

自动驾驶控制算法第六讲

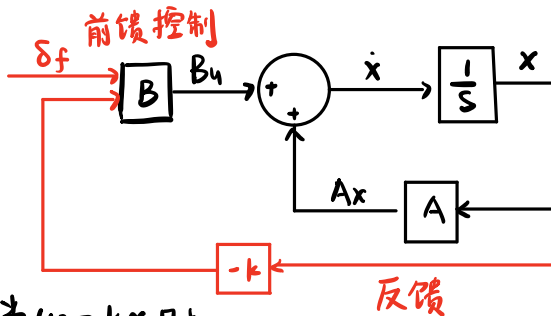
$$k = \text{lqr}(A, B, Q, R) \quad k = \text{dlqr}(\bar{A}, \bar{B}, Q, R)$$

$$\dot{x} = Ax + Bu$$

$$x_{k+1} = \bar{A}x_k + \bar{B}u_k$$

$$u = -kx \quad (\text{反馈控制})$$

$$\dot{x} = Ax + Bu$$



当 $u = -kx$ 时

$$\text{第四讲} \quad e_{ir} = A e_{rr} + Bu + \underbrace{C \dot{\theta}_r}_{\text{前馈控制}}$$

$$\text{若只用 LQR} \quad u = -k e_{rr} \Rightarrow \underline{e_{rr} = (A - Bk) e_{rr} + C \dot{\theta}_r}$$

无论 k 取何值 e_{rr} 与 e_{ir} 不可能同时为零 $\Rightarrow e_{rr}$ 不可能永远为零

$\therefore e_{rr} = 0, e_{ir} = 0$ 不是该微分方程的解 $0 = 0 + C \dot{\theta}_r$ 不可能!

$$\text{前馈控制} \quad e_{ir} = A e_{rr} + Bu + C \dot{\theta}_r$$

$$u = \underbrace{-kx}_{\downarrow \text{由 LQR 计算出的反馈控制}} + \underbrace{\delta_f}_{\text{前馈控制}}$$

由 LQR 计算出的反馈控制

$$\dot{x} = Ax + Bu$$

前馈控制的引入是为了消除稳态误差

(LQR 最终会导致 $\underline{\dot{e}_{rr} = 0, e_{rr} \neq 0}$ ✓)

$$0 = (A - Bk) e_{rr} + C \dot{\theta}_r \quad \underline{e_{rr} = -(A - Bk)^{-1} C \dot{\theta}_r} \quad \text{稳态误差}$$

引入前馈控制后

$$e_{ir} = A e_{rr} + B(-k e_{rr} + \delta_f) + C \dot{\theta}_r$$

$$\text{稳定后, } e_{ir} = 0 \quad e_{rr} = -(A - Bk)^{-1} \cdot (B \delta_f + C \dot{\theta}_r)$$

目的. 选取合适的 δ_f , 使得 $e_{rr} = -(A-Bk)^{-1} \cdot (B\delta_f + (\dot{\theta}_r))$ 尽可能为零

用软件 Mathematica 计算

$$e_{rr} = \begin{pmatrix} \frac{1}{k_1} \left\{ \delta_f - \frac{\dot{\theta}_r}{v_x} \left[a + b - b k_3 - \frac{m N_x^2}{a+b} \left(\frac{b}{c_f} + \frac{a}{c_r} k_3 - \frac{a}{c_r} \right) \right] \right\} \\ 0 \\ - \frac{\dot{\theta}_r}{v_x} \left(b + \frac{a}{a+b} \frac{m N_x^2}{c_{dr}} \right) \\ 0 \end{pmatrix}$$

$\dot{\theta}_r$ 对 e_{rr} 的影响

$$\text{当 } \delta_f = \frac{\dot{\theta}_r}{v_x} \left[a + b - b k_3 - \frac{m N_x^2}{a+b} \left(\frac{b}{c_f} + \frac{a}{c_r} k_3 - \frac{a}{c_r} \right) \right]$$

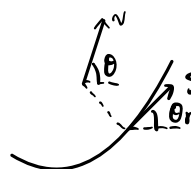
$e_d = 0$ k_3 是反馈 k (k_1, k_2, k_3, k_4) 中的 k_3

先算反馈 k , 再算前馈

$$e_p = - \frac{\dot{\theta}_r}{v_x} \left(b + \frac{a}{a+b} \frac{m N_x^2}{c_{dr}} \right) \text{ 不受 } \delta_f, k \text{ 的影响}$$

无论前馈反馈取何值 $e_p \neq 0$

对 e_p 做化简



$$\begin{aligned} \dot{s} &= \frac{|\vec{v}| \cos(\theta - \theta_r)}{1 - k e_d} = \frac{|\vec{v}| \cos(\beta + \varphi - \theta_r)}{1 - k e_d} = \frac{|\vec{v}| \cos \beta \cos \varphi - |\vec{v}| \sin \beta \sin \varphi}{1 - k e_d} \\ &= \frac{v_x \cos \varphi - v_y \sin \varphi}{1 - k e_d} \end{aligned}$$

曲率 $k = \frac{y''}{(1+y'^2)^{\frac{3}{2}}}$ 定义式 $k = \frac{d\theta}{ds} = \frac{d\theta/dt}{ds/dt} = \frac{\dot{\theta}}{\dot{s}} \quad \dot{\theta} = k \dot{s}$

