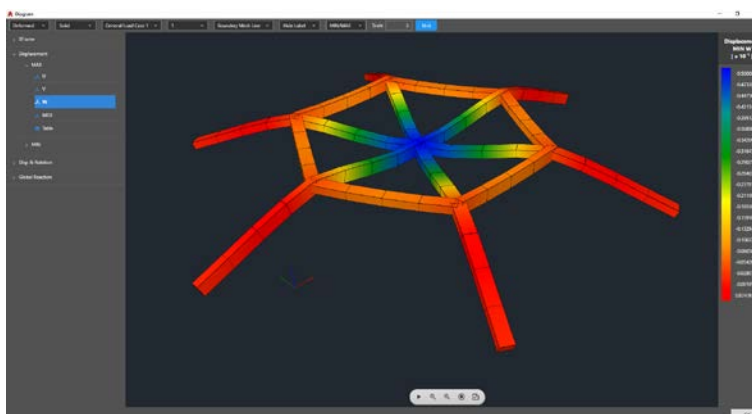
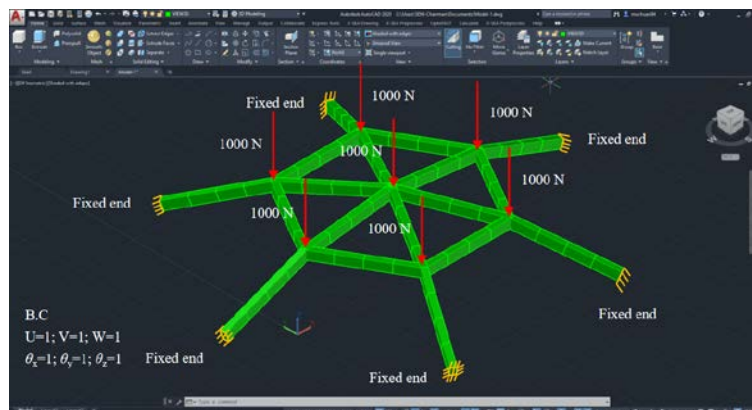


AutoCAD Embedded Finite Element Structural Analysis Software for Offshore & Onshore Structure

“X-SEA AutoCAD”

Verification Report of 2-node Frame element (Xframe)



Verification Example of X-SEA AutoCAD

No: Frame Element 001

Title: Straight Cantilever Beam (Linear Static Analysis)

Problem Description

The beam problem illustrated in Fig.1.1 is analyzed using xframe elements. Four different types of loadings are employed discretely at the free end i.e. extension, in-plane shearing, out-of-plane shearing and twisting moment. The exact displacement for extension, in-plane shear, out-of-plane shear and torsion in the direction of load for the above beam is given below for comparison purpose.

Length $L=6.0$; Height $h=0.2$; Thickness $t=0.1$; $E=1.0 \times 10^7$; $\nu=0.3$; Load $P=\text{unit force}$ at free end.

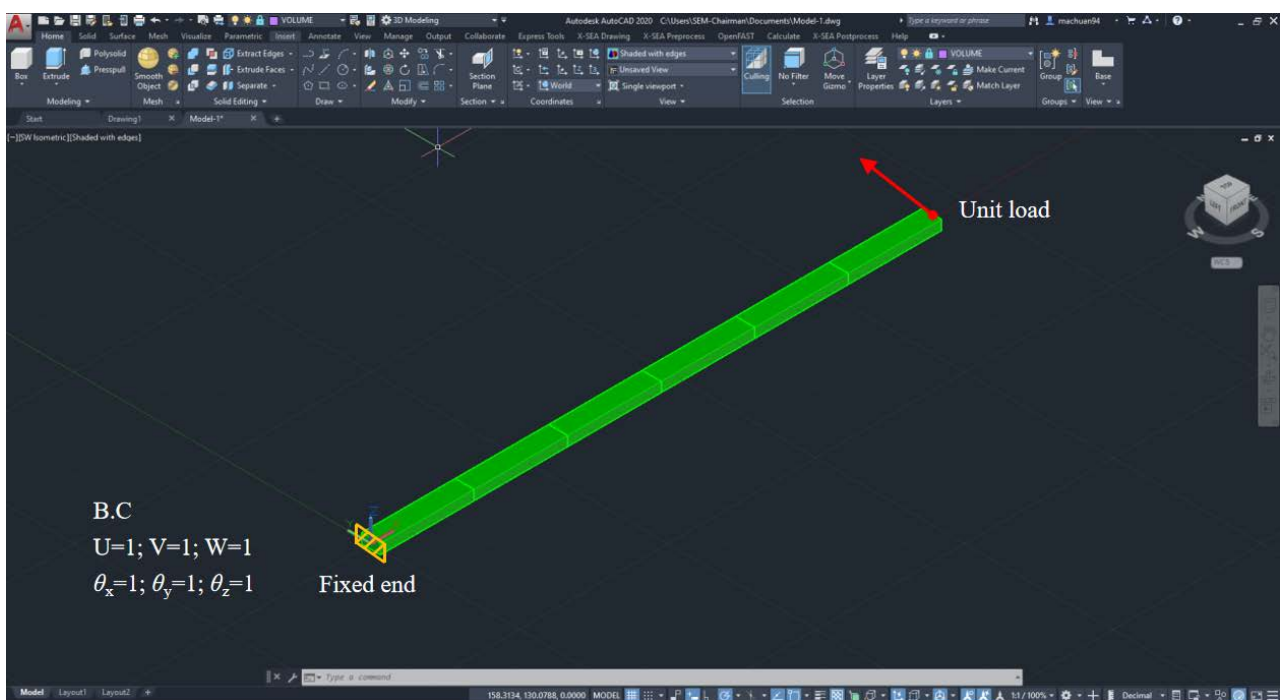


Fig.1.1 Straight cantilever beam model (6 Elements, XFrame)

Results

The results obtained from XFRAME are compared with the above analytical solution in Table 1.1.

Table 1.1 Theoretical and XFrame solutions for beam problems

Problem	Tip load direction	Displacement in direction of load	
		Exact	XFrame
Straight beam	Extension	0.00003	0.000030
	In-plane shear	0.10800	0.108093
	Out-of-plane shear	0.43200	0.432093
	Torsion	0.034243	0.033343
Curved beam	In-plane shear	0.08854	0.087346

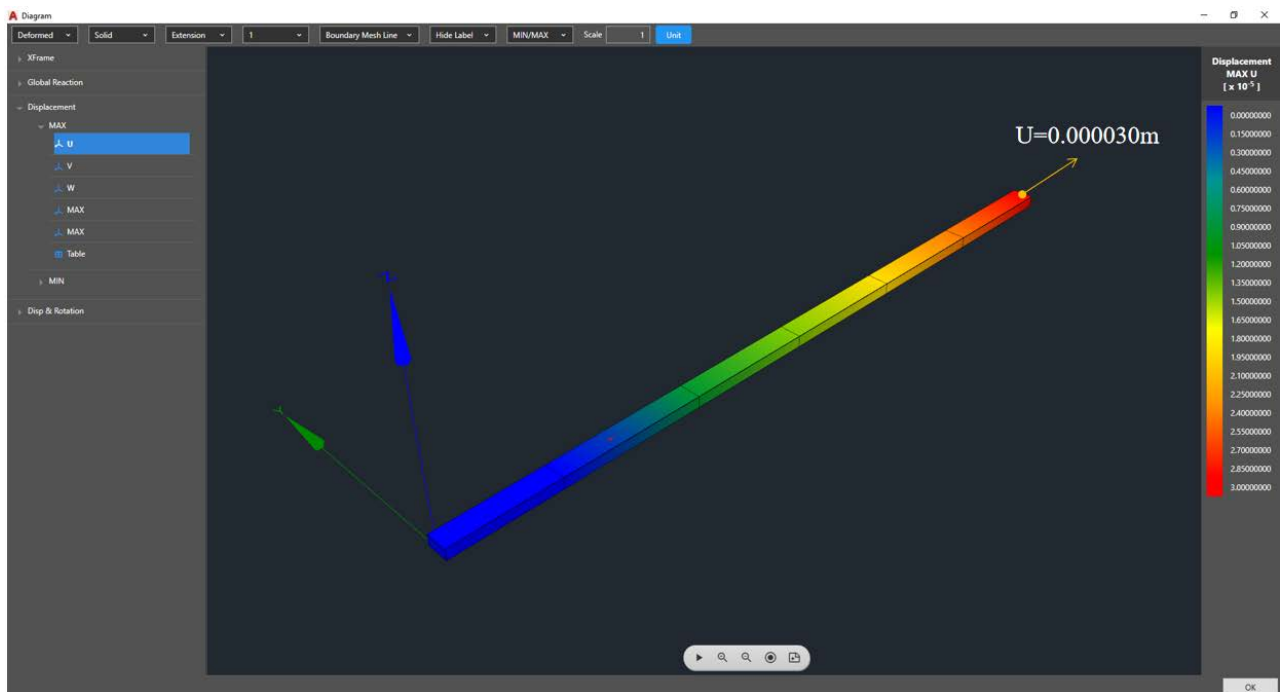


Fig.1.2 Straight cantilever beam's extension (6 Elements, XFrame)

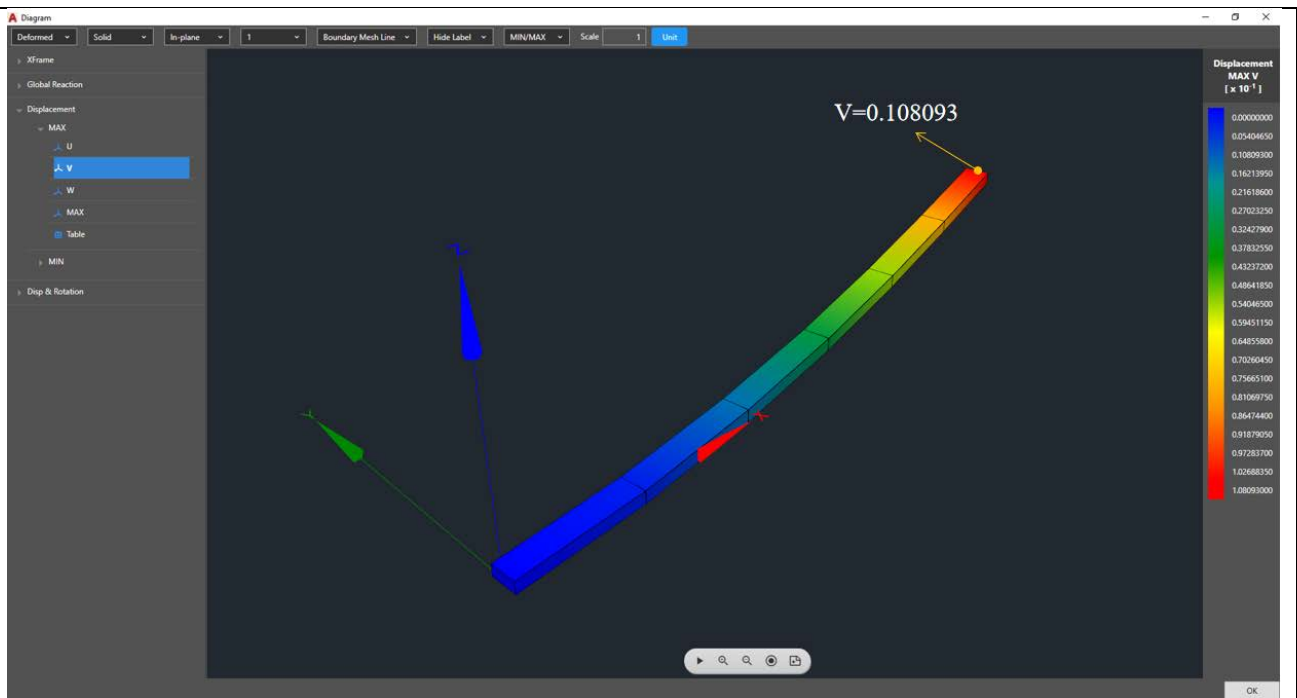


Fig.1.3 Straight cantilever beam's in-plane shear (6 Elements, XFrame)

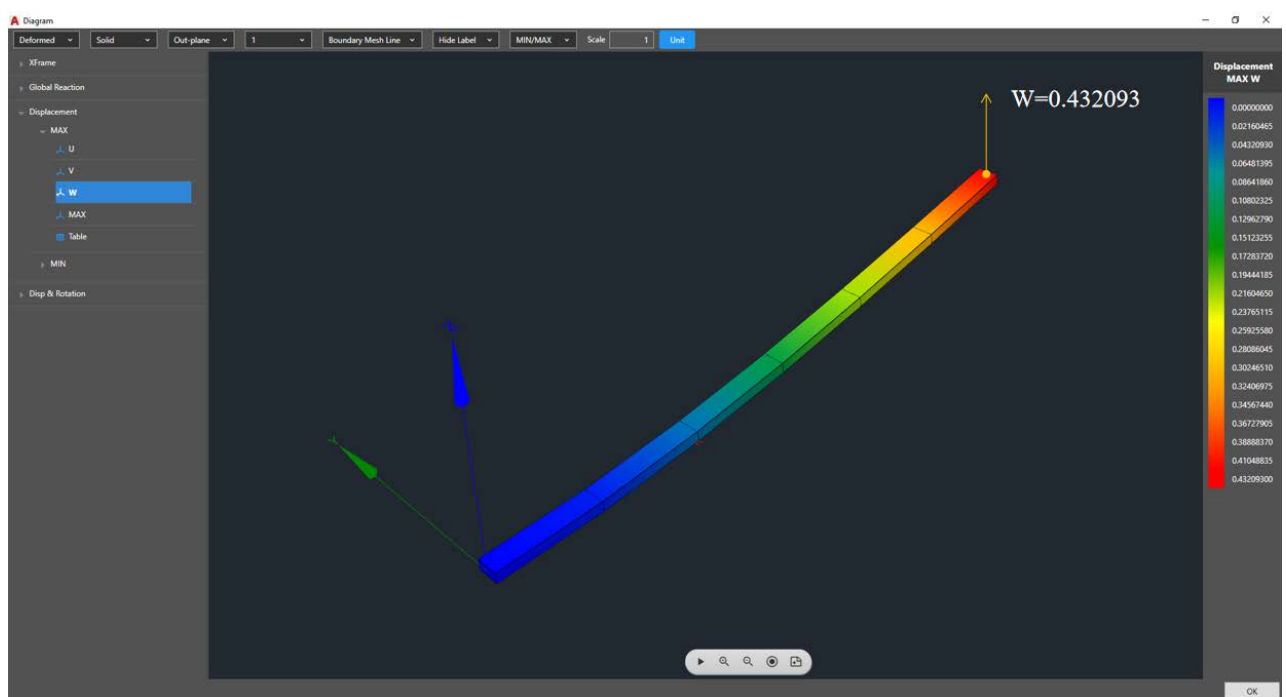


Fig.1.4 Straight cantilever beam's out-of-plane shear (6 Elements, XFrame)

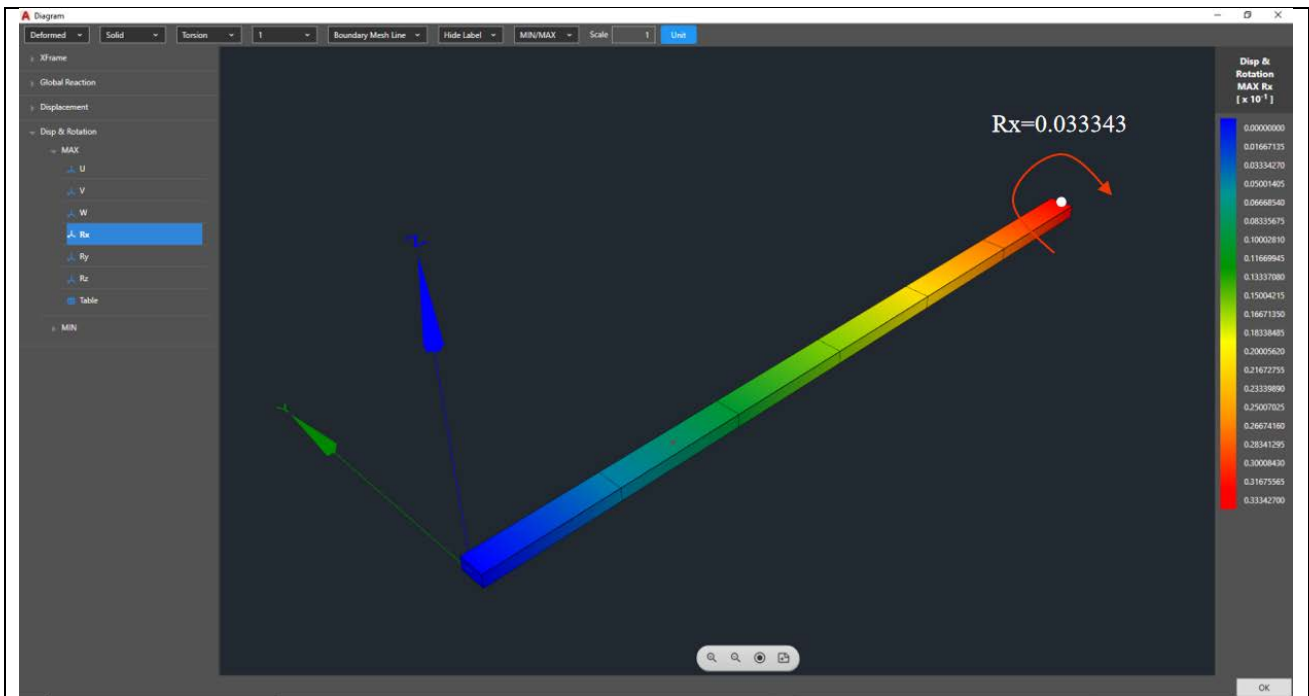


Fig.1.5 Straight cantilever beam's torsion (6 Elements, XFrame)

	XFINASIT Co. LTD
Verification Example of X-SEA AutoCAD	No: Frame Element 002
Title: Curved cantilever beam	
Problem Description	
<p>The curved beam is analyzed using the frame elements. A single in-plane shear load at tip suggests various combinations of the principal deformation modes. The results are compared with analytical vertical displacement at tip obtained by Negi and Jangid (1997).</p> <p>Inner radius=4.12; Outer radius=4.32; Arc=90⁰; Thickness=0.1; E=1.0x10⁷; ν=0.25; Load P=unit in-plane shear force at tip; Mesh size 1x6.</p>	

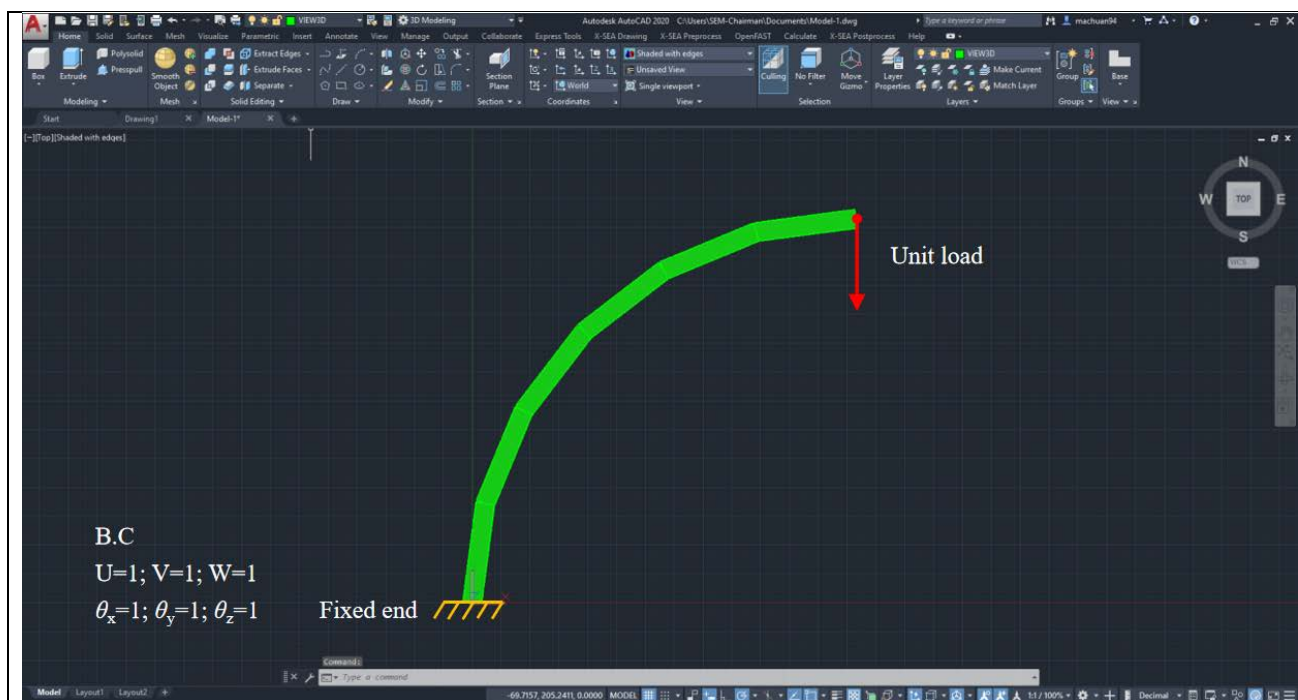


Fig.2.1 Curved cantilever beam model (6 Elements, XFrame)

Results

Table 2.1 Theoretical and XSEA solutions for beam

Problem	Tip load direction	Displacement in direction of load	
		Exact	XFRAME
Straight- beam 1	Extension	0.00003	0.000030
	In-plane shear	0.10800	0.108093
	Out-of-plane shear	0.43200	0.432093
	Torsion	0.034243	0.033343
Curved beam	In-plane shear	0.08854	0.087346

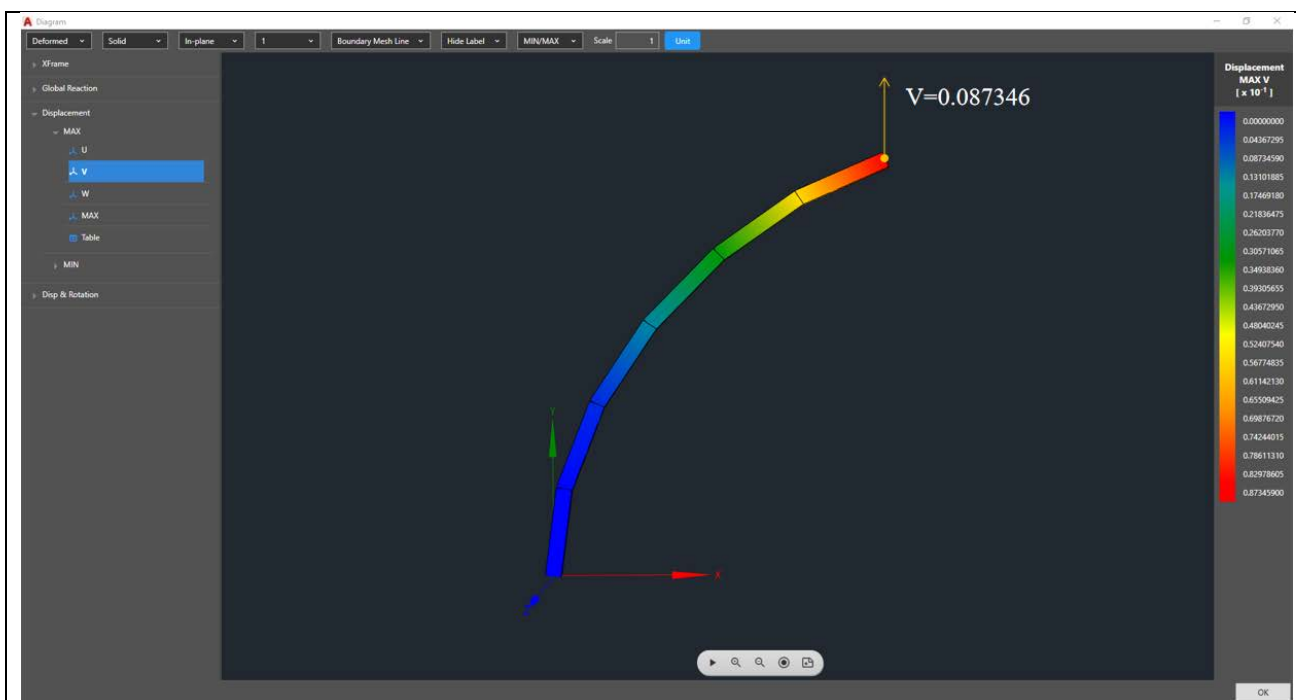


Fig.2.2 Deformation of curved cantilever beam (6 Elements, XFrame)

Title: Column Buckling**Problem Description**

The problems of column buckling are analyzed using the xframe elements and comparing the analytical solutions provided by Chen and Lui (1987).

