

Chalmers University of Technology
MTF 270 - Turbulence Modeling

ASSIGNMENT 1
Case 3 : Flow over a Hill

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Date : April 4, 2022

1 Introduction

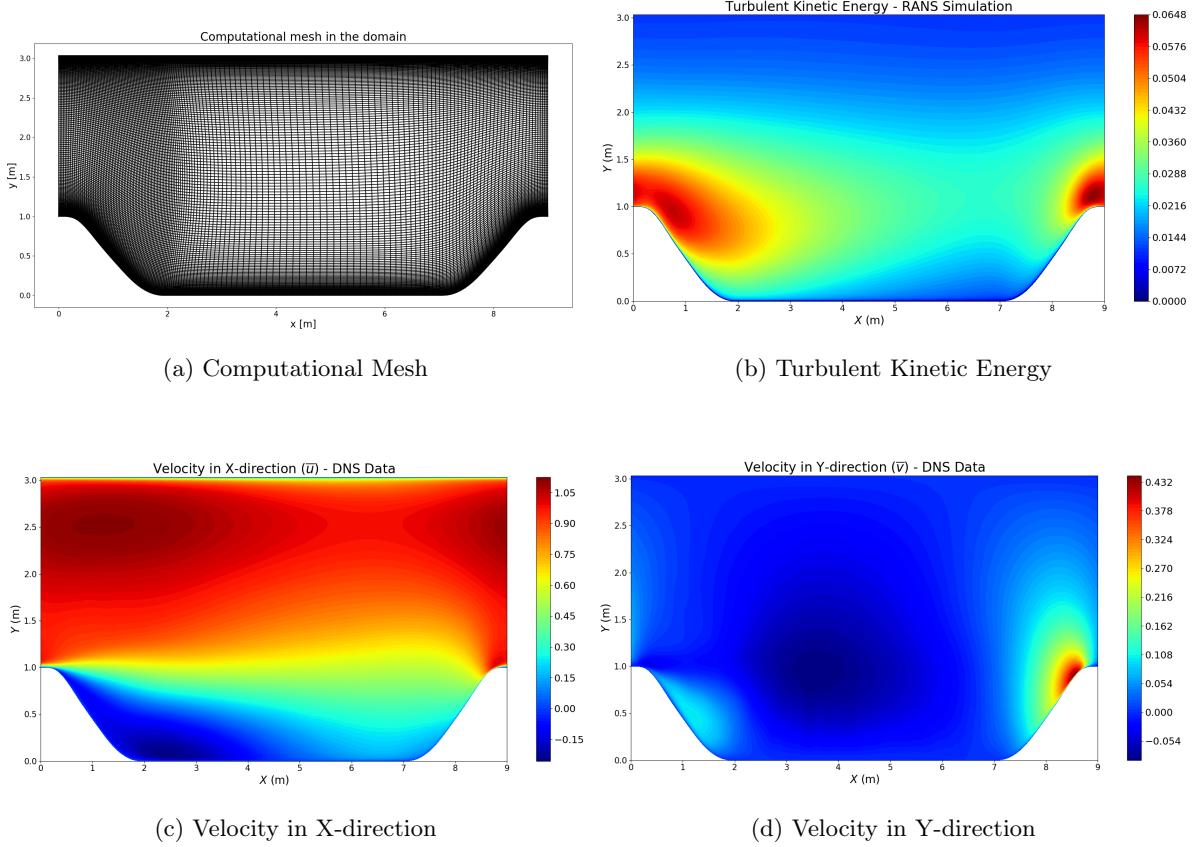


Figure 1: Illustration of given data

The flow over a single hill is simulated in this project. DNS data for the fluctuating as well as the mean flow quantities are provided to us. From figure 1, we can observe that turbulence is present predominantly in two regions, the separation region near the first hill and the stagnation region near the second hill.

2 Results

2.1 Assignment 1.1

Normal Stresses(blue and yellow curve)

@ Lower wall

The normal viscous stress terms ($\text{viscos}^* \text{dudx}$ and $\text{viscos}^* \text{dvdy}$) are negligible. From figure 4 ,the normal Reynolds stress terms $\rho \bar{u}' \bar{u}'$ and $\rho \bar{v}' \bar{v}'$ have a high value at the high turbulence regions specifically near the flow separation region ($x:0m$) and the re-circulation region ($x:4.116m$). Thus the resulting normal

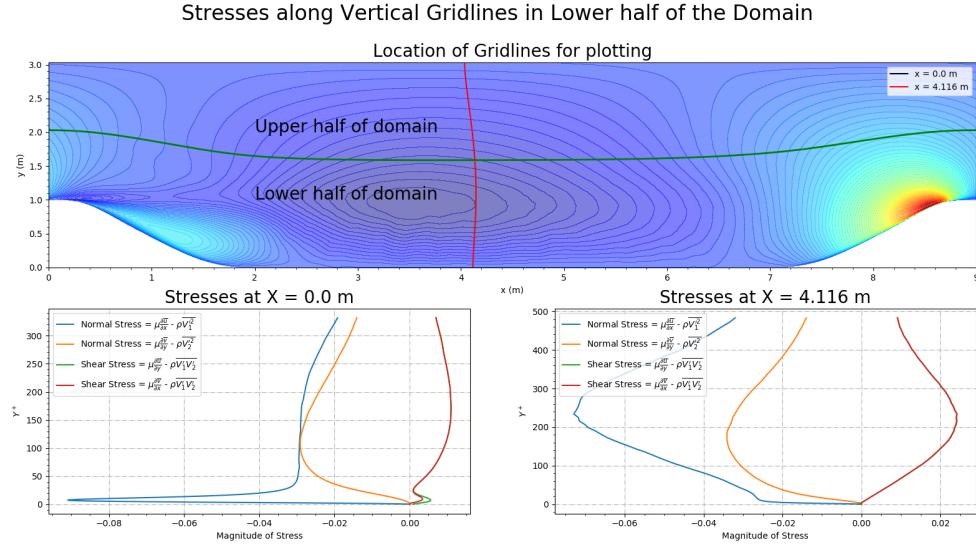


Figure 2: Stresses at different vertical lines - Lower half

stress term is highly negative.

@vertical line (x:0) : The high negative values in the blue curve near the wall is due to the high value of $\rho u' u'$ near the beginning of the flow separation. At the same time the values near the wall at the same location for the yellow curve are not high. As the v component of the flow is high only in the log law region.

@vertical line (x:4.4116) The high negative values in the blue curve and yellow curves are due to the presence of the re-circulation region and separation between the re-circulation flow and the channel flow. The value of $\rho u' u'$ and $\rho v' v'$ are high in the log law region.

@ Upper wall

The value of $\rho u' u'$ is high near the wall ,this causes the blue curve to have a high negative jump near the wall. Both $\rho u' u'$ and $\rho v' v'$ increase in magnitude in the log law region. This is evident in the blue and yellow curves.

Shear Stresses (green and red curves)

@ Lower wall and Upper wall

Since $\rho u' u'$ is same as $\rho v' v'$ and both are dominant in the log law region,both the green and the red curve are equal in the log law region.

The differences between the (dudy) term and the (dvdx) term can be seen in the non-coinciding green and red curve near the wall , in the viscous (inner region).

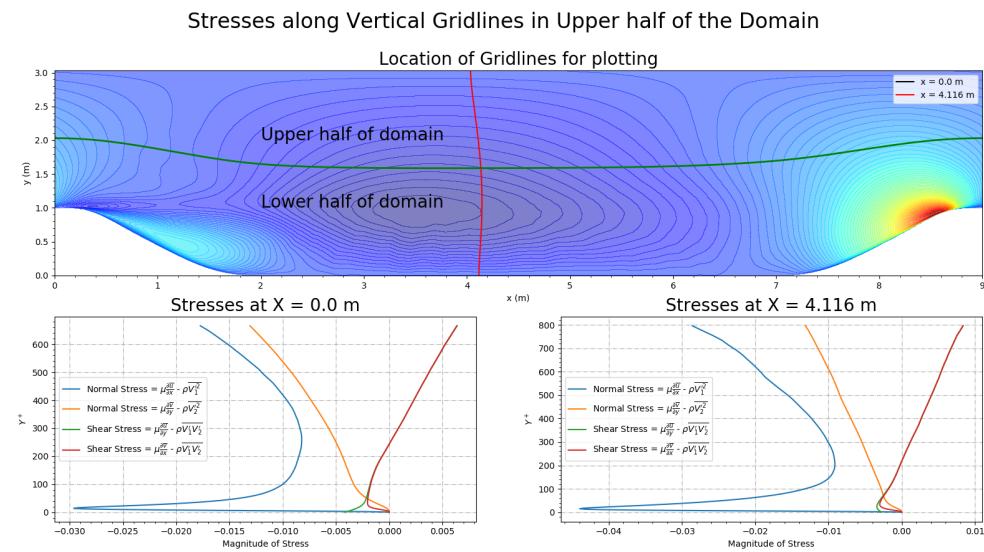


Figure 3: Stresses at different vertical lines - Upper half

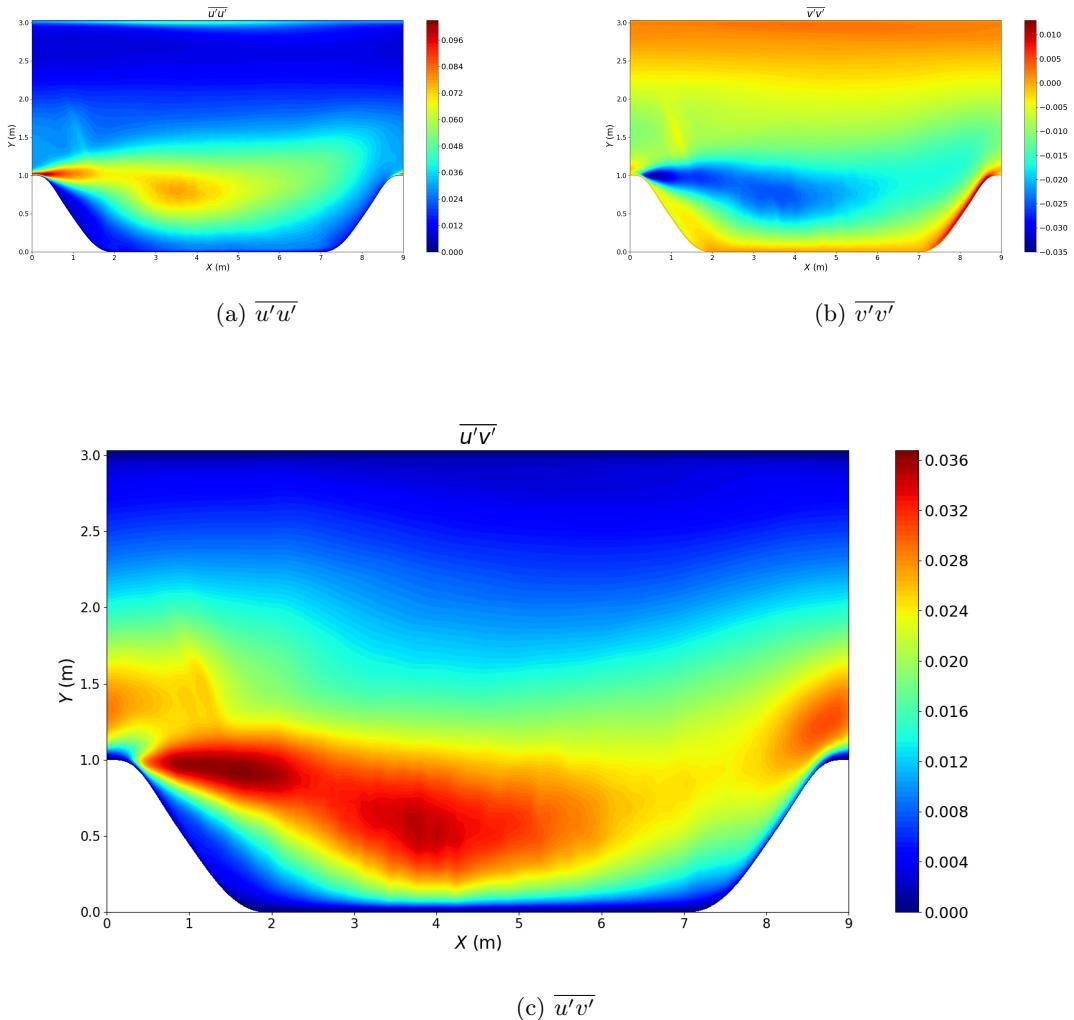


Figure 4: Effect of Limiting Function on Normal Stress and Turbulent Viscosity

2.2 Assignment 1.2

Terms in X-momentum equation at X = 0.0 m in upper half of domain

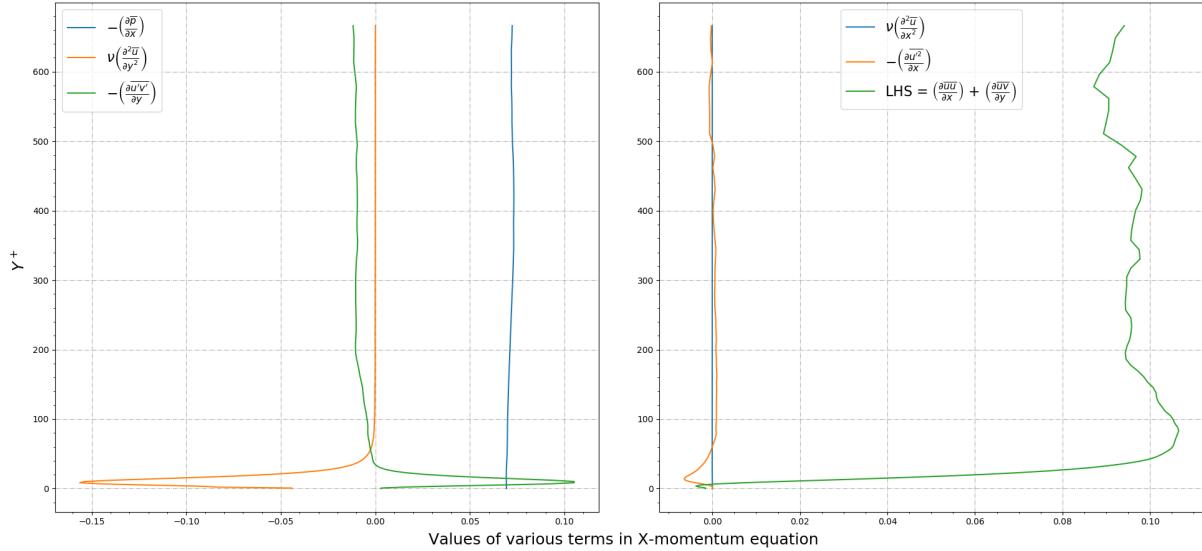


Figure 5: X momentum at X = 0 m in upper half of the domain

Terms in Y-momentum equation at X = 0.0 m in upper half of domain

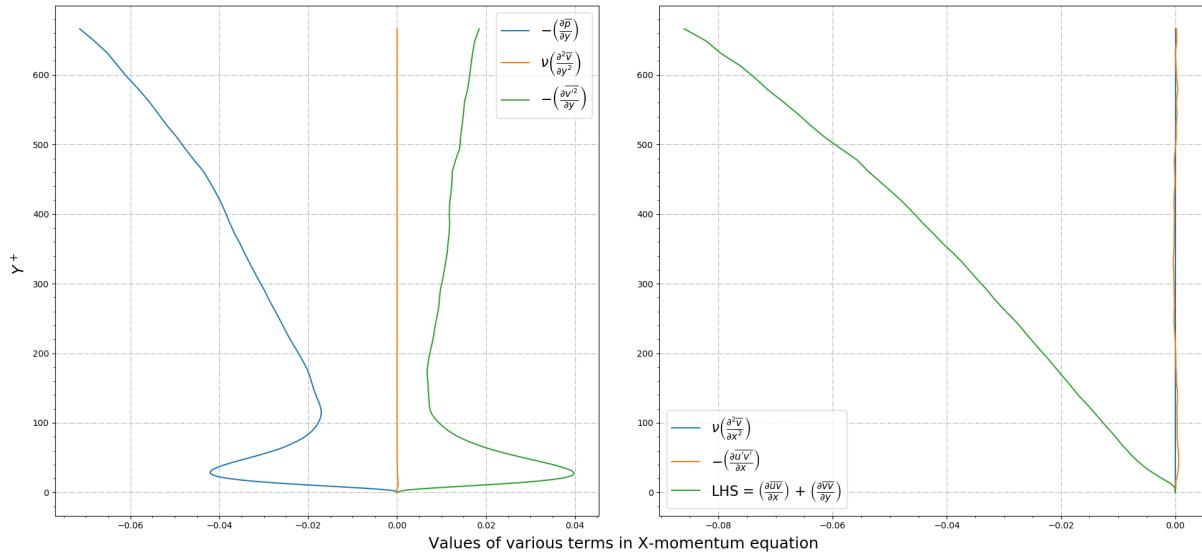


Figure 6: Y momentum at X = 0 m in upper half of the domain

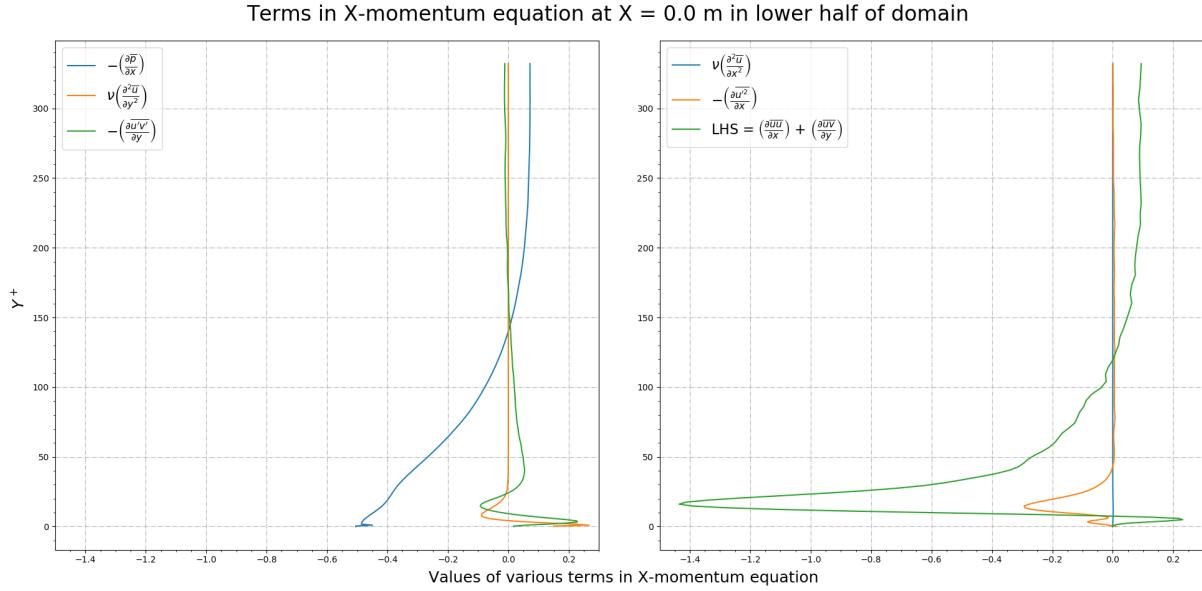


Figure 7: X momentum at X = 0 m in lower half of the domain

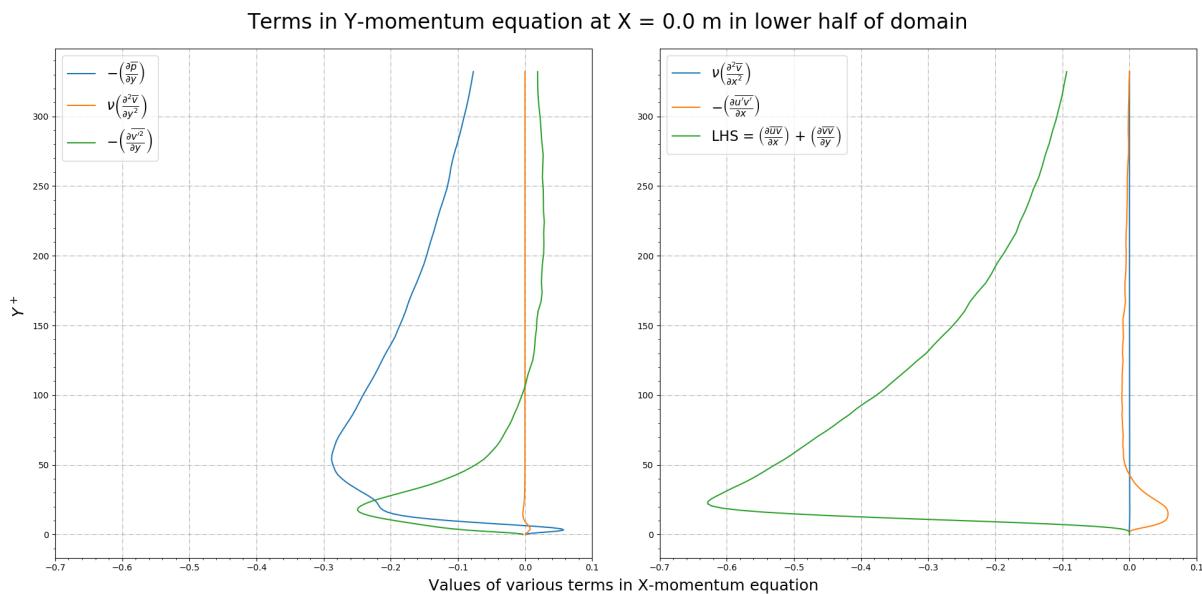


Figure 8: Y momentum at X = 0 m in lower half of the domain

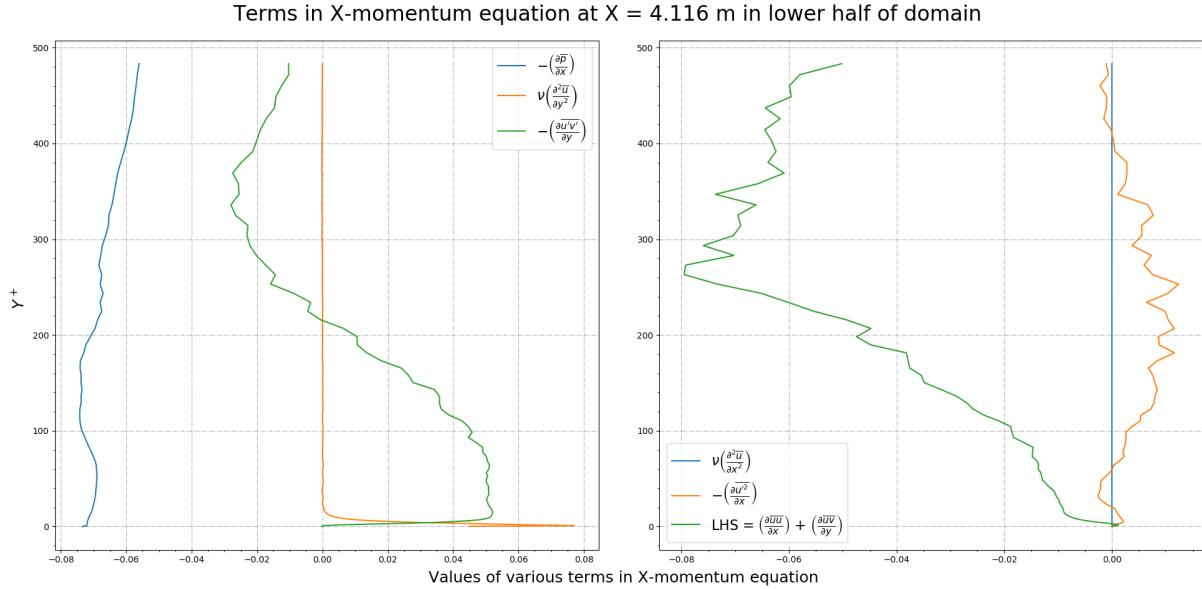


Figure 9: X momentum at X = 4.116 m in lower half of the domain

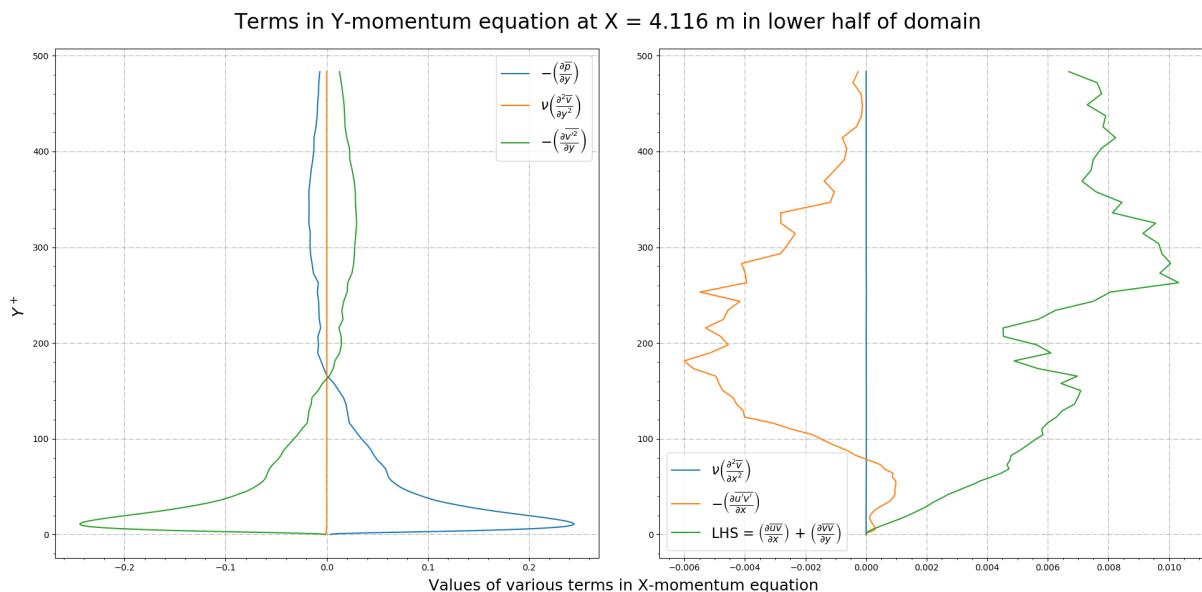


Figure 10: Y momentum at X = 4.116 m in lower half of the domain

@ Upper wall

Since the flow characteristics at the upper wall is similar to a channel flow, it is easier to start the discussion at the upper wall.

