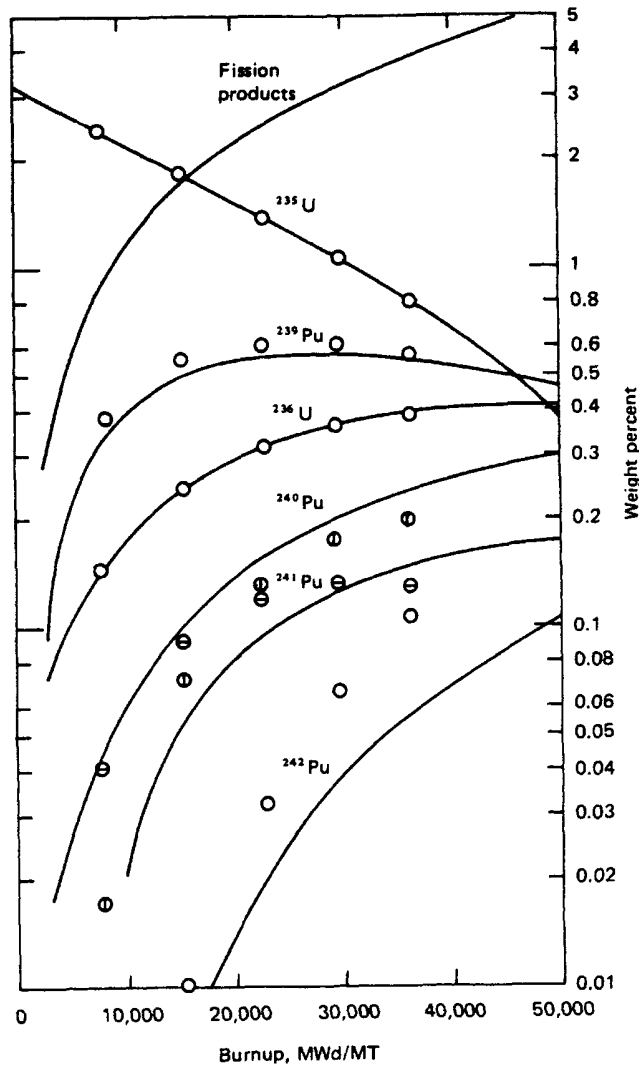


Figure 3.29 Change of nuclide concentrations in PWR with burnup. (○) Equations of this chapter; (⊗)  $^{240}\text{Pu}$ , equations of this chapter; (⊙)  $^{241}\text{Pu}$ , equations of this chapter; (—) computer code CELL.

concentration increases, as a result of its very high absorption cross section at resonance energies, an effect that the equations of this chapter cannot take into account.

### 6.7 Reactivity Changes in PWR

Despite the inability of these equations to represent accurately the concentration of higher plutonium isotopes, the reactivity-limited burnup attainable from fuel initially containing 3.2