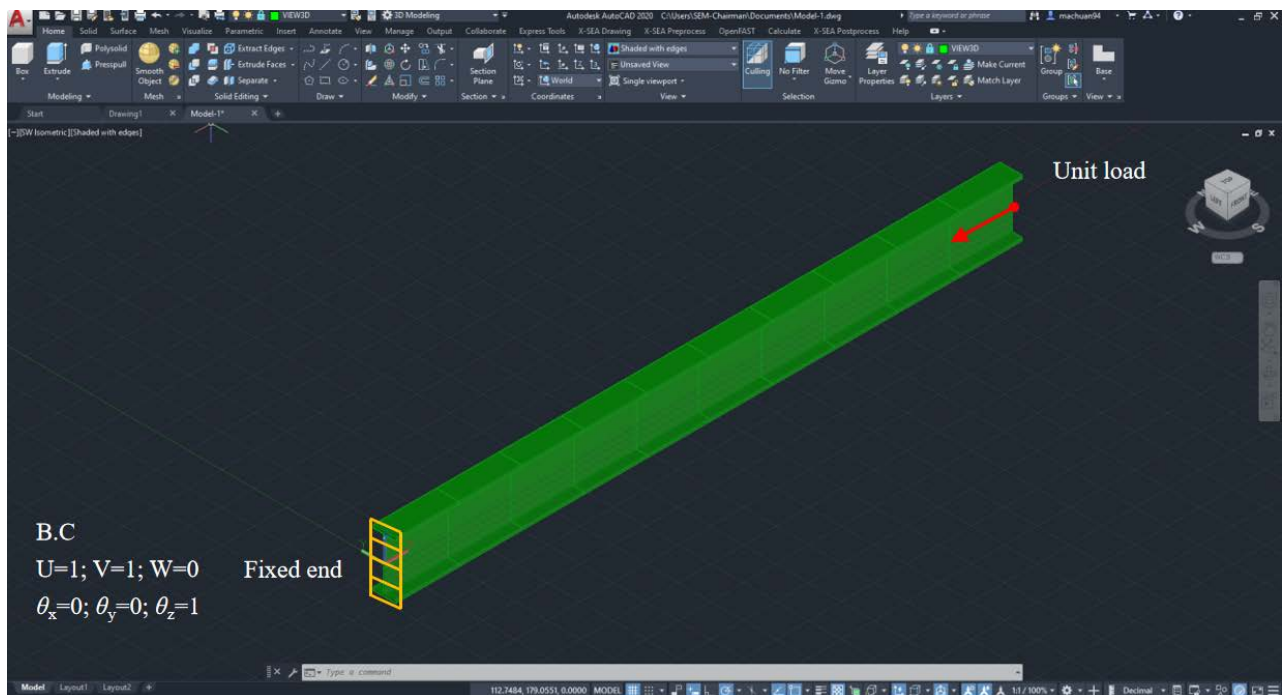
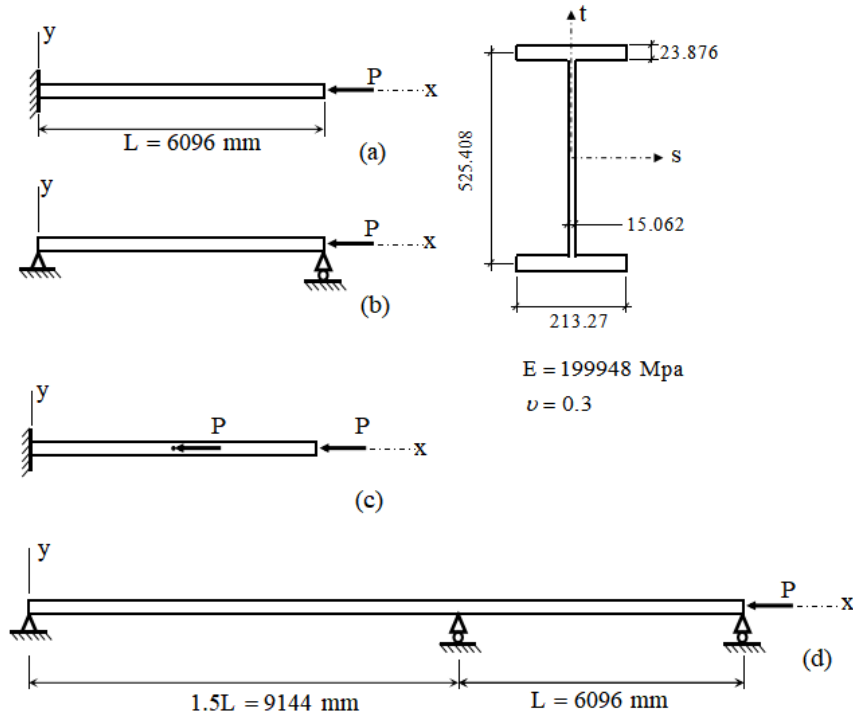


Fig.3.1 Column buckling model (a) Fixed-free column buckling (10 Elements, XFrame)

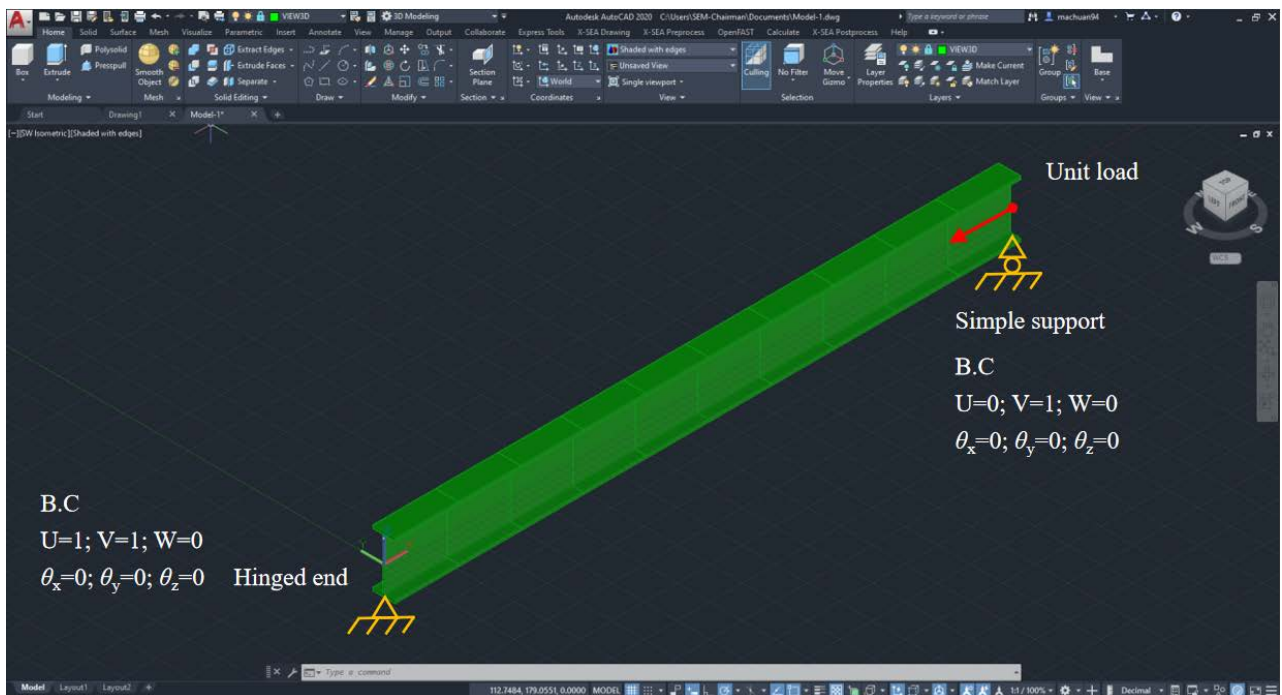


Fig.3.2 Column buckling model (b) Pinned-ended column buckling (10 Elements, XFrame)

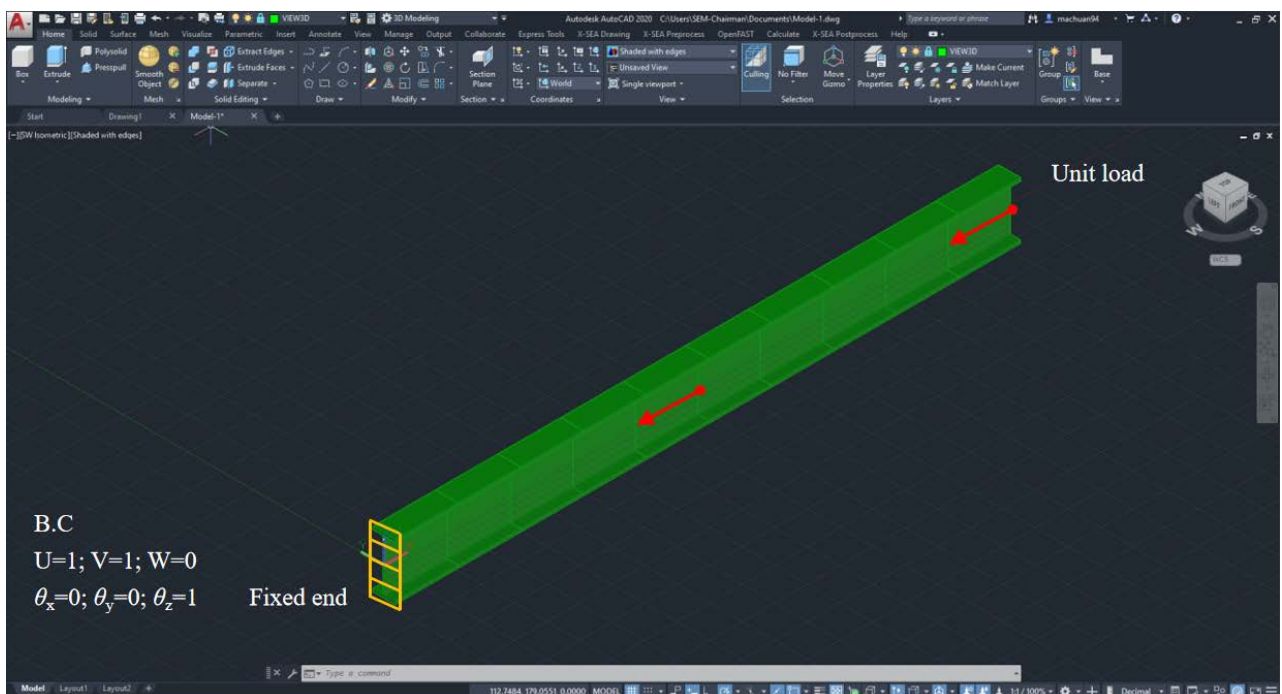


Fig.3.3 Column buckling model (c) Two axial forces cantilever column buckling (10 Elements, XFrame)

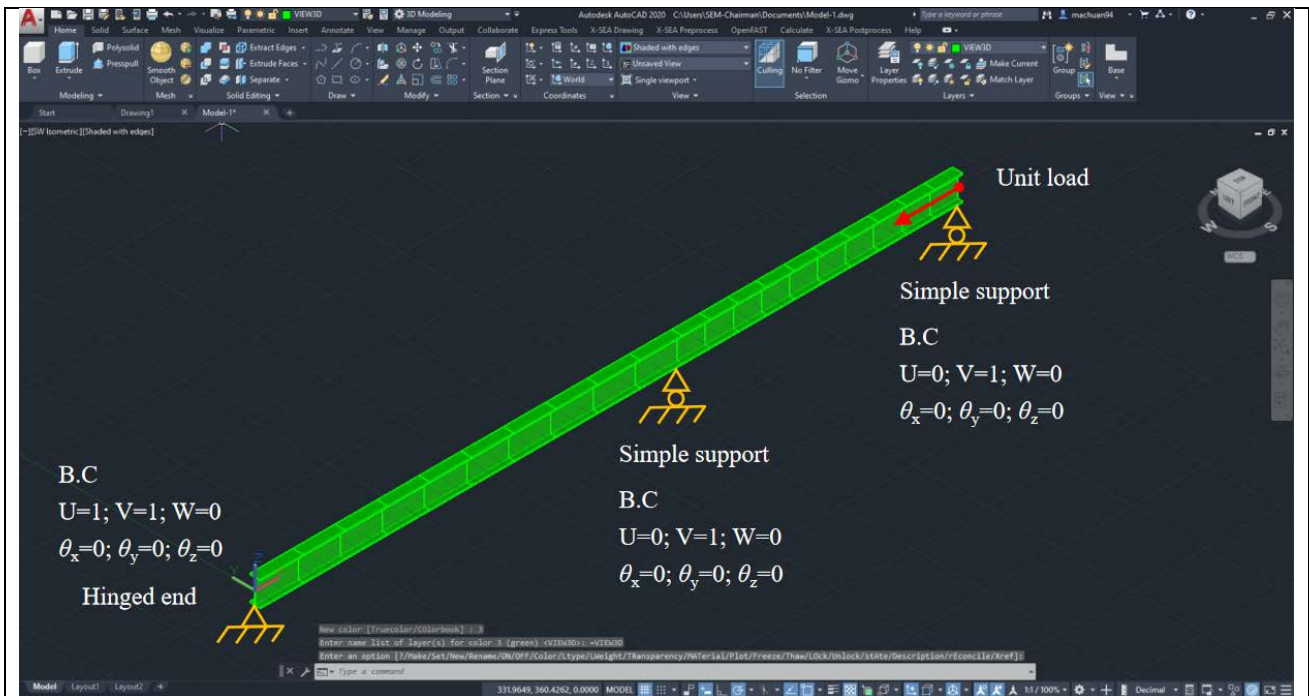


Fig.3.4 Column buckling model (d) Continuous member (20 Elements, XFrame)

Results

The present finite element solutions are compared with the analytical results in Table 3.1. The results calculated by XFRAME give a good agreement with reference.

Table 3.1 Critical loads of column buckling problem ($\times 10^8 \text{N}$)

Case	Number of elements over length L					
	2	4	6	8	10	Exact
(a)	0.112392	0.112295	0.112283	0.112280	0.112278	0.114394
(b)	0.431049	0.426177	0.425566	0.425376	0.425293	0.457577
(c)	0.094146	0.093895	0.093864	0.093854	0.093850	0.095831
(d)	0.263485	0.260890	0.260599	0.260516	0.260481	0.273074

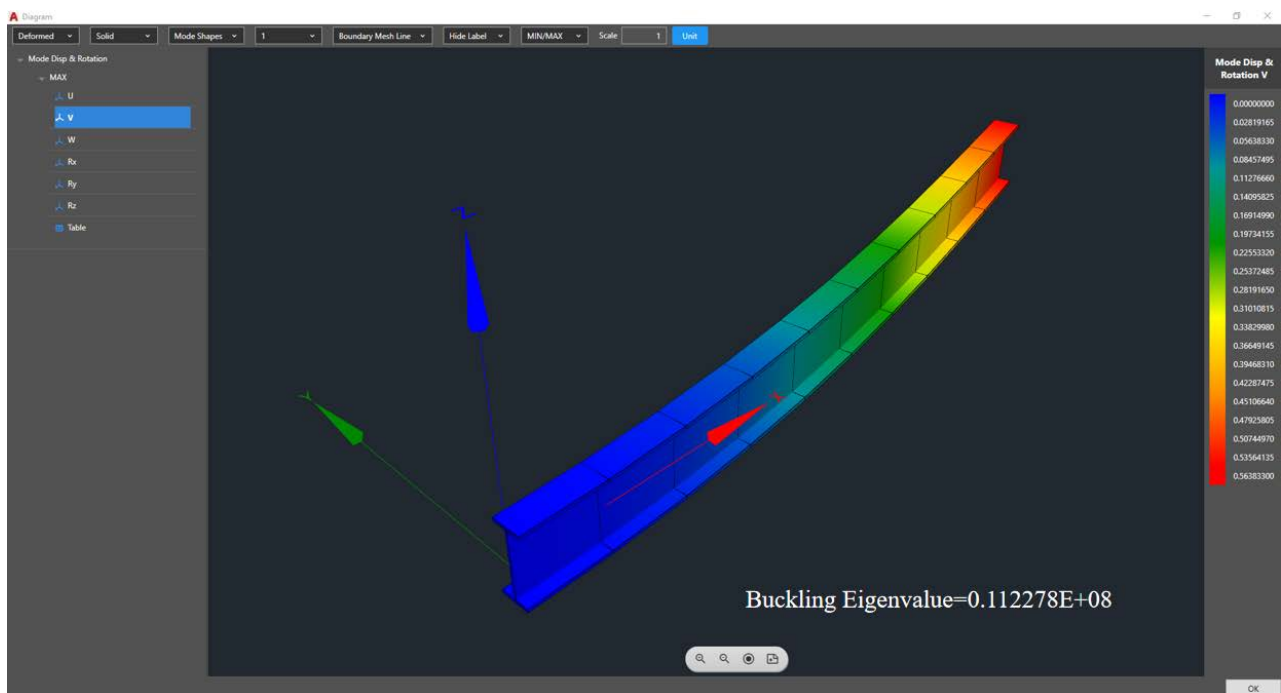


Fig.3.5 Deformation of column buckling (a) Fixed-free column buckling (10 Elements, XFrame)

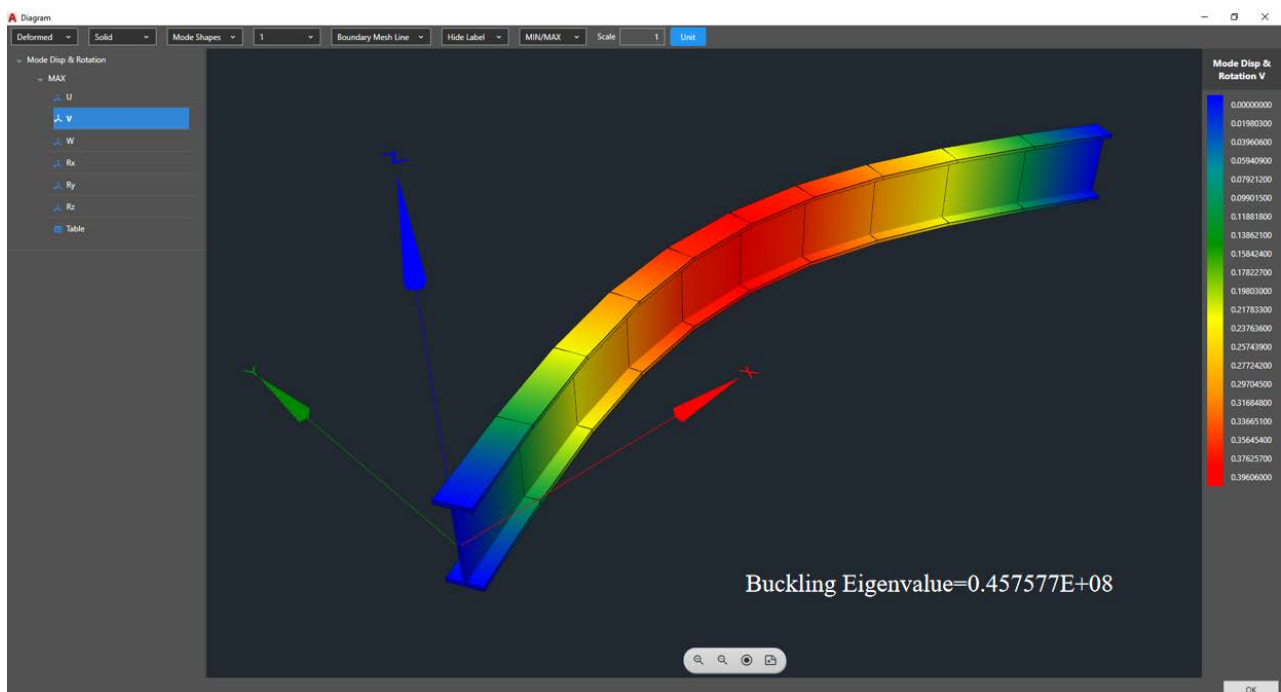


Fig.3.6 Deformation of Column Buckling (b) Pinned-ended column buckling (10 Elements, XFrame)