From figure 5, the pressure gradient term is seen to have a close to constant value along $Y+$, this is the pressure force that drives the flow by creating a constant pressure drop.

Since the viscous force is dominant only in the near wall region (inner region).The only opposing force in the log law region is the gradient of the Reynolds shear force.

Near the wall (Viscous region), the Reynolds shear force is the driving force (it is the opposing force in log law region) and the opposing force is the viscous force.This is seen clearly in the plot.

The x gradients of the viscous and shear stresses are negligible low change in u with respect to x and low change in u' with respect to x

The LHS in both the X momentum and the Y momentum follow a similar behaviour to the pressure force, depicting the influence of pressure force in determining the direction of flow.

@ Lower wall

@ $x=0.0$ m, the flow is driven by the pressure force term, the separation and re-circulation in the flow downstream is felt upstream causing the pressure term to be negative (negative u direction flow). As the $Y+$ is increased the flow pressure term is back in the positive side depicting flow in the positive u direction.

The viscous force and the Reynolds force again follow the same characteristics as explained for the upper wall. The only difference here is the direction of the forces which are mainly due to the re circulation region.

Similar to the upper wall,The LHS in both the X momentum and the Y momentum follow a similar behaviour to the pressure force, depicting the influence of pressure force in determining the direction of flow.

@ $x= 4.116$ m, similar to the discussion in the upper wall region, the Reynolds force is zero at the wall and increases till it reaches total wall force, at the same time the Viscous force reduces to zero in the log law region.

The pressure force term here is on the negative side of the plot depicting flow in the negative u direction, this is explained due to the re-circulation region present.

* Taylor expansion of v_1' , v_2' , v_3' near the wall,

$$v_1' = a_0 + a_1 x_2 + a_2 x_2^2 + \dots$$

$$v_2' = b_0 + b_1 x_2 + b_2 x_2^2 + \dots$$

$$v_3' = c_0 + c_1 x_2 + c_2 x_2^2 + \dots$$

$$\text{BC} \rightarrow v_1' = 0 \quad \text{and} \quad \frac{\partial v_1'}{\partial x_1} = 0 \quad \text{and} \quad \frac{\partial v_3'}{\partial x_3} = 0$$

\therefore it gives,

$$v_1' = a_1 x_2 + a_2 x_2^2 + \dots$$

$$v_2' = b_2 x_2^2 + b_3 x_2^3 + \dots$$

$$v_3' = c_1 x_2 + c_2 x_2^2 + \dots$$

\therefore Time averaging the quantities,

$$\bar{v}_1'^2 = \bar{a}_1^2 x_2^2 + \dots = O(x_2^2)$$

$$\bar{v}_2'^2 = \bar{b}_2^2 x_2^4 + \dots = O(x_2^4)$$

$$\bar{v}_3'^2 = \bar{c}_1^2 x_2^2 + \dots = O(x_2^2)$$

$$\text{also, } \bar{v}_1' v_2' = \bar{a}_1 \bar{b}_2 x_2^3 + \dots = O(x_2^3)$$

Fluctuating terms in x -momentum eqn:

$$\frac{\partial \bar{v}_1'^2}{\partial x_1} = O(x_2^0) \quad , \quad \frac{\partial \bar{v}_1' v_2'}{\partial x_2} = O(x_2^2)$$

$\therefore \frac{\partial \bar{v}_1'^2}{\partial x_1}$ near the wall is non-zero

$\therefore \frac{\partial \bar{v}_1' v_2'}{\partial x_2}$ near the wall approaches to zero.



Figure 11: Taylor's expansion for fluctuating terms

2.3 Assignment 1.3

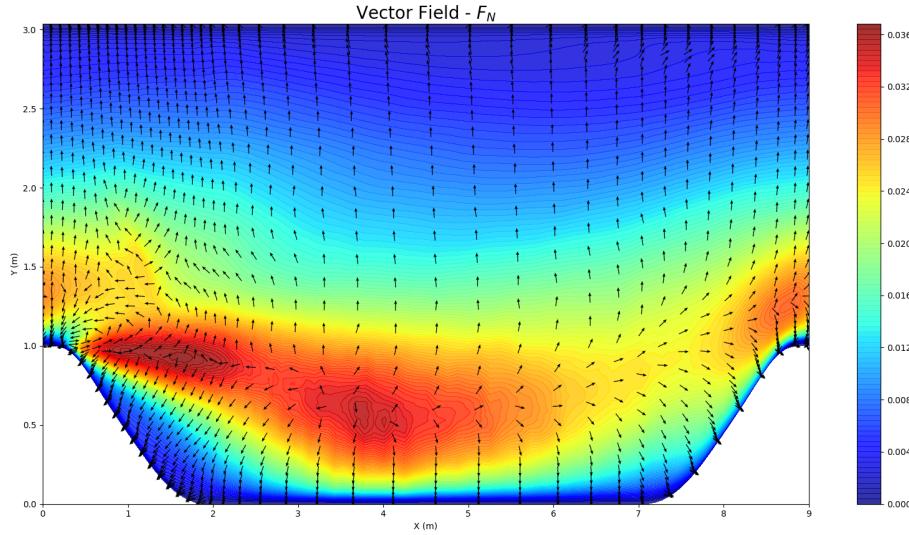


Figure 12: F.N Quiver plot over $\rho \bar{v}' v'$ contour

From Figure 12, the direction of the normal forces originate from the highest value of the viscous stress and point toward the wall.

At the highest value of $\rho \bar{v}' v'$ at any vertical line, the direction of the Normal force vectors point away from the highest value towards the wall. As in nodes above the highest node, point towards the upper wall and nodes below the lowest node point towards the lower wall.

Since $\rho \bar{v}' v'$ is highest at locations with separated flow and re-circulation (areas with high v component), the direction change of the Normal Force vectors is preset in these regions.

2.4 Assignment 1.4

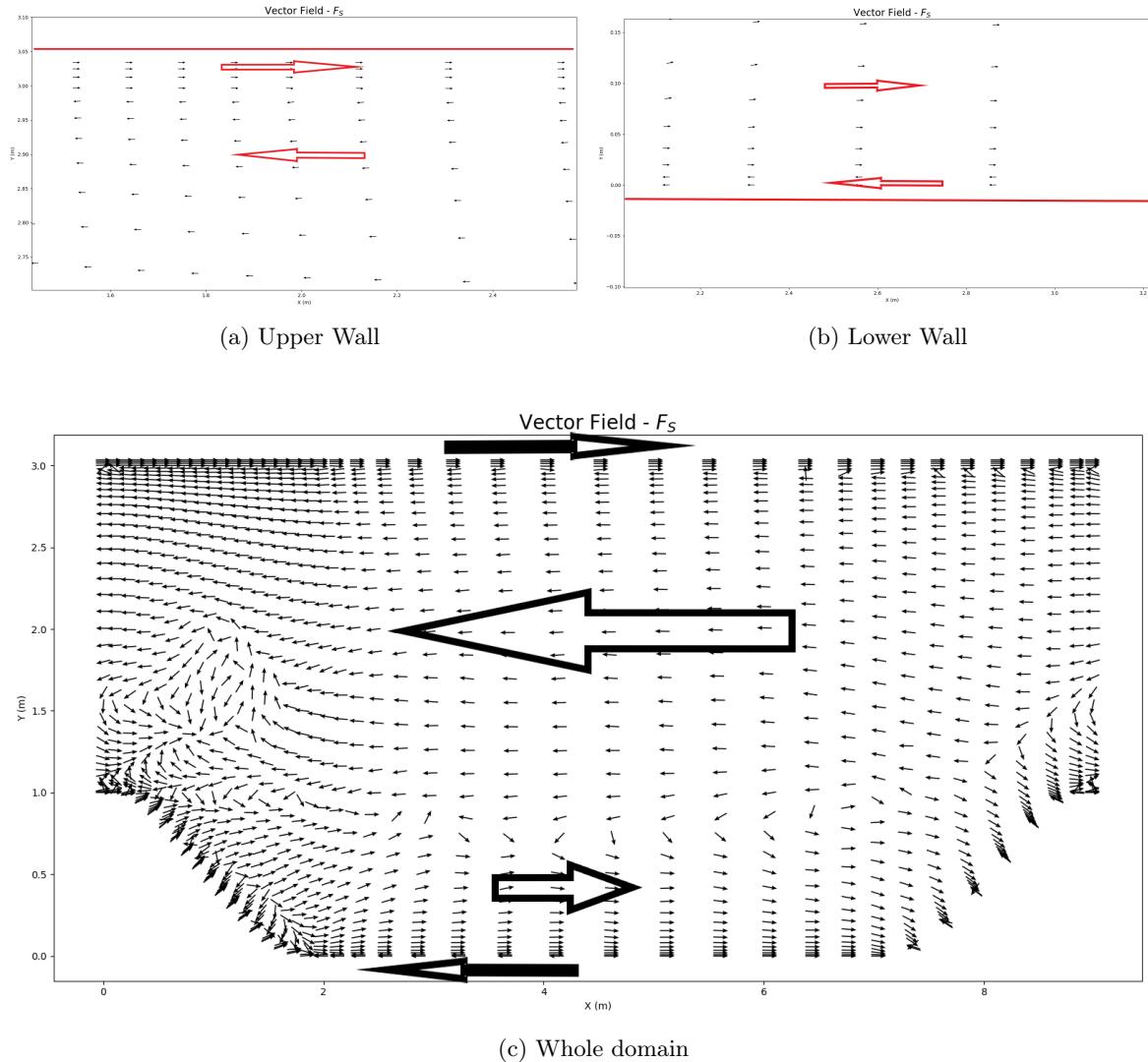


Figure 13: Quiver plot of F_s

From figure 13, the shear force field depict different behaviours across different parts of the domain.

Viscous regions at both the walls:

In the Viscous region (inner region) the Reynolds shear forces act as the driving force for the flow and are opposed by Viscous shear forces. Therefore here the direction of the force will be in the same direction of the flow.

Log law region at both the walls:

In the log law region the Reynolds shear forces act as an opposing force to the flow, here the driving force is the pressure force. Therefore here the direction of the force will be against the direction of the flow.

As seen in the quiver plot for shear force, Near the walls, the direction of the shear force is the same as the flow direction.

Again, the re-circulation region away from the lower wall (log law region) where the flow direction is toward the left, here the Force direction is towards the right. Similarly in the log law region away from the upper wall where the flow is towards the right, here the shear force direction is towards the left.

2.5 Assignment 1.5

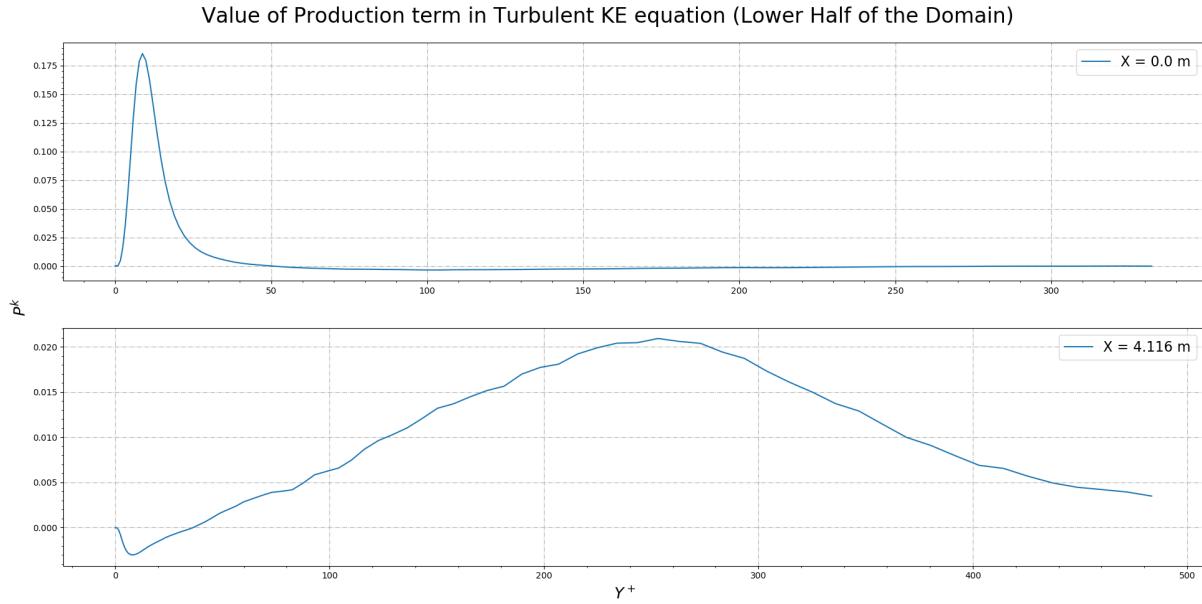


Figure 14: Production term Upper Half of Domain

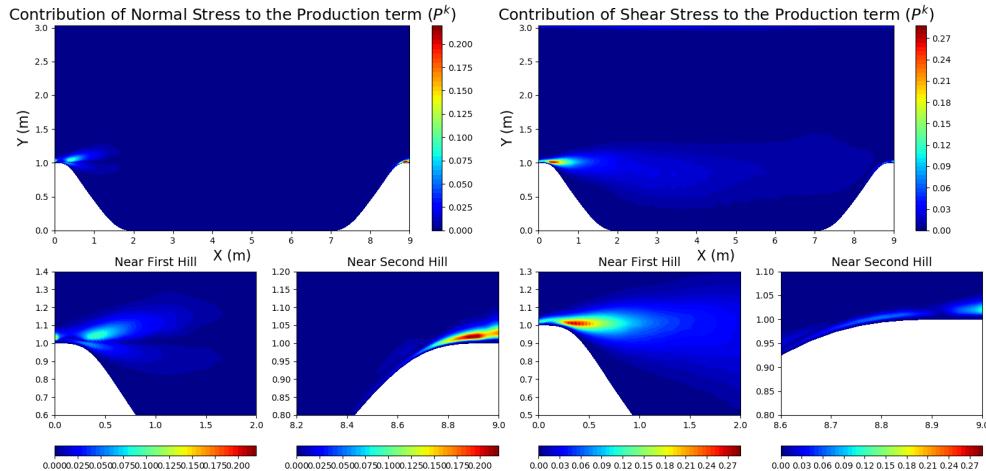


Figure 15: Contribution to Pk term

The value of P_k is highest in regions at high energy containing eddys (small length scales) ,this is present away from the wall and in the log law region. Basically, P_k has the highest values in highly turbulent regions.

From figure 15, regions with high Reynolds stresses are regions with the highest P_k values. P_k is negligible near the walls. In figure 14,The difference in P_k curves at different Vertical lines are due to different Reynolds stress values at these lines.

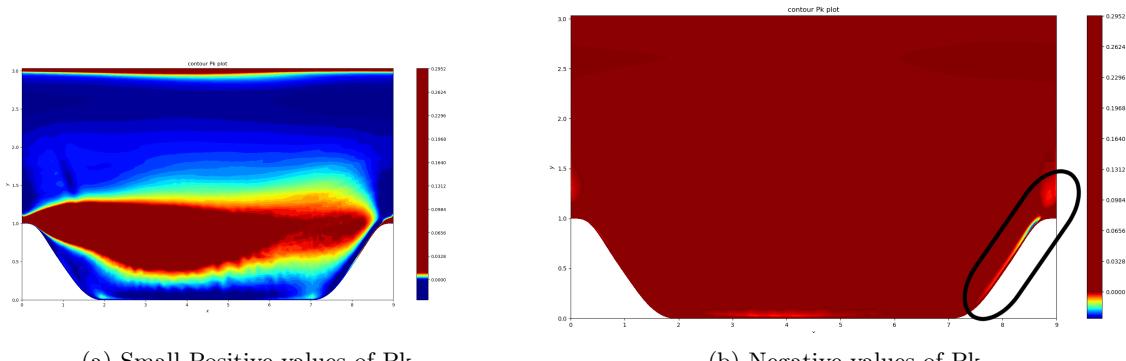


Figure 16: Small Positive and Negative values of Pk

From figure 16, P_k can be visualized as a work term, $P_k > 0$ in regions where the mean flow performs work on the fluctuating velocity field and $P_k < 0$ is regions where the fluctuating velocity field performs work on the mean flow. The latter case happens when the gradient of mean flow velocity is in the opposite direction of fluctuation velocity.

2.6 Assignment 1.6

Figure 17 depicts the dissipation in the domain, the dissipation near the slope of the first hill and slope of the second hill. This is close to the beginning of separation region.

Figure 18 shows the difference in Pk term and the Dissipation term. The completely white regions are regions where the Pk term is equal to the dissipation term.

Note: We are not sure of the explanation but a visual inspection depicts the terms cancel out at the transition from inner region to log law region.

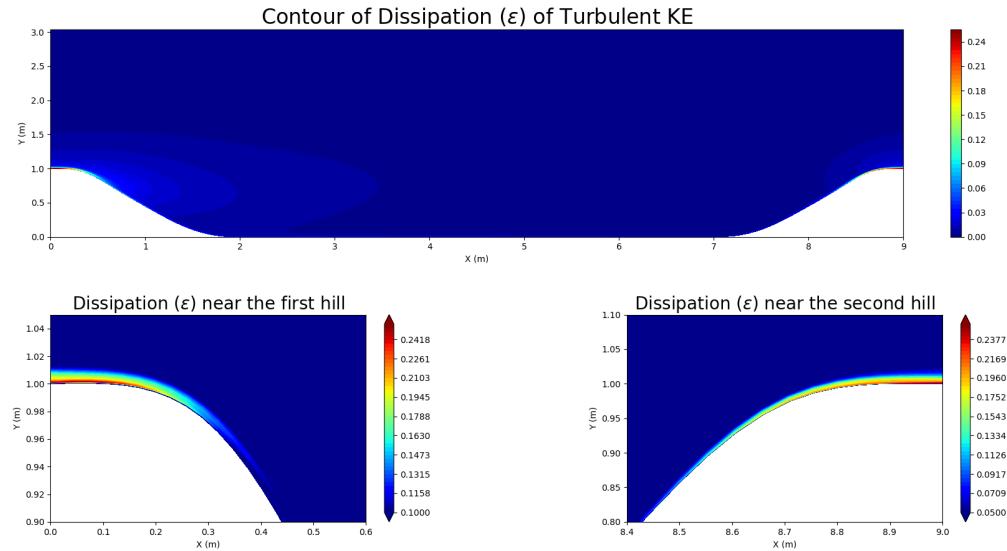


Figure 17: Dissipation

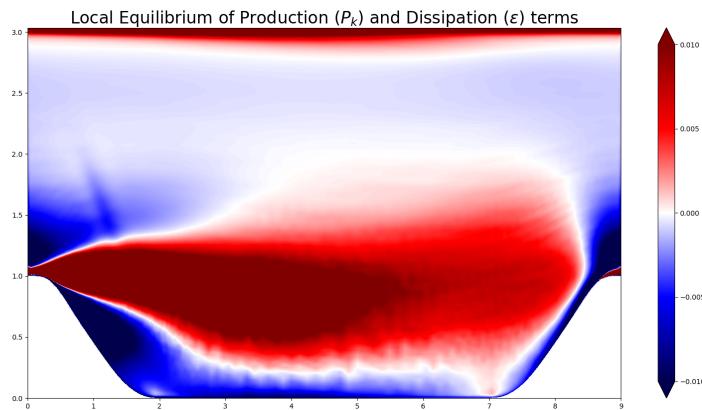


Figure 18: Equilibrium of Pk and Dissipation

2.7 Assignment 1.7

Figure 19 and figure 21 represents the various terms in $\overline{V_1'^2}$ equation for the lower and upper domain respectively. Figure 20 and figure 22 represents the various terms in $\overline{V_1'V_2'}$ equation for the lower and upper domain respectively.

