

# Analog CMOS Integrated Circuit Design Cheat Sheet

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## Model of MOS Transistors

Process parameters ( $n, V_{TH}, KP, V_E$ ):

$$t_{OX} = \frac{L_{min}}{50} \quad (1)$$

$$t_{si} = \sqrt{\frac{2\epsilon_{si}(\Phi - V_{BD})}{qN_B}} \quad (2)$$

$$C_{OX} = \frac{\epsilon_{OX}}{t_{OX}} \quad (3)$$

$$C_D = \frac{\epsilon_{si}}{t_{si}} \quad (4)$$

$$KP = \mu C_{OX} \quad (5)$$

$$\beta = KP \frac{W}{L} \quad (6)$$

$$Q_{dep} = \sqrt{4q\epsilon_{si}|\Phi_F|N_{sub}} \quad (7)$$

$$V_{TH0} = \Phi_{MS} + 2\Phi_F + \frac{Q_{dep}}{C_{OX}} \quad (8)$$

$$V_{TH} = V_{TH0} + \gamma(\sqrt{|2\Phi_F| + V_{BS}} - \sqrt{|2\Phi_F|}) \quad (9)$$

$$n = \frac{\gamma}{\sqrt{|2\Phi_F| + V_{BS}}} = 1 + \frac{C_D}{C_{OX}} \quad (10)$$

In linear region:

$$I_{DS} = \beta[(V_{GS} - V_{TH})V_{DS} - \frac{1}{2}V_{DS}^2] \quad (11)$$

$$R_{on} = \frac{1}{\beta(V_{GS} - V_{TH})} \quad (12)$$

Channel-Length modulation in saturation region:

$$K' = \frac{KP}{2n} \quad (13)$$

$$\lambda = \frac{1}{V_E L} \quad (14)$$

$$I_{DS} = K' \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS}) \quad (15)$$

$$r_o = \frac{\partial V_{DS}}{\partial I_{DS}} \approx \frac{1}{\lambda I_{DS}} = \frac{V_E L}{I_{DS}} \quad (16)$$

Saturation region has three distinctive regions: weak-inversion (exponential region), strong-inversion, and velocity saturation.

## Value Examples In 0.35μm Process Nodes

Names	Symbols	Values
dielectric constant of sub-silicon	$\epsilon_{si}$	1 pF/cm
dielectric constant of gate-oxide	$\epsilon_{OX}$	0.34 pF/cm
electron charge	$q$	$1.6 \times 10^{-19}$ C
minium channel length	$L_{min}$	0.35 μm
width of gate-oxide	$t_{OX}$	0.1 nm
width of depletion layer	$t_{si}$	7 nm
junction built-in voltage	$\Phi$	0.6 V
drain-bulk voltage	$V_{BD}$	-3.3V
gate-oxide capacitance	$C_{OX}$	0.5 μF/cm <sup>2</sup>
depletion layer capacitance	$C_D$	0.1 μF/cm <sup>2</sup>
bulk doping level	$N_B$	$4 \times 10^{17}$ cm <sup>-3</sup>
P type mobility rate	$\mu_p$	250 cm <sup>2</sup> /Vs
N type mobility rate	$\mu_n$	600 cm <sup>2</sup> /Vs
N type KP	$KP_n$	300 μA/V <sup>2</sup>
	$n$	1.2...1.5
	$ 2\Phi_F $	0.6 V
	$\gamma$	0.5...0.8 V <sup>1/2</sup>
N type $K'$	$K'_n$	100 μA/V <sup>2</sup>
P type $K'$	$K'_p$	40 μA/V <sup>2</sup>
	$V_{GSTt}$	70 mV
	$v_{sat}$	10 <sup>7</sup> cm/s
	$\theta L$	0.2 μm/V

## Weak-Inversion

$$I_{DS} = I_{D0} \frac{W}{L} e^{\frac{V_{GS}}{n \frac{KT}{q}}} \quad (17)$$

$$g_m = \frac{\partial I_{DS}}{\partial V_{GS}} = \frac{I_{DS}}{n \frac{KT}{q}} \quad (18)$$

## strong-inversion

Ignore channel-length modulation:

$$I_{DS} = K' \frac{W}{L} (V_{GS} - V_{TH})^2 \quad (19)$$

$$g_m = \frac{2I_{DS}}{V_{GS} - V_{TH}} \quad (20)$$

## Transition Point Between Weak-Inversion and Strong-Inversion

The voltage and current at transition point between weak-inversion and strong-inversion:

$$V_{GSt} = 2n \frac{KT}{q} + V_{TH} \quad (21)$$

$$I_{DS t} \approx K' \frac{W}{L} (2n \frac{KT}{q})^2 \quad (22)$$

EKV model, a smooth model for weak-inversion and strong-inversion regions:

$$I_{DS} = K' \frac{W}{L} (V_{GS} - V_{TH})^2 [\ln(1 + e^{\frac{V_{GS}}{V_{GSt}}})]^2 \quad (23)$$