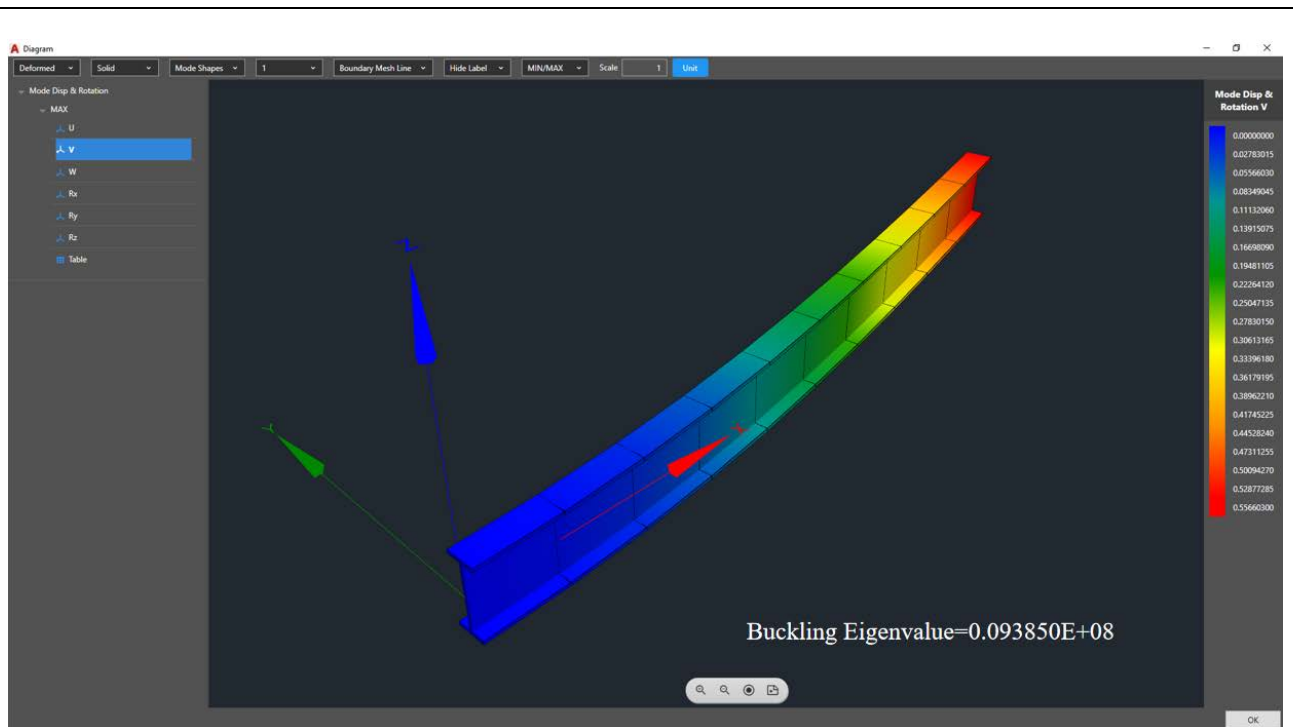


Fig.3.7 Deformation of column buckling (c) Two axial forces cantilever column buckling (10 Elements, XFrame)

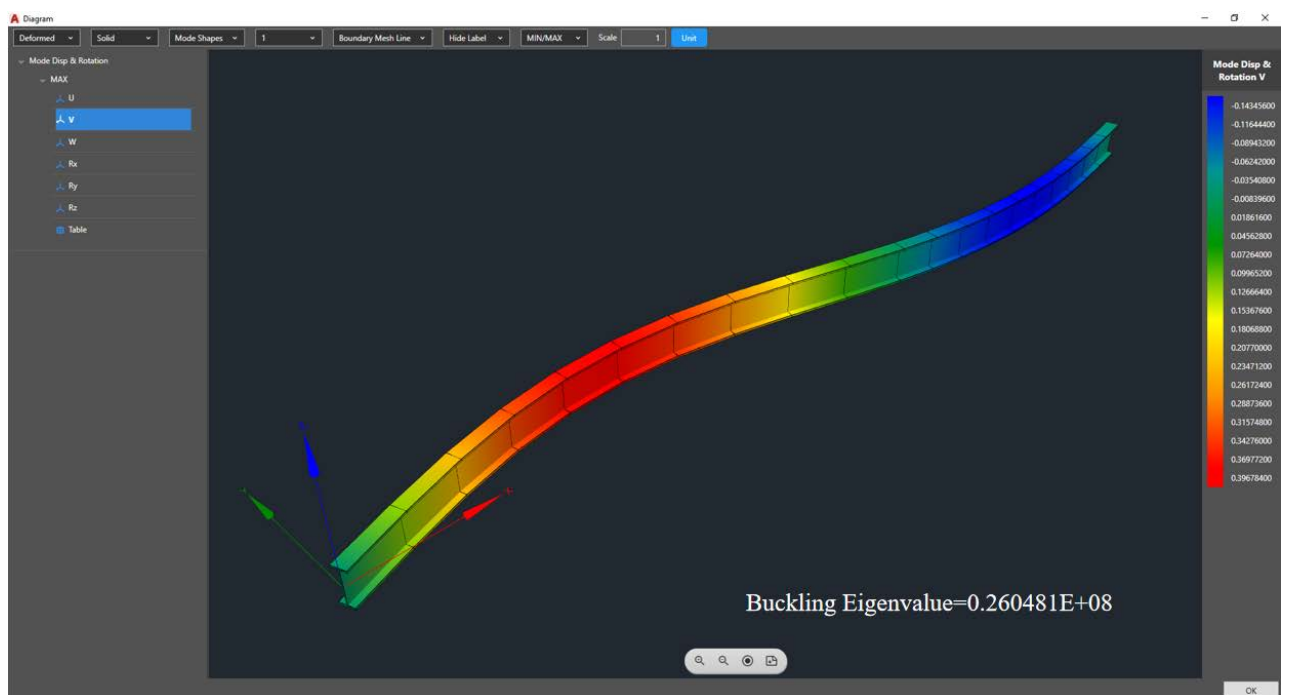


Fig.3.8 Deformation of column buckling (d) Continuous member (20 Elements, XFrame)

Title : Pin-ended Portal frame**Problem Description**

The critical loads for the Portal frame given in Fig.4.1 are calculated using XFRAME element. As the critical loads are different depending on whether the frame is unbraced (sway-permitted case) or braced (sway-prevented case).

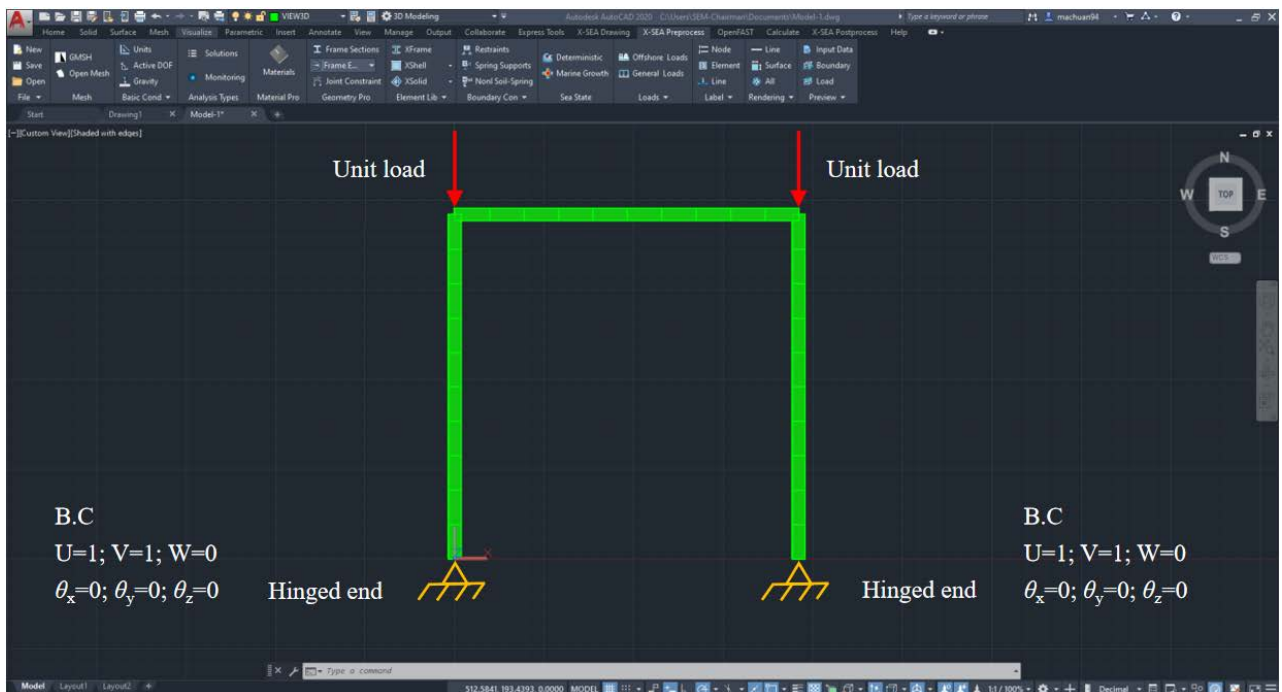
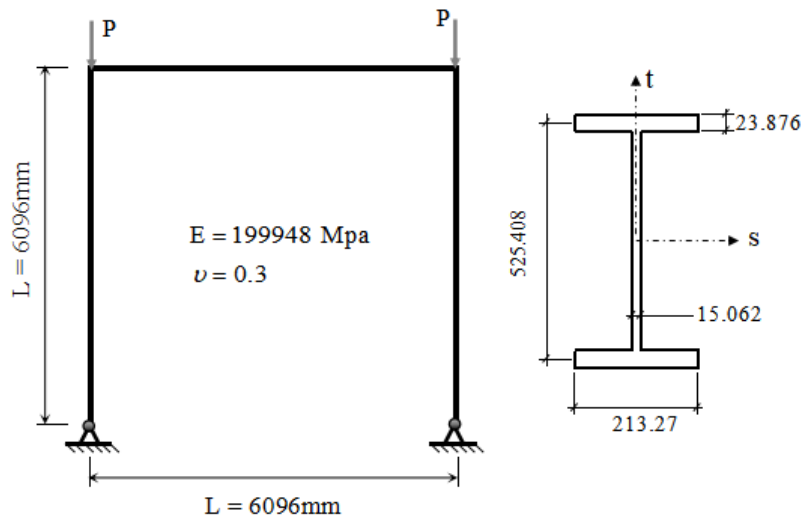


Fig.4.1 Pin-ended portal frame model-Sway permitted (30 Elements, XFrame)

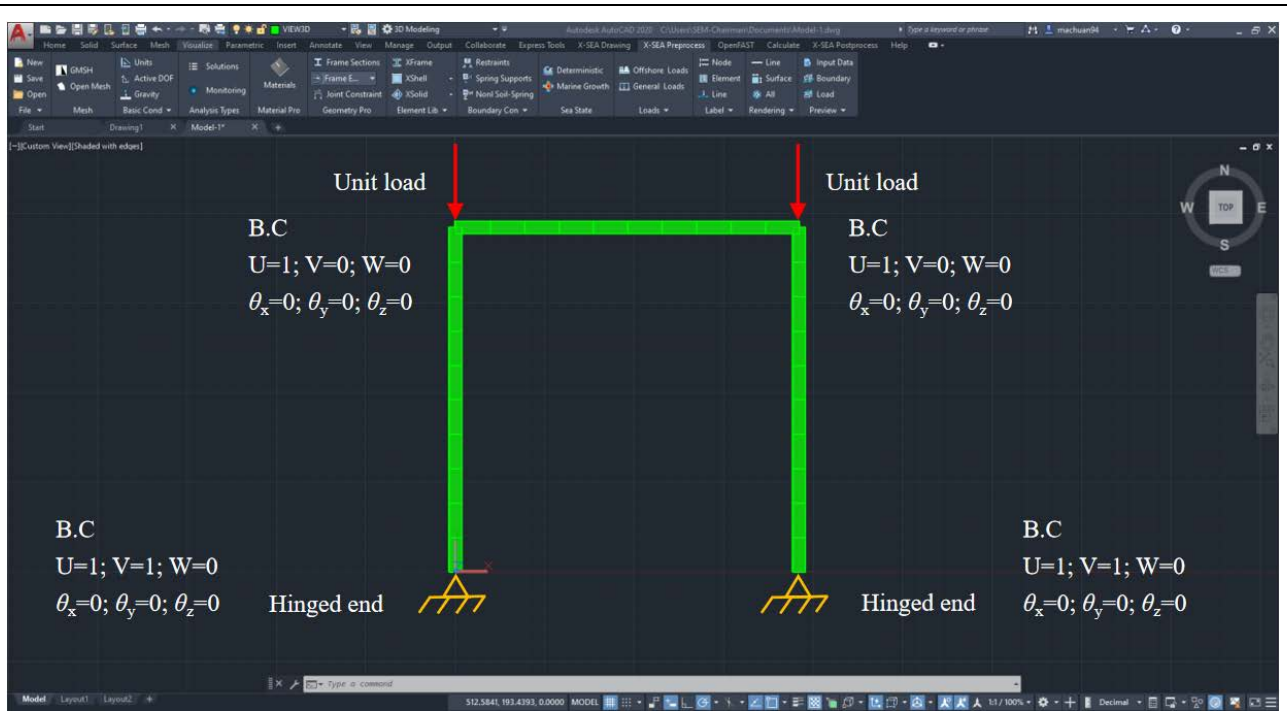
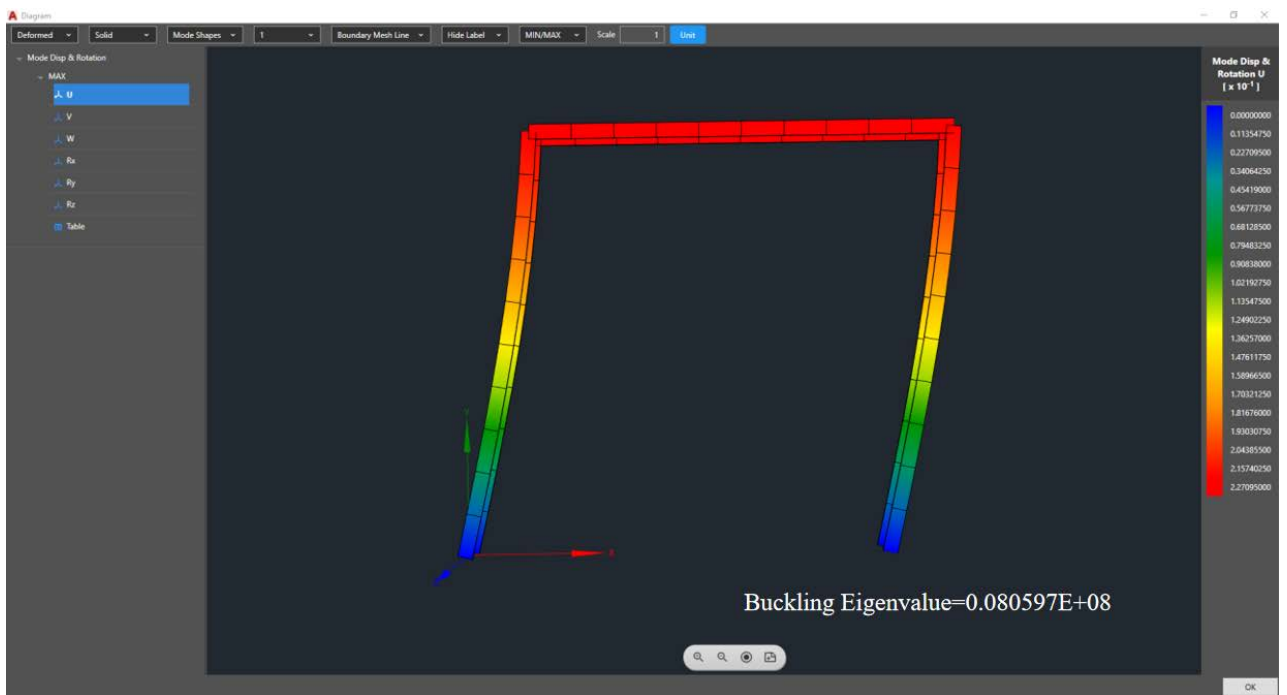


Fig.4.2 Pin-ended portal frame model-Sway prevented (30 Elements, XFrame)

Results

Table 4.1 Comparison of critical loads of pin-ended portal frame ($\times 10^8 \text{N}$)

Case	Analytical solution	XFRAME
Sway-permitted	0.084379	0.080597
Sway-prevented	0.598073	0.542330



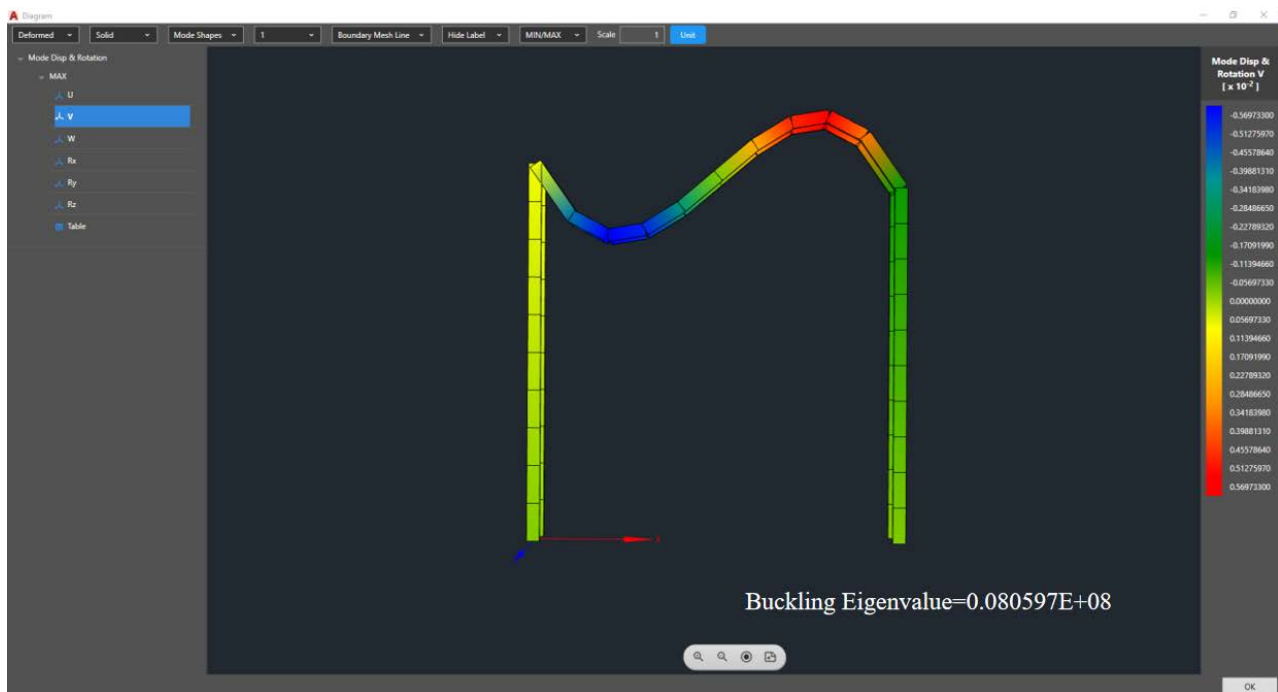
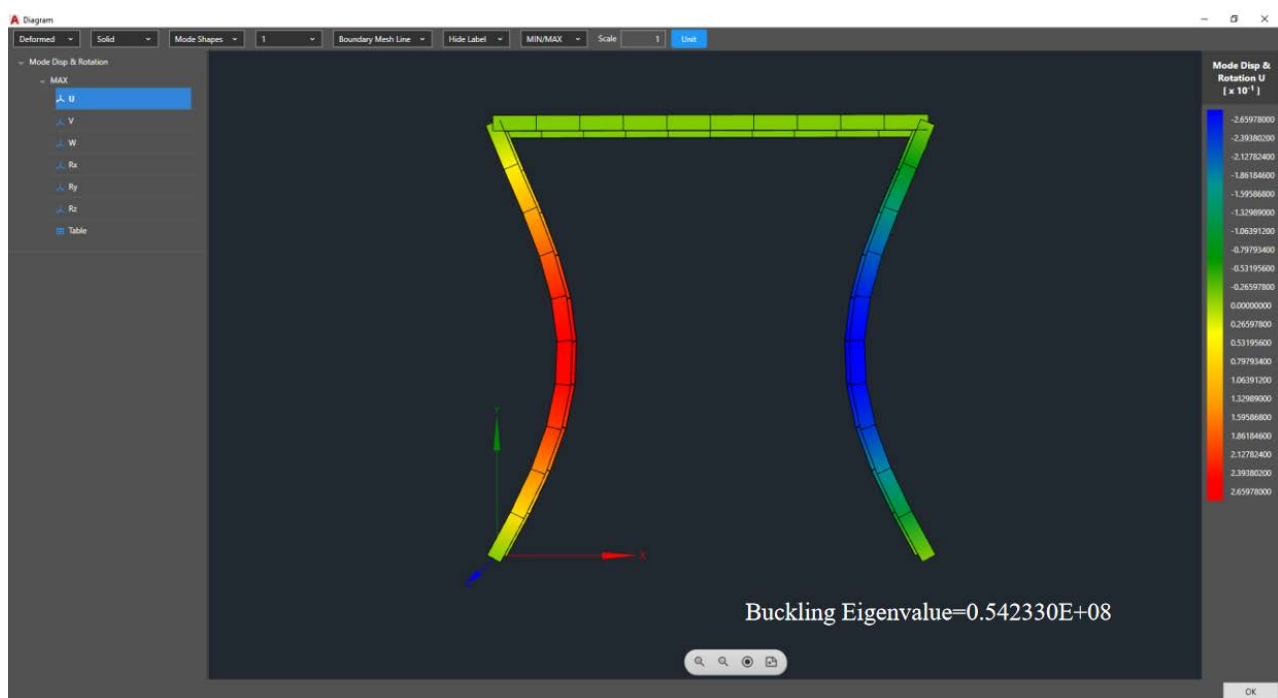


Fig.4.3 Deformation of Pin-ended Portal frame-Sway permitted case (30 Elements, XFrame)



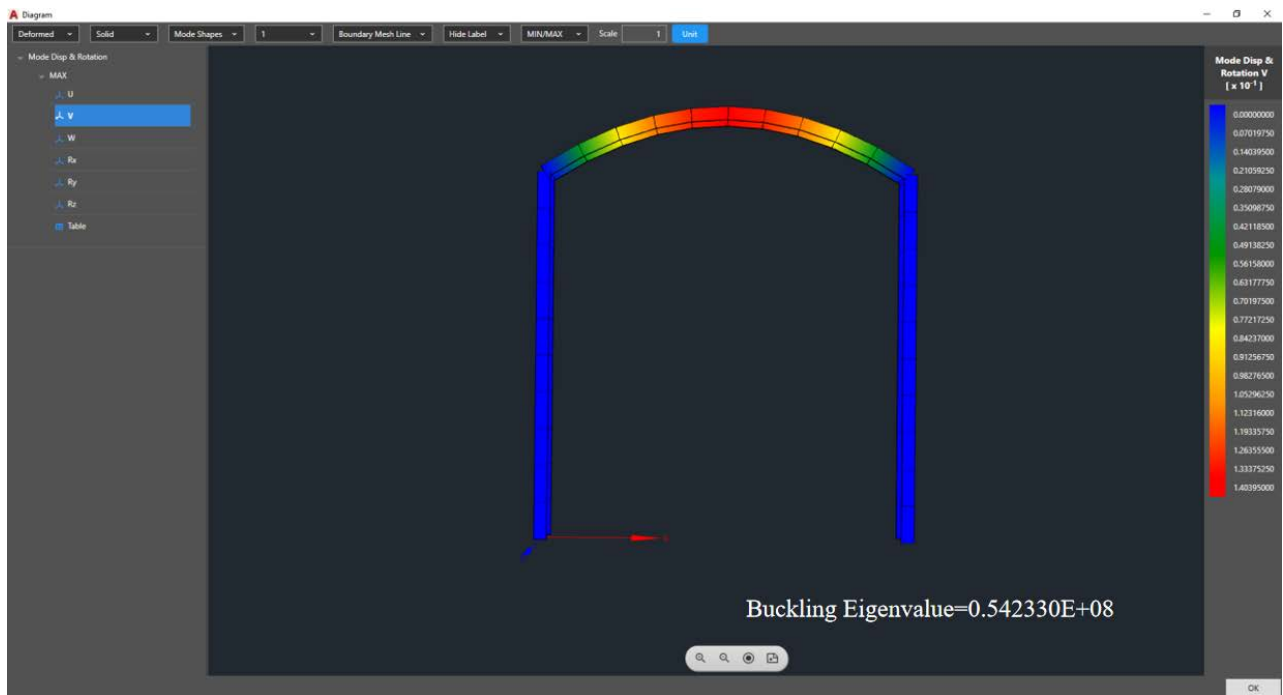


Fig. 4.4 Deformation of pin-ended portal frame-Sway prevented case (30 Elements, XFrame)