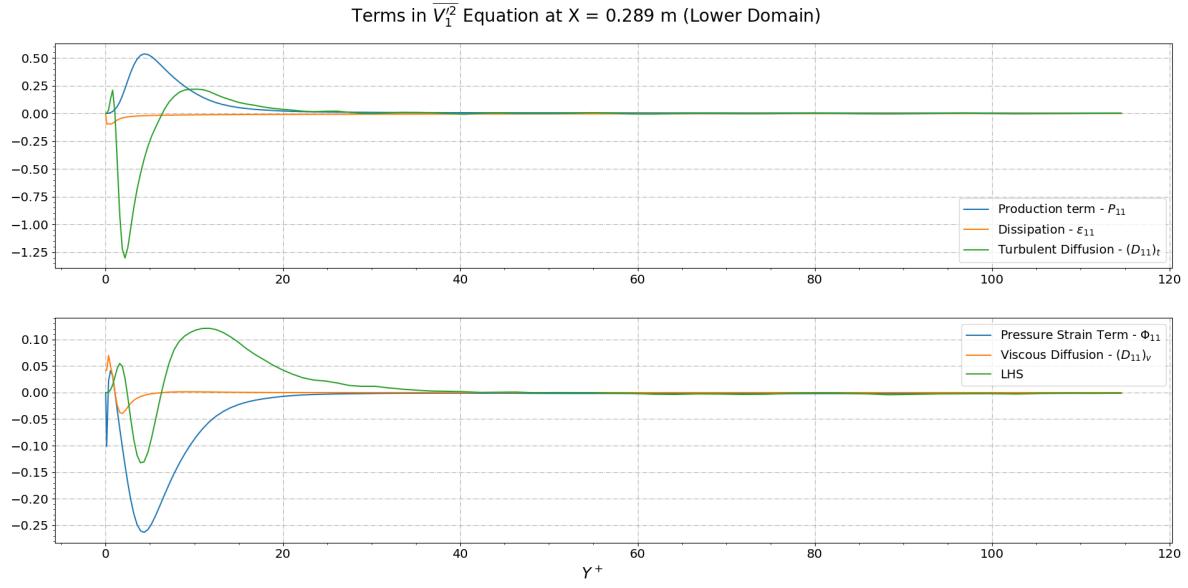


Figure 19: Terms in $\overline{V_1'^2}$ equation in lower domain

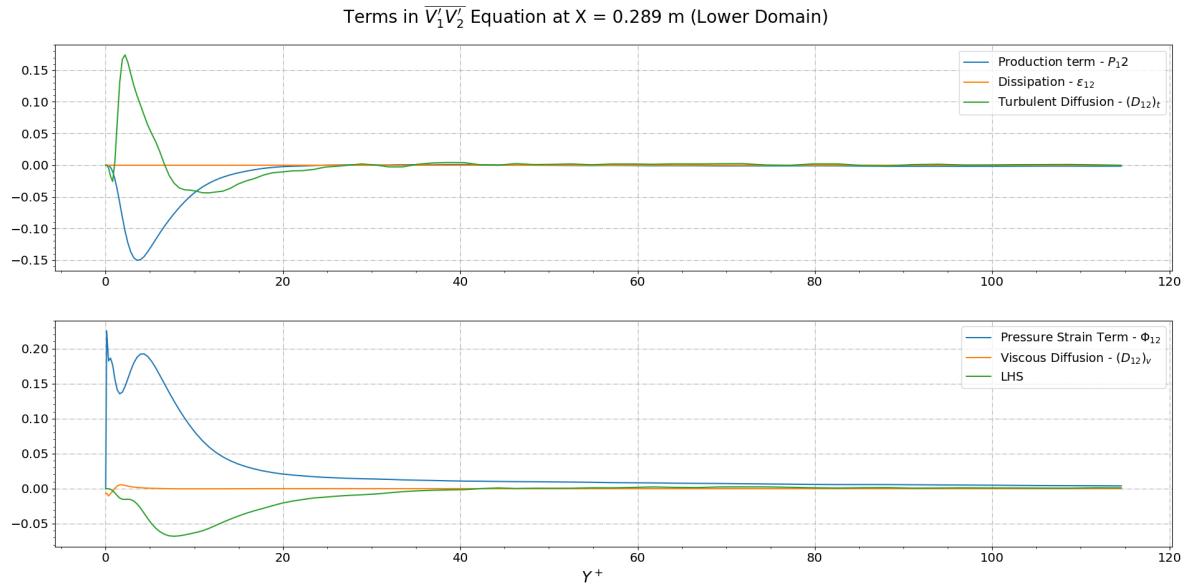


Figure 20: Terms in $\overline{V_1'V_2'}$ equation in lower domain

- For lower domain in $\overline{V_1'^2}$ equation, the production term acts as the main source term, whereas pressure-strain and turbulent diffusion term acts as the sink near the wall. The viscous diffusion

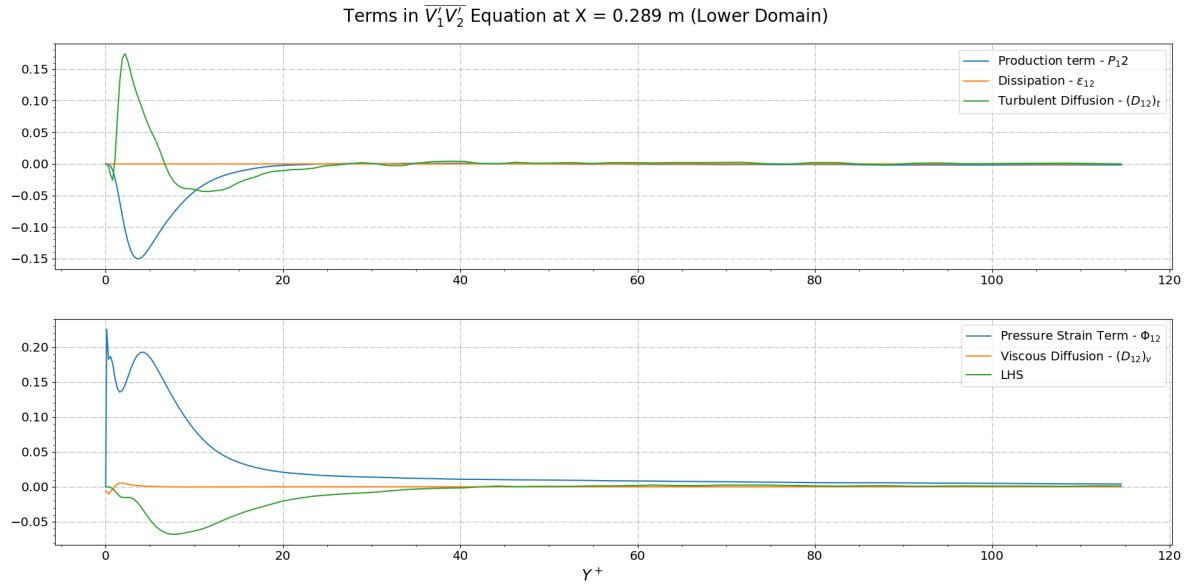


Figure 21: Terms in $\bar{V}_1' \bar{V}_2'$ equation in upper domain

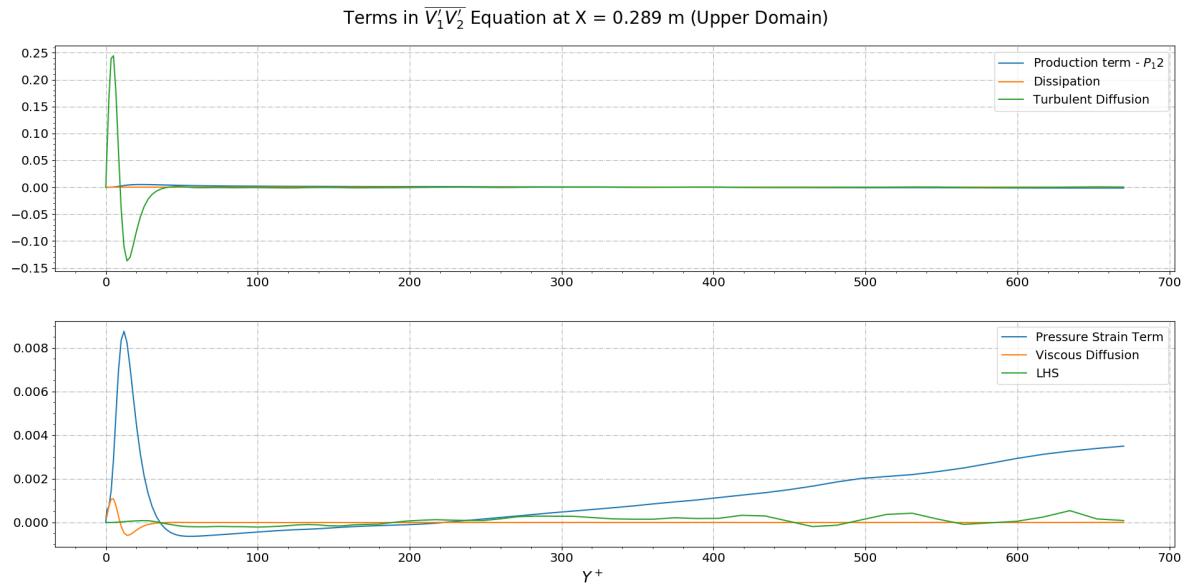


Figure 22: Terms in $\bar{V}_1' \bar{V}_2'$ equation in upper domain

term is higher near the wall but it goes to zero as we enter the log-law region. If we zoom in the outer region, production term balances the pressure-strain term and dissipation term.

- For upper domain in $\bar{V}_1' \bar{V}_2'$ equation, the turbulent diffusion is very high as compared to other quantities. This is because the term is calculated based on the eddy viscosity, which is very high near the upper wall as Boussinesq assumption over-predicts the turbulence due to its isotropic turbulence assumption. Near the wall, viscous diffusion is high and pressure-strain acts as the source term.
- For lower domain in $\bar{V}_1' \bar{V}_2'$ equation, the production term is negative, this implies that the shear stress is negative in this region. The dissipation term is zero. Pressure-strain term and turbulent

diffusion term acts as the sink near the wall. The pressure-strain term is balanced by the production term in outer region.

- For upper domain in $\overline{V_1' V_2'}$ equation, the pressure strain term increases as we go away from the wall, this means the shear stress is being redistributed to the normal stresses (as pressure-strain term is called Robinhood term) in that region.

2.8 Assignment 1.8

Figure 23 and figure 24 compares the Eddy viscosity stresses with the Reynolds stress at two locations in the domain from upper as well as lower domain.

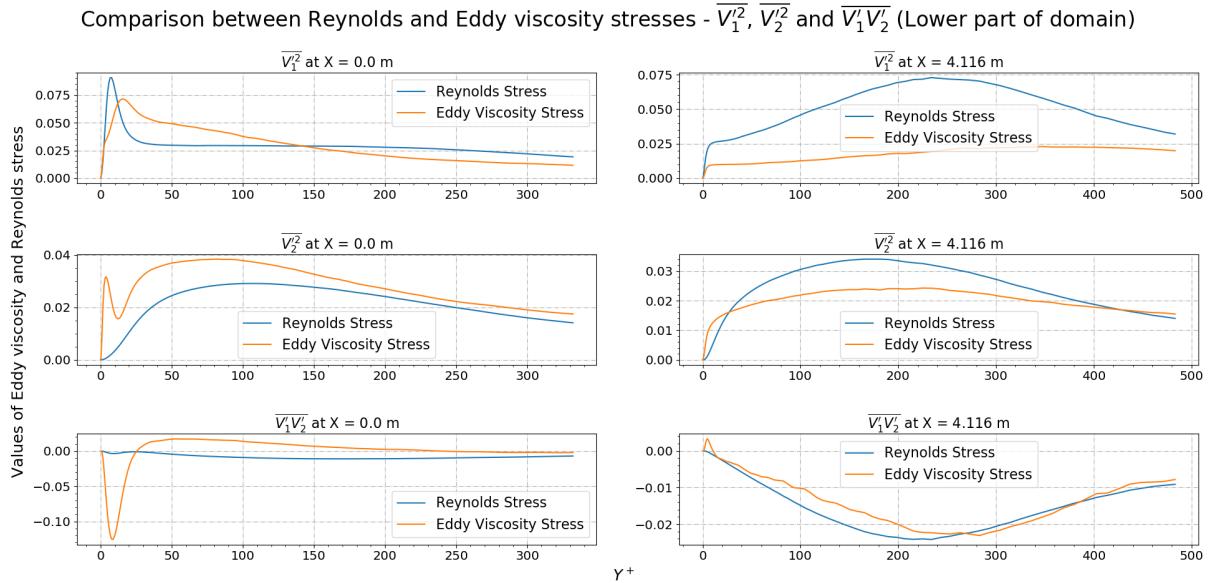


Figure 23: Reynolds and Eddy Viscosity stresses in Lower part of Domain

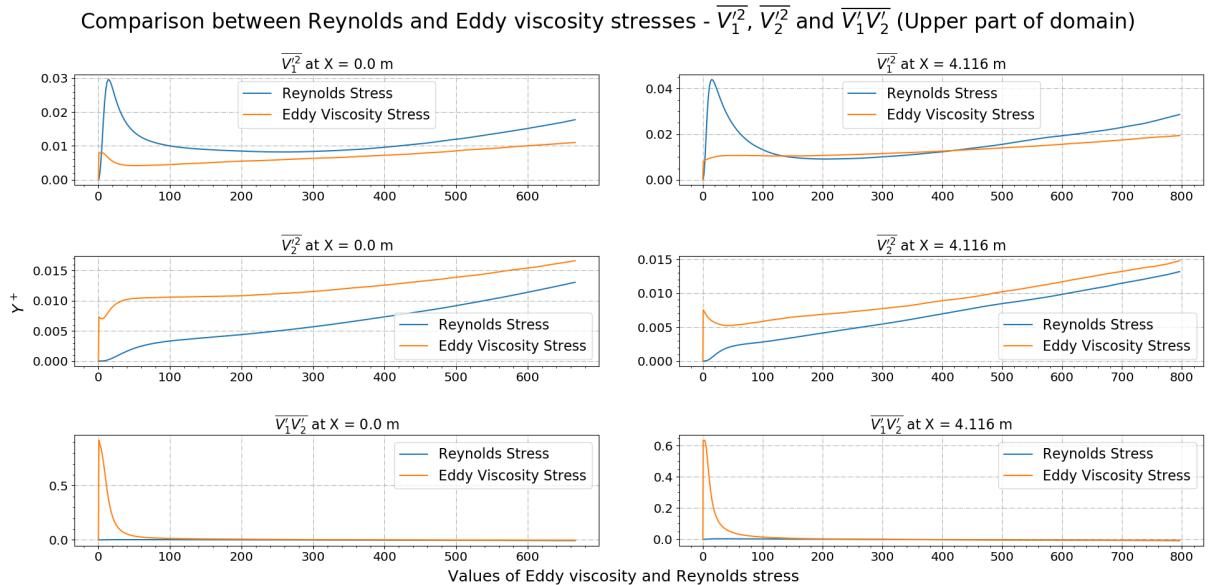


Figure 24: Reynolds and Eddy Viscosity stresses in Upper part of Domain

- In the lower part of the domain (figure 23), the eddy viscosity stresses are larger than the reynolds stress near the wall (in viscous and log-law region). But the reynolds stress in streamwise direction is higher than eddy viscosity stress.

- In the upper part of the domain (figure 24), the wall normal and shear stress calculated by Boussinesq assumption are higher than the Reynolds stress, whereas the Reynolds stress in flow direction is higher than its eddy viscosity counterpart. Thus the assumption of isotropic turbulence tends to over-predict the stresses in eddy viscosity model especially near the wall.
- On the left side of figure 25, the regions where the eddy viscosity stresses are greater than the reynolds stresses can be visualized. Regions with a positive value means that eddy viscosity stress is greater than the reynolds stress.
- The normal stresses are over-predicted along the lower wall in Boussinesq assumption, whereas along the top wall the shear stresses calculated using Boussinesq assumption are larger than the actual ones.
- Due to the higher stresses calculated near the walls than the actual ones in Boussinesq assumption, the turbulent viscosity is also high and that in turn over-predicts the turbulence near walls. Realizability concept can be used to dampen the near wall turbulence which is explained in subsequent sections.
- In the recirculation and other regions, reynolds stresses are higher than the eddy viscosity stresses. This figure better explains the line graphs given in figure 23 and figure 24.

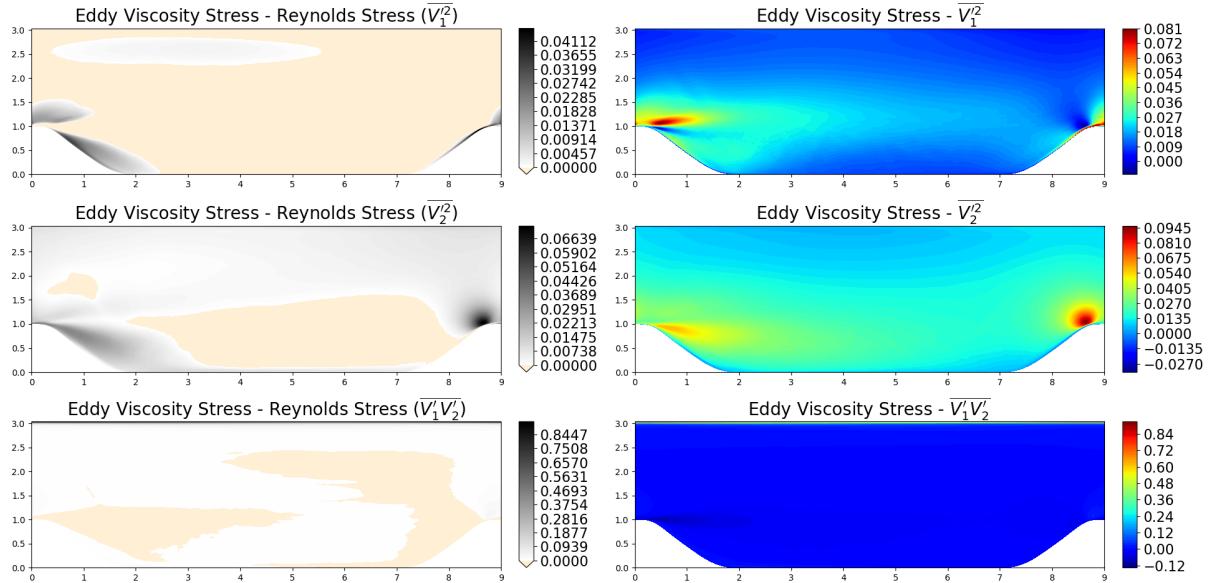


Figure 25: Contour for Reynolds and Eddy Viscosity Stresses

2.9 Assignment 1.9

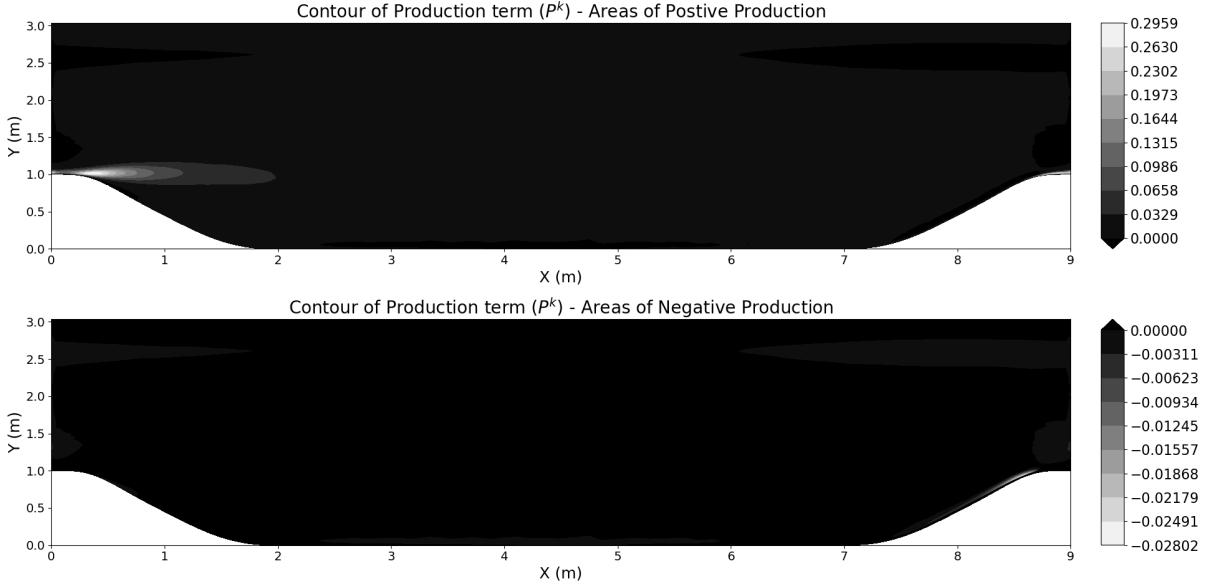


Figure 26: Production term of Turbulent Kinetic Energy - Exact

Figure 26 shows the contour of the exact production term of turbulent kinetic energy. In the top figure, we can see the areas where production term is positive - black means it is negative production. In the bottom figure, we get an idea of how big the negative production terms are.

- It can be seen that the negative production is higher near the second hill, i.e. stagnation region. The production term is the product of an inertial force per unit mass (acceleration) and fluctuating velocity. Hence, the fluctuations are doing work on mean flow field in this region.
- The production term is biggest near separation region, which is likely as turbulence is generated at the hill where flow is separating from the bottom wall.

Figure 27 shows the contour of the production term of turbulent kinetic energy calculated using Boussinesq assumption.

- The turbulence is over-predicted as can be seen from the figure near the top wall. The production value is very much higher than what it is in rest of the domain. This can be because of the isotropic turbulence assumption in Boussinesq hypothesis.
- In rest of the domain, the production is present in separation and stagnation region. One thing is that the production term is positive everywhere, unlike the exact production term shown in figure 26.
- An interesting observation - when we apply the realizability concept, it dampens the turbulence near the top wall, as discussed in section 2.10 below. Due to this, the production term near the top wall also decreases substantially, see figure 28. If we compare figure 27 and 28, near the top wall, using realizability concept gives results closer to the DNS data.

Figure 29 shows that the eigenvectors of modeled Reynolds stress and Strain rate tensor are parallel. This is the reason why the modeled production term in turbulent kinetic energy is always positive.

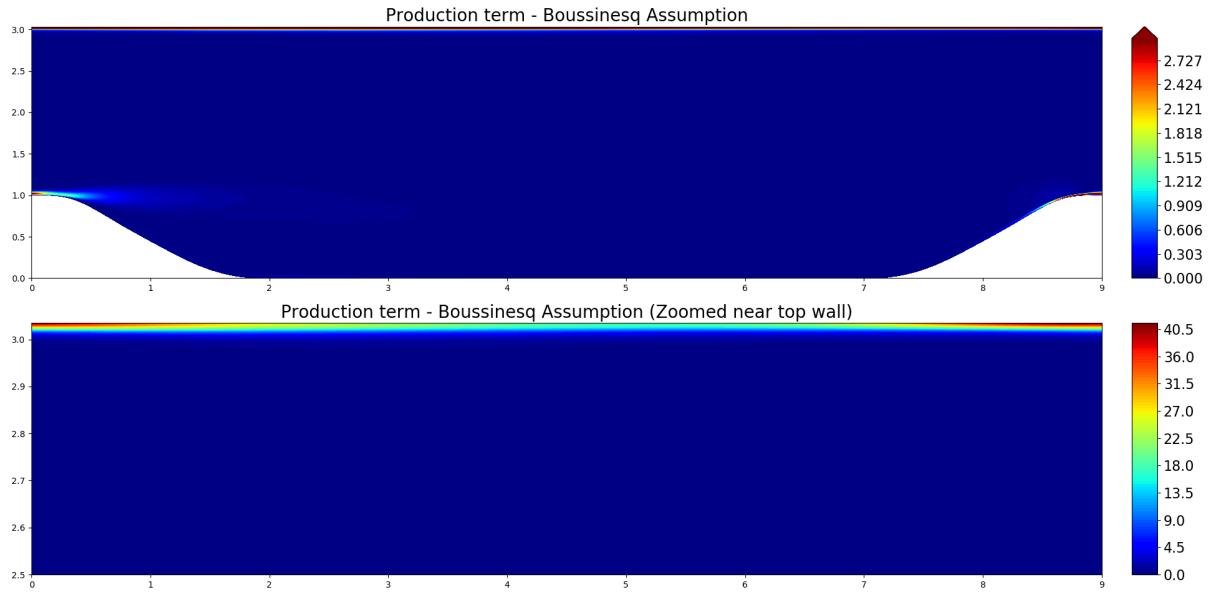


Figure 27: Production term of Turbulent Kinetic Energy - Boussinesq Assumption

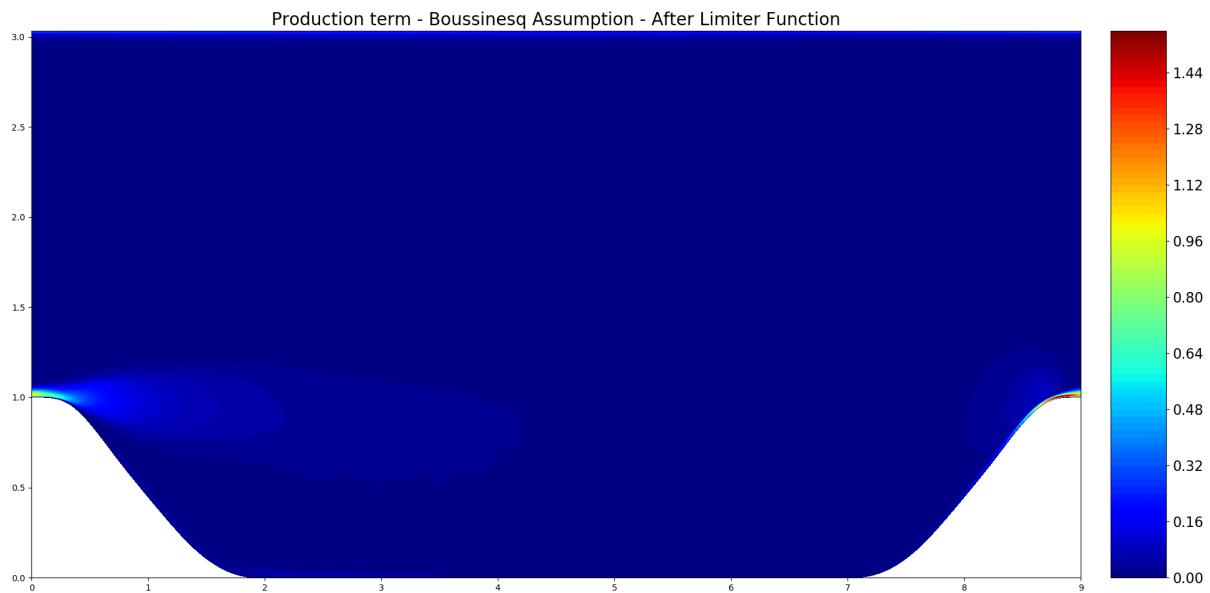


Figure 28: Production term of Turbulent Kinetic Energy - Boussinesq Assumption (After applying the limiter function)

