

# 自动驾驶控制算法第三讲

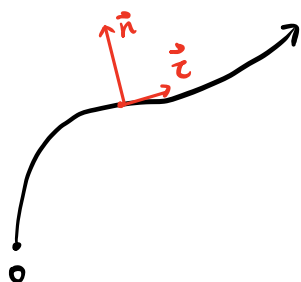
运动学方程  $\dot{x} = v \cos \varphi$

$\dot{y} = v \sin \varphi$

$\dot{\varphi} = \frac{v \tan \delta}{L} \quad \dot{\varphi} = \frac{v}{R} \Rightarrow \frac{1}{R} = \frac{\tan \delta}{L} \quad \tan \delta = \frac{L}{R}$

动力学方程：考虑轮胎特性

当选取 Frenet 坐标系时，可以将纵向控制与横向控制解耦



$\vec{v} = \frac{ds}{dt} \quad \vec{a}_t = \frac{d^2s}{dt^2} \quad a_n = \frac{v^2}{R} = \frac{v^2 \tan \delta}{L}$

$s$  与  $a_t$  直接相关  $a_n$  与  $v, \delta$  有关，当纵向控制稳定以后， $v$  变化不大

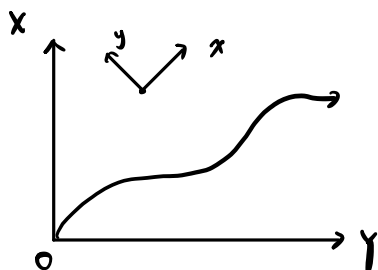
$a_n$  与  $\delta$  有关

运动学  $\begin{cases} \dot{x} = v \cos \varphi \\ \dot{y} = v \sin \varphi \\ \dot{\varphi} = v \frac{\tan \delta}{L} \end{cases} \quad \begin{matrix} v \\ \delta \end{matrix} \Rightarrow \dot{\varphi} \Rightarrow \varphi \Rightarrow \begin{matrix} \dot{x} \\ \dot{y} \end{matrix} \Rightarrow \begin{matrix} x \\ y \end{matrix}$

动力学 + Frenet 坐标系  $a_t \Rightarrow s$   
 $\delta \Rightarrow d$  解耦

$a_t = \frac{d^2s}{dt^2}$

$d = f(v, \delta)$



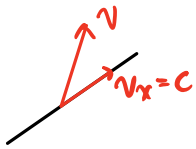
首先建立  $y = f(v, \delta)$   
动力学方程  
再建立  $y = g(d)$   
坐标变换

$\Rightarrow d = h(v, \delta)$

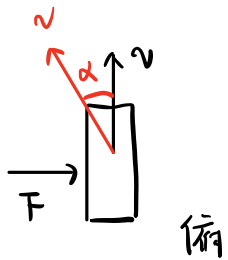
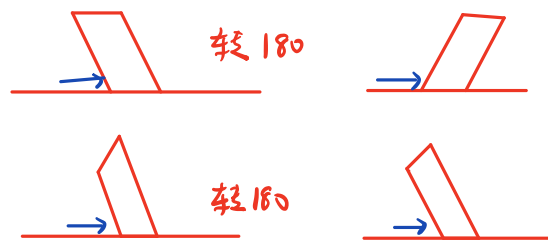
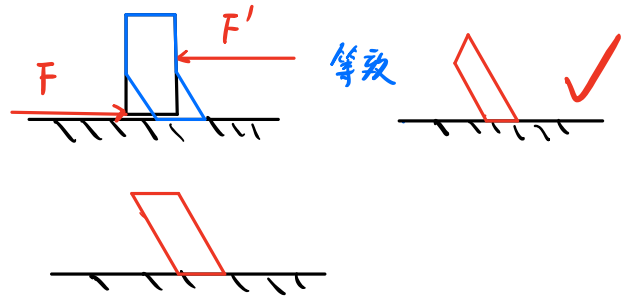
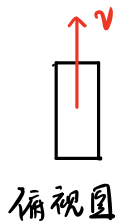
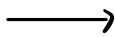
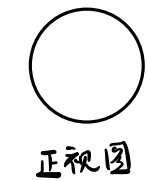
$x$	$s$
$y$	$d$
$\dot{x}$	$\dot{s}$
$\dot{y}$	$\dot{d}$

二自由度车辆动力学方程

假设前轮转角  $\delta$  较小，假设  $v_x = C$



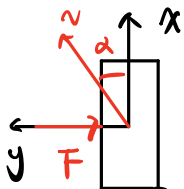
## 轮胎的侧偏特性



$\alpha$  侧偏角 定义  $F = C\alpha$  C 侧偏刚度

侧偏刚度  $\times$  侧偏角 = 侧向力

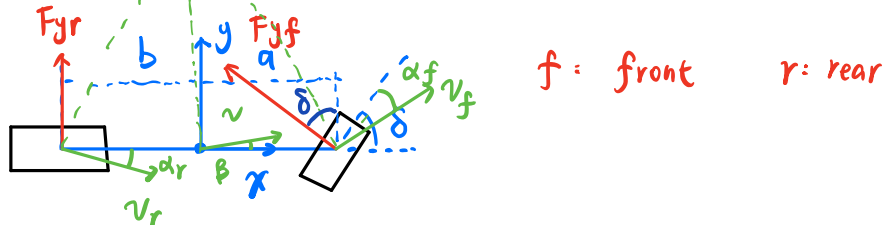
侧偏刚度一定是负数



负的侧偏力  $\Rightarrow$  正的侧偏角

## 自行车模型





$\alpha_r$   $\alpha_f$  都是负的

$$\sum F_y = m a_y \Rightarrow m a_y = F_{yf} \cos \delta + F_{yr}$$

$$\sum M = I \ddot{\psi} \Rightarrow F_{yf} \cos \delta \cdot a - F_{yr} \cdot b = I \ddot{\psi}$$