Title : Cantilever beam under uniformly distributed load**Problem Description**

The cantilever beam shown in Fig. 5.1 is subjected to uniformly distributed load is modeled using ten beam elements to test for nonlinear analysis. The purpose of this example is to compare the large displacement results of XFRAME with those obtained by NONSAP (Bathe et al., 1974)

Length = 10.0; $h = 1.0$; $b = 1.0$; $E = 1.2 \times 10^4$; $\nu = 0.2$;

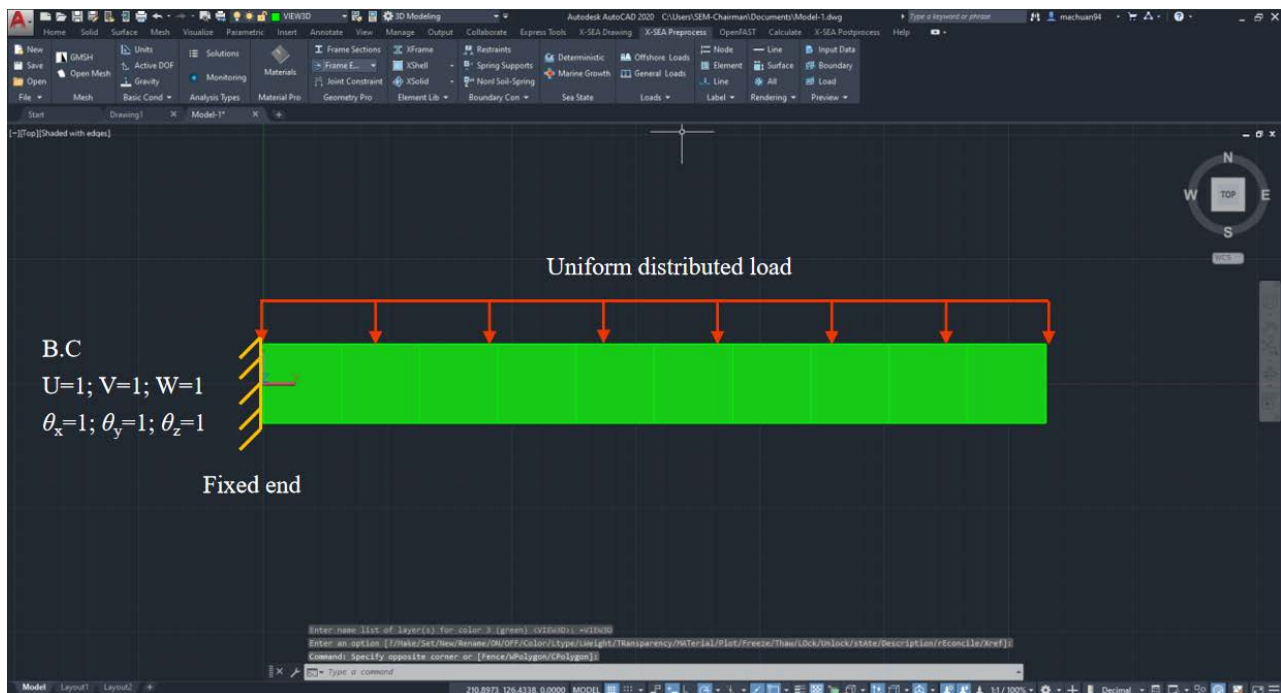
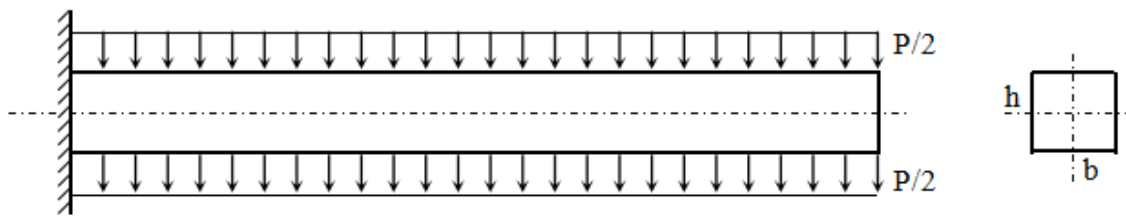


Fig.5.1 Cantilever beam under uniformly distributed load model (10 Elements, XFrame)

Results

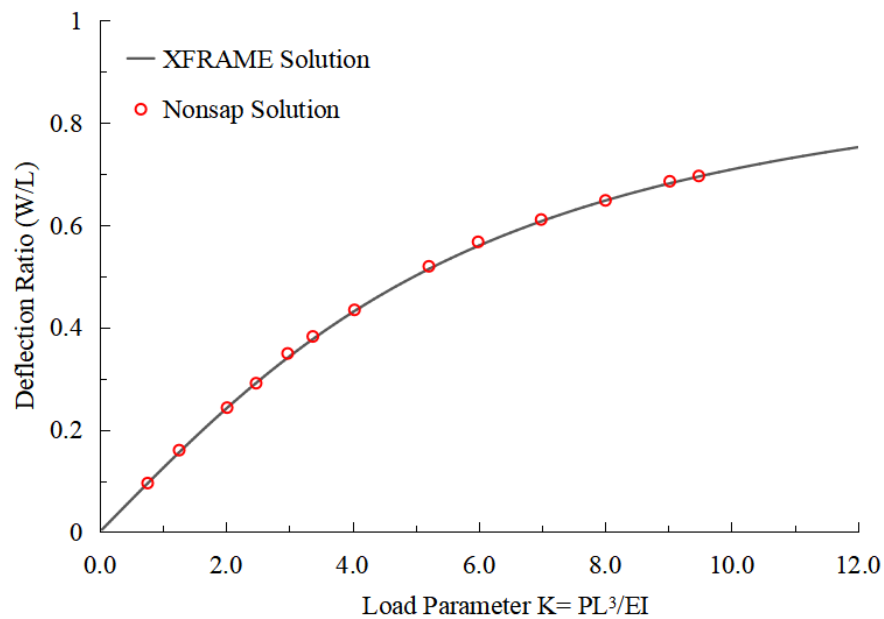


Fig.5.2 Load-displacement relationship of cantilever beam under uniformly distributed load

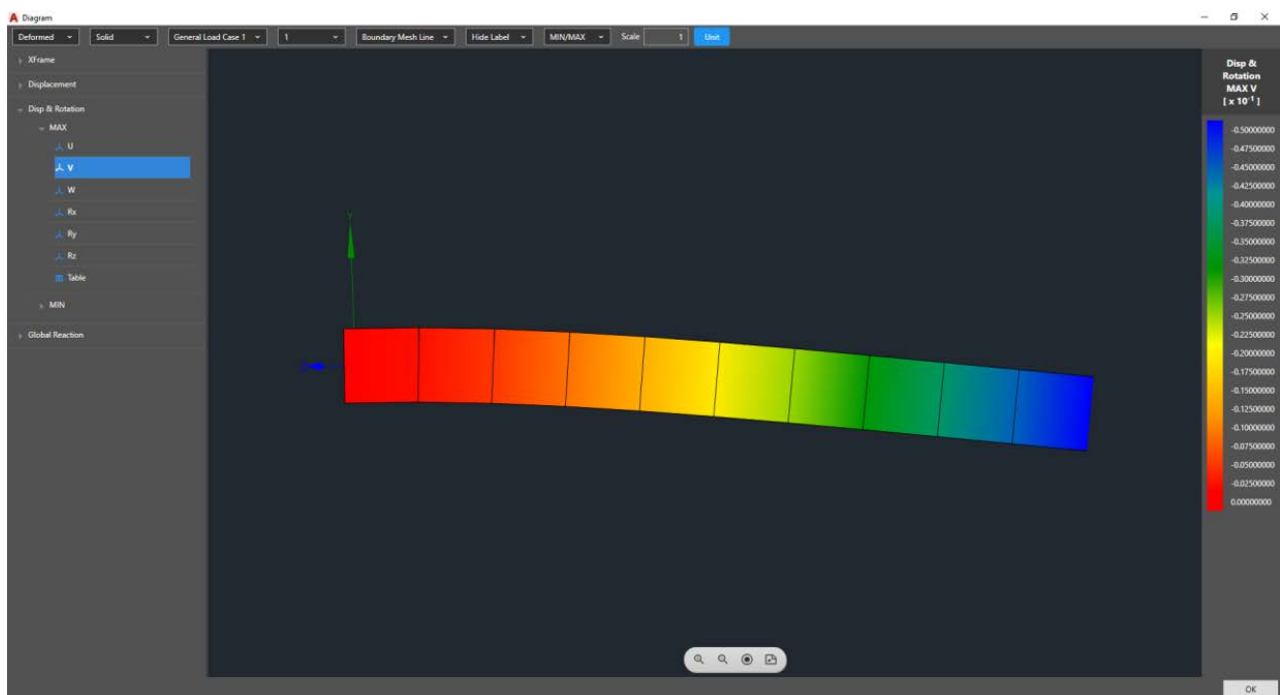


Fig.5.3 Deformation of cantilever beam under uniformly distributed load (10 Elements, XFrame)

Title : Cantilever beam under end load**Problem Description**

In this cantilever analysis subjected to the concentrated tip load, the objective was to demonstrate the effects of aspect ratio in the geometrically nonlinear range for beam and frame analysis.

Length = 100; $h = 0.2$; $b = 12$; $E = 2 \times 10^6$; $\nu = 0.3$;

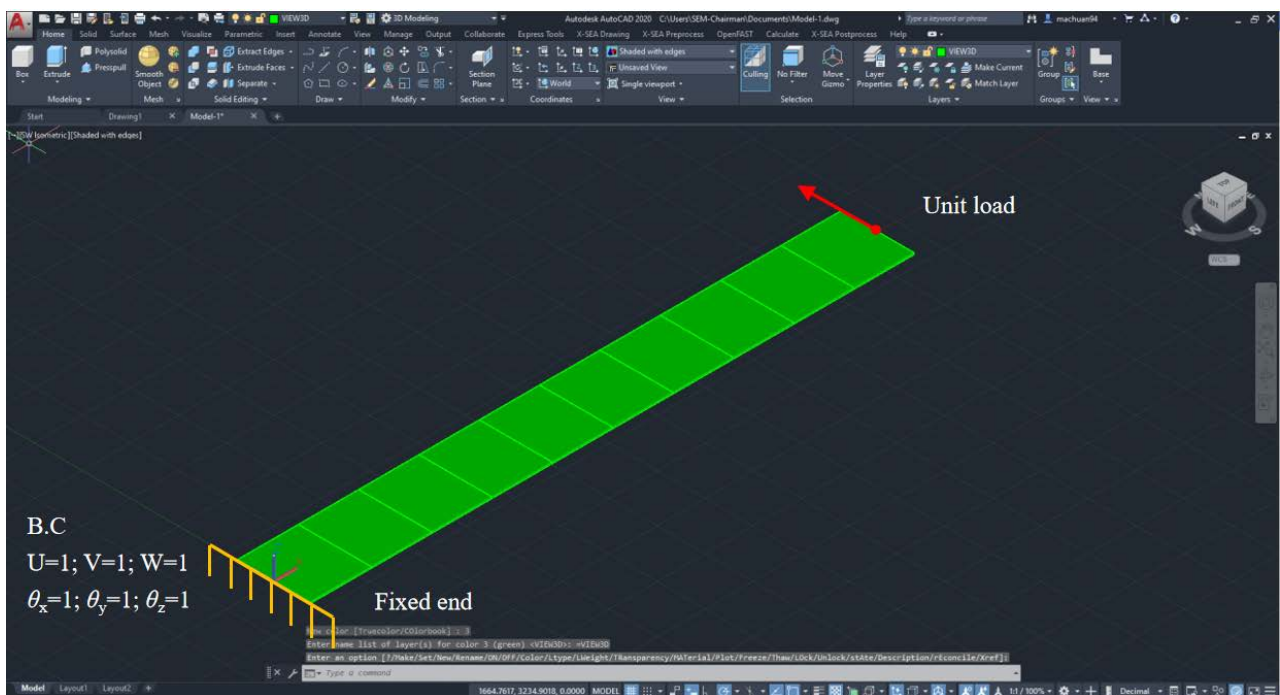
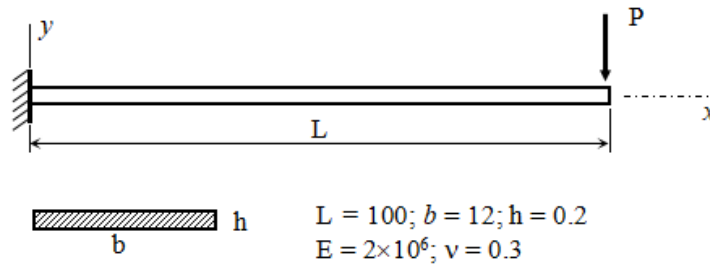


Fig.6.1 Cantilever beam under end load model (10 Elements, XFrame)

Results

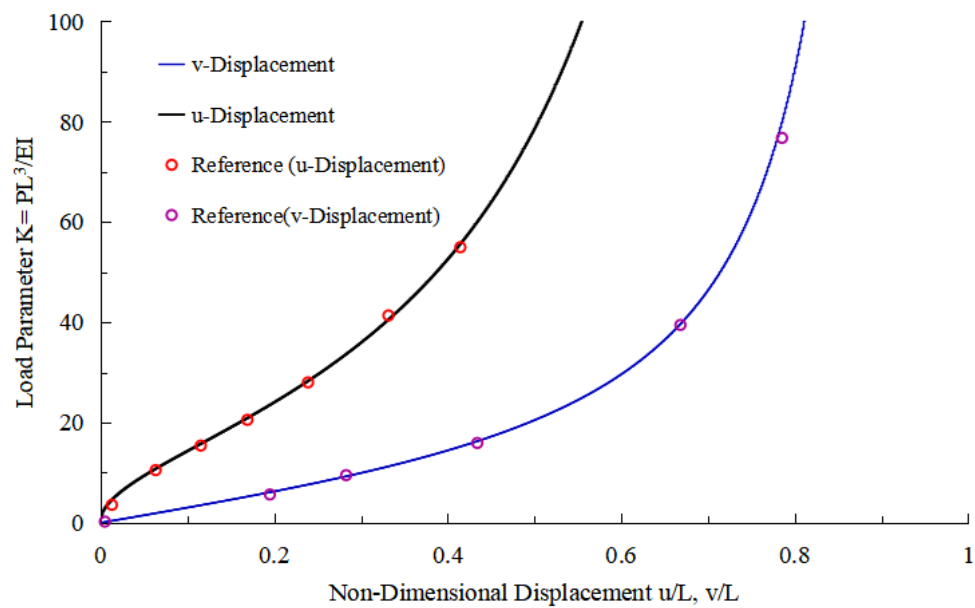


Fig.6.2 Load-displacement relationship of cantilever beam under end load (10 Elements, XFrame)

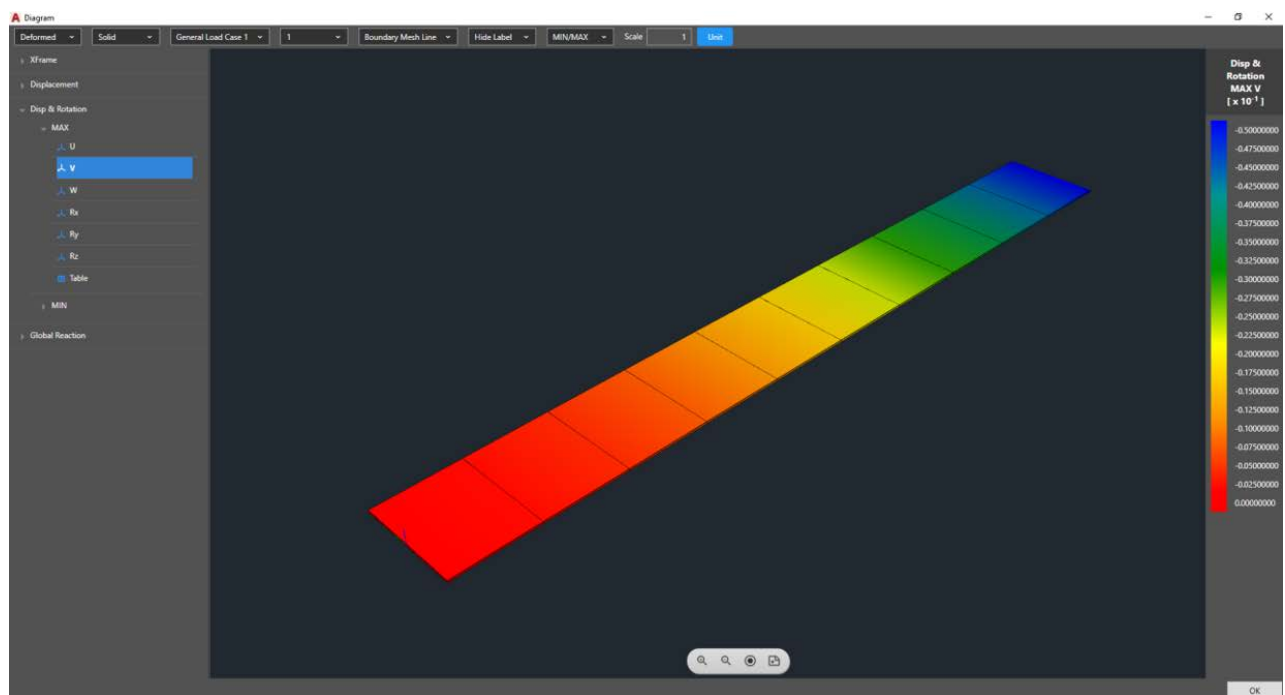


Fig.6.3 Deformation of cantilever beam under end load (10 Elements, XFrame)

Title: Williams toggle frame**Problem Description**

Williams solved the frame problem shown in Fig.7.1 analytically and compared the results with experimental observations. Wood and Zienkiewicz (1977) also idealized this frame using total Lagrangian formulation.

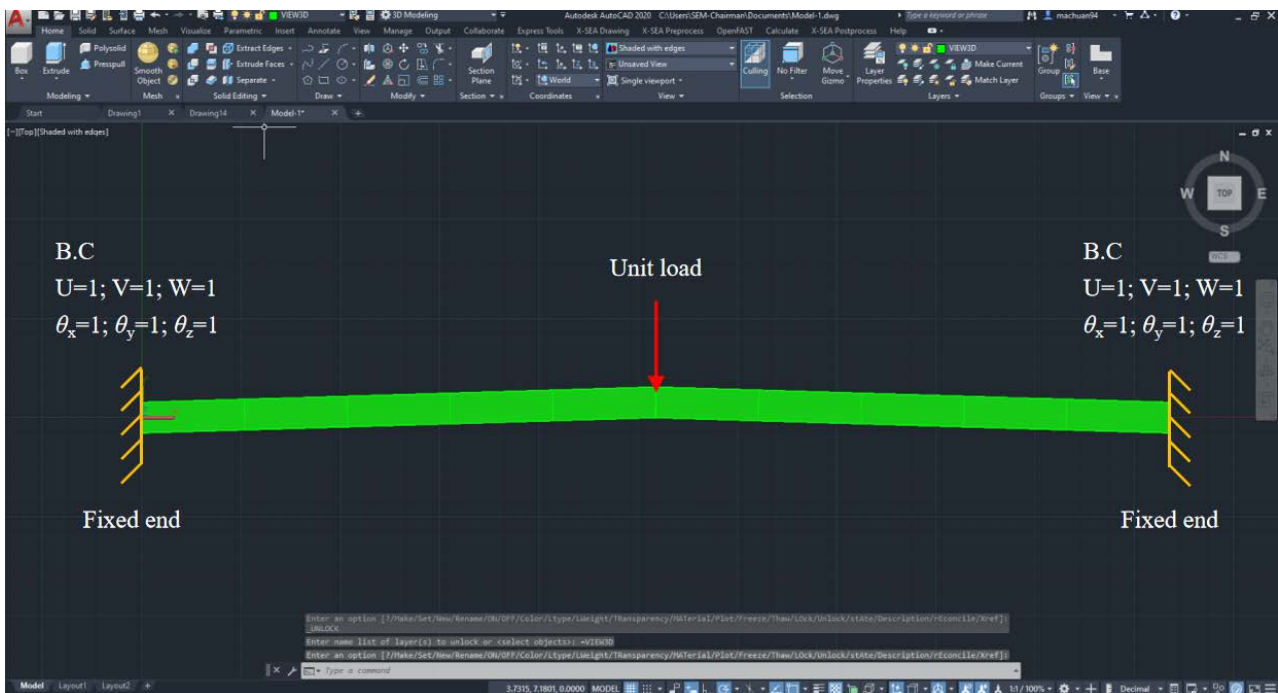
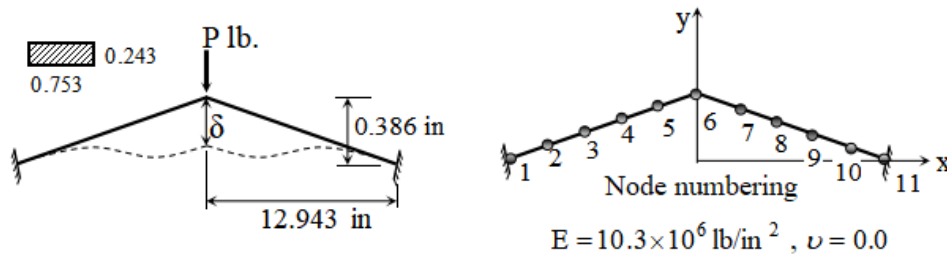


Fig.7.1 Williams Toggle Frame Model (10 Elements, XFrame)

Results

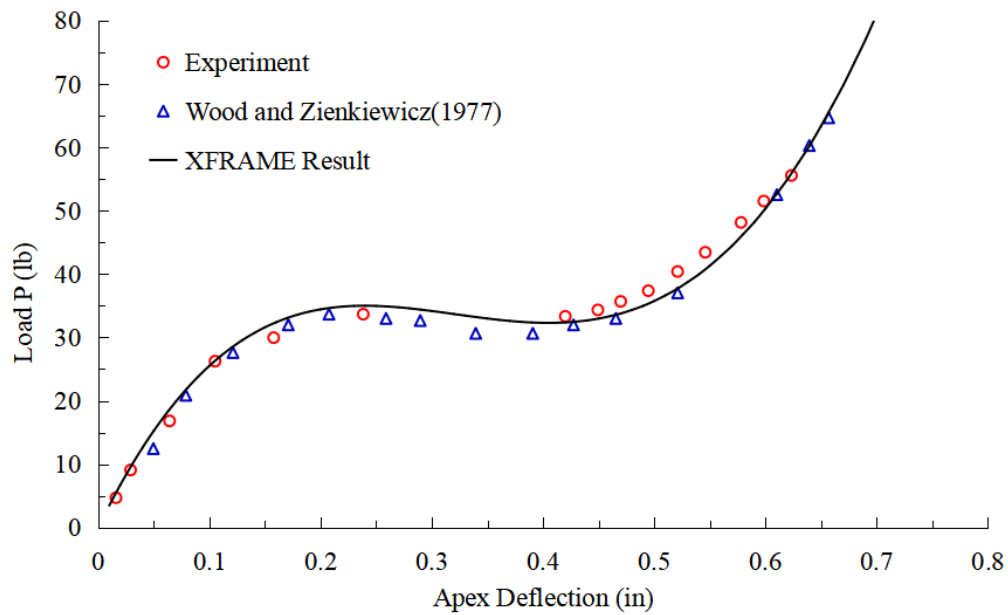


Fig.7.2 Load-Deflection curve of Williams Toggle problem



Fig.7.3 Deformation of Williams Toggle frame (10 Elements, XFrame)

Title: Lee's elastic frame**Problem Description**

Lee's frame along with its geometrical and material properties is shown in Fig.8.1. The frame was modeled with twenty elements. For the loaded node two equilibrium paths are plotted, showing the relationship between load P and vertical and horizontal displacements.