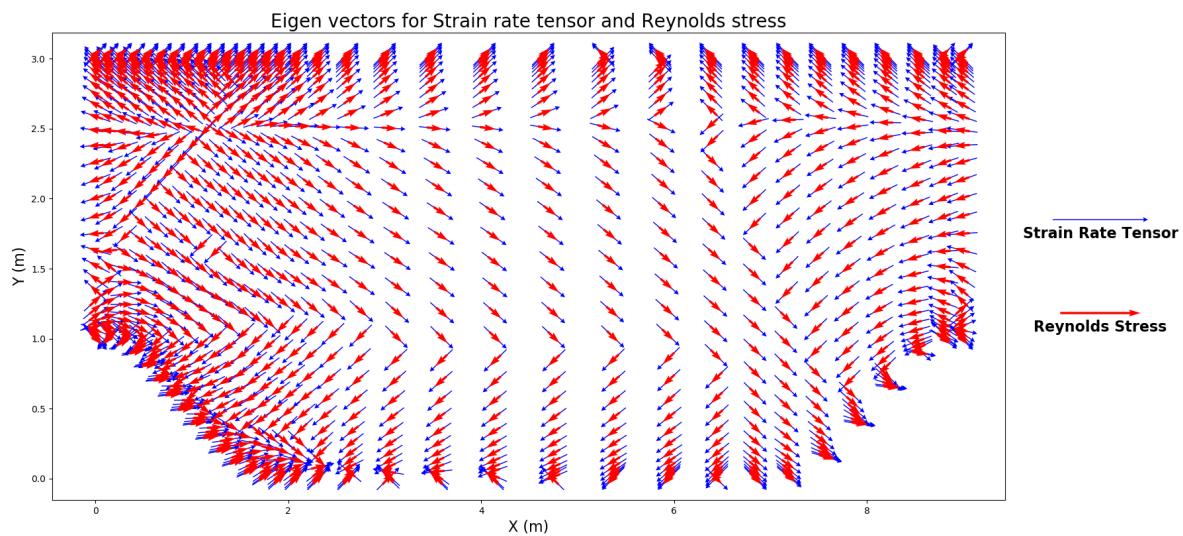


Figure 29: Eigenvectors of Reynolds stress and Strain rate tensor

2.10 Assignment 1.10

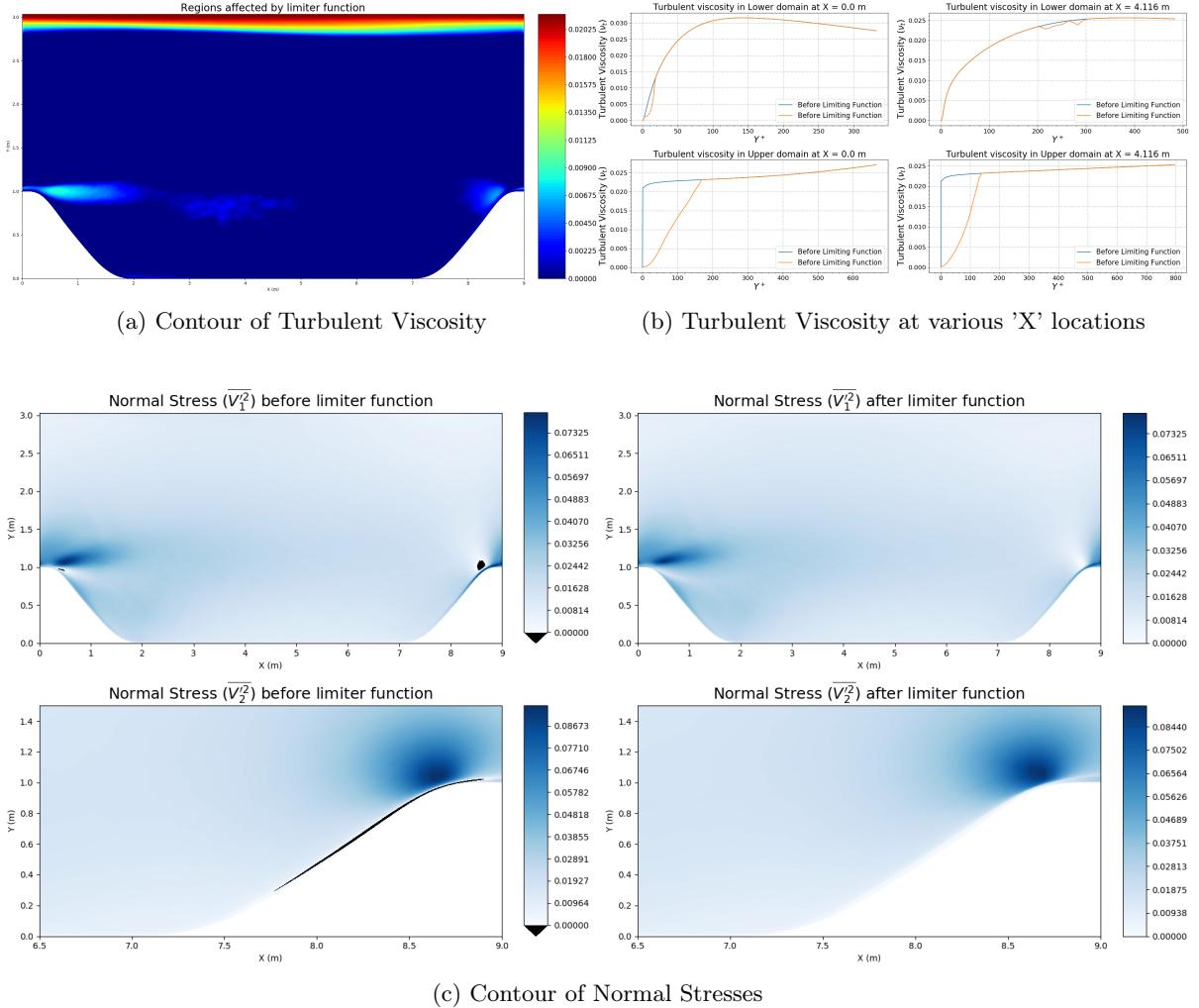


Figure 30: Effect of Limiting Function on Normal Stress and Turbulent Viscosity

The realizability concept is used to limit the normal stresses in stagnation regions such that they are positive at all times. We limit the turbulent viscosity using the eigenvalues of the strain rate tensor.

- In figure 30a we can observe the regions affected by the limiter function. The contour basically is the difference of original turbulent viscosity ($\nu_t)_O$ and modified turbulent viscosity ($\nu_t)_M$. Hence the blue region (value = 0) represents that the limiter function has no effect on that particular region (i.e. $(\nu_t)_O < (\nu_t)_M$).
- It can be seen that the limiter has the most effect near the top wall. Near the top wall, Boussinesq hypothesis over-predicts the turbulence viscosity due to its assumption of isotropic turbulence. Using the realizability concept, we can dampen the turbulent viscosity at the wall.
- Near the hill, where separation (left hill) and stagnation region (right hill) are present, turbulent viscosity is limited by the limiter function. Realizability concept dampens the turbulence in these regions as well.
- In figure 30c, the contour of normal stresses ($\bar{V}_1'^2$ and $\bar{V}_2'^2$) are shown. The sub-figures on left side are for normal stresses calculated using boussinesq assumption using the original turbulent viscosity

$(\nu_t)_O$. Whereas the sub-figures on right side denotes the value of normal stresses calculated using the modified turbulent viscosity $(\nu_t)_M$.

- Originally, the normal stresses are negative at some places, predominantly at the stagnation region near the hill as indicated by black color in figure 30c. After using the limiter function, we can see that the normal stresses are not negative anymore, thus we can conclude that the limiter concept in realizability makes the normal stresses $(\bar{V_i'^2})$ positive.

2.11 Assignment - Backward Facing Step

Various Eddy viscosity as well as Reynolds stress turbulence models were implemented on the given geometry in Star-CCM+. The base mesh size in all the models was constant with addition of prism layers near walls based on the requirement of the turbulence model to resolve or model the boundary layer.

- The Standard $k-\varepsilon$ and Realizable $k-\varepsilon$ model implements wall functions (High y^+ wall treatment) to model the near wall behaviour and needs a y^+ value greater than 30. Hence a base size of 0.1 m was used without any prism layers.
- The Standard and SST $k-\omega$ as well as the RSM Elliptic Blending model uses All y^+ wall treatment and y^+ value is kept below 1 using prism layers to ensure that the viscous sub-layer is properly resolved by the mesh.
- The two layer models for Standard $k-\varepsilon$, Realizable $k-\varepsilon$ and RSM Linear Pressure Term implements a blending function similar to All y^+ wall treatment to model the near wall turbulence. For these models as well, y^+ value is kept below 1.

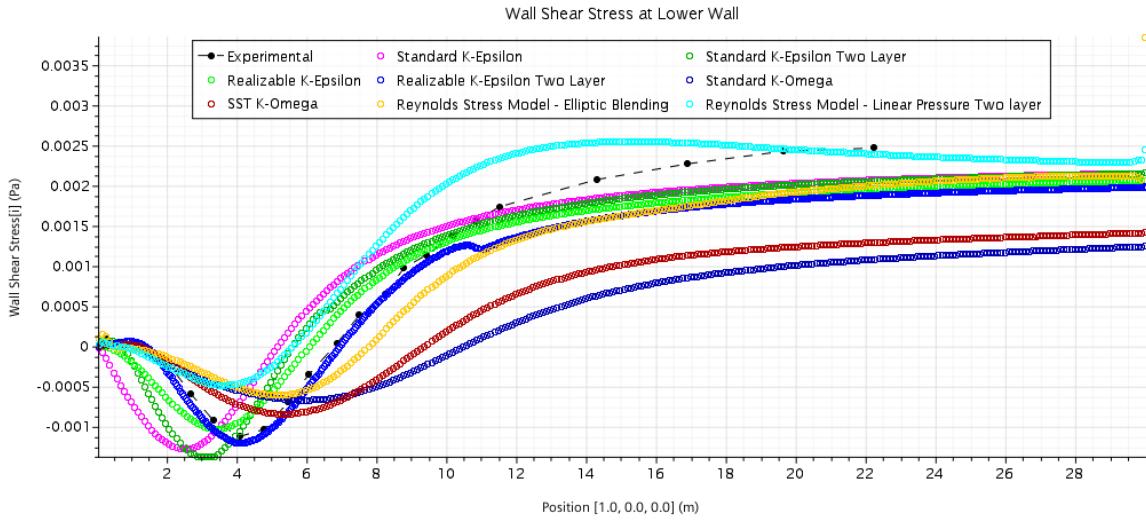


Figure 31: Wall Shear Stress at Lower wall using various Turbulence models

The simulation results for the Wall shear stress and Nusselt number on the lower wall are compared with experimental data as seen in figure 31 and figure 32. From figure 31, we can observe that the realizable $k-\varepsilon$ and realizable $k-\varepsilon$ two layer model is better than other models at predicting the wall shear stress. The $k-\varepsilon$ models perform better than $k-\omega$ models when there is separation due to geometry changes, which can be seen from the results as well. Both Standard and SST $k-\omega$ models are giving an erroneous result. To conclude this study, realizable $k-\varepsilon$ model is better in predicting the wall shear stress and nusselt number for a backward facing step. Based on the computational power available, one can choose between the two layer or high y^+ wall treatment.

Figure 33 and figure 34 are the contours for velocity and turbulent kinetic energy obtained for Realizable $k-\varepsilon$ model. The re-circulation region can be seen near the step. In the shear layer, which starts from the step, the turbulent kinetic energy increases as there is formation of vortices. It is maximum in the region of primary vortex and where the flow is about to reattach the lower wall.

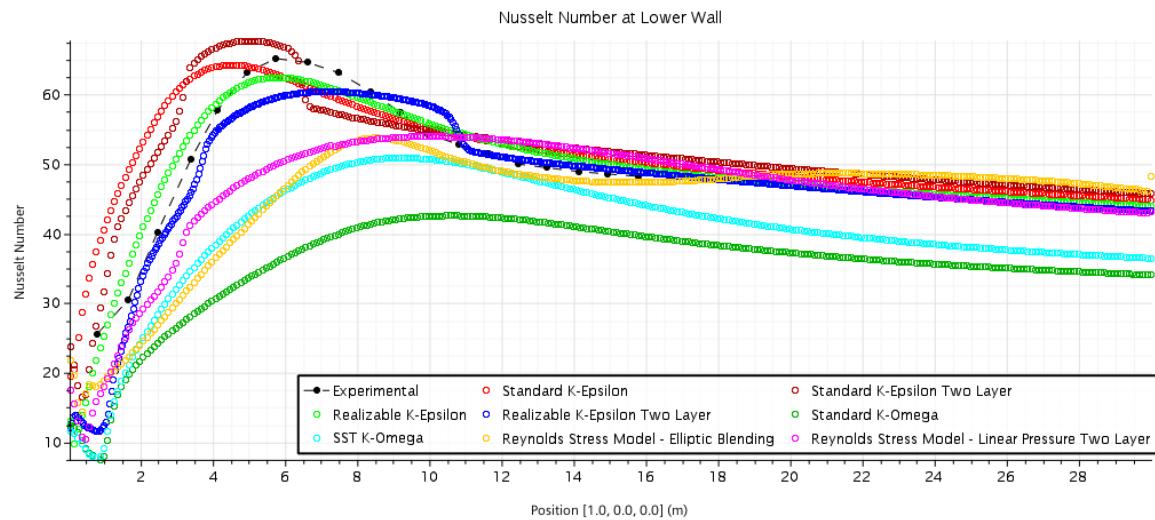


Figure 32: Nusselt Number at Lower wall using various Turbulence models

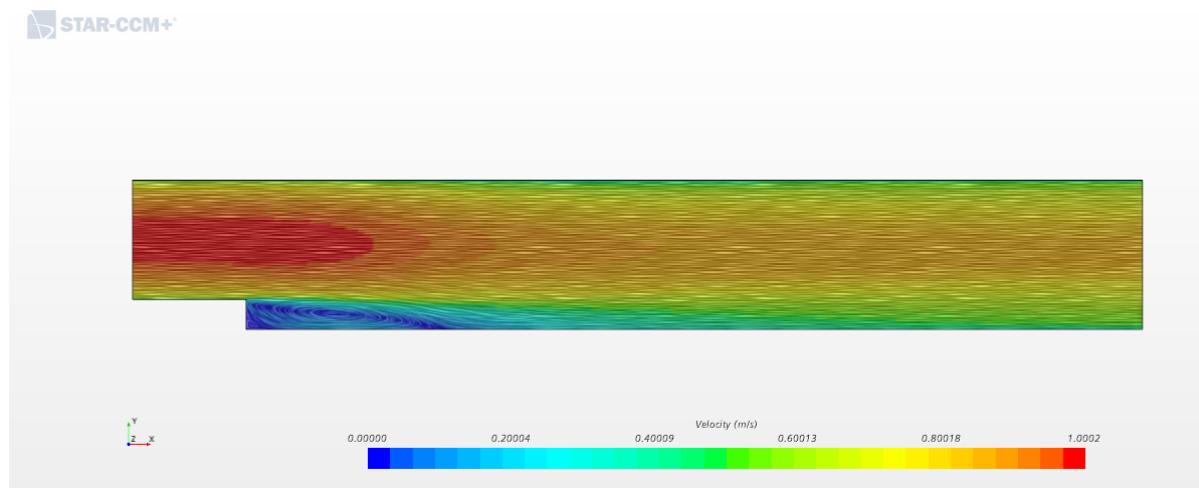


Figure 33: Velocity LIC for Realizable $k - \varepsilon$ model

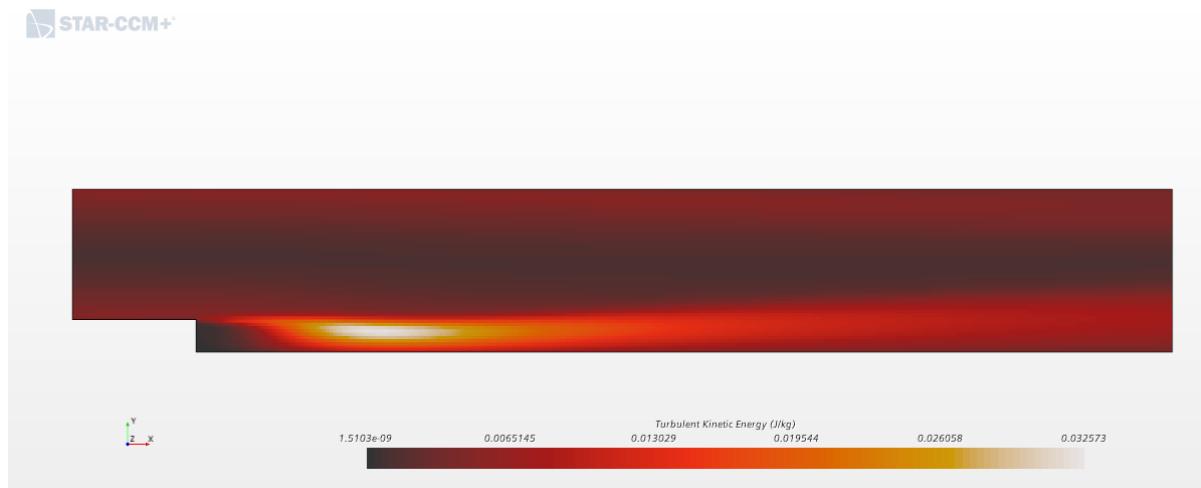


Figure 34: Turbulent Kinetic Energy for Realizable $k - \varepsilon$ model

2.12 Assignment - Asymmetric Diffuser (Turbulence Models)

The turbulence models that were used for Backward facing step are used for this case as well. The base mesh size is kept same in all the cases with a finer mesh near walls to achieve the desired y^+ value as per selected turbulence model.

Figure 35 shows the velocity LIC's for all the turbulence models. A diffuser is characterised by flow separation and re-circulation in the diverging section due to adverse pressure gradient. The Standard $k - \varepsilon$ and Standard $k - \varepsilon$ (two layer) model does not predict the re-circulation region and the flow remains attached throughout, as seen in figure 35a and 35b. Realizable $k - \varepsilon$ is also bad at predicting the separation, but slightly better than Standard $k - \varepsilon$ models, see figure 35c and 35d. The reason behind poor performance of $k - \varepsilon$ models can be due to the fact that they assume isotropic turbulence near the wall. These models basically use wall functions to model the boundary layer in viscous and buffer region. As the boundary layer is not properly resolved, it cannot predict separation arising due to adverse pressure gradient.

Realizable $k - \varepsilon$ (two layer), Standard $k - \omega$, SST $k - \omega$ model and Reynolds stress models are able to model the flow separation and the re-circulation zone. Realizable $k - \varepsilon$ (two layer) and SST $k - \omega$ model are nearly similar when it comes to predicting the flow separation, but the near-wall boundary layer is better resolved in $k - \omega$ model as seen from the comparison with experimental data in figure 36.

Figure 36a - Figure 36j compares the velocity profile at various locations in the diffuser for different turbulence models. Upstream of the diffuser, the velocity profile is nearly the same for all turbulence models as seen from figure 36a. Downstream of the diffuser, the velocity profiles vary drastically as the re-circulation region changes depending on the chosen turbulence model for simulation. The $k - \omega$ (especially, SST variant) and Reynolds stress models agree the most with experiments at nearly all the locations as shown in figure 36. To conclude, we could say that SST $k - \omega$ and Reynolds stress - Elliptic blending model performs well for a asymmetric diffuser geometry. But the Reynolds stress model are computationally heavy and require more iterations to reach a steady state, hence SST $k - \omega$ is preferred over it. Whereas, the $k - \varepsilon$ models are bad at prediction flow separation due to adverse pressure gradient.

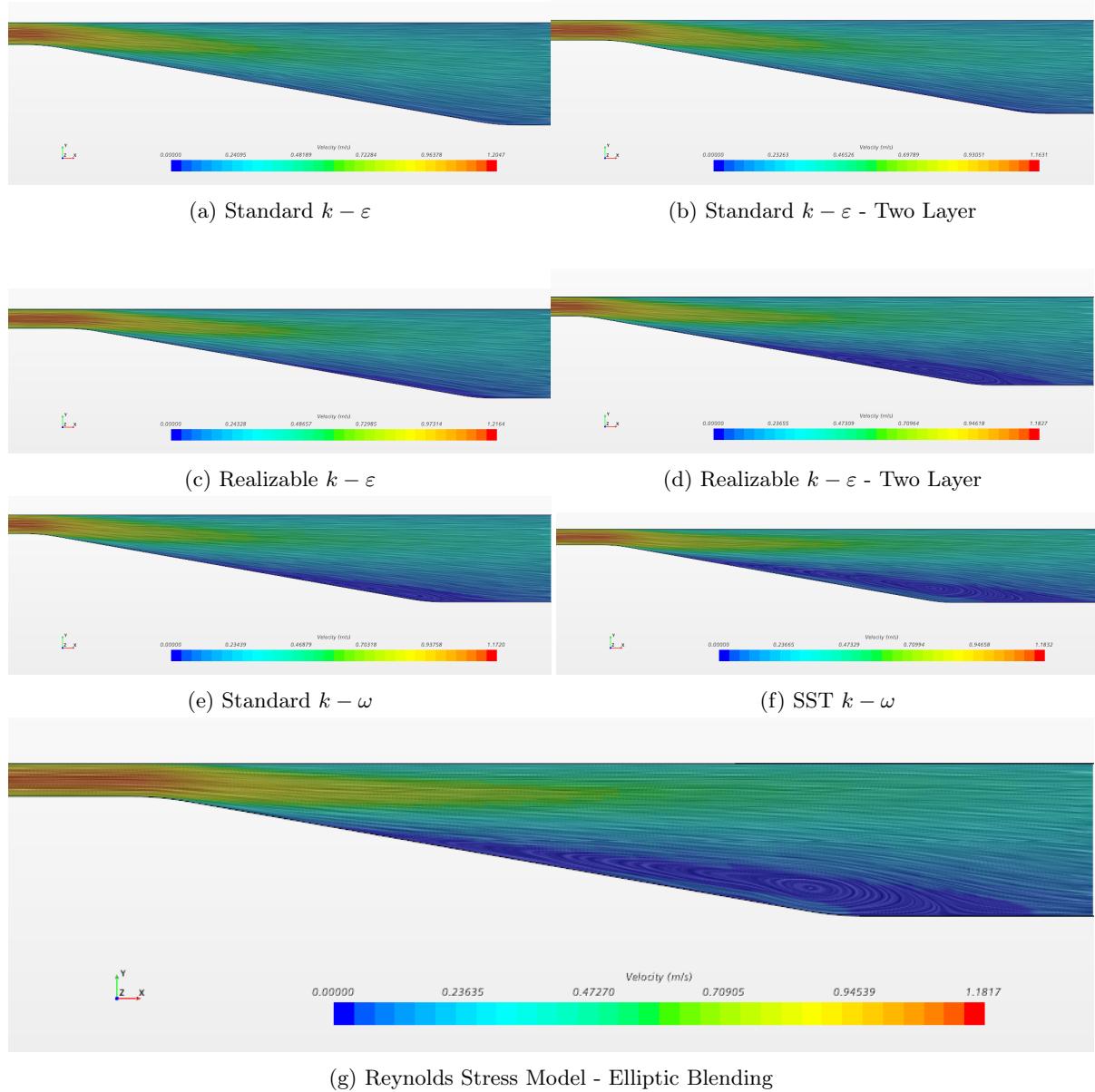


Figure 35: LIC of velocity for various turbulence models

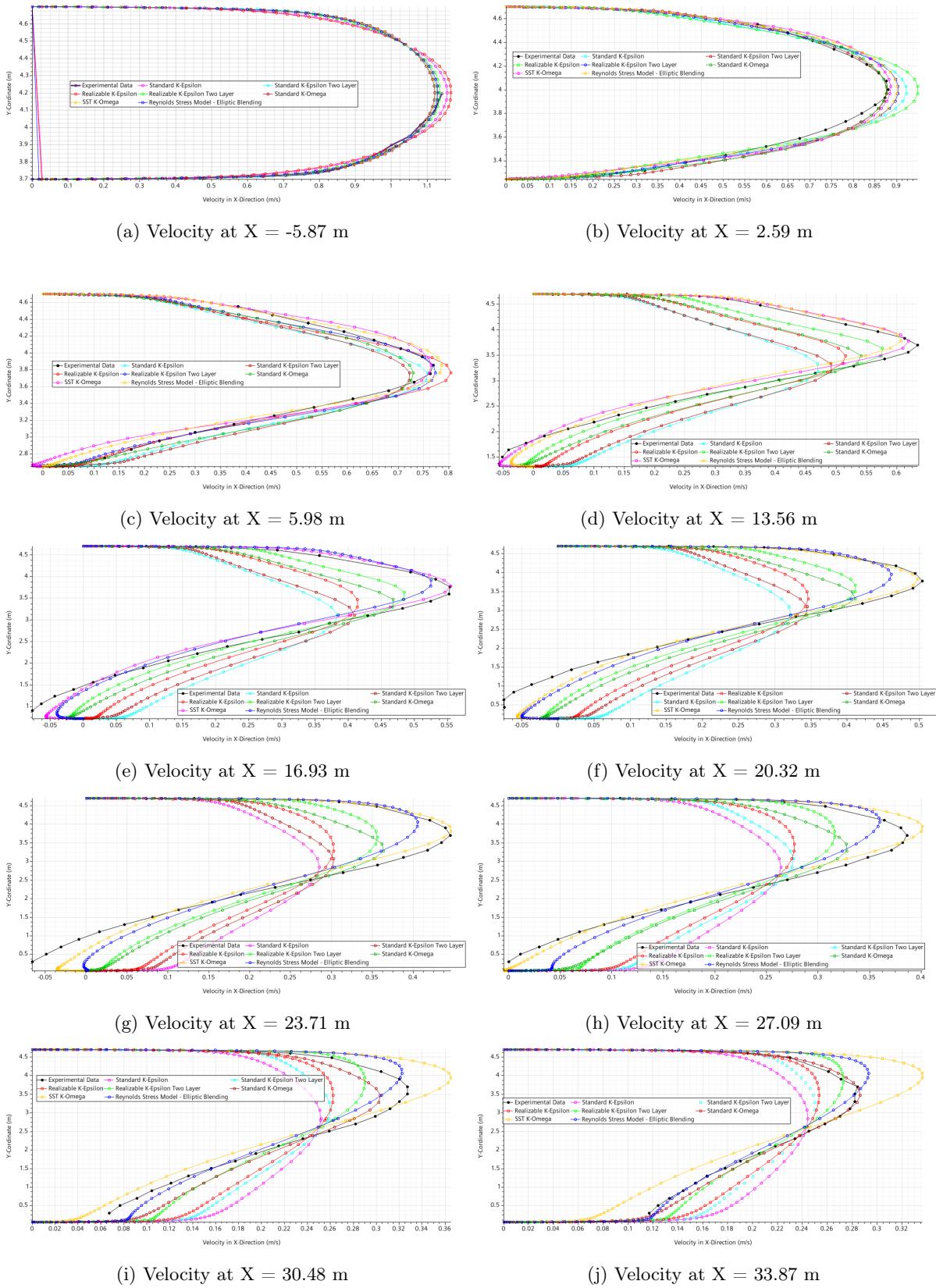


Figure 36: Comparison of Turbulence Models

2.13 Assignment - Asymmetric Diffuser (Pressure Recovery)

The pressure recovery and pressure drop is compared for various turbulence models for the asymmetric diffuser case. Pressure drop is used as a convergence criteria for the simulations. Pressure recovery is an important parameter to evaluate the diffuser performance. The diffuser should convert maximum possible kinetic energy to pressure by decelerating the fluid as a consequence of increase in area. Thus pressure recovery gives a measure of how much static pressure is regained.