$\therefore \dot{\theta}_r = k \dot{s}$ 近似 $|k| \ll 1 \quad |e_p| \ll 1 \quad |N_y| \ll 1$ (无飘移)

$\frac{1}{1 - k e_d} \approx 1 \quad v_x \cos \varphi \approx v_x \quad v_y \sin \varphi \approx 0 \quad \therefore \dot{s} \approx v_x$

$\therefore \dot{\theta}_r = k \dot{s} \approx k v_x$

$$e_p = -k \left(b + \frac{a}{a+b} \frac{m v_x^2}{c_r} \right) \quad k = \frac{1}{R}$$

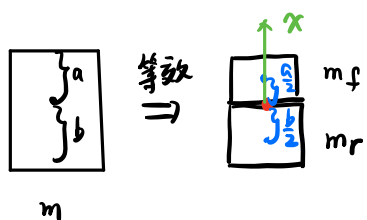
$$= - \left(\frac{b}{R} + \frac{a}{a+b} \frac{m v_x^2}{R c_r} \right)$$

$$a_y = \dot{v}_y + v_x \dot{\varphi} \quad (\text{无侧风移})$$

$$\approx v_x \dot{\varphi} \quad \dot{\varphi} = \frac{\dot{\vec{v}}}{R} = \frac{\dot{\vec{v}}_x + \dot{\vec{v}}_y}{R} \approx \frac{\dot{\vec{v}}_x}{R}$$

$$\approx \frac{v_x^2}{R}$$

$$e_p = - \left(\frac{b}{R} + \frac{a}{a+b} m a_y \cdot \frac{1}{c_r} \right)$$

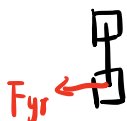


等效的前提

$$\begin{cases} m_f + m_r = m \\ m_f \cdot \frac{a}{2} + m_r \cdot \left(-\frac{b}{2}\right) = 0 \end{cases} \Rightarrow \begin{cases} m_f = \frac{b}{a+b} m \\ m_r = \frac{a}{a+b} m \end{cases}$$

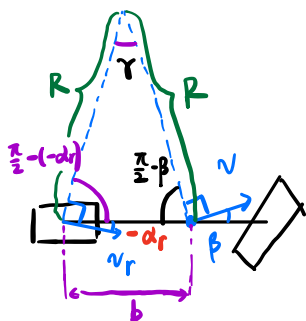
$$e_p = - \left(\frac{b}{R} + \frac{m_r a_y}{c_r} \right)$$

$m_r a_y = F_{yr}$ 后轮侧向力的和

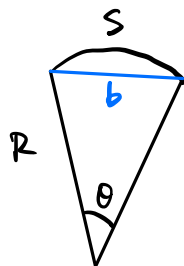


$$= - \left(\frac{b}{R} + dr \right)$$

还可以化简



$$\because R \gg b \quad \gamma \approx \frac{b}{R}$$



$$\theta = \frac{S}{R} \quad \text{弧度制的定义}$$

$$\text{当 } R \gg S \text{ 时 } S \approx b$$

$$\therefore \theta \approx \frac{b}{R}$$

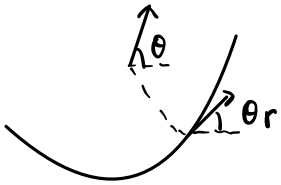
在 Δ 中有 $\gamma + \frac{\pi}{2} - \beta + \frac{\pi}{2} - (-dr) = \pi$

$$\Rightarrow -\beta = -(\gamma + \alpha_r) = -\left(\frac{b}{R} + \alpha_r\right)$$

$$\therefore e_\varphi = -\beta$$

$$e_\varphi \text{ 不是航向误差} \quad e_\varphi = \varphi - \theta_r \quad \text{航向误差为 } \theta - \theta_r \quad \theta = \varphi + \beta$$

$$e_\varphi \text{ 的稳态误差为 } -\beta \quad e_\varphi = \varphi - \theta_r \quad \Rightarrow -\beta = \varphi - \theta_r \quad \underline{\varphi + \beta = \theta_r} \quad \checkmark$$



虽然 e_φ 不可能通过 δ_f , K 去调节, 但是我们不用去理会

\therefore 最终目的是 $\theta - \theta_r = 0 \Rightarrow e_\varphi = -\beta$ 而 e_φ 的稳态误差正好是 $-\beta$

\therefore 不用去管

$$\delta_f = \frac{\dot{\theta}_r}{v_x} \left[a + b - b k_3 - \frac{m v_x^2}{a+b} \left(\frac{b}{c_f} + \frac{a}{c_r} k_3 - \frac{a}{c_r} \right) \right]$$

$$\theta_r = k v_x$$

$$\delta_f = k \left[a + b - b k_3 - \frac{m v_x^2}{a+b} \left(\frac{b}{c_f} + \frac{a}{c_r} k_3 - \frac{a}{c_r} \right) \right]$$

$$u = -\underbrace{K e_{rr}}_{\substack{\downarrow \\ l_{qr} \\ \text{反馈控制}}} + \underbrace{\delta_f}_{\substack{\uparrow \\ \text{前馈控制}}}$$

$$e_{11} = \begin{pmatrix} 0 \\ 0 \\ -\beta \\ 0 \end{pmatrix}$$

e_φ 是不是航向误差 (很微妙)