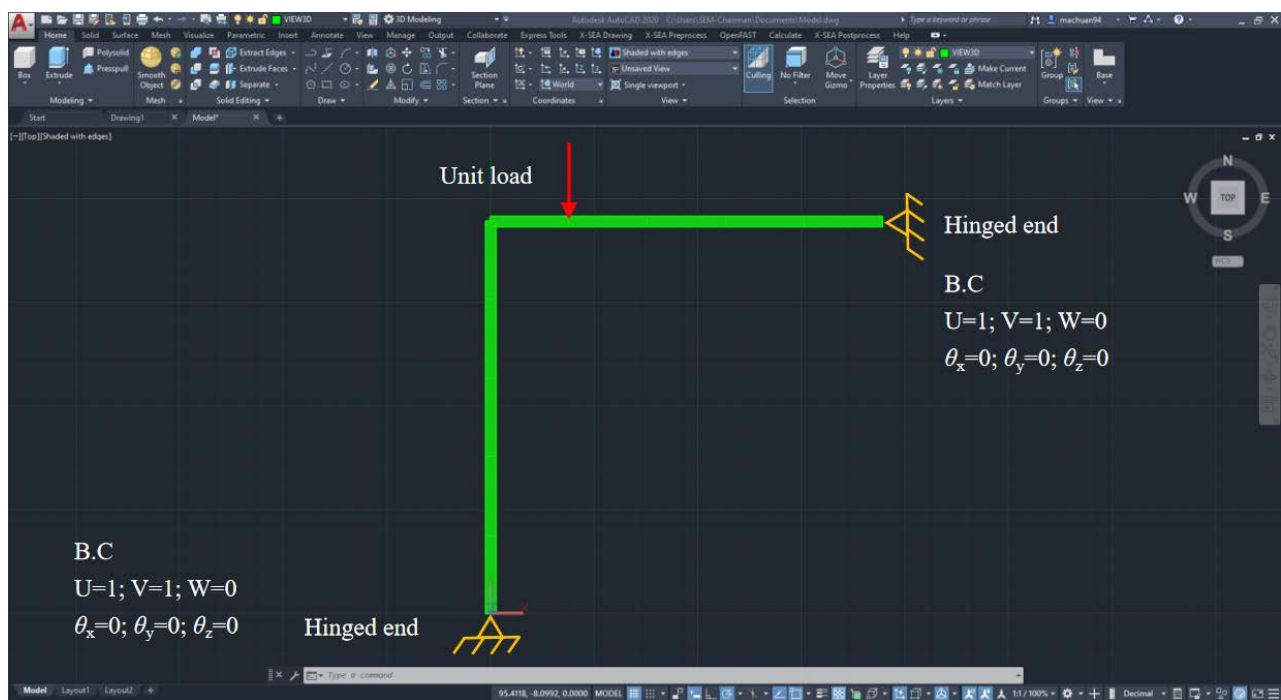
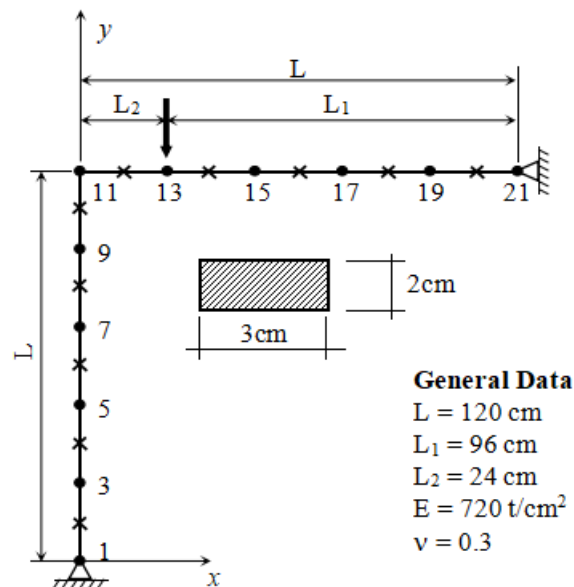


Fig.8.1 Lee's elastic frame model (10 Elements, XFrame)

Results

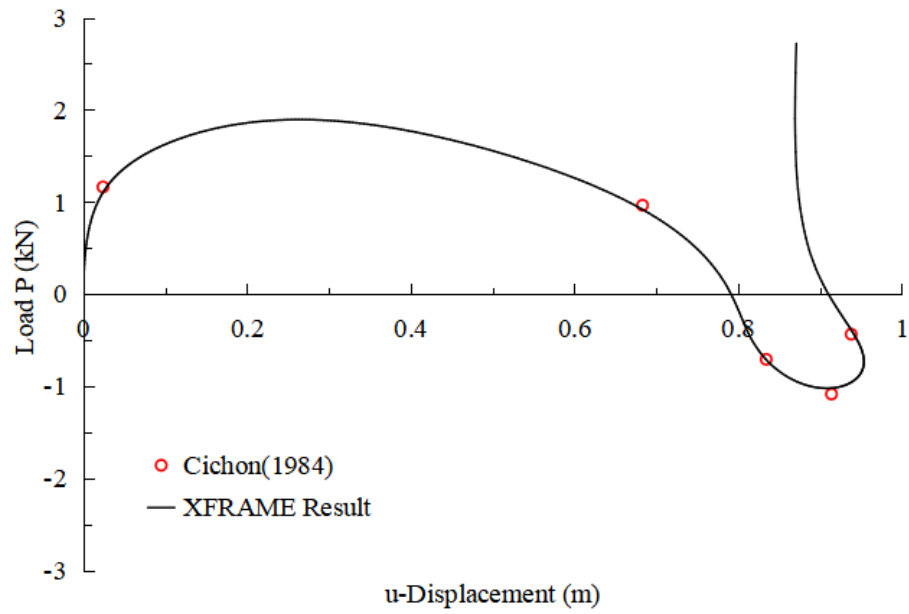


Fig.8.2 Nonlinear load and X-displacement relationship of Lee's frame

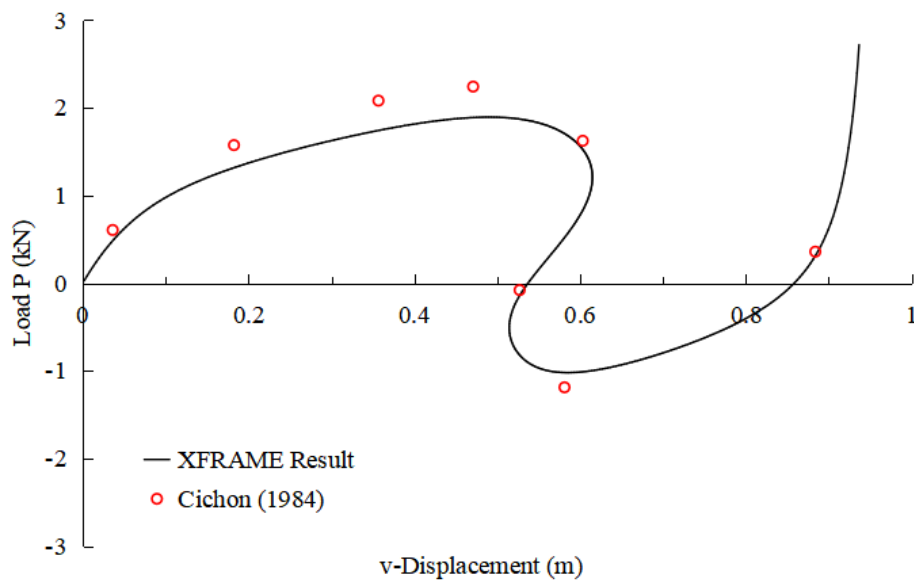


Fig.8.3 Nonlinear load and Y-displacement relationship of Lee's frame

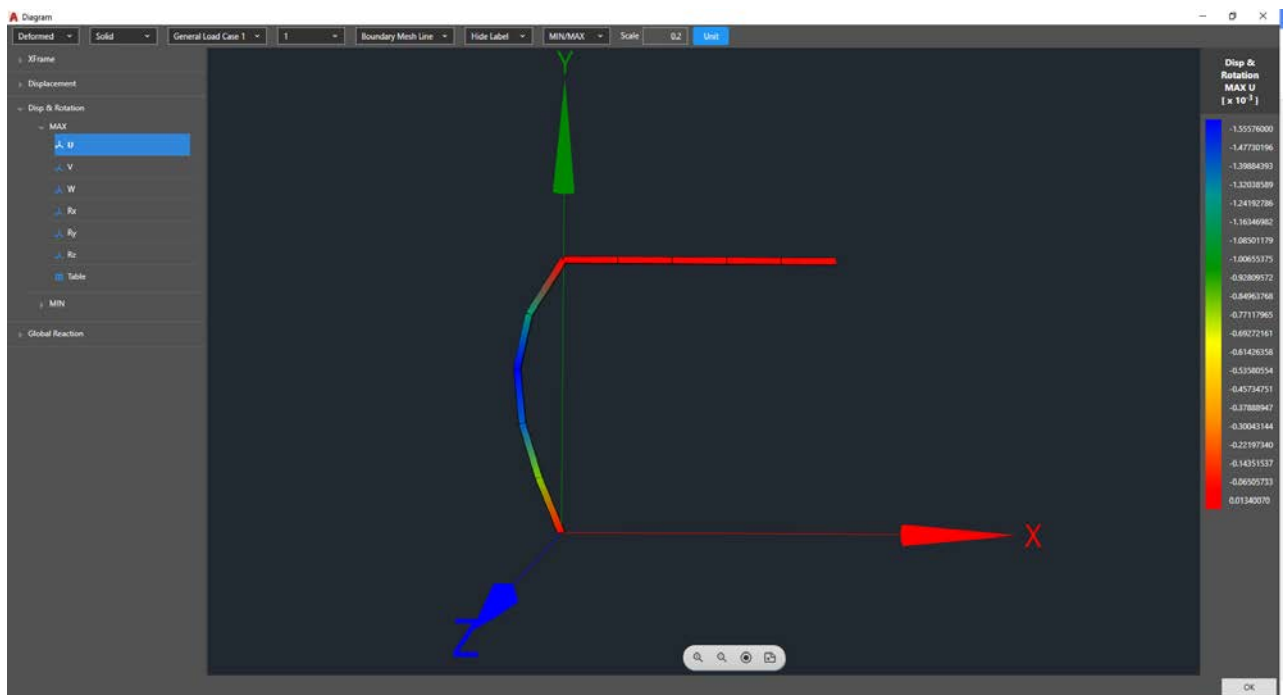


Fig.8.4 Vertical deformation of Lee's elastic frame model result (10 Elements, XFrame)

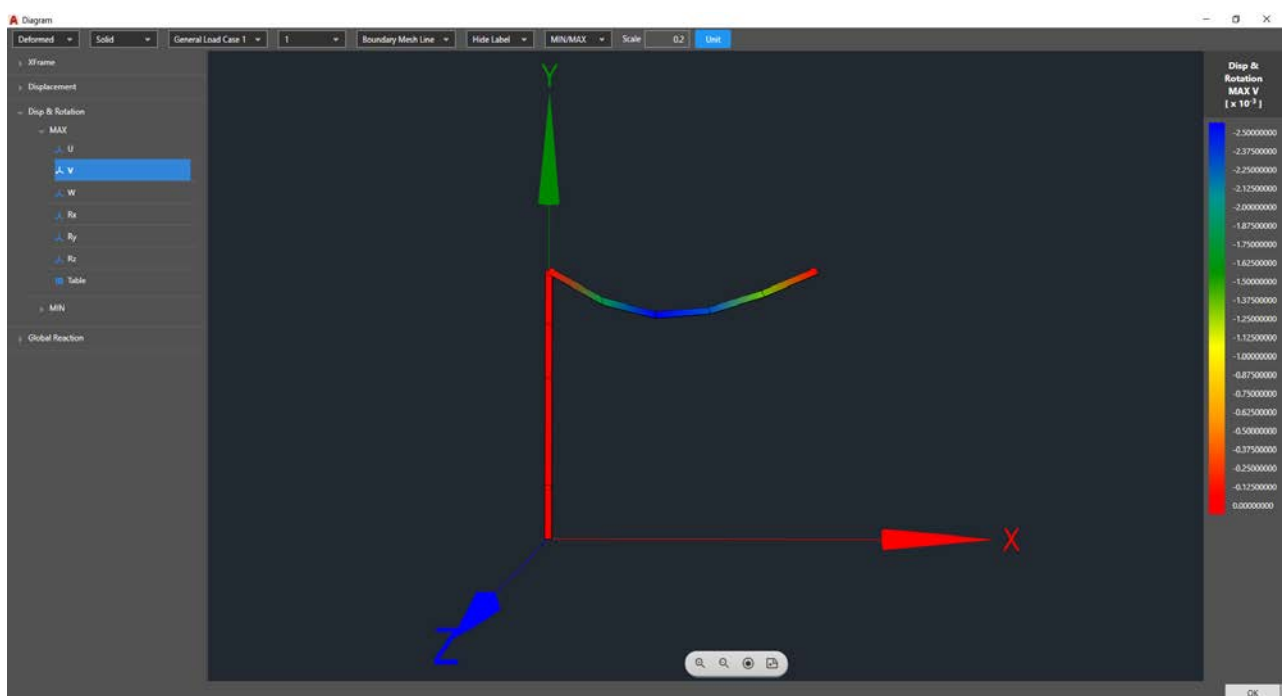
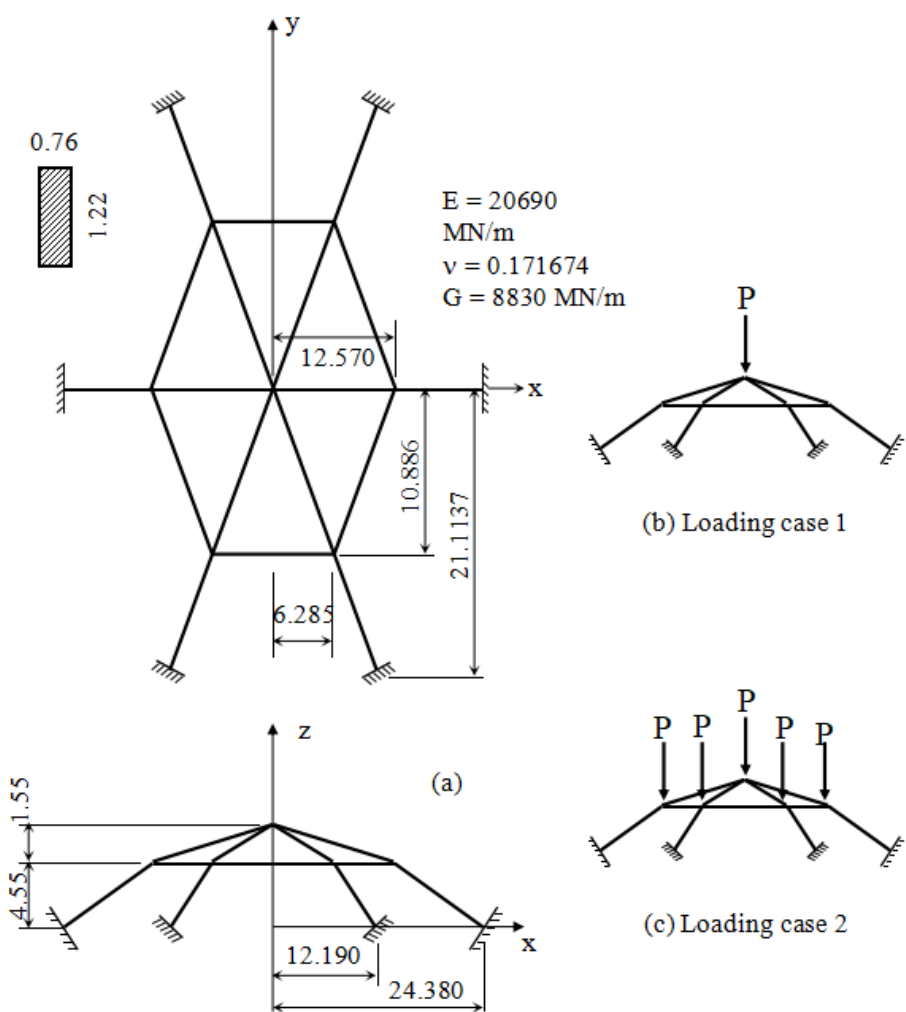


Fig.8.5 Horizontal deformation of Lee's elastic frame model result (10 Elements, XFrame)

Title: Static instability analysis of Framed Dome

Problem Description

The framed dome problem illustrates the nonlinear static analysis of space frames under two different loading conditions. The first loading case considered is that of a single concentrated load at the crown point. The loading second system consists of concentrated vertical loads of equal magnitude P at the crown point and also at the end points of the horizontal members.



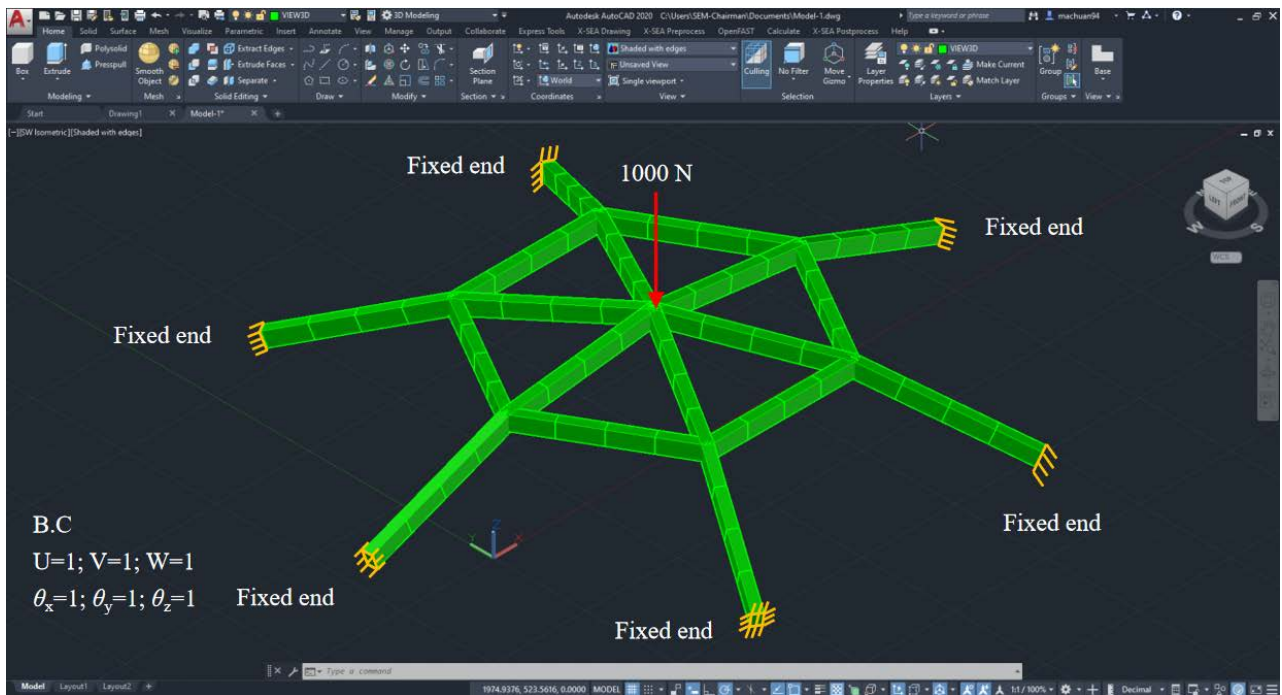


Fig.9.1 Framed dome model under load case 1 (72 Elements, XFrame)