$$\text{Pressure Recovery} = \text{Static Pressure @ Outlet} - \text{Static Pressure @ Inlet} \quad (1)$$

$$\text{Pressure Drop} = \text{Total Pressure @ Inlet} - \text{Total Pressure @ Outlet} \quad (2)$$

Table 1: Pressure Recovery and Pressure Drop for various Turbulence models

Turbulence Models	Pressure Recovery (Pa)	Pressure Drop (Pa)
Standard K- ε	-0.2150548	0.7785385
Standard K- ε Two Layer	0.0638940	0.4994603
Realizable K- ε	-0.2030131	0.7660116
Realizable K- ε Two Layer	0.0588291	0.5040755
Standard K- ω	0.0608963	0.5009818
SST K- ω	0.0487484	0.5104201
Reynolds Stress Model - Elliptic Blending	0.0263190	0.5369382

The Standard and Realizable $k - \varepsilon$ model is a poor choice of turbulence model for this type of flow as we saw in earlier section. Additionally, it gives an erroneous value of pressure recovery as well. The reason could be since the y^+ values are less than 1, but these models use a high y^+ near wall treatment which requires for $y^+ > 30$. Due to this bad meshing approach, they are far away from predicting the correct flow behaviour even when compared to its two layer model counterparts.

A Appendix

```
 1 import scipy.io as sio
 2 import numpy as np
 3 import matplotlib.pyplot as plt
 4 from dphidx_dy import dphidx_dy
 5 from WallDistance import WallDistance
 6 from WallNormal import WallNormal
 7 from IPython import display
 8 from matplotlib.ticker import (MultipleLocator, FormatStrFormatter,
 9                                 AutoMinorLocator)
10 #plt.rcParams.update({'font.size': 20})
11
12 # makes sure figures are updated when using ipython
13 display.clear_output()
14
15 # read data file
16 tec=np.genfromtxt("tec.dat", dtype=None, comments="#")
17
18 #text='VARIABLES = X Y P U V u2 v2 w2 uv mu_sgs prod'
19
20 x=tec[:,0]
21 y=tec[:,1]
22 p=tec[:,2]
23 u=tec[:,3]
24 v=tec[:,4]
25 uu=tec[:,5]
26 vv=tec[:,6]
27 ww=tec[:,7]
28 uv=tec[:,8]
29 k=0.5*(uu+vv+ww)
30
31 if max(y) == 1.:
32     ni=170
33     nj=194
34     nu=1./10000.
35 else:
36     nu=1./10595.
37     if max(x) > 8.:
38         nj=162
39         ni=162
40     else:
41         ni=402
42         nj=162
43
44 viscos=nu
45
46 u2d=np.reshape(u,(nj,ni))
47 v2d=np.reshape(v,(nj,ni))
48 p2d=np.reshape(p,(nj,ni))
49 x2d=np.reshape(x,(nj,ni))
50 y2d=np.reshape(y,(nj,ni))
51 uu2d=np.reshape(uu,(nj,ni)) #=mean{v'_1v'_1}
52 uv2d=np.reshape(uv,(nj,ni)) #=mean{v'_1v'_2}
53 vv2d=np.reshape(vv,(nj,ni)) #=mean{v'_2v'_2}
54 k2d=np.reshape(k,(nj,ni))
55
56 u2d=np.transpose(u2d)
57 v2d=np.transpose(v2d)
58 p2d=np.transpose(p2d)
59 x2d=np.transpose(x2d)
60 y2d=np.transpose(y2d)
61 uu2d=np.transpose(uu2d)
62 vv2d=np.transpose(vv2d)
63 uv2d=np.transpose(uv2d)
```

```
64 k2d=np.transpose(k2d)
65
66 # set periodic b.c on west boundary
67 #u2d[0,:] = u2d[-1,:]
68 #v2d[0,:] = v2d[-1,:]
69 #p2d[0,:] = p2d[-1,:]
70 #uu2d[0,:] = uu2d[-1,:]
71
72 # read k and eps from a 2D RANS simulations. They should be used for computing the
# damping function f
73 k_eps_RANS = np.loadtxt("k_eps_RANS.dat")
74 k_RANS=k_eps_RANS[:,0]
75 diss_RANS=k_eps_RANS[:,1]
76 vist_RANS=k_eps_RANS[:,2]
77
78 ntstep=k_RANS[0]
79
80 k_RANS_2d=np.reshape(k_RANS,(ni,nj))/ntstep
81 diss_RANS_2d=np.reshape(diss_RANS,(ni,nj))/ntstep
82 vist_RANS_2d=np.reshape(vist_RANS,(ni,nj))/ntstep
83
84 # set small values on k & eps at upper and lower boundaries to prevent NaN on division
85 diss_RANS_2d[:,0]= 1e-10
86 k_RANS_2d[:,0]= 1e-10
87 vist_RANS_2d[:,0]= nu
88 diss_RANS_2d[:, -1]= 1e-10
89 k_RANS_2d[:, -1]= 1e-10
90 vist_RANS_2d[:, -1]= nu
91
92 # set Neumann of p at upper and lower boundaries
93 p2d[:,1]=p2d[:,2]
94 p2d[:, -1]=p2d[:, -1-1]
95
96 # x and y are fo the cell centers. The dphidx_dy routine needs the face coordinate, xf2d
# , yf2d
97 # load them
98 xc_yc = np.loadtxt("xc_yc.dat")
99 xf=xc_yc[:,0]
100 yf=xc_yc[:,1]
101 xf2d=np.reshape(xf,(nj,ni))
102 yf2d=np.reshape(yf,(nj,ni))
103 xf2d=np.transpose(xf2d)
104 yf2d=np.transpose(yf2d)
105
106 # delete last row
107 xf2d = np.delete(xf2d, -1, 0)
108 yf2d = np.delete(yf2d, -1, 0)
109 # delete last columns
110 xf2d = np.delete(xf2d, -1, 1)
111 yf2d = np.delete(yf2d, -1, 1)
112
113 # compute the gradient dudx, dudy at point P
114 dudx= np.zeros((ni,nj))
115 dudy= np.zeros((ni,nj))
116 dvdx= np.zeros((ni,nj))
117 dvdy= np.zeros((ni,nj))
118
119 dudx,dudy=dphidx_dy(xf2d,yf2d,u2d)
120 dvdx,dvdy=dphidx_dy(xf2d,yf2d,v2d)
121 ''
122 ##### vector plot
123 fig1 = plt.figure("Figure 1")
124 k=2# plot every forth vector
125 ss=3.2 #vector length
126 plt.quiver(x2d[:,::k,::k],y2d[:,::k,::k],u2d[:,::k,::k],v2d[:,::k,::k])
127 plt.xlabel("$x$")
```

```
128 plt.ylabel("$y$")
129 plt.title("vector plot")
130
131 ##### contour plot
132 fig2 = plt.figure("Figure 2")
133 plt.contourf(x2d,y2d,u2d,100,cmap='jet')
134 plt.xlabel("$X$ (m)", fontsize=20)
135 plt.ylabel("$Y$ (m)", fontsize=20)
136 plt.title("Velocity in X-direction ($\overline{u}$) - DNS Data", fontsize=24)
137 cb = plt.colorbar()
138 cb.ax.tick_params(labelsize=18)
139 plt.xticks(fontsize=15)
140 plt.yticks(fontsize=15)
141
142 fig3 = plt.figure("Figure 3")
143 plt.contourf(x2d,y2d,v2d,100,cmap='jet')
144 plt.xlabel("$X$ (m)", fontsize=20)
145 plt.ylabel("$Y$ (m)", fontsize=20)
146 plt.title("Velocity in Y-direction ($\overline{v}$) - DNS Data", fontsize=24)
147 cb = plt.colorbar()
148 cb.ax.tick_params(labelsize=18)
149 plt.xticks(fontsize=15)
150 plt.yticks(fontsize=15)
151
152 fig4 = plt.figure("Figure 4")
153 plt.contourf(x2d,y2d,p2d,100,cmap='jet')
154 plt.xlabel("$X$ (m)", fontsize=20)
155 plt.ylabel("$Y$ (m)", fontsize=20)
156 plt.title("Pressure ($\overline{P}$) - DNS Data", fontsize=24)
157 cb = plt.colorbar()
158 cb.ax.tick_params(labelsize=18)
159 plt.xticks(fontsize=15)
160 plt.yticks(fontsize=15)
161
162 ##### contour plot
163 fig5 = plt.figure("Figure 5")
164 plt.contourf(x2d,y2d,k_RANS_2d,100,cmap='jet')
165 plt.xlabel("$X$ (m)", fontsize=20)
166 plt.ylabel("$Y$ (m)", fontsize=20)
167 plt.title("Turbulent Kinetic Energy - RANS Simulation", fontsize=24)
168 cb = plt.colorbar()
169 cb.ax.tick_params(labelsize=18)
170 plt.xticks(fontsize=15)
171 plt.yticks(fontsize=15)
172
173 ****
174 # plot uv
175 fig6 = plt.figure("Figure 6")
176 i=10
177 plt.plot(uv2d[i,:],y2d[i,:],'b-')
178 plt.xlabel('$\overline{u}^{\prime} \overline{v}^{\prime}$')
179 plt.ylabel('y/H')
180 ''
181 #%%
182 # Plot Mesh for Visualization
183 a = np.transpose(xf2d)
184 b = np.transpose(yf2d)
185 fig1 = plt.figure()
186 axes = fig1.add_axes([0.1,0.1,0.8,0.8])
187 axes.plot(xf2d,yf2d,color='black')
188 axes.plot(a,b,color='black')
189 #axes.plot(x2d[:,81],y2d[:,81],color='red',lw=2)
190 axes.tick_params(axis="x", labelsize=15)
191 axes.tick_params(axis="y", labelsize=15)
192 axes.set_xlabel('x [m]', fontsize=20)
193 axes.set_ylabel('y [m]', fontsize=20)
```

```

194 axes.set_title('Computational mesh in the domain', fontsize=24)
195
196 # Finding Y+ value in the domain
197 #yplus[:,0-81] - lowerhalf of the domain
198 #yplus[:,82-162] - upper half of the domain.
199
200 # Diffusion term in momentum equation
201 dub_dx, dub_dy = dphidx_dy(xf2d, yf2d, u2d)
202 dvb_dx, dvb_dy = dphidx_dy(xf2d, yf2d, v2d)
203
204 tau_wall = np.zeros((ni,nj))
205 yplus = np.zeros((ni,nj))
206 for i in range(ni):
207     for j in range(1,nj-1):
208         tau_wall[i,j] = nu * np.abs(dub_dy[i,0])
209         if j<=81:
210             yplus[i,j] = (y2d[i,j]-y2d[i,0]) * np.sqrt(np.abs(dub_dy[i,0]/nu))
211         else:
212             yplus[i,j] = (y2d[i,-1]-y2d[i,j]) * np.sqrt(np.abs(dub_dy[i,-1]/nu))
213
214 #%% Assignment 1.1 - Plot the stresses along vertical grid lines at high and low
215 # turbulence regions
216 # Plot uu2d, vv2d, uv2d at two locations in the domain
217 gl1 = 0
218 gl2 = 100
219
220 tau11 = (nu * dub_dx) - uu2d
221 tau12 = (nu * dub_dy) - uv2d
222 tau22 = (nu * dvb_dy) - vv2d
223 tau21 = (nu * dvb_dx) - uv2d
224
225 # Near bottom wall
226 fig2 = plt.figure()
227 ax1 = plt.subplot2grid((2,2), (0,0), colspan=2)
228 ax2 = plt.subplot2grid((2,2), (1,0))
229 ax3 = plt.subplot2grid((2,2), (1,1))
230 ax1.contourf(x2d,y2d,v2d,cmap='jet',levels=100,alpha=0.5)
231 ax1.plot(x2d[gl1,:],y2d[gl1,:],color='black')
232 ax1.plot(x2d[gl2,:],y2d[gl2,:],color='red')
233 ax1.plot(x2d[:,81],y2d[:,81],color='green',lw=2)
234 ax1.set_title('Location of Gridlines for plotting', fontsize=20)
235 ax1.text(2, 2, 'Upper half of domain', fontsize=20, color="black")
236 ax1.text(2, 1, 'Lower half of domain', fontsize=20, color="black")
237 ax2.plot(tau11[gl1,0:81],yplus[gl1,0:81])
238 ax2.plot(tau22[gl1,0:81],yplus[gl1,0:81])
239 ax2.plot(tau12[gl1,0:81],yplus[gl1,0:81])
240 ax2.plot(tau21[gl1,0:81],yplus[gl1,0:81])
241 ax2.set_title('Stresses at X = '+str(np.around(x2d[gl1,0],3))+ ' m', fontsize=20)
242 ax3.plot(tau11[gl2,0:81],yplus[gl2,0:81])
243 ax3.plot(tau22[gl2,0:81],yplus[gl2,0:81])
244 ax3.plot(tau12[gl2,0:81],yplus[gl2,0:81])
245 ax3.plot(tau21[gl2,0:81],yplus[gl2,0:81])
246 ax3.set_title('Stresses at X = '+str(np.around(x2d[gl2,0],3))+ ' m', fontsize=20)
247 #ax3.set_ylim(0,100)
248 for ax in [ax1,ax2,ax3]:
249     ax.tick_params(labelsize='medium')
250     ax.xaxis.set_minor_locator(AutoMinorLocator())
251     ax.yaxis.set_minor_locator(AutoMinorLocator())
252     if ax == ax1:
253         ax.legend(['x = '+str(np.around(x2d[gl1,0],3))+ ' m', 'x = '+str(np.around(x2d[gl2,0],3))+ ' m'], loc='best')
254         ax.set_xlabel('x (m)')
255         ax.set_ylabel('y (m)')
256     else:
257         ax.legend(['Normal Stress = $\mu\frac{\partial\overline{u}}{\partial x}$ - $\rho\overline{V_1^2}$'],

```

```

257         r'Normal Stress = $\mu\frac{\partial\overline{v}}{\partial y} - \$\rho\overline{V_2^2}$',
258         r'Shear Stress = $\mu\frac{\partial\overline{u}}{\partial y} - \$\rho\overline{V_1}\overline{V_2}$',
259         r'Shear Stress = $\mu\frac{\partial\overline{v}}{\partial x} - \$\rho\overline{V_1}\overline{V_2}$', loc='best')
260     ax.grid(True, linestyle='-.')
261     ax.set_xlabel('Magnitude of Stress')
262     ax.set_ylabel(r'$Y$')
263 fig2.suptitle('Stresses along Vertical Gridlines in Lower half of the Domain', fontsize=24)
264 '',
265 fig2a = plt.figure()
266 ax1 = plt.subplot2grid((2,2), (0,0), colspan=2)
267 ax2 = plt.subplot2grid((2,2), (1,0))
268 ax3 = plt.subplot2grid((2,2), (1,1))
269 ax1.contourf(x2d,y2d,v2d,cmap='jet',levels=50,alpha=0.5)
270 ax1.plot(x2d[gl1,:],y2d[gl1,:],color='black')
271 ax1.plot(x2d[gl2,:],y2d[gl2,:],color='red')
272 ax1.plot(x2d[:,81],y2d[:,81],color='green',lw=2)
273 ax1.set_title('Location of Gridlines for plotting',fontsize=20)
274 ax1.text(2, 2, 'Upper half of domain', fontsize=20, color="black")
275 ax1.text(2, 1, 'Lower half of domain', fontsize=20, color="black")
276 ax2.plot(uu2d[gl1,0:81],yplus[gl1,0:81])
277 ax2.plot(vv2d[gl1,0:81],yplus[gl1,0:81])
278 ax2.plot(uv2d[gl1,0:81],yplus[gl1,0:81])
279 ax2.set_title('Stresses at X = '+str(np.around(x2d[gl1,0],3))+' m',fontsize=20)
280 ax3.plot(uu2d[gl2,0:81],yplus[gl2,0:81])
281 ax3.plot(vv2d[gl2,0:81],yplus[gl2,0:81])
282 ax3.plot(uv2d[gl2,0:81],yplus[gl2,0:81])
283 ax3.set_title('Stresses at X = '+str(np.around(x2d[gl2,0],3))+' m',fontsize=20)
284 #ax3.set_ylim(0,100)
285 for ax in [ax1,ax2,ax3]:
286     ax.tick_params(labelsize='medium')
287     ax.xaxis.set_minor_locator(AutoMinorLocator())
288     ax.yaxis.set_minor_locator(AutoMinorLocator())
289     if ax == ax1:
290         ax.legend(['x = '+str(np.around(x2d[gl1,0],3))+' m', 'x = '+str(np.around(x2d[gl2,0],3))+' m'],loc='best')
291         ax.set_xlabel('x (m)')
292         ax.set_ylabel('y (m)')
293     else:
294         ax.legend([r'Normal Stress = $\overline{V_1^2}$',r'Normal Stress = $\overline{V_2^2}$',
295                   r'Shear Stress = $\overline{V_1}\overline{V_2}$'], loc='best')
296         ax.grid(True, linestyle='-.')
297         ax.set_xlabel('Magnitude of Stress')
298         ax.set_ylabel(r'$Y$')
299 fig2a.suptitle('Stresses along Vertical Gridlines in Lower half of the Domain', fontsize=24)
300 '',
301 '# Near top wall
302 fig2b = plt.figure()
303 ax1 = plt.subplot2grid((2,2), (0,0), colspan=2)
304 ax2 = plt.subplot2grid((2,2), (1,0))
305 ax3 = plt.subplot2grid((2,2), (1,1))
306 ax1.contourf(x2d,y2d,v2d,cmap='jet',levels=100,alpha=0.5)
307 ax1.plot(x2d[gl1,:],y2d[gl1,:],color='black')
308 ax1.plot(x2d[gl2,:],y2d[gl2,:],color='red')
309 ax1.plot(x2d[:,81],y2d[:,81],color='green',lw=2)
310 ax1.set_title('Location of Gridlines for plotting',fontsize=20)
311 ax1.text(2, 2, 'Upper half of domain', fontsize=20, color="black")
312 ax1.text(2, 1, 'Lower half of domain', fontsize=20, color="black")
313 ax2.plot(tau11[gl1,82:],yplus[gl1,82:])
314 ax2.plot(tau22[gl1,82:],yplus[gl1,82:])