假设  $\delta$  较小  $\cos \delta \approx 1$

$$m a_y = F_{yf} + F_{yr} = C_{\alpha f} \alpha_f + C_{\alpha r} \alpha_r$$

$$I \ddot{\psi} = F_{yf} \cdot a - F_{yr} \cdot b = a C_{\alpha f} \alpha_f - b C_{\alpha r} \alpha_r$$

$a_y$  与  $y$  的关系, 以及  $\alpha_f, \alpha_r$  的具体表达式

$$v_y = \dot{y}$$

$$a_y = \ddot{y} + v_x \dot{\psi}$$

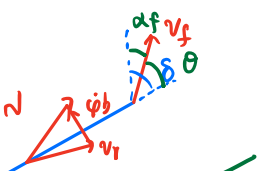
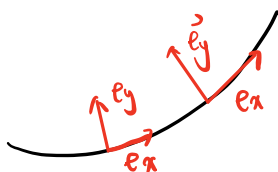
$$\vec{a} = \frac{d\vec{v}}{dt} = \frac{d(v_x \vec{e}_x + v_y \vec{e}_y)}{dt}$$

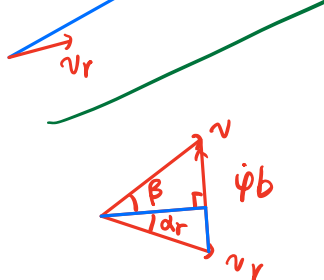
在直角坐标系中  $\vec{e}_x, \vec{e}_y$  为常矢量  $\dot{\vec{e}}_x, \dot{\vec{e}}_y = 0$

$$\Rightarrow \vec{a} = \frac{dv_x}{dt} \vec{e}_x + v_x \cdot \frac{d\vec{e}_x}{dt} + \frac{dv_y}{dt} \vec{e}_y + v_y \cdot \frac{d\vec{e}_y}{dt} \neq 0$$

在直角坐标  $\vec{a} = \dot{v}_x \vec{e}_x + \dot{v}_y \vec{e}_y \therefore a_y = \dot{v}_y$

在车身坐标  $\vec{e}_x, \vec{e}_y$  不是常矢量 (Frenet 公式) (非惯性系)

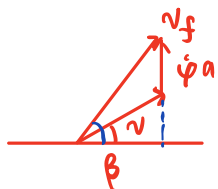




$$v \cos \beta = v_x$$

$$\dot{\varphi} b - v \sin \beta = \dot{\varphi} b - v_y$$

$$\tan \alpha_r = \frac{\dot{\varphi} b - v_y}{v_x} \approx \alpha_r \quad \because \alpha_r \text{ 是小的} \quad \therefore \alpha_r = \frac{v_y - \dot{\varphi} b}{v_x}$$



$$\tan \theta = \frac{\dot{\varphi} a + v_y}{v_x}$$

$$\alpha_f = \theta - \delta = \frac{\dot{\varphi} a + v_y}{v_x} - \delta$$

$$m \dot{v}_y = C_{\alpha_f} \alpha_f + C_{\alpha_r} \alpha_r \Rightarrow m(\dot{v}_y + v_x \dot{\varphi}) = C_{\alpha_f} \left( \frac{\dot{\varphi} a + v_y}{v_x} - \delta \right) + C_{\alpha_r} \left( \frac{v_y - \dot{\varphi} b}{v_x} \right)$$

$$I \ddot{\varphi} = a C_{\alpha_f} \alpha_f - b C_{\alpha_r} \alpha_r \Rightarrow I \ddot{\varphi} = a C_{\alpha_f} \left( \frac{\dot{\varphi} a + v_y}{v_x} - \delta \right) - b C_{\alpha_r} \left( \frac{v_y - \dot{\varphi} b}{v_x} \right)$$

$$v_y \Leftrightarrow \dot{y}$$

$$\begin{pmatrix} \ddot{y} \\ \ddot{\varphi} \end{pmatrix} = \begin{pmatrix} \frac{C_{\alpha_f} + C_{\alpha_r}}{m v_x} & \frac{a C_{\alpha_f} - b C_{\alpha_r}}{m v_x} - v_x \\ \frac{a C_{\alpha_f} - b C_{\alpha_r}}{I v_x} & \frac{a^2 C_{\alpha_f} + b^2 C_{\alpha_r}}{I v_x} \end{pmatrix} \begin{pmatrix} \dot{y} \\ \dot{\varphi} \end{pmatrix} + \begin{pmatrix} -\frac{C_{\alpha_f}}{m} \\ -\frac{a C_{\alpha_f}}{I} \end{pmatrix} \delta \quad \uparrow$$

设  $x = \begin{pmatrix} \dot{y} \\ \dot{\varphi} \end{pmatrix}$   $u = \delta$   $\uparrow$   $\dot{x} = Ax + Bu$  通过控制  $\delta$ , 实现对  $y, \varphi$  的控制