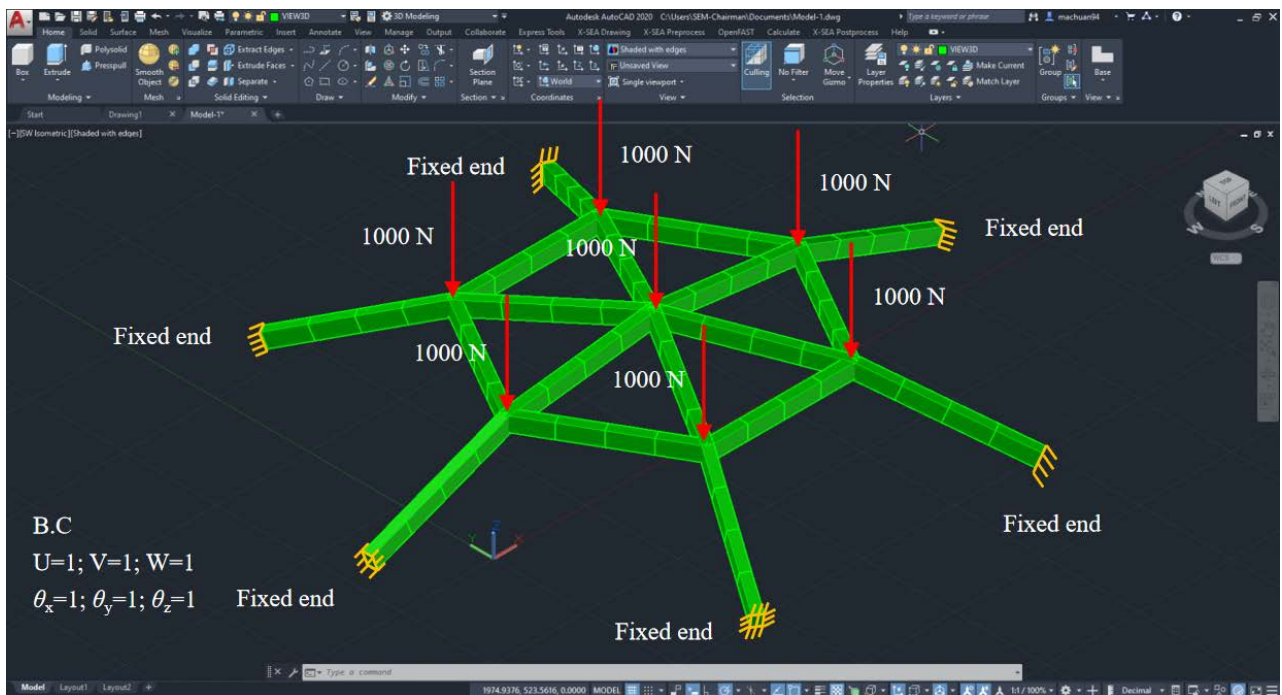


Fig. 9.2 Framed dome model under load case 2 (72 Elements, XFrame)

Results

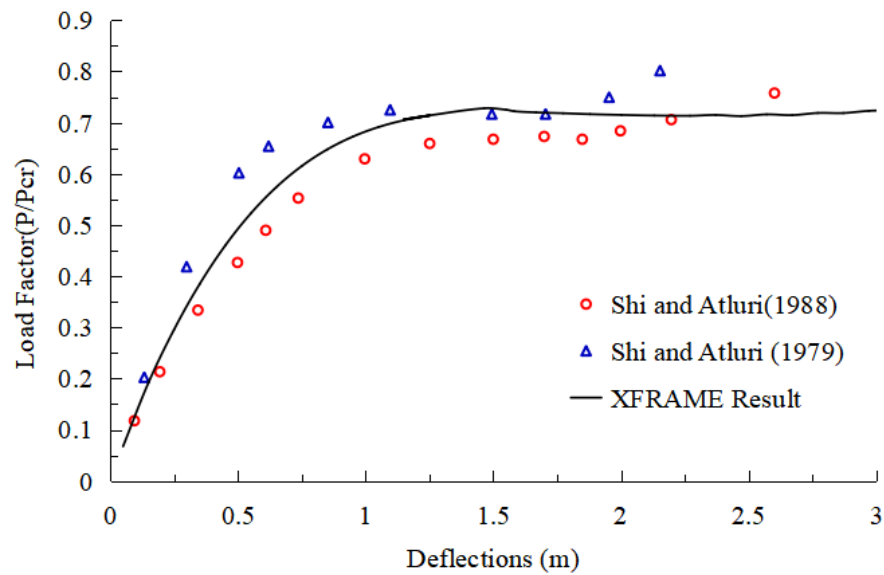


Fig.9.3 Load-Deflection curves for vertical displacement under load case 1

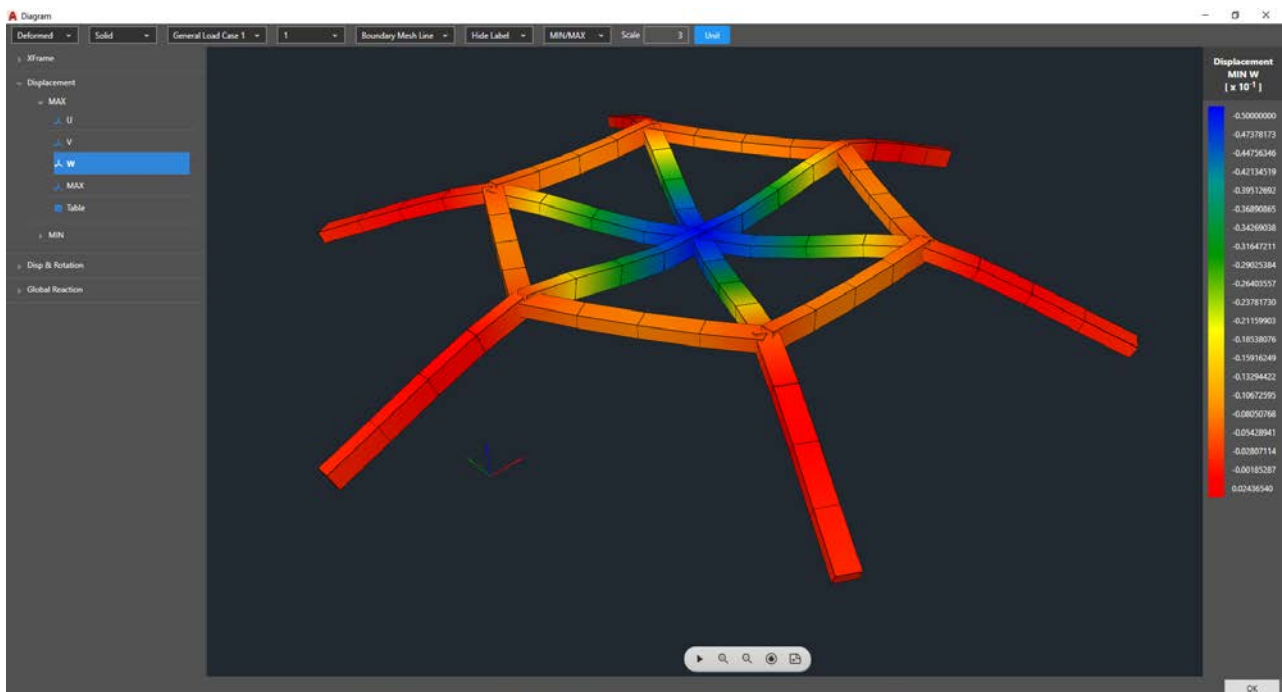


Fig.9.4 Deformation of framed dome model under load case 1 (72 Elements, XFrame)

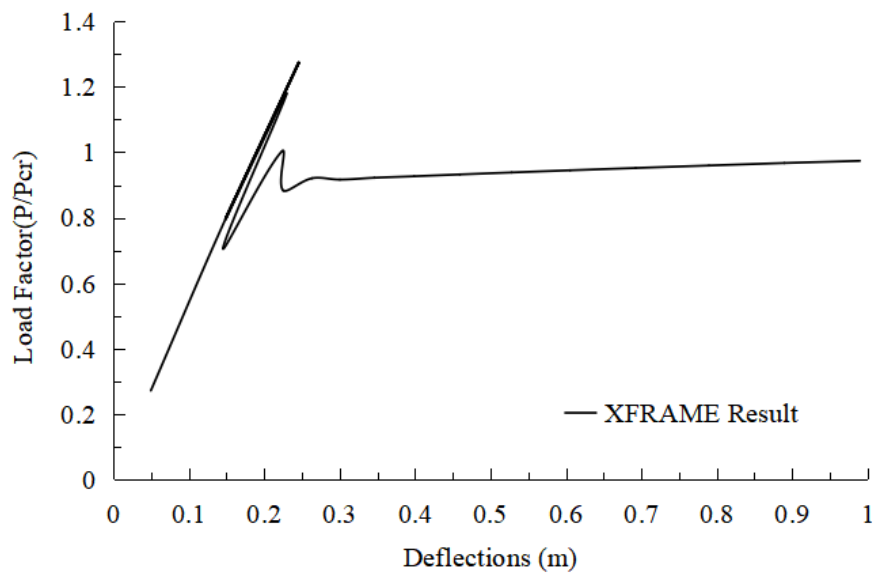


Fig.9.5 Load-Deflection curves for vertical displacement under load case 2

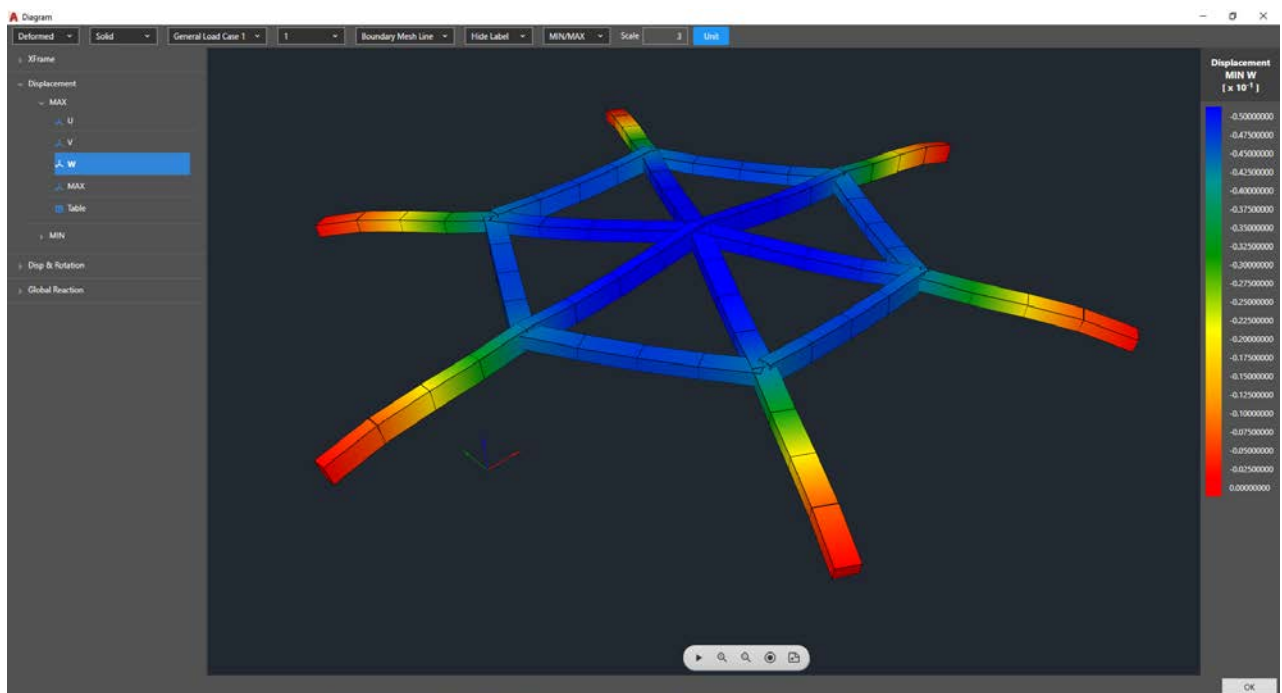


Fig.9.6 Deformation of framed dome model under load case 2 (72 Elements, XFrame)

Title: Lee's elasto-plastic frame**Problem Description**

The final example deals with the elasto-plastic behavior of Lee's frame subjected to point load at node 1SHELL ELEMENT15 Dr. KiDu Kim³. This problem was previously analyzed by Park and Lee (1996). The geometrical and material data for the members, which are identical, is given in Fig. 10.1.

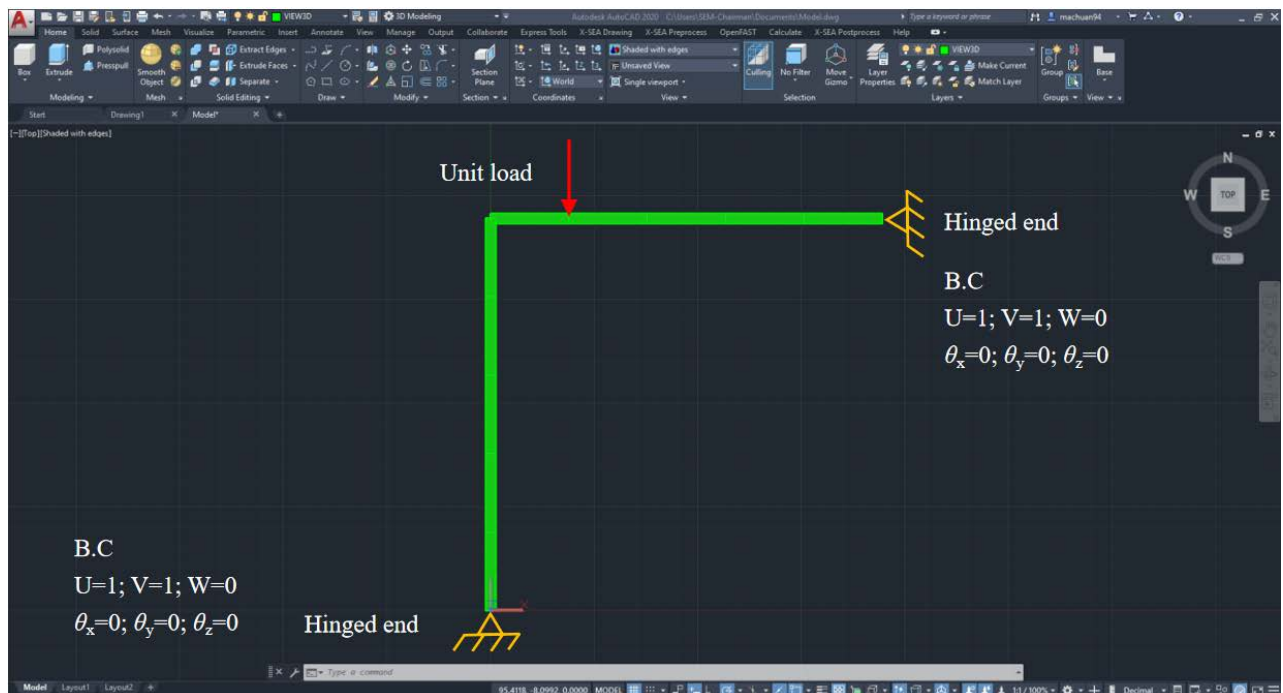
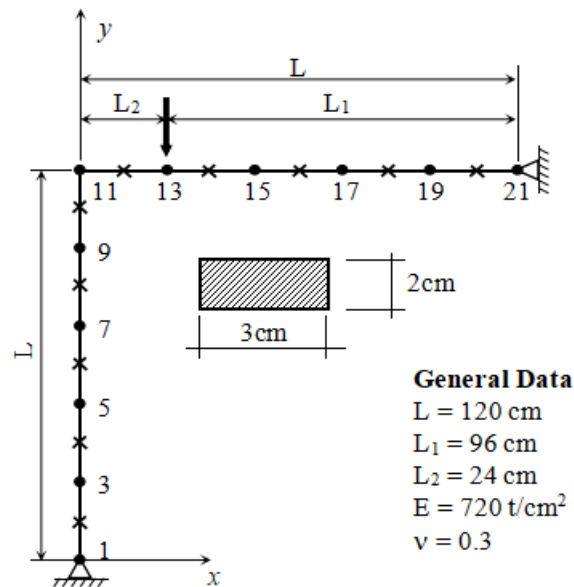


Fig.10.1 Lee's elastic frame model (10 Elements, XFrame)

Results

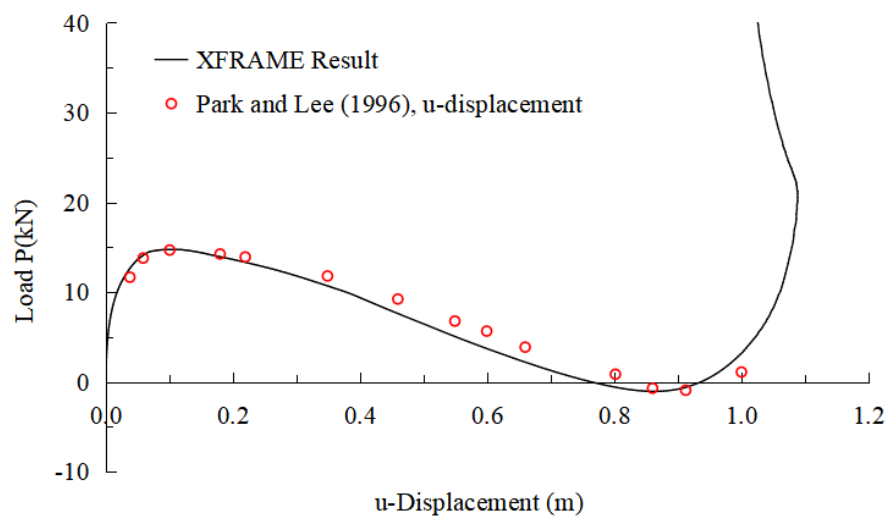


Fig. 10.2 Nonlinear load and X-displacement relationship of Lee's elasto-plastic frame

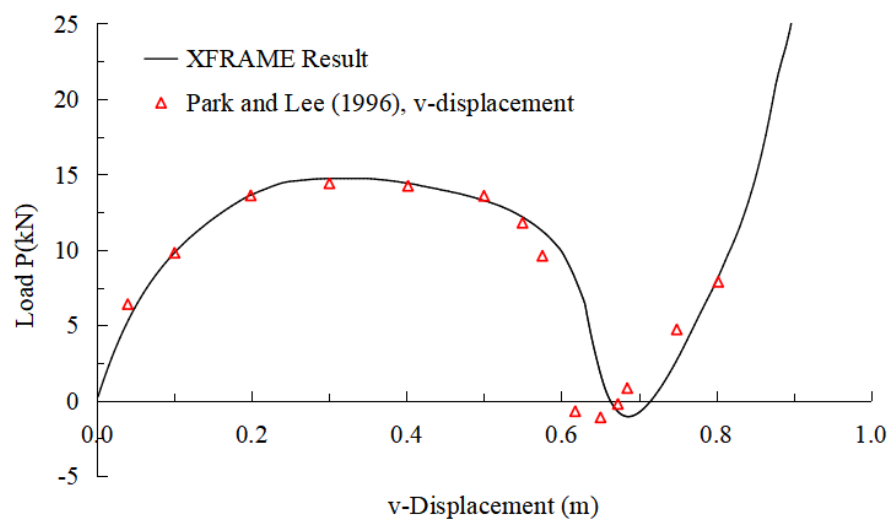


Fig. 10.3 Nonlinear load and Y-displacement relationship of Lee's elasto-plastic frame

Title: Frame Element Numerical Examples-1

Problem Description

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

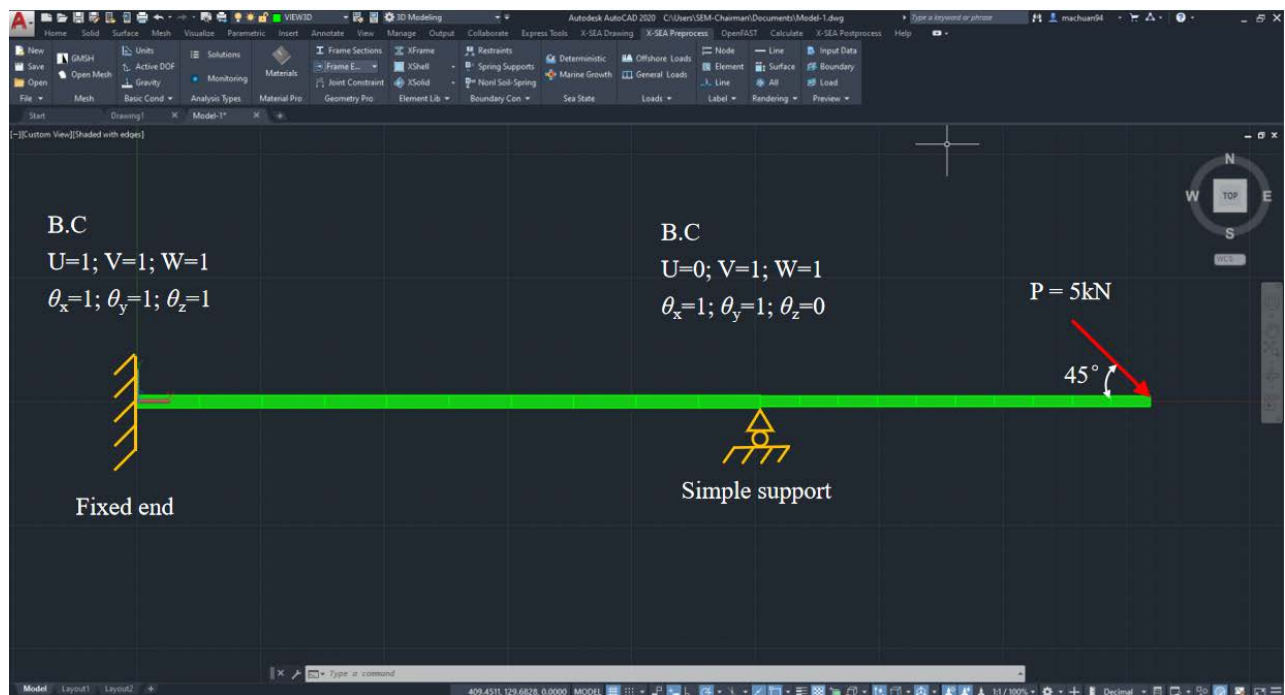
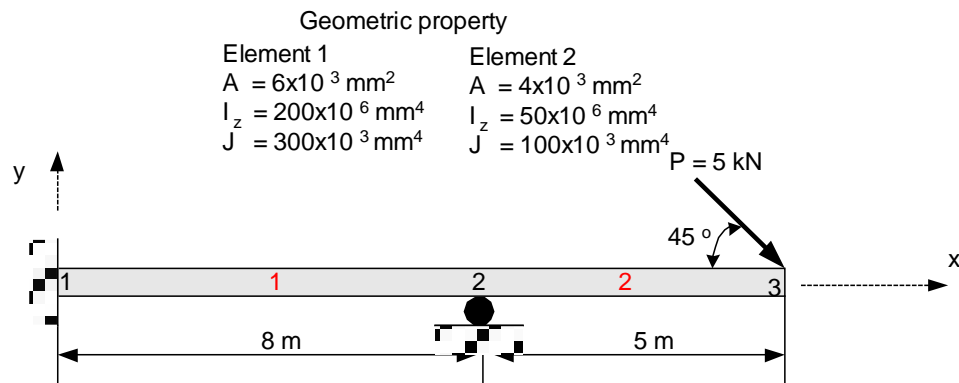


Fig.11.1 Frame model-1 (20 Elements, XFrame)

Results



Fig.11.2 Displacement of beam in y direction (20 Elements, XFrame)

Table 11.1 Displacement at node 2 and 3

Element type	Node 2		Node 3		
	U (mm)	R _z (rad)	U (mm)	V (mm)	R _z (rad)

Reference	0.24E-01	-0.88E-03	0.46E-01	-0.1915E+02	-0.53E-02
XSEA	0.2358E-01	-0.8841E-03	0.4568E-01	-0.1916E+02	-0.5304E-02

Table 11.2 Reaction at node 1

Element type	F_x (N)	F_y (N)	M_z (N·mm)
Reference	-0.36E+04	-0.33E+04	-0.88E+07
XSEA	-0.3536E+04	-0.3315E+04	-0.8839E+07

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Verification Example of X-SEA AutoCAD

No: Frame Element 012

Title: Frame Element Numerical Examples-2

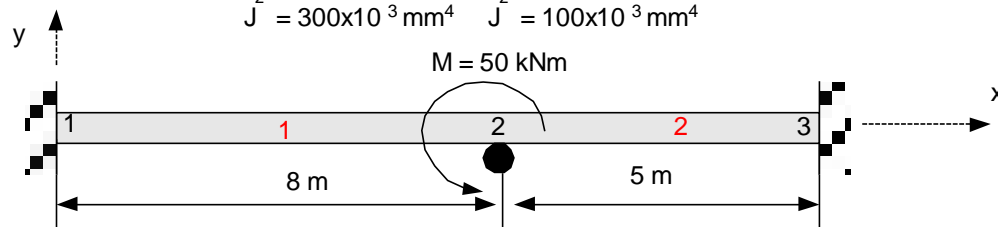
Problem Description

Beam is supported and loaded as follows.