```

```

316 ax2.plot(tau12[g11,82:],yplus[g11,82:])
317 ax2.plot(tau21[g11,82:],yplus[g11,82:])
318 ax2.set_title('Stresses at X = '+str(np.around(x2d[g11,0],3))+', m', fontsize=20)
319 ax3.plot(tau11[g12,82:],yplus[g12,82:])
320 ax3.plot(tau22[g12,82:],yplus[g12,82:])
321 ax3.plot(tau12[g12,82:],yplus[g12,82:])
322 ax3.plot(tau21[g12,82:],yplus[g12,82:])
323 ax3.set_title('Stresses at X = '+str(np.around(x2d[g12,0],3))+', m', fontsize=20)
324 #ax3.set_ylim(0,100)
325 for ax in [ax1,ax2,ax3]:
326     ax.tick_params(labelsize='medium')
327     ax.xaxis.set_minor_locator(AutoMinorLocator())
328     ax.yaxis.set_minor_locator(AutoMinorLocator())
329     if ax == ax1:
330         ax.legend(['x = '+str(np.around(x2d[g11,0],3))+', m', 'x = '+str(np.around(x2d[g12,0],3))+', m'], loc='best')
331         ax.set_xlabel('x (m)')
332         ax.set_ylabel('y (m)')
333     else:
334         ax.legend([r'Normal Stress = $\mu\frac{\partial\overline{u}}{\partial x}$ - $\rho\overline{v}_1^2$',
335                   r'Normal Stress = $\mu\frac{\partial\overline{v}}{\partial y}$ - $\rho\overline{u}_1^2$',
336                   r'Shear Stress = $\mu\frac{\partial\overline{u}}{\partial y} - \mu\frac{\partial\overline{v}}{\partial x}$',
337                   r'Shear Stress = $\mu\frac{\partial\overline{v}}{\partial x} - \mu\overline{u}_1\overline{v}_1$'], loc='best')
338         ax.grid(True, linestyle='-.')
339         ax.set_xlabel('Magnitude of Stress')
340         ax.set_ylabel(r'$Y$')
341 fig2b.suptitle('Stresses along Vertical Gridlines in Upper half of the Domain', fontsize=24)
342
343
344 # %%Assignment 1.2 - Compute and plot all terms in Momentum Equation
345 # Convection term
346 dubub_dx,dubub_dy = dphidx_dy(xf2d,yf2d,np.multiply(u2d,u2d))
347 dubvb_dx,dubvb_dy = dphidx_dy(xf2d,yf2d,np.multiply(u2d,v2d))
348 dvbvb_dx,dvbvb_dy = dphidx_dy(xf2d,yf2d,np.multiply(v2d,v2d))
349
350 # Pressure source term
351 dpb_dx,dpb_dy = dphidx_dy(xf2d,yf2d,p2d)
352
353 # Diffusion term
354 d2ub_dxdx,d2ub_dxdy = dphidx_dy(xf2d,yf2d,dub_dx)
355 d2ub_dydx,d2ub_dydy = dphidx_dy(xf2d,yf2d,dub_dy)
356 d2vb_dxdx,d2vb_dxdy = dphidx_dy(xf2d,yf2d,dvb_dx)
357 d2vb_dydx,d2vb_dydy = dphidx_dy(xf2d,yf2d,dvb_dy)
358
359 # Reynolds stress term
360 dufuf_dx,dufuf_dy = dphidx_dy(xf2d,yf2d,uu2d)
361 dvfvf_dx,dvfvf_dy = dphidx_dy(xf2d,yf2d,vv2d)
362 dufvf_dx,dufvf_dy = dphidx_dy(xf2d,yf2d,uv2d)
363
364 #mom_x = dubub_dx + dubvb_dy + dpb_dx - nu*(d2ub_dxdx - d2ub_dydy) + dufuf_dx + dvfvf_dy
365 #mom_y = dubvb_dx + dvbvb_dy + dpb_dy - nu*(d2vb_dxdx - d2vb_dydy) + dufvf_dx + dvfvf_dy
366
367 # In lower Domain
368 fig3,axes = plt.subplots(nrows=1,ncols=2,constrained_layout=True)
369 axes[0].plot(-dpb_dx[g11,0:81],yplus[g11,0:81],label=r'$-\left(\frac{\partial p}{\partial x}\right)$')
370 axes[0].plot(nu*d2ub_dydy[g11,0:81],yplus[g11,0:81],label=r'$\nu\left(\frac{\partial^2 u}{\partial x^2}\right)$')
371 axes[0].plot(-dufvf_dy[g11,0:81],yplus[g11,0:81],label=r'$-\left(\frac{\partial v}{\partial x}\right)$')
372 axes[1].plot(nu*d2ub_dxdx[g11,0:81],yplus[g11,0:81],label=r'$\nu\left(\frac{\partial^2 u}{\partial y^2}\right)$')

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    ^{2}\overline{u} \ {\partial{x^2}}\right)$')
373 axes[1].plot(-dufuf_dx[g11,0:81],yplus[g11,0:81],label=r'$-\left(\frac{\partial \overline{u}^{2}}{\partial x}\right)$')
374 axes[1].plot((dubub_dx[g11,0:81]+dubvb_dy[g11,0:81]),yplus[g11,0:81],
375     label=r'LHS = $\left(\frac{\partial \overline{u}}{\partial x}\right)\left(\frac{\partial \overline{u}}{\partial y}\right) + \left(\frac{\partial \overline{v}}{\partial x}\right)\left(\frac{\partial \overline{v}}{\partial y}\right)$')
376 for ax in axes:
377     ax.tick_params(labelsize='medium')
378     ax.xaxis.set_minor_locator(AutoMinorLocator())
379     ax.yaxis.set_minor_locator(AutoMinorLocator())
380     ax.grid(True, linestyle='-.')
381     ax.legend(fontsize=16, loc='best')
382     ax.set_xlabel('x', color=(0, 0, 0, 0), fontsize=20)
383     ax.set_ylabel('y', color=(0, 0, 0, 0), fontsize=20)
384     ax.set_xlim([-1.5,0.3])
385 fig3.add_subplot(111, frameon=False)
386 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
387 plt.xlabel("Values of various terms in X-momentum equation", fontsize=18)
388 plt.ylabel(r"$Y^+$", fontsize=18)
389 fig3.suptitle('Terms in X-momentum equation at X = '+str(np.around(x2d[g11,0],3))+', in
lower half of domain', fontsize=24)
390
391 fig3a, axes = plt.subplots(nrows=1, ncols=2, constrained_layout=True)
392 axes[0].plot(-dpb_dy[g11,0:81],yplus[g11,0:81],label=r'$-\left(\frac{\partial \overline{p}}{\partial y}\right)$')
393 axes[0].plot(nu*d2vb_dydy[g11,0:81],yplus[g11,0:81],label=r'$\nu\left(\frac{\partial^2 \overline{v}}{\partial y^2}\right)$')
394 axes[0].plot(-dvvf_dy[g11,0:81],yplus[g11,0:81],label=r'$-\left(\frac{\partial \overline{v}}{\partial y}\right)$')
395 axes[1].plot(nu*d2vb_dxdx[g11,0:81],yplus[g11,0:81],label=r'$\nu\left(\frac{\partial^2 \overline{v}}{\partial x^2}\right)$')
396 axes[1].plot(-dufvf_dx[g11,0:81],yplus[g11,0:81],label=r'$-\left(\frac{\partial \overline{v}}{\partial x}\right)$')
397 axes[1].plot((dubvb_dx[g11,0:81]+dvvf_dy[g11,0:81]),yplus[g11,0:81],
398     label=r'LHS = $\left(\frac{\partial \overline{u}}{\partial x}\right)\left(\frac{\partial \overline{v}}{\partial y}\right) + \left(\frac{\partial \overline{v}}{\partial x}\right)\left(\frac{\partial \overline{v}}{\partial y}\right)$')
399 for ax in axes:
400     ax.tick_params(labelsize='medium')
401     ax.xaxis.set_minor_locator(AutoMinorLocator())
402     ax.yaxis.set_minor_locator(AutoMinorLocator())
403     ax.grid(True, linestyle='-.')
404     ax.legend(fontsize=16, loc='best')
405     ax.set_xlabel('x', color=(0, 0, 0, 0), fontsize=20)
406     ax.set_ylabel('y', color=(0, 0, 0, 0), fontsize=20)
407     ax.set_xlim([-0.7,0.1])
408 fig3a.add_subplot(111, frameon=False)
409 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
410 plt.xlabel("Values of various terms in X-momentum equation", fontsize=18)
411 plt.ylabel(r"$Y^+$", fontsize=18)
412 fig3a.suptitle('Terms in Y-momentum equation at X = '+str(np.around(x2d[g11,0],3))+', in
lower half of domain', fontsize=24)
413
414 fig4, axes = plt.subplots(nrows=1, ncols=2, constrained_layout=True)
415 axes[0].plot(-dpb_dx[g12,0:81],yplus[g12,0:81],label=r'$-\left(\frac{\partial \overline{p}}{\partial x}\right)$')
416 axes[0].plot(nu*d2ub_dydy[g12,0:81],yplus[g12,0:81],label=r'$\nu\left(\frac{\partial^2 \overline{u}}{\partial y^2}\right)$')
417 axes[0].plot(-dufvf_dy[g12,0:81],yplus[g12,0:81],label=r'$-\left(\frac{\partial \overline{u}}{\partial y}\right)$')
418 axes[1].plot(nu*d2ub_dxdx[g12,0:81],yplus[g12,0:81],label=r'$\nu\left(\frac{\partial^2 \overline{u}}{\partial x^2}\right)$')
419 axes[1].plot(-dufuf_dx[g12,0:81],yplus[g12,0:81],label=r'$-\left(\frac{\partial \overline{u}}{\partial x}\right)$')
420 axes[1].plot((dubub_dx[g12,0:81]+dubvb_dy[g12,0:81]),yplus[g12,0:81],label=r'LHS = $\left(\frac{\partial \overline{u}}{\partial x}\right)\left(\frac{\partial \overline{u}}{\partial y}\right) + \left(\frac{\partial \overline{v}}{\partial x}\right)\left(\frac{\partial \overline{v}}{\partial y}\right)$')

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421 for ax in axes:
422     ax.tick_params(labelsize='medium')
423     ax.xaxis.set_minor_locator(AutoMinorLocator())
424     ax.yaxis.set_minor_locator(AutoMinorLocator())
425     ax.grid(True, linestyle='-.')
426     ax.legend(fontsize=16, loc='best')
427     ax.set_xlabel('..', color=(0, 0, 0, 0), fontsize=20)
428     ax.set_ylabel('..', color=(0, 0, 0, 0), fontsize=20)
429 fig4.add_subplot(111, frameon=False)
430 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
431 plt.xlabel("Values of various terms in X-momentum equation", fontsize=18)
432 plt.ylabel(r"$Y^+$", fontsize=18)
433 fig4.suptitle('Terms in X-momentum equation at X = ' + str(np.around(x2d[g12, 0], 3)) + ' m in
lower half of domain', fontsize=24)
434
435 fig4a, axes = plt.subplots(nrows=1, ncols=2, constrained_layout=True)
436 axes[0].plot(-dpb_dy[g12, 0:81], yplus[g12, 0:81], label=r'$-\left(\frac{\partial \overline{p}}{\partial y}\right)$')
437 axes[0].plot(nu*d2vb_dydy[g12, 0:81], yplus[g12, 0:81], label=r'$\nu \left(\frac{\partial^2 \overline{v}}{\partial y^2}\right)$')
438 axes[0].plot(-dvfvf_dy[g12, 0:81], yplus[g12, 0:81], label=r'$-\left(\frac{\partial \overline{v}^{\prime 2}}{\partial y}\right)$')
439 axes[1].plot(nu*d2vb_dx[g12, 0:81], yplus[g12, 0:81], label=r'$\nu \left(\frac{\partial^2 \overline{v}}{\partial x^2}\right)$')
440 axes[1].plot(-duvf_dx[g12, 0:81], yplus[g12, 0:81], label=r'$-\left(\frac{\partial \overline{v}^{\prime}}{\partial x}\right)$')
441 axes[1].plot((dubvb_dx[g12, 0:81]+dvvb_dy[g12, 0:81]), yplus[g12, 0:81], label=r'LHS = $\left(\frac{\partial \overline{u}}{\partial x}\right)\left(\frac{\partial \overline{v}}{\partial y}\right) + \left(\frac{\partial \overline{v}}{\partial x}\right)\left(\frac{\partial \overline{u}}{\partial y}\right)$')
442 for ax in axes:
443     ax.tick_params(labelsize='medium')
444     ax.xaxis.set_minor_locator(AutoMinorLocator())
445     ax.yaxis.set_minor_locator(AutoMinorLocator())
446     ax.grid(True, linestyle='-.')
447     ax.legend(fontsize=16, loc='best')
448     ax.set_xlabel('..', color=(0, 0, 0, 0), fontsize=20)
449     ax.set_ylabel('..', color=(0, 0, 0, 0), fontsize=20)
450 fig4a.add_subplot(111, frameon=False)
451 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
452 plt.xlabel("Values of various terms in X-momentum equation", fontsize=18)
453 plt.ylabel(r"$Y^+$", fontsize=18)
454 fig4a.suptitle('Terms in Y-momentum equation at X = ' + str(np.around(x2d[g12, 0], 3)) + ' m
in lower half of domain', fontsize=24)
455
456 # In Upper Domain
457 grid = 0
458 fig3b, axes = plt.subplots(nrows=1, ncols=2, constrained_layout=True)
459 axes[0].plot(-dpb_dx[grid, 82:], yplus[grid, 82:], label=r'$-\left(\frac{\partial \overline{p}}{\partial x}\right)$')
460 axes[0].plot(nu*d2ub_dydy[grid, 82:], yplus[grid, 82:], label=r'$\nu \left(\frac{\partial^2 \overline{u}}{\partial y^2}\right)$')
461 axes[0].plot(-duvf_dy[grid, 82:], yplus[grid, 82:], label=r'$-\left(\frac{\partial \overline{u}^{\prime 2}}{\partial y}\right)$')
462 axes[1].plot(nu*d2ub_dx[g12, 82:], yplus[grid, 82:], label=r'$\nu \left(\frac{\partial^2 \overline{u}}{\partial x^2}\right)$')
463 axes[1].plot(-duf_dx[grid, 82:], yplus[grid, 82:], label=r'$-\left(\frac{\partial \overline{u}^{\prime}}{\partial x}\right)$')
464 axes[1].plot((dubub_dx[grid, 82:]+dubb_dy[grid, 82:]), yplus[grid, 82:], label=r'LHS = $\left(\frac{\partial \overline{u}}{\partial x}\right)\left(\frac{\partial \overline{u}}{\partial y}\right) + \left(\frac{\partial \overline{u}}{\partial y}\right)\left(\frac{\partial \overline{u}}{\partial x}\right)$')
465 for ax in axes:
466     ax.tick_params(labelsize='medium')
467     ax.xaxis.set_minor_locator(AutoMinorLocator())
468     ax.yaxis.set_minor_locator(AutoMinorLocator())
469     ax.grid(True, linestyle='-.')
470     ax.legend(fontsize=16, loc='best')

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471     ax.set_xlabel('x', color=(0, 0, 0, 0), fontsize=20)
472     ax.set_ylabel('y', color=(0, 0, 0, 0), fontsize=20)
473 fig3b.add_subplot(111, frameon=False)
474 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
475 plt.xlabel("Values of various terms in X-momentum equation", fontsize=18)
476 plt.ylabel(r"$Y^+$", fontsize=18)
477 fig3b.suptitle('Terms in X-momentum equation at $X = ' + str(np.around(x2d[grid], 3)) + '$\n' + 'in upper half of domain', fontsize=24)
478
479 fig4b, axes = plt.subplots(nrows=1, ncols=2, constrained_layout=True)
480 axes[0].plot(-dpb_dy[grid, 82:], yplus[grid, 82:], label=r'$-\frac{\partial \overline{p}}{\partial y}$')
481 axes[0].plot(nu*d2vb_dydx[grid, 82:], yplus[grid, 82:], label=r'$\nu \frac{\partial \overline{v}}{\partial x}$')
482 axes[0].plot(-dvvf_dy[grid, 82:], yplus[grid, 82:], label=r'$-\frac{\partial \overline{v}^2}{\partial y}$')
483 axes[1].plot(nu*d2vb_dx2d[grid, 82:], yplus[grid, 82:], label=r'$\nu \frac{\partial \overline{v}}{\partial x^2}$')
484 axes[1].plot(-dufv_dx[grid, 82:], yplus[grid, 82:], label=r'$-\frac{\partial \overline{v}}{\partial x}$')
485 axes[1].plot((dubvb_dx[grid, 82:]+dvbvb_dy[grid, 82:]), yplus[grid, 82:], label=r'LHS = $\left(\frac{\partial \overline{v}}{\partial x} + \frac{\partial \overline{v}}{\partial y}\right)$')
486 for ax in axes:
487     ax.tick_params(labelsize='medium')
488     ax.xaxis.set_minor_locator(AutoMinorLocator())
489     ax.yaxis.set_minor_locator(AutoMinorLocator())
490     ax.grid(True, linestyle='-.')
491     ax.legend(fontsize=16, loc='best')
492     ax.set_xlabel('x', color=(0, 0, 0, 0), fontsize=20)
493     ax.set_ylabel('y', color=(0, 0, 0, 0), fontsize=20)
494 fig4b.add_subplot(111, frameon=False)
495 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
496 plt.xlabel("Values of various terms in X-momentum equation", fontsize=18)
497 plt.ylabel(r"$Y^+$", fontsize=18)
498 fig4b.suptitle('Terms in Y-momentum equation at $X = ' + str(np.around(x2d[grid], 3)) + '$\n' + 'in upper half of domain', fontsize=24)
499
500 # %%Assignment 1.3 - Plot the vector field F_N
501 k = 2
502 k1 = 1
503 Mag = np.hypot(dufuf_dx, dvfvf_dy)
504 V1 = (-dufuf_dx/Mag)
505 V2 = (-dvfvf_dy/Mag)
506 fig6 = plt.figure()
507 axes = fig6.add_axes([0.1, 0.1, 0.8, 0.8])
508 cc = axes.quiver(x2d[:, :k1, :, k1], y2d[:, k1, :, k1], V1[:, k1, :, k1], V2[:, k1, :, k1], Mag, pivot='mid', cmap='Reds', width=0.001, headwidth=5, headlength=6)
509 fig6.colorbar(cc, ax=axes)
510 axes.set_xlabel('X (m)')
511 axes.set_ylabel('Y (m)')
512 axes.set_title(r'Vector Field - $F_N$', fontsize=20)
513
514 fig6a = plt.figure()
515 axes = fig6a.add_axes([0.1, 0.1, 0.8, 0.8])
516 cc = axes.contourf(x2d, y2d, vv2d, 100, cmap='jet', alpha=0.8)
517 fig6a.colorbar(cc, ax=axes)
518 axes.quiver(x2d[:, :, k, :, k], y2d[:, :, k, :, k], V1[:, :, k, :, k], V2[:, :, k, :, k], pivot='mid', width=0.001, headwidth=4, headlength=5)
519 axes.set_xlabel('X (m)')
520 axes.set_ylabel('Y (m)')
521 axes.set_title(r'Vector Field - $F_N$', fontsize=20)
522
523
524 # %%Assignment 1.4 - Plot the vector field F_S
525 k = 2

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526 k1 = 1
527 Mag1 = np.hypot(dufvf_dy,dufvf_dx)
528 VV1 = (-dufvf_dy/Mag1)
529 VV2 = (-dufvf_dx/Mag1)
530 fig7 = plt.figure()
531 axes = fig7.add_axes([0.1,0.1,0.8,0.8])
532 cc = axes.quiver(x2d[:,k1],y2d[:,k1],VV1[:,k1],VV2[:,k1],Mag,pivot='mid',cmap='Reds',width=0.001,headwidth=5,headlength=6)
533 fig7.colorbar(cc,ax=axes)
534 axes.set_xlabel('X (m)')
535 axes.set_ylabel('Y (m)')
536 axes.set_title(r'Vector Field - $F_{S}$',fontsize=20)
537
538 fig7a = plt.figure()
539 axes = fig7a.add_axes([0.1,0.1,0.8,0.8])
540 cc = axes.contourf(x2d,y2d,vv2d,100,cmap='jet',alpha=0.8)
541 fig6a.colorbar(cc,ax=axes)
542 axes.quiver(x2d[:,k1],y2d[:,k1],VV1[:,k1],VV2[:,k1],pivot='mid',width=0.001,headwidth=4,headlength=5)
543 axes.set_xlabel('X (m)')
544 axes.set_ylabel('Y (m)')
545 axes.set_title(r'Vector Field - $F_{S}$',fontsize=20)
546
547 # %%Assignment 1.5 - Plot the production terms
548 NS = (np.multiply(uu2d,dub_dx) + np.multiply(vv2d,dvb_dy))
549 SS = (np.multiply(uv2d,dub_dy) + np.multiply(uv2d,dvb_dx))
550 Pk = -(NS + SS)
551 SS[:,(0,-1)] = 1e-20
552 NS[:,(0,-1)] = 1e-20
553
554 fig8,axes = plt.subplots(nrows=2,ncols=1,constrained_layout=True)
555 axes[0].plot(yplus[g11,0:81],Pk[g11,0:81],label='X = '+str(np.around(x2d[g11,0],3))+ ' m')
556 axes[1].plot(yplus[g12,0:81],Pk[g12,0:81],label='X = '+str(np.around(x2d[g12,0],3))+ ' m')
557 for ax in axes:
558     ax.tick_params(labelsize='medium')
559     ax.xaxis.set_minor_locator(AutoMinorLocator())
560     ax.yaxis.set_minor_locator(AutoMinorLocator())
561     ax.grid(True, linestyle='-.')
562     ax.legend(fontsize=16,loc='best')
563     ax.set_xlabel(' ', color=(0, 0, 0, 0),fontsize=20)
564     ax.set_ylabel(' ', color=(0, 0, 0, 0),fontsize=20)
565 fig8.add_subplot(111, frameon=False)
566 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
567 plt.xlabel(r'$Y^{+}$', fontsize=18)
568 plt.ylabel(r'$P^{+k}$', fontsize=18)
569 fig8.suptitle('Value of Production term in Turbulent KE equation (Upper Half of the Domain)', fontsize=24)
570
571 NS_contribution = np.divide(np.abs(NS),(np.abs(SS)+np.abs(NS)))
572 NS_contribution[:,0] = 0
573 NS_contribution[:,0] = 0
574 SS_contribution = np.divide(np.abs(SS),(np.abs(SS)+np.abs(NS)))
575 SS_contribution[:,0] = 0
576 SS_contribution[:,0] = 0
577
578 fig9,axes = plt.subplots(nrows=2,ncols=1,constrained_layout=True)
579 vmin1 = 0
580 vmax1 = np.max(np.max(Pk))
581 v1 = np.linspace(vmin1,vmax1,10)
582 vmin2 = np.min(np.min(Pk))
583 vmax2 = 0
584 v2 = np.linspace(vmin2,vmax2,10)
585 a1 = axes[0].contourf(x2d,y2d,Pk,cmap='gist_gray',levels=v1,extend='min')
586 a1.cmap.set_under('black')

```

```

587 a2 = axes[1].contourf(x2d,y2d,Pk,cmap='gist_yarg',levels=v2,extend='max')
588 a2.cmap.set_over('black')
589 cb1 = fig9.colorbar(a1,ax=axes[0])
590 cb2 = fig9.colorbar(a2,ax=axes[1])
591 cb1.ax.tick_params(labelsize=16)
592 cb2.ax.tick_params(labelsize=16)
593 a1.ax.tick_params(labelsize=14)
594 a2.ax.tick_params(labelsize=14)
595 axes[0].set_title(r'Contour of Production term  $(P^k)$  - Areas of Postive Production',
596                      fontsize=20)
596 axes[1].set_title(r'Contour of Production term  $(P^k)$  - Areas of Negative Production',
597                      fontsize=20)
597 for ax in axes:
598     ax.set_xlabel('X (m)',fontsize=18)
599     ax.set_ylabel('Y (m)',fontsize=18)
600
601 fig9a = plt.figure()
602 ax1 = plt.subplot2grid((2,4), (0,0), colspan=2)
603 ax2 = plt.subplot2grid((2,4), (0,2), colspan=2)
604 ax3 = plt.subplot2grid((2,4), (1,0))
605 ax4 = plt.subplot2grid((2,4), (1,1))
606 ax5 = plt.subplot2grid((2,4), (1,2))
607 ax6 = plt.subplot2grid((2,4), (1,3))
608 a1 = ax1.contourf(x2d,y2d,np.multiply(np.abs(Pk),NS_contribution),cmap='jet',levels=50)
609 fig9a.colorbar(a1,ax=ax1)
610 ax1.set_title(r'Contribution of Normal Stress to the Production term  $(P^k)$ ',fontsize
611 =18)
611 a2 = ax2.contourf(x2d,y2d,np.multiply(np.abs(Pk),SS_contribution),cmap='jet',levels=50)
612 fig9a.colorbar(a2,ax=ax2)
613 ax2.set_title(r'Contribution of Shear Stress to the Production term  $(P^k)$ ',fontsize
614 =18)
614 a3 = ax3.contourf(x2d,y2d,np.multiply(np.abs(Pk),NS_contribution),cmap='jet',levels=50)
615 fig9a.colorbar(a3,ax=ax3,orientation='horizontal')
616 ax3.set_xlim(0,2)
617 ax3.set_ylim(0.6,1.4)
618 ax3.set_title(r'Near First Hill',fontsize=14)
619 a4 = ax4.contourf(x2d,y2d,np.multiply(np.abs(Pk),NS_contribution),cmap='jet',levels=50)
620 fig9a.colorbar(a4,ax=ax4,orientation='horizontal')
621 ax4.set_xlim(8.2,9)
622 ax4.set_ylim(0.8,1.2)
623 ax4.set_title(r'Near Second Hill',fontsize=14)
624 a5 = ax5.contourf(x2d,y2d,np.multiply(np.abs(Pk),SS_contribution),cmap='jet',levels=50)
625 fig9a.colorbar(a5,ax=ax5,orientation='horizontal')
626 ax5.set_xlim(0,2)
627 ax5.set_ylim(0.5,1.3)
628 ax5.set_title(r'Near First Hill',fontsize=14)
629 a6 = ax6.contourf(x2d,y2d,np.multiply(np.abs(Pk),SS_contribution),cmap='jet',levels=50)
630 fig9a.colorbar(a6,ax=ax6,orientation='horizontal')
631 ax6.set_xlim(8.6,9)
632 ax6.set_ylim(0.8,1.1)
633 ax6.set_title(r'Near Second Hill',fontsize=14)
634 for ax in [ax1,ax2]:
635     ax.set_xlabel('X (m)',fontsize=16)
636     ax.set_ylabel('Y (m)',fontsize=16)
637
638 # %%Assignment 1.6 - Plot the dissipation and compare with production
639 # Dissipation plot
640 vmin = 0.1
641 vmin2 = 0.05
642 vmax = np.max(np.max(diss_RANS_2d))
643 v = np.linspace(vmin, vmax, 50, endpoint=True)
644 v2 = np.linspace(vmin2, vmax, 50, endpoint=True)
645 fig10 = plt.figure()
646 ax1 = plt.subplot2grid((2,2), (0,0), colspan=2)
647 ax2 = plt.subplot2grid((2,2), (1,0))
648 ax3 = plt.subplot2grid((2,2), (1,1))