Let:

$$v = \frac{V_{GS}}{V_{GSt}} \quad (24)$$

$$i = \frac{I_{DS}}{I_{DS t}} = [\ln(1 + e^v)]^2 \quad (25)$$

then,

$$v = \ln(e^{\sqrt{i}} - 1) \quad (26)$$

$$V_{GS} - V_{TH} = V_{GSTt} \ln(e^{\sqrt{i}} - 1) \quad (27)$$

where:

$$V_{GSTt} = V_{GSt} - V_{TH} = 2n \frac{KT}{q} \quad (28)$$

When  $v = 1$ ,  $i = 1$ , we also have:

$$I_{DS t} = K' \frac{W}{L} (V_{GSt} - V_{TH})^2 \quad (29)$$

## Velocity Saturation

$$I_{DS} = WC_{OX} v_{sat} (V_{GS} - V_{TH}) \quad (30)$$

$$g_m = WC_{OX} v_{sat} \quad (31)$$

## Transition Point Between Strong-Inversion and Velocity Saturation

A smooth model for strong-inversion and velocity saturation regions:

$$I_{DS} = \frac{K' \frac{W}{L} (V_{GS} - V_{TH})^2}{1 + \theta(V_{GS} - V_{TH})} \quad (32)$$

where:

$$\theta = \frac{\mu}{2n} \frac{1}{v_{sat} L} \quad (33)$$

$\theta L$  is constant:

$$\theta L = \frac{\mu}{2n} \frac{1}{v_{sat}} \quad (34)$$

$$g_{m, sat} = WC_{OX} v_{sat} = \frac{K' W}{\theta L} \quad (35)$$

The voltage and current at transition point between strong-inversion and velocity saturation:

$$V_{GSt} = \frac{1}{\theta} + V_{TH} = 2nL \frac{v_{sat}}{\mu} + V_{TH} \quad (36)$$

$$I_{DS t} = K' W L (2n \frac{v_{sat}}{\mu})^2 \quad (37)$$

## 2nd Order Time-constants and Transfer-Constants (TTCs)

A system with 2 frequency-dependent elements, th transfer function in complex-frequency form:

$$H_s = \frac{a_0 + a_1 s + a_2 s^2}{b_1 s + b_2 s^2} \quad (38)$$

where:

$$a_0 = H^0 \quad (39)$$

$$b_1 = \tau_1^0 + \tau_2^0 \quad (40)$$

$$a_1 = \tau_1^0 H^1 + \tau_2^0 H^2 \quad (41)$$

$$b_2 = \tau_1^0 \tau_2^1 = \tau_2^0 \tau_1^2 \quad (42)$$

$$a_2 = \tau_1^0 \tau_2^1 H^{12} = \tau_2^0 \tau_1^2 H^{12} \quad (43)$$

## General Time-constants and Transfer-Constants (TTCs)

A system with  $N$  frequency-dependent elements, th transfer function:

$$H_s = \frac{a_0 + a_1 s + a_2 s^2 \dots + a_n s^n + \dots}{b_1 s + b_2 s^2 \dots + b_n s^n + \dots} \quad (44)$$

where:

$$a_0 = H^0 \quad (45)$$

$$b_1 = \sum_{i=1}^N \tau_i^0 \quad (46)$$

$$a_1 = \sum_{i=1}^N \tau_i^0 H^i \quad (47)$$

$$b_2 = \sum_{i=1}^{i < j} \sum_{j=i+1}^{j \leq N} \tau_i^0 \tau_j^i \quad (48)$$

$$a_2 = \sum_{i=1}^{i < j} \sum_{j=i+1}^{j \leq N} \tau_i^0 \tau_j^i H^{ij} \quad (49)$$

$$b_n = \sum_{i=1}^{i < j} \sum_{j=i+1}^{j < k} \sum_{k=j+1 \dots}^{k < \dots \leq N} \tau_i^0 \tau_j^i \tau_k^{ij} \dots \quad (50)$$

$$a_n = \sum_{i=1}^{i < j} \sum_{j=i+1}^{j < k} \sum_{k=j+1 \dots}^{k < \dots \leq N} \tau_i^0 \tau_j^i \tau_k^{ij} \dots H^{ijk \dots} \quad (51)$$

and for capacitor,

$$\tau_i^0 = C_i R_i^0 \quad (52)$$

$$\tau_i^{jk \dots} = C_i R_i^{jk \dots} \quad (53)$$

or for inductor,

$$\tau_i^0 = \frac{L_i}{R_i^0} \quad (54)$$

$$\tau_i^{jk \dots} = \frac{L_i}{R_i^{jk \dots}} \quad (55)$$

In the form of zeros and poles:

$$H_s = a_0 \frac{(1 - \frac{s}{z_1})(1 - \frac{s}{z_2}) \dots (1 - \frac{s}{z_m})}{(1 - \frac{s}{p_1})(1 - \frac{s}{p_2}) \dots (1 - \frac{s}{p_n})} \quad (56)$$

## Operational-Amp: Biasing Circuits