E=199.96GPa; v=0.03.

Geometric property

Element 1	Element 2
A = 6x10 ³ mm ²	A = 4x10 ³ mm ²
I _z = 200x10 ⁶ mm ⁴	I _z = 50x10 ⁶ mm ⁴
J = 300x10 ³ mm ⁴	J = 100x10 ³ mm ⁴



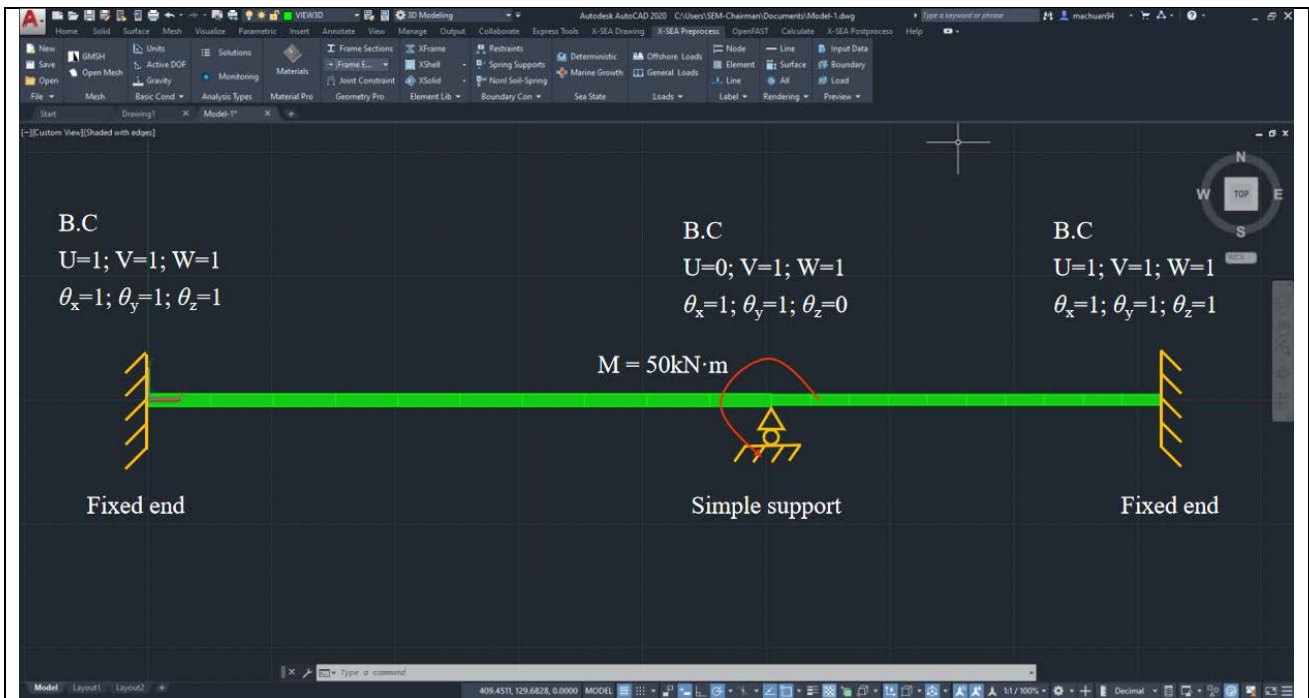


Fig.12.1 Frame model-2 (20 Elements, XFrame)

Results

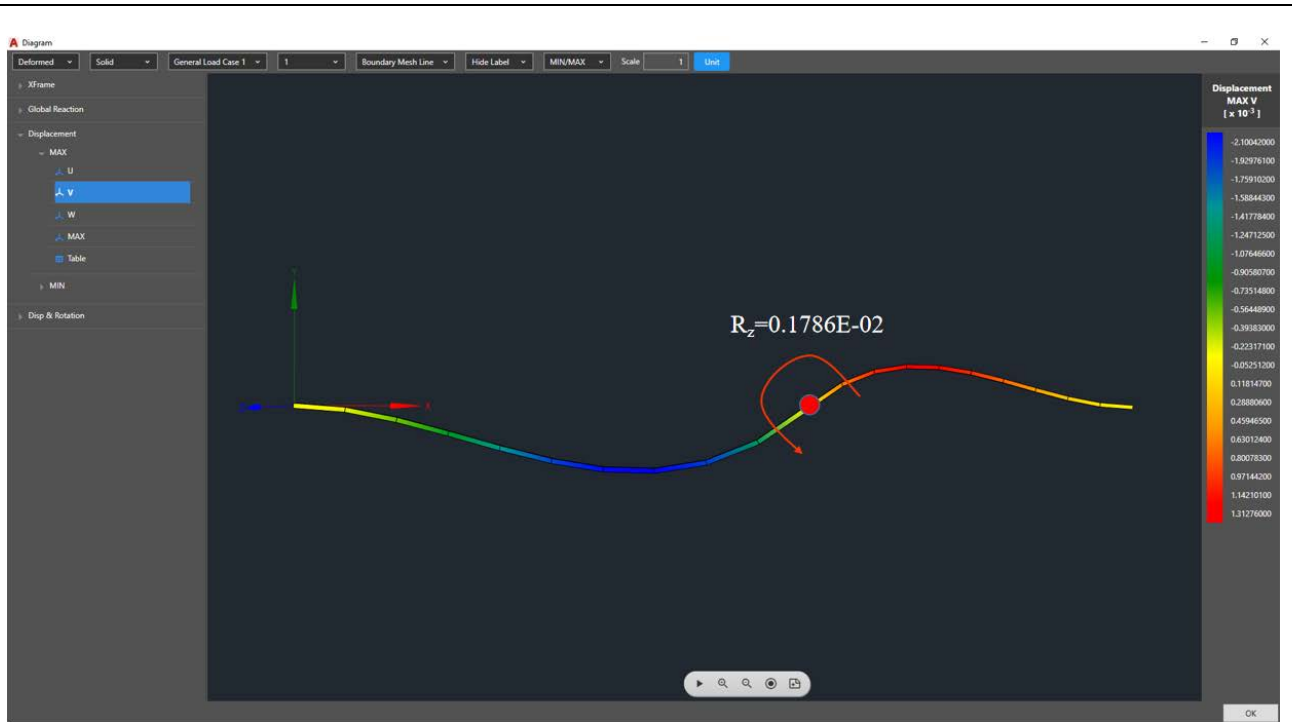


Fig.12.2 Displacement of beam in y direction (20 Elements, XFrame)

Table 12.1 Displacement at node 2

Element type	R_z (rad)
Reference	0.1786E-02
XSEA	0.1786E-02

Table 12.2 Reaction at node 1

Element type	Node 1		Node 3	
	F_y (N)	M_z (N·mm)	F_y (N)	M_z (N·mm)
Reference	0.67E+04	0.1786E+08	-0.429E+04	0.714E+07
XSEA	0.6696E+04	0.1786E+08	-0.4286E+04	0.7143E+07

Title: Frame Element Numerical Examples-3

Problem Description

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

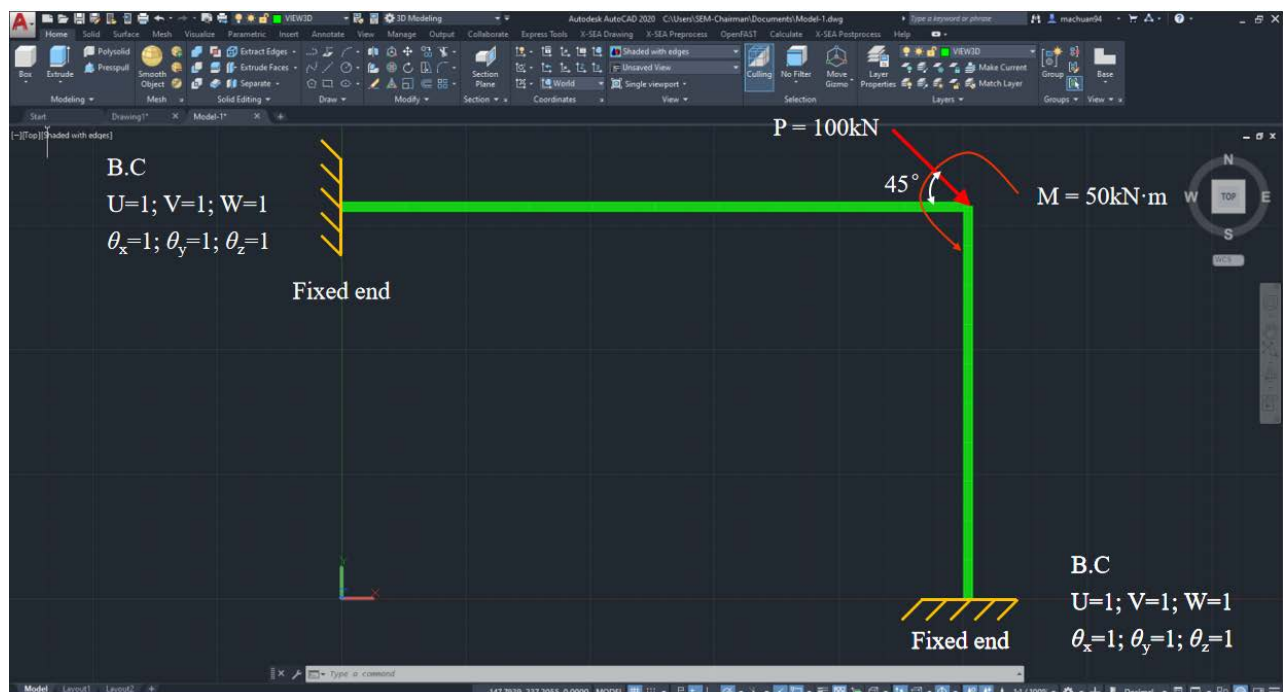
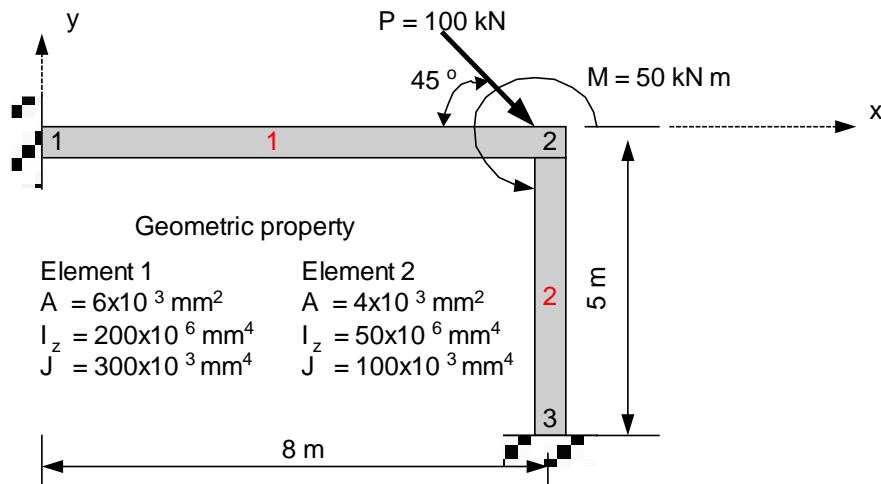


Fig.13.1 Frame model-3 (20 Elements, XFrame)

Results

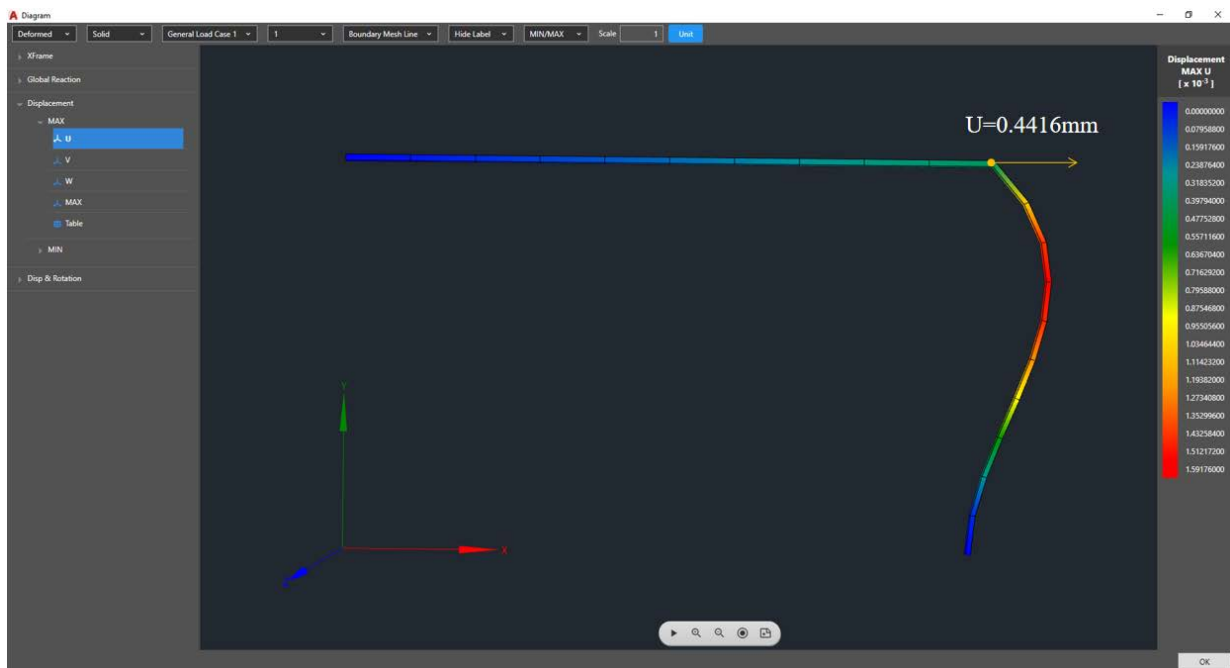


Fig.13.2 Displacement of beam in X direction (20 Elements, XFrame)

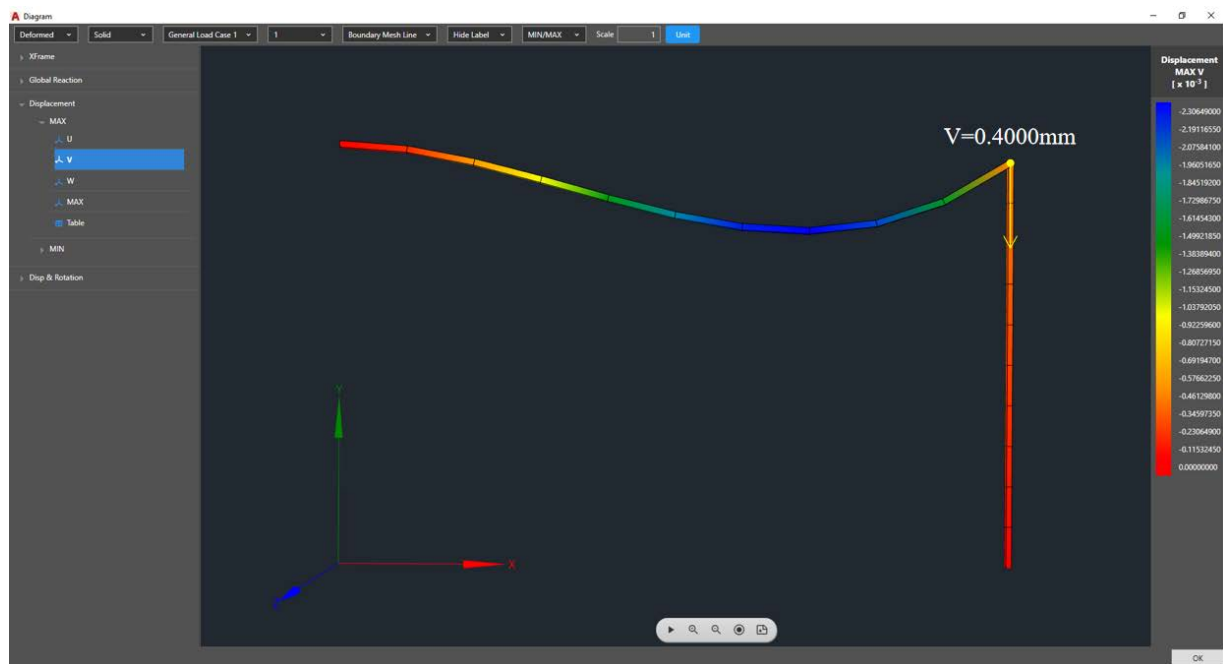


Fig.13.3 Displacement of beam in Y direction (20 Elements, XFrame)

Table 13.1 Displacement at node 2

Element type	U (mm)	V (mm)	R _z (rad)
Reference	0.4414	-0.3998	0.1690E-02
XSEA	0.4416	-0.4000	0.1695E-02

Title: Frame Element Numerical Examples-4

Problem Description

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

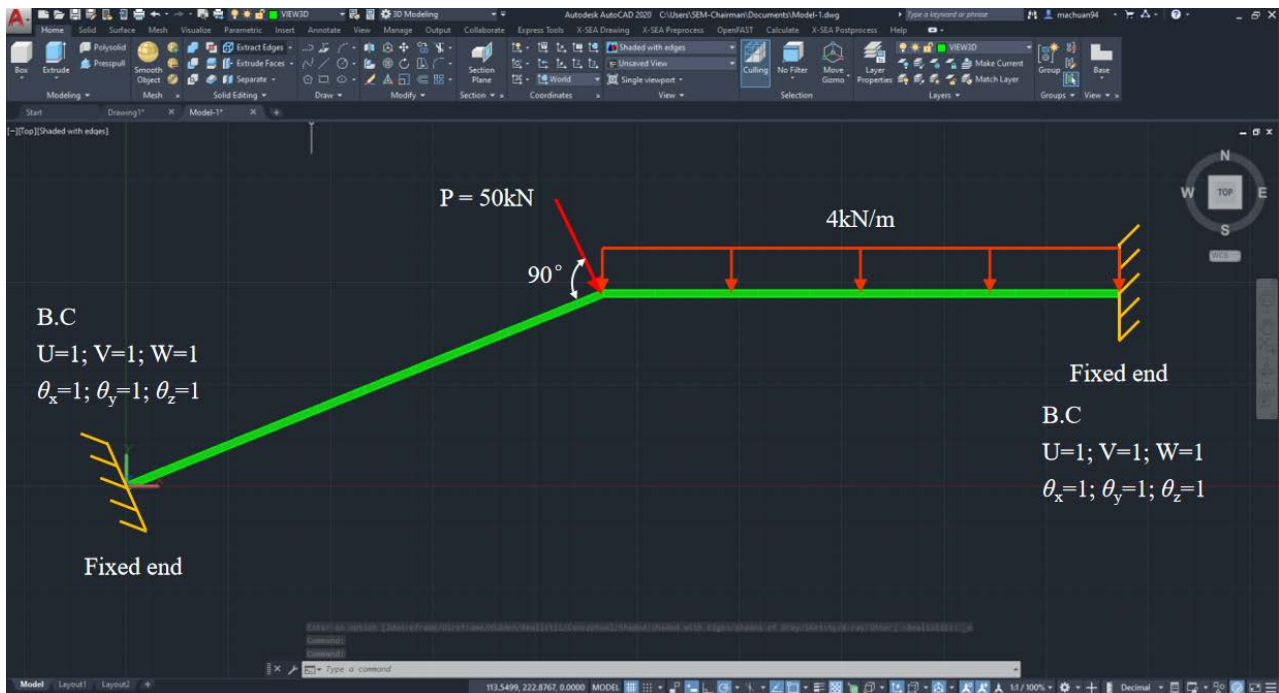
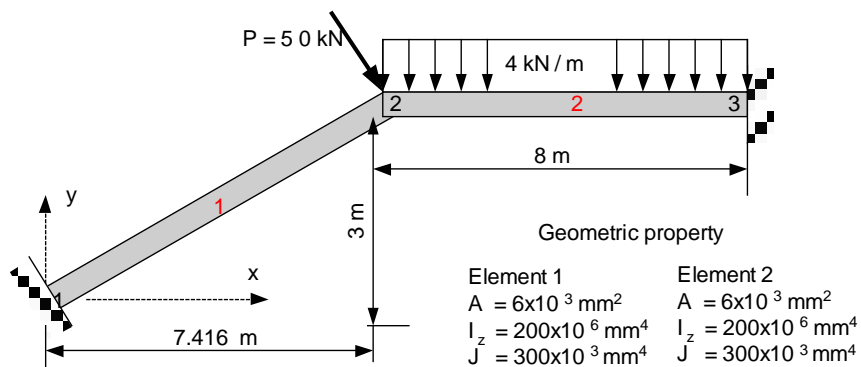


Fig.14.1 Frame model-4 (20 Elements, XFrame)