```

```
649 cax1 = ax1.contourf(x2d,y2d,diss_RANS_2d,cmap='jet',levels=50)
650 cax2 = ax2.contourf(x2d,y2d,diss_RANS_2d,cmap='jet',levels=v,extend='both')
651 cax2.cmap.set_over('darkred')
652 cax2.cmap.set_under('darkblue')
653 cax3 = ax3.contourf(x2d,y2d,diss_RANS_2d,cmap='jet',levels=v2,extend='both')
654 cax3.cmap.set_over('darkred')
655 cax3.cmap.set_under('darkblue')
656 for ax in [ax1,ax2,ax3]:
657     ax.set_xlabel('X (m)')
658     ax.set_ylabel('Y (m)')
659 cb1 = fig10.colorbar(cax1,ax=ax1,fraction=0.05)
660 cb2 = fig10.colorbar(cax2,ax=ax2,fraction=0.1)
661 cb3 = fig10.colorbar(cax3,ax=ax3,fraction=0.1)
662 ax2.set_xlim(0,0.6)
663 ax2.set_ylim(0.9,1.05)
664 ax3.set_xlim(8.4,9)
665 ax3.set_ylim(0.8,1.1)
666 plt.tight_layout()
667 ax1.set_title(r'Contour of Dissipation ($\epsilon$) of Turbulent KE', fontsize=24)
668 ax2.set_title(r'Dissipation ($\epsilon$) near the first hill', fontsize=20)
669 ax3.set_title(r'Dissipation ($\epsilon$) near the second hill', fontsize=20)
670
671 # Production and dissipation equilibrium
672 vmin = -0.01
673 vmax = 0.01
674 v = np.linspace(vmin, vmax, 50, endpoint=True)
675 #v = np.append(v,0.24)
676 fig11, axes = plt.subplots()
677 css = axes.contourf(x2d,y2d,Pk-diss_RANS_2d,cmap='seismic',levels=v,extend='both')
678 #cs.cmap.set_over('dimgray')
679 #cs.cmap.set_under('bisque')
680 #cs.changed()
681 cb = fig11.colorbar(css,ticks=[-0.01,-0.005,0,0.005,0.01])
682 axes.set_title(r'Local Equilibrium of Production ($P_k$) and Dissipation ($\epsilon$) terms', fontsize=24)
683
684 # %%Assign 1.7 - Reynolds Stress Equation
685 # Constants for Modelling
686 C_mu = 0.09
687 C_1 = 1.5
688 C_2 = 0.6
689 C_1w = 0.5
690 C_2w = 0.3
691 sigma_k = 1
692
693 # Damping function - f
694 #f = k_RANS_2d**1.5 / (2.55 * diss_RANS_2d * [(np.absolute(nx[:,0] * (x2d-x2d[:,0])) + (np.absolute(ny[:,0] * (y2d-y2d[:,0]))))]
695 distance = np.zeros((ni,nj))
696 for i in range(ni):
697     for j in range(nj):
698         distance[i,j] = WallDistance(x2d,y2d,x2d[i,j],y2d[i,j])
699 distance[:,(0,-1)] = 1e-10
700
701 f = (k_RANS_2d**1.5) / (2.55 * diss_RANS_2d * distance)
702 f[:,(0,-1)] = 1e-10
703 f_abs = f.copy()
704
705 # Normalize damping function
706 for i in range(ni):
707     for j in range(nj):
708         if j <= 81:
709             f[i,j] = f_abs[i,j]/(np.amax(f_abs[:,81:], axis=1)[i])
710         else:
711             f[i,j] = f_abs[i,j]/(np.amax(f_abs[:,81:], axis=1)[i])
712
```

```
713 # Wall Normals for Pressure Strain Term Calculations
714 nx_bottom,ny_bottom,nx_top,ny_top = WallNormal(xf2d,yf2d)
715 nx_bottom = np.transpose(np.array([nx_bottom,]*nj))
716 ny_bottom = np.transpose(np.array([ny_bottom,]*nj))
717 nx_top = np.transpose(np.array([nx_top,]*nj))
718 ny_top = np.transpose(np.array([ny_top,]*nj))
719
720 # Model Diffusion terms
721 Constant = (np.divide(np.multiply(k_RANS_2d,k_RANS_2d),diss_RANS_2d) * (C_mu/sigma_k))
722
723 d2ufuf_dx dx, d2ufuf_dy dy = dphidx_dy(xf2d,yf2d,dufuf_dx)
724 d2ufuf_dy dx, d2ufuf_dy dy = dphidx_dy(xf2d,yf2d,dufuf_dy)
725 d2vfvf_dx dx, d2vfvf_dy dy = dphidx_dy(xf2d,yf2d,dvfvf_dx)
726 d2vfvf_dy dx, d2vfvf_dy dy = dphidx_dy(xf2d,yf2d,dvfvf_dy)
727 d2ufvf_dx dx, d2ufvf_dy dy = dphidx_dy(xf2d,yf2d,dufvf_dx)
728 d2ufvf_dy dx, d2ufvf_dy dy = dphidx_dy(xf2d,yf2d,dufvf_dy)
729
730 # For Reynolds Stress - u'v'
731 LHS_12 = np.multiply(u2d,dufvf_dx) + np.multiply(v2d,dufvf_dy)
732 LHS_21 = LHS_12
733 # Production - u'v'
734 P_12 = -(np.multiply(uu2d,dvb_dx) + np.multiply(uv2d,dvb_dy) + np.multiply(uv2d,dub_dx)
735 + np.multiply(vv2d,dub_dy))
736 P_21 = P_12
737 # Turbulent Diffusion - u'v'
738 diff_12 = np.multiply(Constant,(d2ufvf_dx dx+d2ufvf_dy dy))
739 diff_21 = diff_12
740 # Viscous Diffusion - u'v'
741 diffvisc_12 = nu * (d2ufvf_dx dx + d2ufvf_dy dy)
742 diffvisc_21 = diffvisc_12
743 # Dissipation - u'v'
744 diss_12 = np.zeros((ni,nj))
745 diss_21 = np.zeros((ni,nj))
746 # Pressure-strain term - u'v'
747 phi12_1 = -C_1 * np.divide(diss_RANS_2d,k_RANS_2d) * (uv2d - (2/3 * k_RANS_2d))
748 phi12_2 = -C_2 * (P_12 - (2/3 * Pk))
749 phi21_1 = phi12_1
750 phi21_2 = phi12_2
751
752 # For Reynolds Stress - u'u'
753 LHS_11 = np.multiply(u2d,dufuf_dx) + np.multiply(v2d,dufuf_dy)
754 # Production - u'u'
755 P_11 = -2 * (np.multiply(uu2d,dub_dx) + np.multiply(uv2d,dub_dy))
756 # Turbulent Diffusion - u'u'
757 diff_11 = np.multiply(Constant,(d2ufuf_dx dx+d2ufuf_dy dy))
758 diffvisc_11 = nu * (d2ufuf_dx dx + d2ufuf_dy dy)
759 # Dissipation - u'u'
760 diss_11 = (2/3) * diss_RANS_2d
761 # Pressure-strain term - u'u'
762 phi11_1 = -C_1 * np.divide(diss_RANS_2d,k_RANS_2d) * (uu2d - (2/3 * k_RANS_2d))
763 phi11_2 = -C_2 * (P_11 - (2/3 * Pk))
764
765 # For Reynolds Stress - v'v'
766 LHS_22 = np.multiply(u2d,dvfvf_dx) + np.multiply(v2d,dvfvf_dy)
767 # Production - v'v'
768 P_22 = -2 * (np.multiply(uv2d,dvb_dx) + np.multiply(vv2d,dvb_dy))
769 # Turbulent Diffusion - v'v'
770 diff_22 = np.multiply(Constant,(d2vfvf_dx dx+d2vfvf_dy dy))
771 # Viscous Diffusion - v'v'
772 diffvisc_22 = nu * (d2vfvf_dx dx + d2vfvf_dy dy)
773 # Dissipation - v'v'
774 diss_22 = (2/3) * diss_RANS_2d
775 # Pressure-strain term - v'v'
776 phi22_1 = -C_1 * np.divide(diss_RANS_2d,k_RANS_2d) * (vv2d - (2/3 * k_RANS_2d))
777 phi22_2 = -C_2 * (P_22 - (2/3 * Pk))
```

```

778
779 # Pressure Strain IP Terms (near wall terms)
780 phi11_1w = np.zeros((ni,nj))
781 phi11_2w = np.zeros((ni,nj))
782 phi12_1w = np.zeros((ni,nj))
783 phi12_2w = np.zeros((ni,nj))
784 phi22_1w = np.zeros((ni,nj))
785 phi22_2w = np.zeros((ni,nj))
786 phi21_1w = np.zeros((ni,nj))
787 phi21_2w = np.zeros((ni,nj))
788 for i in range(ni):
789     for j in range (nj):
790         if j<=81:
791             phi11_1w[i,j] = C_1w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((uu2d[i,j]*nx_bottom[i,j]*nx_bottom[i,j])+(2*uv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])+(vv2d[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*uu2d[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*uv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])-(1.5*uu2d[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*uv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])) * f[i,j]
792             phi11_2w[i,j] = C_2w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((phi11_2[i,j]*nx_bottom[i,j]*nx_bottom[i,j])+(2*phi12_2[i,j]*nx_bottom[i,j]*ny_bottom[i,j])+(phi22_2[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*phi11_2[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*phi12_2[i,j]*nx_bottom[i,j]*ny_bottom[i,j])-(1.5*phi11_2[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*phi12_2[i,j]*nx_bottom[i,j]*ny_bottom[i,j])) * f[i,j]
793             phi22_1w[i,j] = C_1w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((uu2d[i,j]*nx_bottom[i,j]*nx_bottom[i,j])+(2*uv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])+(vv2d[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*uv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])-(1.5*vv2d[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*uv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])) * f[i,j]
794             phi22_2w[i,j] = C_2w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((phi11_2[i,j]*nx_bottom[i,j]*nx_bottom[i,j])+(2*phi12_2[i,j]*nx_bottom[i,j]*ny_bottom[i,j])+(phi22_2[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*phi11_2[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*phi12_2[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*phi22_2[i,j]*ny_bottom[i,j]*ny_bottom[i,j])) * f[i,j]
795             phi12_1w[i,j] = C_1w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * (((1.5*uu2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])-(1.5*uv2d[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*uv2d[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*vv2d[i,j]*nx_bottom[i,j]*ny_bottom[i,j])) * f[i,j]
796             phi12_2w[i,j] = C_2w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * (((1.5*phi11_2[i,j]*nx_bottom[i,j]*ny_bottom[i,j])-(1.5*phi12_2[i,j]*ny_bottom[i,j]*ny_bottom[i,j])-(1.5*phi12_2[i,j]*nx_bottom[i,j]*nx_bottom[i,j])-(1.5*phi22_2[i,j]*nx_bottom[i,j]*ny_bottom[i,j])) * f[i,j]
797         else:
798             phi11_1w[i,j] = C_1w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((uu2d[i,j]*nx_top[i,j])+(2*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])+(vv2d[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*uu2d[i,j]*nx_top[i,j]*nx_top[i,j])-(1.5*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])-(1.5*uu2d[i,j]*nx_top[i,j]*nx_top[i,j])-(1.5*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])) * f[i,j]
799             phi11_2w[i,j] = C_2w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((phi11_2[i,j]*nx_top[i,j])+(2*phi12_2[i,j]*nx_top[i,j]*ny_top[i,j])+(phi22_2[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*phi11_2[i,j]*nx_top[i,j]*nx_top[i,j])-(1.5*phi12_2[i,j]*nx_top[i,j]*ny_top[i,j])-(1.5*phi11_2[i,j]*nx_top[i,j]*ny_top[i,j])) * f[i,j]
800             phi22_1w[i,j] = C_1w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((uu2d[i,j]*nx_top[i,j])+(2*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])+(vv2d[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])-(1.5*vv2d[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])) * f[i,j]
801             phi22_2w[i,j] = C_2w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((phi11_2[i,j]*nx_top[i,j])+(2*phi12_2[i,j]*nx_top[i,j]*ny_top[i,j])+(phi22_2[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*phi11_2[i,j]*nx_top[i,j]*nx_top[i,j])-(1.5*phi12_2[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*phi22_2[i,j]*ny_top[i,j]*ny_top[i,j])) * f[i,j]
802             phi12_1w[i,j] = C_1w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * (((1.5*uu2d[i,j]*nx_top[i,j]*ny_top[i,j])-(1.5*uv2d[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*uv2d[i,j]*nx_top[i,j]*ny_top[i,j])-(1.5*vv2d[i,j]*ny_top[i,j]*ny_top[i,j])) * f[i,j]

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803     nx_top[i,j]*nx_top[i,j])-(1.5*vv2d[i,j]*nx_top[i,j]*ny_top[i,j])) * f[i,j]
804         phi12_2w[i,j] = C_2w * (diss_RANS_2d[i,j]/k_RANS_2d[i,j]) * ((1.5*phi11_2[i,
805             j]*nx_top[i,j]*ny_top[i,j])-(1.5*phi12_2[i,j]*ny_top[i,j]*ny_top[i,j])-(1.5*phi12_2[
806                 i,j]*nx_top[i,j]*nx_top[i,j])-(1.5*phi22_2[i,j]*nx_top[i,j]*ny_top[i,j])) * f[i,j]
807
808 phi21_1w = phi12_1w
809 phi21_2w = phi12_2w
810
811 PS_11 = phi11_1 + phi11_2 + phi11_1w + phi11_2w
812 PS_12 = phi12_1 + phi12_2 + phi12_1w + phi12_2w
813 PS_22 = phi22_1 + phi22_2 + phi22_1w + phi22_2w
814 PS_21 = phi21_1 + phi21_2 + phi21_1w + phi21_2w
815
816 # Take the terms in stress equation of 11 and 12 for comparision along line i=5
817 gl3 = 10
818 fig12, axes = plt.subplots(nrows=2, ncols=1, constrained_layout=True)
819 axes[0].plot(yplus[gl3,0:81], P_11[gl3,0:81], label=r'Production term - $P_{11}$')
820 axes[1].plot(yplus[gl3,0:81], PS_11[gl3,0:81], label=r'Pressure Strain Term - $\Phi_{11}$')
821 axes[0].plot(yplus[gl3,0:81], -diss_11[gl3,0:81], label=r'Dissipation - $\epsilon_{11}$')
822 axes[0].plot(yplus[gl3,0:81], diff_11[gl3,0:81], label=r'Turbulent Diffusion - $(D_{11})_{t}$')
823 axes[1].plot(yplus[gl3,0:81], diffvisc_11[gl3,0:81], label=r'Viscous Diffusion - $(D_{11})_{v}$')
824 axes[1].plot(yplus[gl3,0:81], LHS_11[gl3,0:81], label=r'LHS')
825 #axes[1].plot(yplus[gl3,0:81], P_12[gl3,0:81], label=r'Production term - $P_{12}$')
826 #axes[1].plot(yplus[gl3,0:81], PS_12[gl3,0:81], label=r'Pressure Strain Term - $\Phi_{12}$')
827 #axes[1].plot(yplus[gl3,0:81], -diss_12[gl3,0:81], label=r'Dissipation - $\epsilon_{12}$')
828 #axes[1].plot(yplus[gl3,0:81], diff_12[gl3,0:81], label=r'Turbulent Diffusion - $(D_{12})_{t}$')
829 #axes[1].plot(yplus[gl3,0:81], diffvisc_12[gl3,0:81], label=r'Viscous Diffusion - $(D_{12})_{v}$')
830 #axes[1].plot(yplus[gl3,0:81], LHS_12[gl3,0:81], label=r'LHS')
831 for ax in axes:
832     ax.tick_params(labelsize='x-large')
833     ax.xaxis.set_minor_locator(AutoMinorLocator())
834     ax.yaxis.set_minor_locator(AutoMinorLocator())
835     ax.grid(True, linestyle='-.')
836     ax.legend(fontsize=14, loc='best')
837     ax.set_xlabel('x', color=(0, 0, 0, 0), fontsize=20)
838     ax.set_ylabel('y', color=(0, 0, 0, 0), fontsize=20)
839 fig12.add_subplot(111, frameon=False)
840 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
841 plt.xlabel(r'$Y^+$', fontsize=18)
842 plt.ylabel(r'$P^k$', fontsize=18)
843 fig12.suptitle(r'Terms in $\overline{V_1}^{\prime\prime}$ Equation at X = '+str(np.around(
844     (x2d[gl3,0],3))+ m (Lower Domain)', fontsize=20)
845
846 fig12a, axes = plt.subplots(nrows=2, ncols=1, constrained_layout=True)
847 #axes[0].plot(yplus[gl3,0:81], P_11[gl3,0:81], label=r'Production term - $P_{11}$')
848 #axes[0].plot(yplus[gl3,0:81], PS_11[gl3,0:81], label=r'Pressure Strain Term - $\Phi_{11}$')
849 #axes[0].plot(yplus[gl3,0:81], -diss_11[gl3,0:81], label=r'Dissipation - $\epsilon_{11}$')
850 #axes[0].plot(yplus[gl3,0:81], diff_11[gl3,0:81], label=r'Turbulent Diffusion - $(D_{11})_{t}$')
851 #axes[0].plot(yplus[gl3,0:81], diffvisc_11[gl3,0:81], label=r'Viscous Diffusion - $(D_{11})_{v}$')
852 #axes[0].plot(yplus[gl3,0:81], LHS_11[gl3,0:81], label=r'LHS')
853 axes[0].plot(yplus[gl3,0:81], P_12[gl3,0:81], label=r'Production term - $P_{12}$')
854 axes[1].plot(yplus[gl3,0:81], PS_12[gl3,0:81], label=r'Pressure Strain Term - $\Phi_{12}$')
855 axes[0].plot(yplus[gl3,0:81], -diss_12[gl3,0:81], label=r'Dissipation - $\epsilon_{12}$')
856 axes[0].plot(yplus[gl3,0:81], diff_12[gl3,0:81], label=r'Turbulent Diffusion - $(D_{12})_{t}$')
857 axes[1].plot(yplus[gl3,0:81], diffvisc_12[gl3,0:81], label=r'Viscous Diffusion - $(D_{12})_{v}$')

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    _{v}$$)
854 axes[1].plot(yplus[g13,0:81],LHS_12[g13,0:81],label=r'LHS')
855 for ax in axes:
856     ax.tick_params(labelsize='x-large')
857     ax.xaxis.set_minor_locator(AutoMinorLocator())
858     ax.yaxis.set_minor_locator(AutoMinorLocator())
859     ax.grid(True, linestyle='-.')
860     ax.legend(fontsize=14, loc='best')
861     ax.set_xlabel(' ', color=(0, 0, 0, 0), fontsize=20)
862     ax.set_ylabel(' ', color=(0, 0, 0, 0), fontsize=20)
863 fig12a.add_subplot(111, frameon=False)
864 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
865 plt.xlabel(r'$Y^+$', fontsize=18)
866 #plt.ylabel(r'$P^{k}$', fontsize=18)
867 fig12a.suptitle(r'Terms in $\overline{{V}_1\prime}{V}_2\prime$ Equation at X =
868     '+str(np.around(x2d[g13,0],3))+', m (Lower Domain)', fontsize=20)
869
870 fig12b, axes = plt.subplots(nrows=2, ncols=1, constrained_layout=True)
871 axes[0].plot(yplus[g13,82:],P_11[g13,82:],label=r'Production term - $P_{11}$')
872 axes[1].plot(yplus[g13,82:],PS_11[g13,82:],label=r'Pressure Strain Term')
873 axes[0].plot(yplus[g13,82:],-diss_11[g13,82:],label=r'Dissipation')
874 axes[0].plot(yplus[g13,82:],diff_11[g13,82:],label=r'Turbulent Diffusion')
875 axes[1].plot(yplus[g13,82:],diffvisc_11[g13,82:],label=r'Viscous Diffusion')
876 axes[1].plot(yplus[g13,82:],LHS_11[g13,82:],label=r'LHS')
877 #axes[1].plot(yplus[g13,82:],P_12[g13,82:],label=r'Production term - $P_{12}$')
878 #axes[1].plot(yplus[g13,82:],PS_12[g13,82:],label=r'Pressure Strain Term')
879 #axes[1].plot(yplus[g13,82:],-diss_12[g13,82:],label=r'Dissipation')
880 #axes[1].plot(yplus[g13,82:],diff_12[g13,82:],label=r'Turbulent Diffusion')
881 #axes[1].plot(yplus[g13,82:],diffvisc_12[g13,82:],label=r'Viscous Diffusion')
882 #axes[1].plot(yplus[g13,82:],LHS_12[g13,82:],label=r'LHS')
883 for ax in axes:
884     ax.tick_params(labelsize='x-large')
885     ax.xaxis.set_minor_locator(AutoMinorLocator())
886     ax.yaxis.set_minor_locator(AutoMinorLocator())
887     ax.grid(True, linestyle='-.')
888     ax.legend(fontsize=14, loc='best')
889     ax.set_xlabel(' ', color=(0, 0, 0, 0), fontsize=20)
890     ax.set_ylabel(' ', color=(0, 0, 0, 0), fontsize=20)
891 fig12b.add_subplot(111, frameon=False)
892 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
893 plt.xlabel(r'$Y^+$', fontsize=18)
894 #plt.ylabel(r'$P^{k}$', fontsize=18)
895 fig12b.suptitle(r'Terms in $\overline{{V}_1\prime\prime}{V}_2\prime$ Equation at X =
896     '+str(np.around(x2d[g13,0],3))+', m (Upper Domain)', fontsize=20)
897
897 fig12c, axes = plt.subplots(nrows=2, ncols=1, constrained_layout=True)
898 #axes[0].plot(yplus[g13,82:],P_11[g13,82:],label=r'Production term - $P_{11}$')
899 #axes[0].plot(yplus[g13,82:],PS_11[g13,82:],label=r'Pressure Strain Term')
900 #axes[0].plot(yplus[g13,82:],-diss_11[g13,82:],label=r'Dissipation')
901 #axes[0].plot(yplus[g13,82:],diff_11[g13,82:],label=r'Turbulent Diffusion')
902 #axes[0].plot(yplus[g13,82:],diffvisc_11[g13,82:],label=r'Viscous Diffusion')
903 #axes[0].plot(yplus[g13,82:],LHS_11[g13,82:],label=r'LHS')
904 axes[0].plot(yplus[g13,82:],P_12[g13,82:],label=r'Production term - $P_{12}$')
905 axes[1].plot(yplus[g13,82:],PS_12[g13,82:],label=r'Pressure Strain Term')
906 axes[0].plot(yplus[g13,82:],-diss_12[g13,82:],label=r'Dissipation')
907 axes[0].plot(yplus[g13,82:],diff_12[g13,82:],label=r'Turbulent Diffusion')
908 axes[1].plot(yplus[g13,82:],diffvisc_12[g13,82:],label=r'Viscous Diffusion')
909 axes[1].plot(yplus[g13,82:],LHS_12[g13,82:],label=r'LHS')
910 for ax in axes:
911     ax.tick_params(labelsize='x-large')
912     ax.xaxis.set_minor_locator(AutoMinorLocator())
913     ax.yaxis.set_minor_locator(AutoMinorLocator())
914     ax.grid(True, linestyle='-.')
915     ax.legend(fontsize=14, loc='best')
916     ax.set_xlabel(' ', color=(0, 0, 0, 0), fontsize=20)

```

```

917     ax.set_ylabel(' ', color=(0, 0, 0, 0), fontsize=20)
918 fig12c.add_subplot(111, frameon=False)
919 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
920 plt.xlabel(r'$Y^+$', fontsize=18)
921 #plt.ylabel(r'$P^k$', fontsize=18)
922 fig12c.suptitle(r'Terms in $\overline{V_1 \prime} \{ V_2 \ prime \}' $ Equation at X =
923     '+str(np.around(x2d[gl3,0],3))+', m (Upper Domain)', fontsize=20)
924
925 #%% Assignment 1.8 - Reynold's Stresses using Boussinesq Assumption
926 # Calculating Reynolds Stresses
927 visc_turb = C_mu * ((k_RANS_2d**2)/diss_RANS_2d)
928 S11 = 0.5 * (dub_dx + dub_dx)
929 S12 = 0.5 * (dub_dy + dvb_dx)
930 S22 = 0.5 * (dvb_dy + dvb_dy)
931 uu2d_B = (-2 * visc_turb * S11) + ((2/3) * k_RANS_2d)
932 vv2d_B = (-2 * visc_turb * S22) + ((2/3) * k_RANS_2d)
933 uv2d_B = (-2 * visc_turb * S12)
934
935 # Comparision of Eddy-viscosity and Reynolds stress - Contour plots
936 vmax1 = np.max(uu2d_B-uu2d)
937 vmax2 = np.max(vv2d_B-vv2d)
938 vmax3 = np.max(uv2d_B-uv2d)
939 v1 = np.linspace(0,vmax1,100)
940 v2 = np.linspace(0,vmax2,100)
941 v3 = np.linspace(0,vmax3,100)
942 fig13, axes = plt.subplots(3,2,constrained_layout=True)
943 axes = axes.reshape(-1)
944 C1 = axes[0].contourf(x2d,y2d,uu2d_B-uu2d,levels=v1,cmap='binary',extend='min')
945 C1.cmap.set_under('papayawhip')
946 C2 = axes[1].contourf(x2d,y2d,uu2d_B,100,cmap='jet')
947 cb1 = fig13.colorbar(C1,ax=axes[0])
948 cb2 = fig13.colorbar(C2,ax=axes[1])
949 cb1.ax.tick_params(labelsize=16)
950 cb2.ax.tick_params(labelsize=16)
951 axes[0].set_title(r'Eddy Viscosity Stress - Reynolds Stress ($\overline{V_1 \ prime^2}$)', fontsize=20)
952 axes[1].set_title(r'Eddy Viscosity Stress - $\overline{V_1 \ prime^2}$', fontsize=20)
953 C3 = axes[2].contourf(x2d,y2d,vv2d_B-vv2d,levels=v2,cmap='binary',extend='min')
954 C3.cmap.set_under('papayawhip')
955 C4 = axes[3].contourf(x2d,y2d,vv2d_B,100,cmap='jet')
956 cb3 = fig13.colorbar(C3,ax=axes[2])
957 cb4 = fig13.colorbar(C4,ax=axes[3])
958 cb3.ax.tick_params(labelsize=16)
959 cb4.ax.tick_params(labelsize=16)
960 axes[2].set_title(r'Eddy Viscosity Stress - Reynolds Stress ($\overline{V_2 \ prime^2}$)', fontsize=20)
961 axes[3].set_title(r'Eddy Viscosity Stress - $\overline{V_2 \ prime^2}$', fontsize=20)
962 C5 = axes[4].contourf(x2d,y2d,uv2d_B-uv2d,levels=v3,cmap='binary',extend='min')
963 C5.cmap.set_under('papayawhip')
964 C6 = axes[5].contourf(x2d,y2d,uv2d_B,100,cmap='jet')
965 cb5 = fig13.colorbar(C5,ax=axes[4])
966 cb6 = fig13.colorbar(C6,ax=axes[5])
967 cb5.ax.tick_params(labelsize=16)
968 cb6.ax.tick_params(labelsize=16)
969 axes[4].set_title(r'Eddy Viscosity Stress - Reynolds Stress ($\overline{V_1 \ prime} \{ V_2 \ prime \}$)', fontsize=20)
970 axes[5].set_title(r'Eddy Viscosity Stress - $\overline{V_1 \ prime} \{ V_2 \ prime \}$', fontsize=20)
971
972 # Comparision of Eddy-viscosity and Reynolds stress - Line plots
973 fig14, axes = plt.subplots(3,2,constrained_layout=True)
974 axes = axes.reshape(-1)
975 gl4 = 0

```

```

976 gl15 = 100
977 axes[0].plot(yplus[g14,:81],uu2d[g14,:81],label='Reynolds Stress')
978 axes[0].plot(yplus[g14,:81],uu2d_B[g14,:81],label='Eddy Viscosity Stress')
979 axes[0].set_title(r'$\overline{{V_1}^{\prime\prime}}$ at X = '+str(np.around(x2d[g14,0],3))
  +' m', fontsize=16)
980 axes[1].plot(yplus[g15,:81],uu2d[g15,:81],label='Reynolds Stress')
981 axes[1].plot(yplus[g15,:81],uu2d_B[g15,:81],label='Eddy Viscosity Stress')
982 axes[1].set_title(r'$\overline{{V_1}^{\prime\prime}}$ at X = '+str(np.around(x2d[g15,0],3))
  +' m', fontsize=16)
983 axes[2].plot(yplus[g14,:81],vv2d[g14,:81],label='Reynolds Stress')
984 axes[2].plot(yplus[g14,:81],vv2d_B[g14,:81],label='Eddy Viscosity Stress')
985 axes[2].set_title(r'$\overline{{V_2}^{\prime\prime}}$ at X = '+str(np.around(x2d[g14,0],3))
  +' m', fontsize=16)
986 axes[3].plot(yplus[g15,:81],vv2d[g15,:81],label='Reynolds Stress')
987 axes[3].plot(yplus[g15,:81],vv2d_B[g15,:81],label='Eddy Viscosity Stress')
988 axes[3].set_title(r'$\overline{{V_2}^{\prime\prime}}$ at X = '+str(np.around(x2d[g15,0],3))
  +' m', fontsize=16)
989 axes[4].plot(yplus[g14,:81],uv2d[g14,:81],label='Reynolds Stress')
990 axes[4].plot(yplus[g14,:81],uv2d_B[g14,:81],label='Eddy Viscosity Stress')
991 axes[4].set_title(r'$\overline{{V_1}^{\prime}\{V_2}^{\prime}}$ at X = '+str(np.
  arround(x2d[g14,0],3))+ ' m', fontsize=16)
992 axes[5].plot(yplus[g15,:81],uv2d[g15,:81],label='Reynolds Stress')
993 axes[5].plot(yplus[g15,:81],uv2d_B[g15,:81],label='Eddy Viscosity Stress')
994 axes[5].set_title(r'$\overline{{V_1}^{\prime}\{V_2}^{\prime}}$ at X = '+str(np.
  arround(x2d[g15,0],3))+ ' m', fontsize=16)
995 for ax in axes:
996     ax.tick_params(labelsize='x-large')
997     ax.xaxis.set_minor_locator(AutoMinorLocator())
998     ax.yaxis.set_minor_locator(AutoMinorLocator())
999     ax.grid(True, linestyle='-.')
1000    ax.legend(fontsize=16, loc='best')
1001    ax.set_xlabel('x', color=(0, 0, 0, 0), fontsize=20)
1002    ax.set_ylabel('y', color=(0, 0, 0, 0), fontsize=20)
1003 fig14.add_subplot(111, frameon=False)
1004 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
1005 plt.ylabel("Values of Eddy viscosity and Reynolds stress", fontsize=18)
1006 plt.xlabel(r"$Y^+$", fontsize=18)
1007 fig14.suptitle('Comparison between Reynolds and Eddy viscosity stresses - $\overline{{V_1}^{\prime\prime}}$, $\overline{{V_2}^{\prime\prime}}$ and $\overline{{V_1}^{\prime}\{V_2}^{\prime}}$ (Lower part of domain)', fontsize=24)
1008
1009 fig14a, axes = plt.subplots(3,2, constrained_layout=True)
1010 axes = axes.reshape(-1)
1011 axes[0].plot(yplus[g14,82:],uu2d[g14,82:],label='Reynolds Stress')
1012 axes[0].plot(yplus[g14,82:],uu2d_B[g14,82:],label='Eddy Viscosity Stress')
1013 axes[0].set_title(r'$\overline{{V_1}^{\prime\prime}}$ at X = '+str(np.around(x2d[g14,0],3))
  +' m', fontsize=16)
1014 axes[1].plot(yplus[g15,82:],uu2d[g15,82:],label='Reynolds Stress')
1015 axes[1].plot(yplus[g15,82:],uu2d_B[g15,82:],label='Eddy Viscosity Stress')
1016 axes[1].set_title(r'$\overline{{V_1}^{\prime\prime}}$ at X = '+str(np.around(x2d[g15,0],3))
  +' m', fontsize=16)
1017 axes[2].plot(yplus[g14,82:],vv2d[g14,82:],label='Reynolds Stress')
1018 axes[2].plot(yplus[g14,82:],vv2d_B[g14,82:],label='Eddy Viscosity Stress')
1019 axes[2].set_title(r'$\overline{{V_2}^{\prime\prime}}$ at X = '+str(np.around(x2d[g14,0],3))
  +' m', fontsize=16)
1020 axes[3].plot(yplus[g15,82:],vv2d[g15,82:],label='Reynolds Stress')
1021 axes[3].plot(yplus[g15,82:],vv2d_B[g15,82:],label='Eddy Viscosity Stress')
1022 axes[3].set_title(r'$\overline{{V_2}^{\prime\prime}}$ at X = '+str(np.around(x2d[g15,0],3))
  +' m', fontsize=16)
1023 axes[4].plot(yplus[g14,82:],uv2d[g14,82:],label='Reynolds Stress')
1024 axes[4].plot(yplus[g14,82:],uv2d_B[g14,82:],label='Eddy Viscosity Stress')
1025 axes[4].set_title(r'$\overline{{V_1}^{\prime}\{V_2}^{\prime}}$ at X = '+str(np.
  arround(x2d[g14,0],3))+ ' m', fontsize=16)
1026 axes[5].plot(yplus[g15,82:],uv2d[g15,82:],label='Reynolds Stress')
1027 axes[5].plot(yplus[g15,82:],uv2d_B[g15,82:],label='Eddy Viscosity Stress')
1028 axes[5].set_title(r'$\overline{{V_1}^{\prime}\{V_2}^{\prime}}$ at X = '+str(np.

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    around(x2d[g15,0],3))+', m', fontsize=16)
1029 for ax in axes:
1030     ax.tick_params(labelsize='x-large')
1031     ax.xaxis.set_minor_locator(AutoMinorLocator())
1032     ax.yaxis.set_minor_locator(AutoMinorLocator())
1033     ax.grid(True, linestyle='-.')
1034     ax.legend(fontsize=16, loc='best')
1035     ax.set_xlabel(' ', color=(0, 0, 0, 0), fontsize=20)
1036     ax.set_ylabel(' ', color=(0, 0, 0, 0), fontsize=20)
1037 fig14a.add_subplot(111, frameon=False)
1038 plt.tick_params(labelcolor="none", top=False, bottom=False, left=False, right=False)
1039 plt.xlabel("Values of Eddy viscosity and Reynolds stress", fontsize=18)
1040 plt.ylabel(r"$Y^+$", fontsize=18)
1041 fig14a.suptitle('Comparison between Reynolds and Eddy viscosity stresses - $\overline{V_1}^{\prime\prime}$, $\overline{V_2}^{\prime\prime}$ and $\overline{V_1}^{\prime}$ $\overline{V_2}^{\prime}$ (Upper part of domain)', fontsize=24)
1042
1043 # Production term of Reynolds stress - Boussinesq assumption
1044 Pk_B = 2 * visc_turb * (S11*S11 + 2*S12*S12 + S22*S22)
1045 #Pk_BB = 2 * visc_turb_modified * (S11*S11 + 2*S12*S12 + S22*S22)
1046 vmin = np.min(Pk_B)
1047 vmax = 3
1048 v = np.linspace(vmin,vmax,100)
1049 fig15, axes = plt.subplots(2,1, constrained_layout=True)
1050 C1 = axes[0].contourf(x2d,y2d,Pk_B, levels=v, extend='max', cmap='jet')
1051 C2 = axes[1].contourf(x2d,y2d,Pk_B, 100, cmap='jet')
1052 axes[1].set_ylim(2.5,y2d[0,-1])
1053 cb1 = fig15.colorbar(C1,ax=axes[0])
1054 cb2 = fig15.colorbar(C2,ax=axes[1])
1055 cb1.ax.tick_params(labelsize=16)
1056 cb2.ax.tick_params(labelsize=16)
1057 axes[0].set_title(r'Production term - Boussinesq Assumption', fontsize=20)
1058 axes[1].set_title(r'Production term - Boussinesq Assumption (Zoomed near top wall)', fontsize=20)
1059
1060 fig15a, axes = plt.subplots(1,1, constrained_layout=True)
1061 C1 = axes.contourf(x2d,y2d,Pk_BB,100,cmap='jet')
1062 cb1 = fig15a.colorbar(C1,ax=axes)
1063 cb1.ax.tick_params(labelsize=16)
1064 axes.set_title(r'Production term - Boussinesq Assumption - After Limiter Function', fontsize=20)
1065
1066 #%% Assignment 1.9 - Eigenvectors of Reynolds Stress and Strain rate tensor
1067 EVx_SRT = np.zeros((ni,nj))
1068 EVy_SRT = np.zeros((ni,nj))
1069 EVx_RS = np.zeros((ni,nj))
1070 EVy_RS = np.zeros((ni,nj))
1071 EigenValue1 = np.zeros((ni,nj))
1072 EigenValue2 = np.zeros((ni,nj))
1073
1074 for i in range(ni):
1075     for j in range(nj):
1076         value1, vector1 = np.linalg.eig(np.array([[S11[i,j],S12[i,j]],[S12[i,j],S22[i,j]]]))
1077         EVx_SRT[i,j]=vector1[0,0]
1078         EVy_SRT[i,j]=vector1[1,0]
1079         EigenValue1[i,j] = value1[0]
1080         EigenValue2[i,j] = value1[1]
1081         value2, vector2 = np.linalg.eig(np.array([[uu2d_B[i,j],uv2d_B[i,j]],[uv2d_B[i,j],vv2d_B[i,j]]]))
1082         EVx_RS[i,j]=vector2[0,0]
1083         EVy_RS[i,j]=vector2[1,0]
1084
1085 k=5
1086 fig16 = plt.figure()
1087 axes = fig16.add_axes([0.1,0.1,0.75,0.75])

```

```
1088 q1 = axes.quiver(x2d[:, :, :], y2d[:, :, :], -EVx_SRT[:, :, :], -EVy_SRT[:, :, :], color='blue', pivot='mid', width=0.001, scale=30, headwidth=5, headlength=5)
1089 q2 = axes.quiver(x2d[:, :, :], y2d[:, :, :], EVx_RS[:, :, :], EVy_RS[:, :, :], color='red', pivot='mid')
1090 axes.quiverkey(q1, X=1.1, Y=0.6, U=3, label='Strain Rate Tensor', labelpos='S', fontproperties={'weight':'bold', 'size':16})
1091 axes.quiverkey(q2, X=1.1, Y=0.4, U=5, label='Reynolds Stress', labelpos='S', fontproperties={'weight':'bold', 'size':16})
1092 axes.set_title('Eigen vectors for Strain rate tensor and Reynolds stress', fontsize=20)
1093 axes.set_xlabel('X (m)', fontsize=16)
1094 axes.set_ylabel('Y (m)', fontsize=16)
1095
1096 #%% Assignment 1.10 -
1097 lambda1 = np.zeros((ni, nj))
1098 visc_turb_modified = np.zeros((ni, nj))
1099
1100 for i in range(ni):
1101     for j in range(nj):
1102         if EigenValue1[i, j] >= EigenValue2[i, j]:
1103             lambda1[i, j] = EigenValue1[i, j]
1104         else:
1105             lambda1[i, j] = EigenValue2[i, j]
1106
1107 for i in range(ni):
1108     for j in range(nj):
1109         if visc_turb[i, j] >=((k_RANS_2d[i, j]/3)*(1/np.abs(lambda1[i, j]))):
1110             visc_turb_modified[i, j] = ((k_RANS_2d[i, j]/3)*(1/np.abs(lambda1[i, j])))
1111         else:
1112             visc_turb_modified[i, j] = visc_turb[i, j]
1113
1114 uu2d_B_lim = (-2 * visc_turb_modified * S11) + ((2/3) * k_RANS_2d)
1115 vv2d_B_lim = (-2 * visc_turb_modified * S22) + ((2/3) * k_RANS_2d)
1116 uv2d_B_lim = (-2 * visc_turb_modified * S12)
1117
1118 fig17 = plt.figure()
1119 ax1 = plt.subplot2grid((2, 2), (0, 0), colspan=2)
1120 ax2 = plt.subplot2grid((2, 2), (1, 0))
1121 ax3 = plt.subplot2grid((2, 2), (1, 1))
1122 cax1 = ax1.contourf(x2d, y2d, visc_turb - visc_turb_modified, cmap='jet', levels=50)
1123 cax2 = ax2.contourf(x2d, y2d, visc_turb, cmap='jet', levels=50)
1124 cax3 = ax3.contourf(x2d, y2d, visc_turb_modified, cmap='jet', levels=50)
1125 for ax in [ax1, ax2, ax3]:
1126     ax.set_xlabel('X (m)')
1127     ax.set_ylabel('Y (m)')
1128 cb1 = fig17.colorbar(cax1, ax=ax1, fraction=0.1)
1129 cb1.ax.tick_params(labelsize=16)
1130 cb2 = fig17.colorbar(cax2, ax=ax2, fraction=0.1)
1131 cb2.ax.tick_params(labelsize=16)
1132 cb3 = fig17.colorbar(cax3, ax=ax3, fraction=0.1)
1133 cb3.ax.tick_params(labelsize=16)
1134 plt.tight_layout()
1135 ax1.set_title(r'Regions affected by limiter function', fontsize=24)
1136 ax2.set_title(r'Turbulent Viscosity ($\nu_{t}$) before limiter function', fontsize=20)
1137 ax3.set_title(r'Turbulent Viscosity ($\nu_{t}$) after limiter function', fontsize=20)
1138 for ax in [ax1, ax2, ax3]:
1139     ax.tick_params(labelsize='x-large')
1140
1141 fig18, axes = plt.subplots(2, 2, constrained_layout=True)
1142 axes = axes.reshape(-1)
1143 vmax1 = np.max(uu2d_B)
1144 vmax2 = np.max(uu2d_B_lim)
1145 vmax3 = np.max(vv2d_B)
1146 vmax4 = np.max(vv2d_B_lim)
1147 vmin1 = np.min(uu2d_B)
1148 vmin2 = np.min(uu2d_B_lim)
1149 vmin3 = np.min(vv2d_B)
```

```

1150 vmin4 = np.min(vv2d_B_lim)
1151 v1 = np.linspace(0,vmax1,100)
1152 v2 = np.linspace(vmin2,vmax2,100)
1153 v3 = np.linspace(0,vmax3,100)
1154 v4 = np.linspace(vmin4,vmax4,100)
1155 cax1 = axes[0].contourf(x2d,y2d,uu2d_B,levels=v1,cmap='Blues',extend='min')
1156 cax1.cmap.set_under('black')
1157 cax2 = axes[1].contourf(x2d,y2d,uu2d_B_lim,levels=v2,cmap='Blues')
1158 cax3 = axes[2].contourf(x2d,y2d,vv2d_B,levels=v3,cmap='Blues',extend='min')
1159 cax3.cmap.set_under('black')
1160 axes[2].set_xlim(6.5,9)
1161 axes[2].set_ylim(0,1.5)
1162 cax4 = axes[3].contourf(x2d,y2d,vv2d_B_lim,levels=v4,cmap='Blues')
1163 axes[3].set_xlim(6.5,9)
1164 axes[3].set_ylim(0,1.5)
1165 axes[0].set_title(r'Normal Stress ($\overline{V_1}^{\prime 2}$) before limiter function', fontsize=18)
1166 axes[1].set_title(r'Normal Stress ($\overline{V_1}^{\prime 2}$) after limiter function', fontsize=18)
1167 axes[2].set_title(r'Normal Stress ($\overline{V_2}^{\prime 2}$) before limiter function', fontsize=18)
1168 axes[3].set_title(r'Normal Stress ($\overline{V_2}^{\prime 2}$) after limiter function', fontsize=18)
1169 for axe,cax in zip(axes,[cax1,cax2,cax3,cax4]):
1170     axe.set_xlabel('X (m)')
1171     axe.set_ylabel('Y (m)')
1172     fig18.colorbar(cax,ax=axe)
1173
1174 fig19,axes = plt.subplots(2,2,constrained_layout=True)
1175 axes = axes.reshape(-1)
1176 axes[0].plot(plusplus[g11,:81],visc_turb[g11,:81],label='Before Limiting Function')
1177 axes[0].plot(plusplus[g11,:81],visc_turb_modified[g11,:81],label='Before Limiting Function')
1178 axes[0].set_title('Turbulent viscosity in Lower domain at X = ' + str(np.around(x2d[g11,0],3)) + ' m', fontsize=20)
1179 axes[1].plot(plusplus[g12,:81],visc_turb[g12,:81],label='Before Limiting Function')
1180 axes[1].plot(plusplus[g12,:81],visc_turb_modified[g12,:81],label='Before Limiting Function')
1181 axes[1].set_title('Turbulent viscosity in Lower domain at X = ' + str(np.around(x2d[g12,0],3)) + ' m', fontsize=20)
1182 axes[2].plot(plusplus[g11,82:],visc_turb[g11,82:],label='Before Limiting Function')
1183 axes[2].plot(plusplus[g11,82:],visc_turb_modified[g11,82:],label='Before Limiting Function')
1184 axes[2].set_title('Turbulent viscosity in Upper domain at X = ' + str(np.around(x2d[g11,0],3)) + ' m', fontsize=20)
1185 axes[3].plot(plusplus[g12,82:],visc_turb[g12,82:],label='Before Limiting Function')
1186 axes[3].plot(plusplus[g12,82:],visc_turb_modified[g12,82:],label='Before Limiting Function')
1187 axes[3].set_title('Turbulent viscosity in Upper domain at X = ' + str(np.around(x2d[g12,0],3)) + ' m', fontsize=20)
1188 for ax in axes:
1189     ax.tick_params(labelsize='x-large')
1190     ax.xaxis.set_minor_locator(AutoMinorLocator())
1191     ax.yaxis.set_minor_locator(AutoMinorLocator())
1192     ax.grid(True, linestyle='-.')
1193     ax.legend(fontsize=16, loc='best')
1194     ax.set_ylabel(r'Turbulent Viscosity ($\nu_{t}$)', fontsize=20)
1195     ax.set_xlabel(r'$Y^{+}$', fontsize=20)
1196
1197 fig20,axes = plt.subplots(1,1,constrained_layout=True)
1198 cax1 = axes.contourf(x2d,y2d,visc_turb-visc_turb_modified,cmap='jet',levels=100)
1199 axes.set_xlabel('X (m)')
1200 axes.set_ylabel('Y (m)')
1201 cb1 = fig20.colorbar(cax1,ax=axes,fraction=0.1)
1202 cb1.ax.tick_params(labelsize=16)
1203 axes.set_title(r'Regions affected by limiter function', fontsize=24)

```

```

1204 """
1205 limiter = np.zeros((ni,nj))
1206 for i in range(ni):
1207     for j in range(nj):
1208         limiter[i,j] = ((k_RANS_2d[i,j]/3)*(1/np.abs(lambda1[i,j])))
1209 result = np.zeros((ni,nj))
1210 for i in range(ni):
1211     for j in range(nj):
1212         if limiter[i,j]>=visc_turb[i,j]:
1213             result[i,j] = 1
1214         else:
1215             result[i,j] = 0
1216 """
1 # -*- coding: utf-8 -*-
2 """
3 Created on Sun Apr 19 18:22:49 2020
4
5 @author: Amey
6 """
7 def WallDistance(x2d,y2d,point_x,point_y):
8     import numpy as np
9     ni = len(x2d)
10    dist_LW = np.zeros(ni)
11    dist_UP = np.zeros(ni)
12    for i in range(ni):
13        dist_LW[i] = np.sqrt(((point_x-x2d[i,0])**2) + ((point_y-y2d[i,0])**2))
14        dist_UP[i] = np.sqrt(((point_x-x2d[i,-1])**2) + ((point_y-y2d[i,-1])**2))
15
16    if min(dist_LW)<=min(dist_UP):
17        min_dist = min(dist_LW)
18    else:
19        min_dist = min(dist_UP)
20
21    return min_dist
2
1 # -*- coding: utf-8 -*-
2 """
3 Created on Sun Apr 19 20:06:05 2020
4
5 @author: Amey
6 """
7 def WallNormal(xf2d,yf2d):
8     import numpy as np
9     # Bottom Wall
10    sx_bottom = np.diff(xf2d[:,0],axis=0)
11    sy_bottom = np.diff(yf2d[:,0],axis=0)
12
13    d=np.sqrt(sx_bottom**2+sy_bottom**2)
14    nx_bottom=-sy_bottom/d
15    ny_bottom=sx_bottom/d
16    # Top Wall
17    sx_top = np.diff(xf2d[:, -1],axis=0)
18    sy_top = np.diff(yf2d[:, -1],axis=0)
19
20    d=np.sqrt(sx_top**2+sy_top**2)
21    nx_top=-sy_top/d
22    ny_top=sx_top/d
23
24    nx_bottom = np.insert(nx_bottom,0,nx_bottom[0],axis=0)
25    ny_bottom = np.insert(ny_bottom,0,ny_bottom[0],axis=0)
26    nx_top = np.insert(nx_top,0,nx_top[0],axis=0)
27    ny_top = np.insert(ny_top,0,ny_top[0],axis=0)
28    nx_bottom = np.insert(nx_bottom,-1,nx_bottom[-1],axis=0)
29    ny_bottom = np.insert(ny_bottom,-1,ny_bottom[-1],axis=0)
30    nx_top = np.insert(nx_top,-1,nx_top[-1],axis=0)

```

```
31     ny_top = np.insert(ny_top,-1,ny_top[-1],axis=0)
32
33     return nx_bottom,ny_bottom,nx_top,ny_top
```