Results

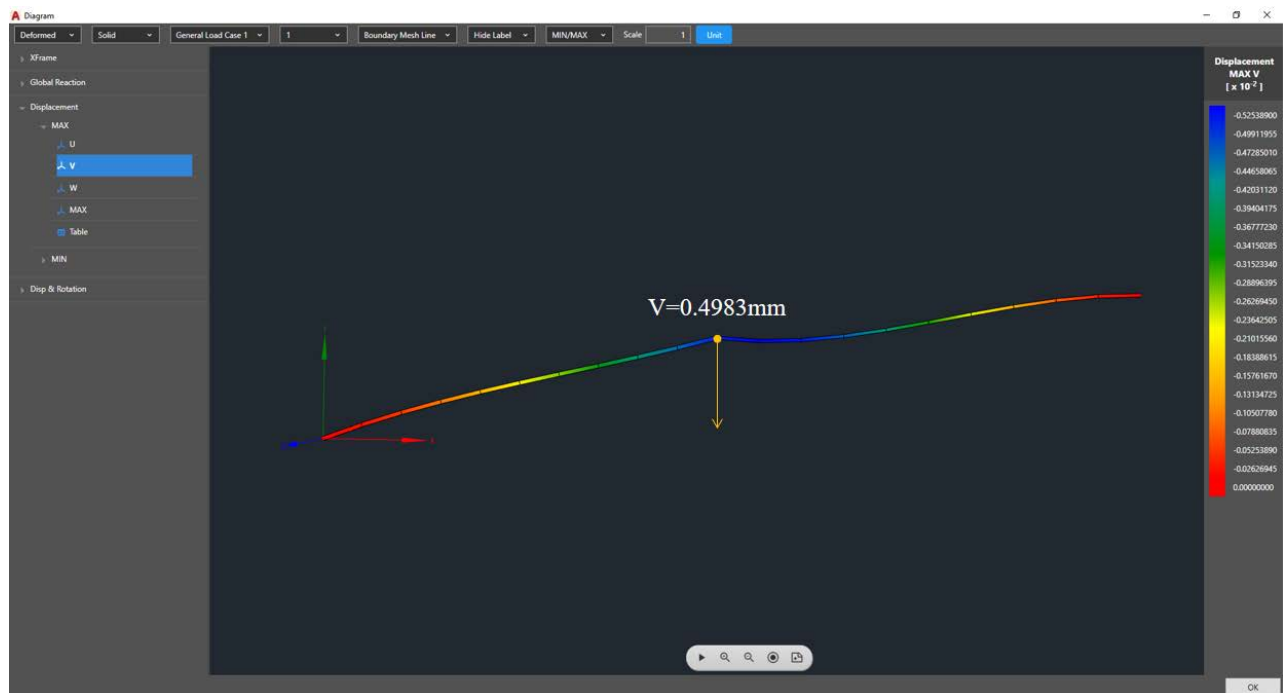


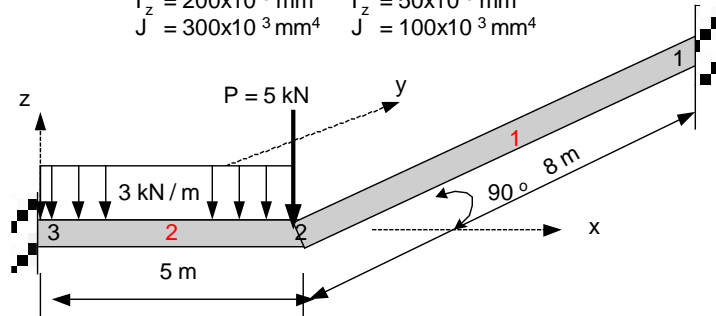
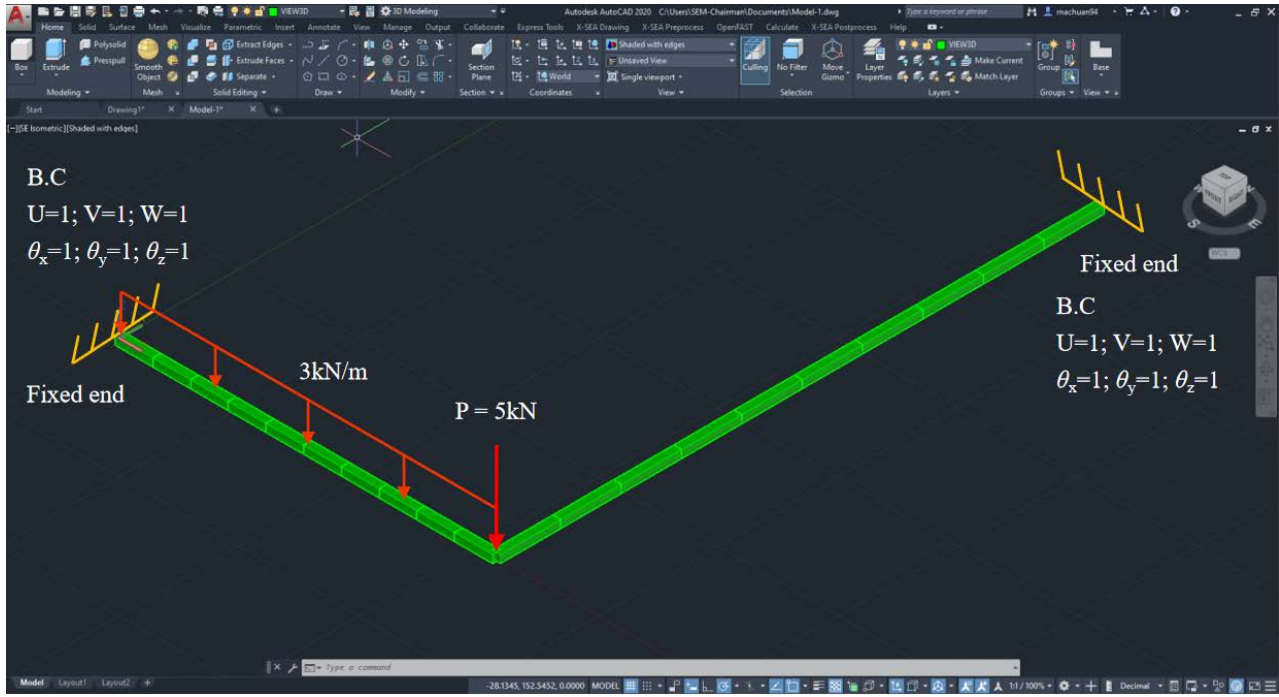
Fig.14.2 Displacement of beam in y direction (20 Elements, XFrame)

Table 14.1 Displacement at node 2

Element type	U (mm)	V (mm)	R _z (rad)
Reference	0.9982	-0.4996E+01	-0.5340E-03
XSEA	0.9953	-0.4983E+01	-0.5344E-03

Table 14.2 Reaction at node 1 and 3

Element type	Node 1			Node 3		
	F _x (N)	F _y (N)	M _z (N·mm)	F _x (N)	F _y (N)	M _z (N·mm)
Reference	0.1310E+06	0.5540E+05	0.1343E+08	-0.1497E+06	0.2270E+05	-0.4541E+08
XSEA	0.1305E+06	0.5568E+05	0.1337E+08	-0.1493E+06	0.2267E+05	-0.4536E+08

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Verification Example of X-SEA AutoCAD	No: Frame Element 015								
Title: Frame Element Numerical Examples-5									
Problem Description <p>Beam is supported and loaded as follows.</p> <p>$E=199.96\text{GPa}$; $\nu=0.03$.</p> <div style="text-align: center;"> <p>Geometric property</p> <table> <tr> <td>Element 1</td><td>Element 2</td></tr> <tr> <td>$A = 6 \times 10^{-3} \text{ mm}^2$</td><td>$A = 4 \times 10^{-3} \text{ mm}^2$</td></tr> <tr> <td>$I_z = 200 \times 10^{-6} \text{ mm}^4$</td><td>$I_z = 50 \times 10^{-6} \text{ mm}^4$</td></tr> <tr> <td>$J = 300 \times 10^{-3} \text{ mm}^4$</td><td>$J = 100 \times 10^{-3} \text{ mm}^4$</td></tr> </table> </div> 		Element 1	Element 2	$A = 6 \times 10^{-3} \text{ mm}^2$	$A = 4 \times 10^{-3} \text{ mm}^2$	$I_z = 200 \times 10^{-6} \text{ mm}^4$	$I_z = 50 \times 10^{-6} \text{ mm}^4$	$J = 300 \times 10^{-3} \text{ mm}^4$	$J = 100 \times 10^{-3} \text{ mm}^4$
Element 1	Element 2								
$A = 6 \times 10^{-3} \text{ mm}^2$	$A = 4 \times 10^{-3} \text{ mm}^2$								
$I_z = 200 \times 10^{-6} \text{ mm}^4$	$I_z = 50 \times 10^{-6} \text{ mm}^4$								
$J = 300 \times 10^{-3} \text{ mm}^4$	$J = 100 \times 10^{-3} \text{ mm}^4$								
									
<p style="text-align: center;">Fig.15.1 Frame model-5 (20 Elements, XFrame)</p>									

Results

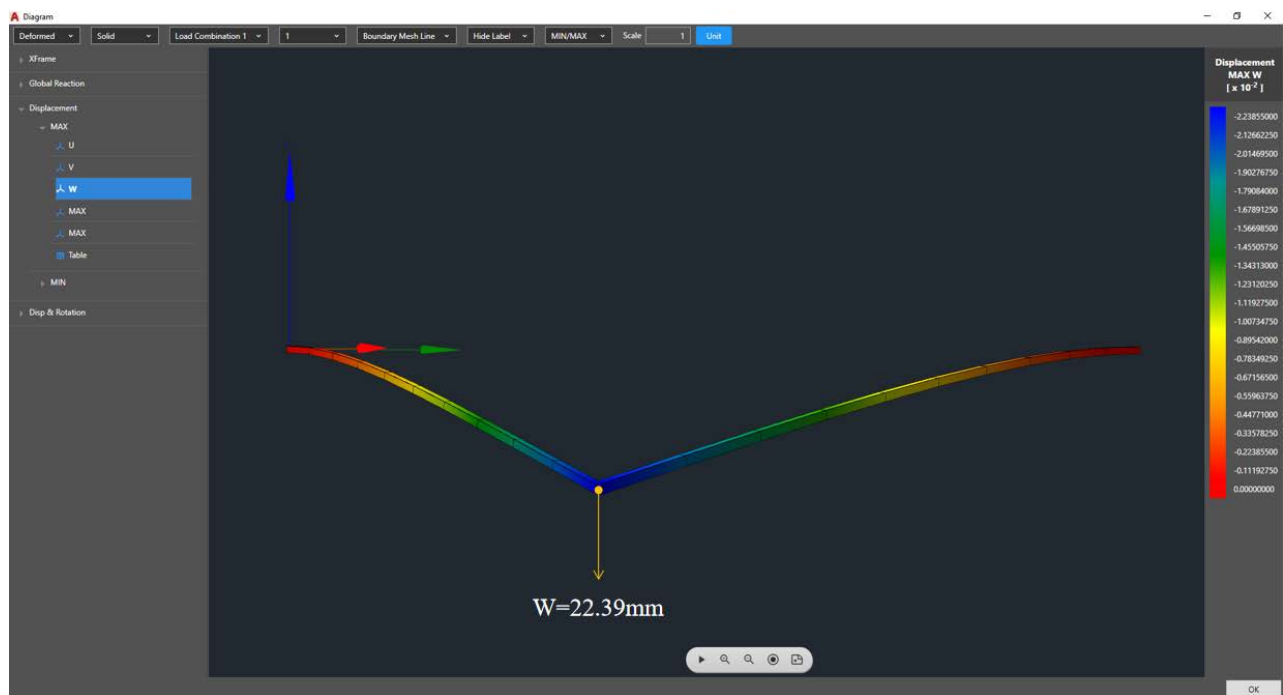


Fig.15.2 Displacement of beam in Z direction (20 Elements, XFrame)

Table 15.1 Displacement at node 2

Element type	W (mm)	R_x (rad)	R_y (rad)
Reference	-0.2237E+02	0.4195E-03	0.5931E-03
XSEA	-0.2239E+02	0.4197E-02	0.5932E-02

Table 15.2 Reaction at node 1 and 3

Element type	Node 1			Node 3		
	F_z (N)	M_x (N)	M_y (N·mm)	F_z (N)	M_x (N)	M_y (N·mm)
Reference	0.5250E+04	-0.4194E+08	-0.1711E+05	0.1474E+05	-0.6450E+04	-0.3621E+08
XSEA	0.5247E+04	-0.4197E+08	-0.2159E+05	0.1474E+05	-0.8148E+04	-0.3624E+08

Title: Frame Element Numerical Examples-6

Problem Description

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

Geometric property

Element 1	Element 2
$A = 6650 \text{ mm}^2$	$A = 6650 \text{ mm}^2$
$I_z = 118.6 \times 10^6 \text{ mm}^4$	$I_z = 118.6 \times 10^6 \text{ mm}^4$
$J_z = 300 \times 10^3 \text{ mm}^4$	$J_z = 300 \times 10^3 \text{ mm}^4$

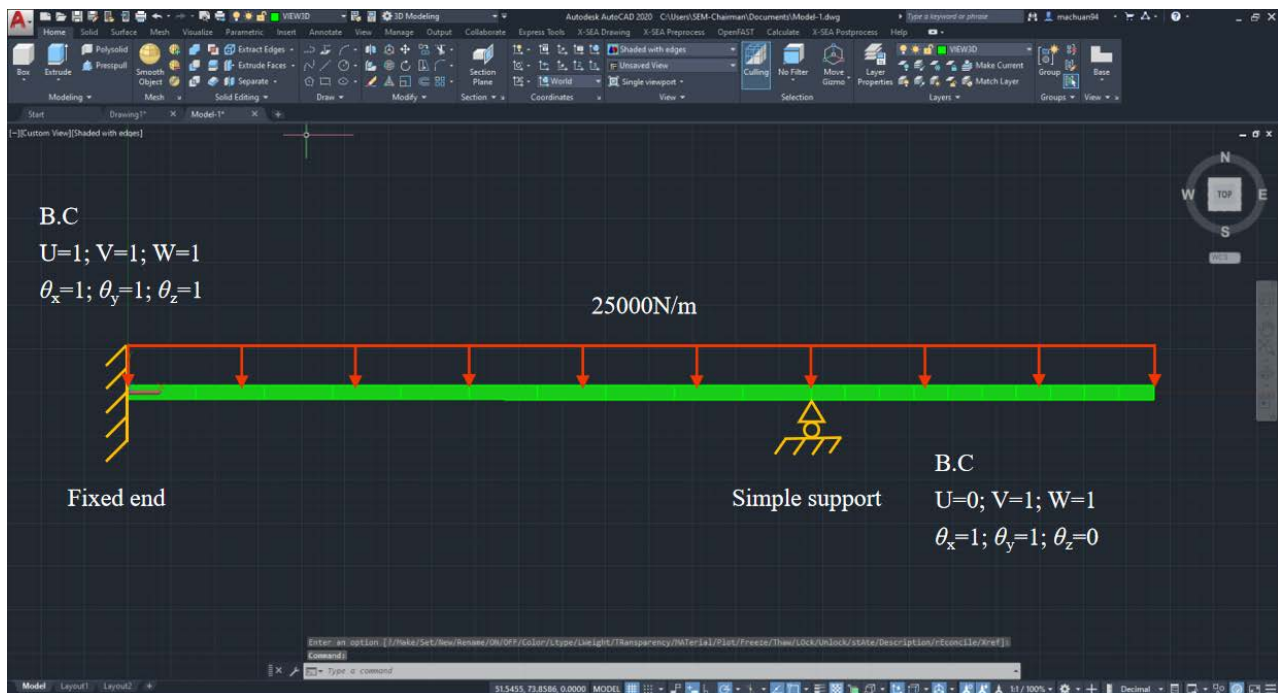
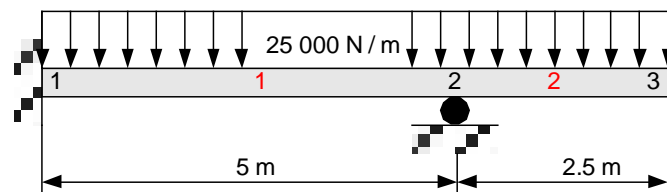


Fig.16.1 Frame model-6 (20Elements, XFrame)

Results

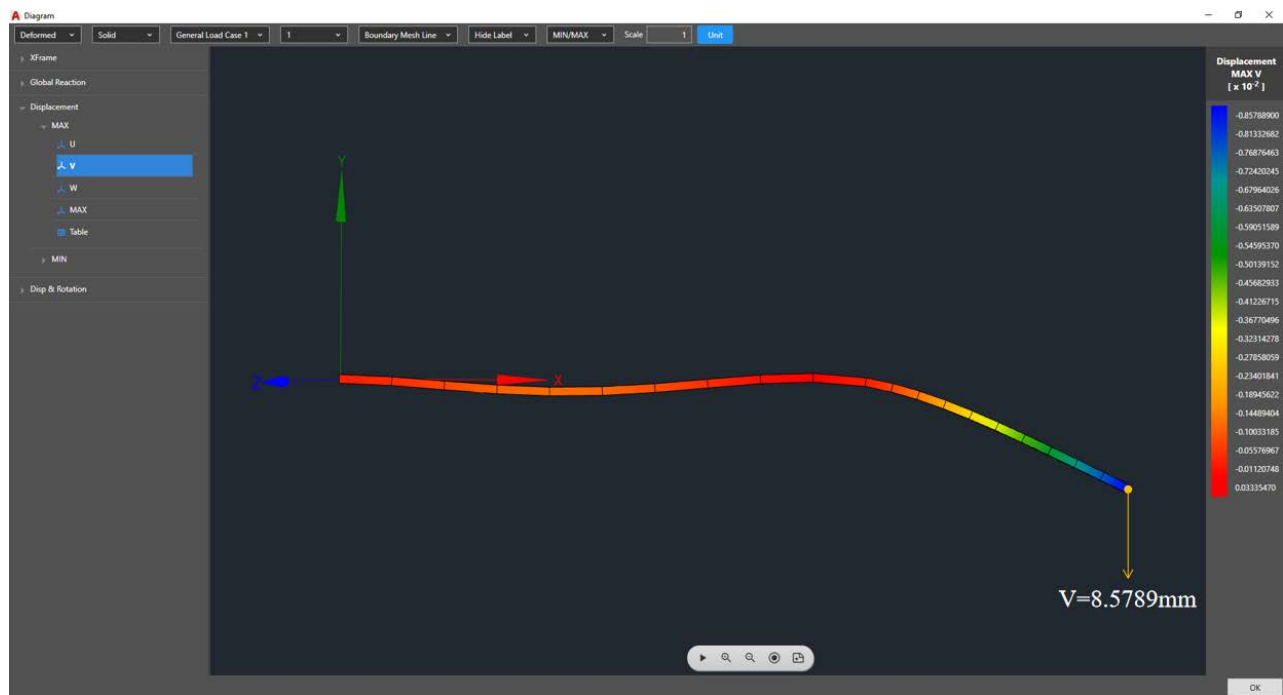


Fig.16.2 Displacement of beam in Y direction (20Elements, XFrame)

Table 16.1 Displacement at node 2 and 3

Element type	Node 2	Node 3	
	R_z (rad)	V (mm)	R_z (rad)
Reference	-0.1372E-02	-0.8577E+01	-0.4117E-02
XSEA	-0.1372E-02	-0.8579E+01	-0.4118E-02

Table 16.2 Reaction at node 1

Element type	Node 1	
	F_y (N)	M_x (N)
Reference	0.54687E+05	0.39062E+08
XSEA	0.54688E+05	0.39063E+08

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Verification Example of X-SEA AutoCAD

No: Frame Element 017

Title: Frame Element Numerical Examples-7

Problem Description

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

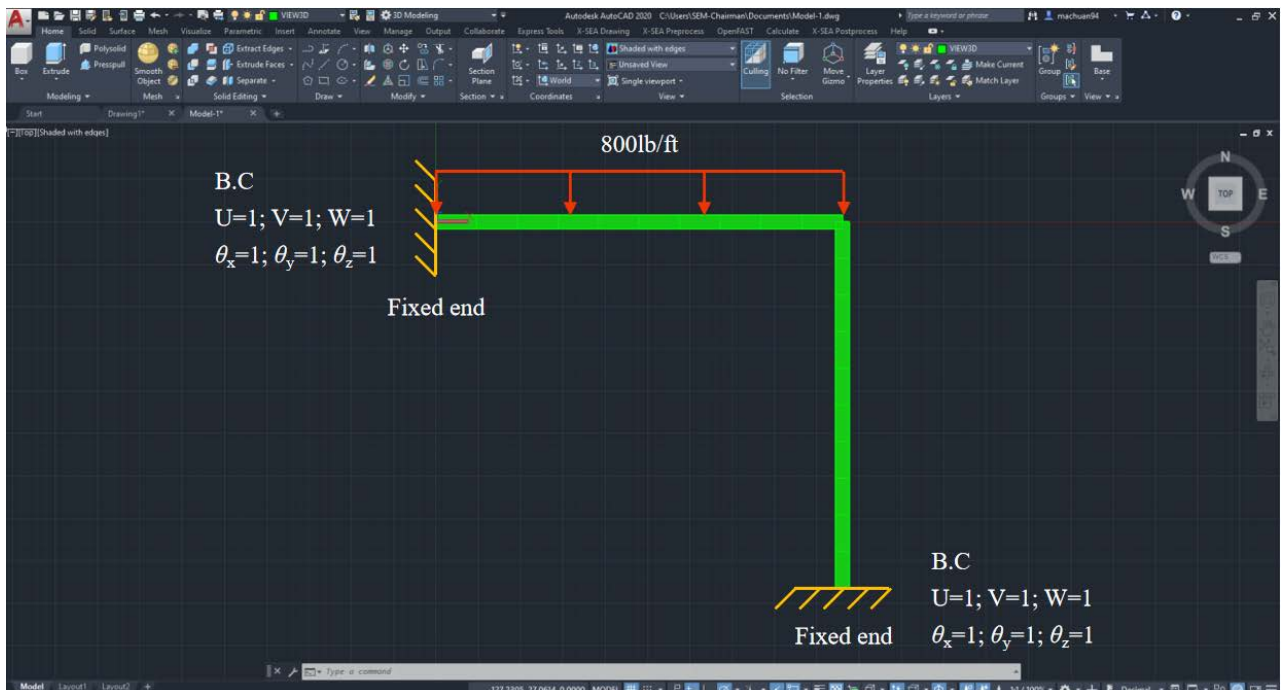
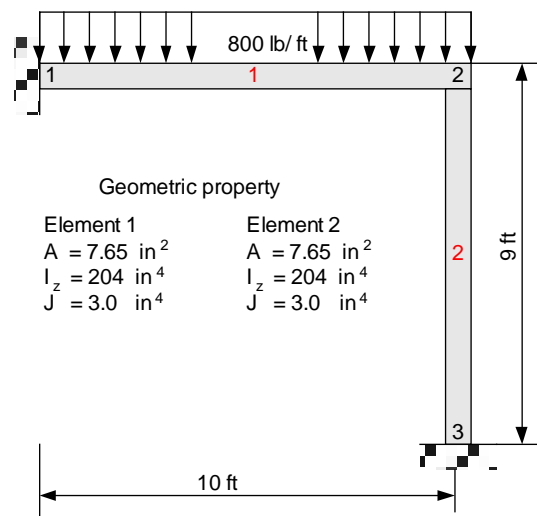


Fig.17.1 Frame model-7 (20Elements, XFrame)

Results

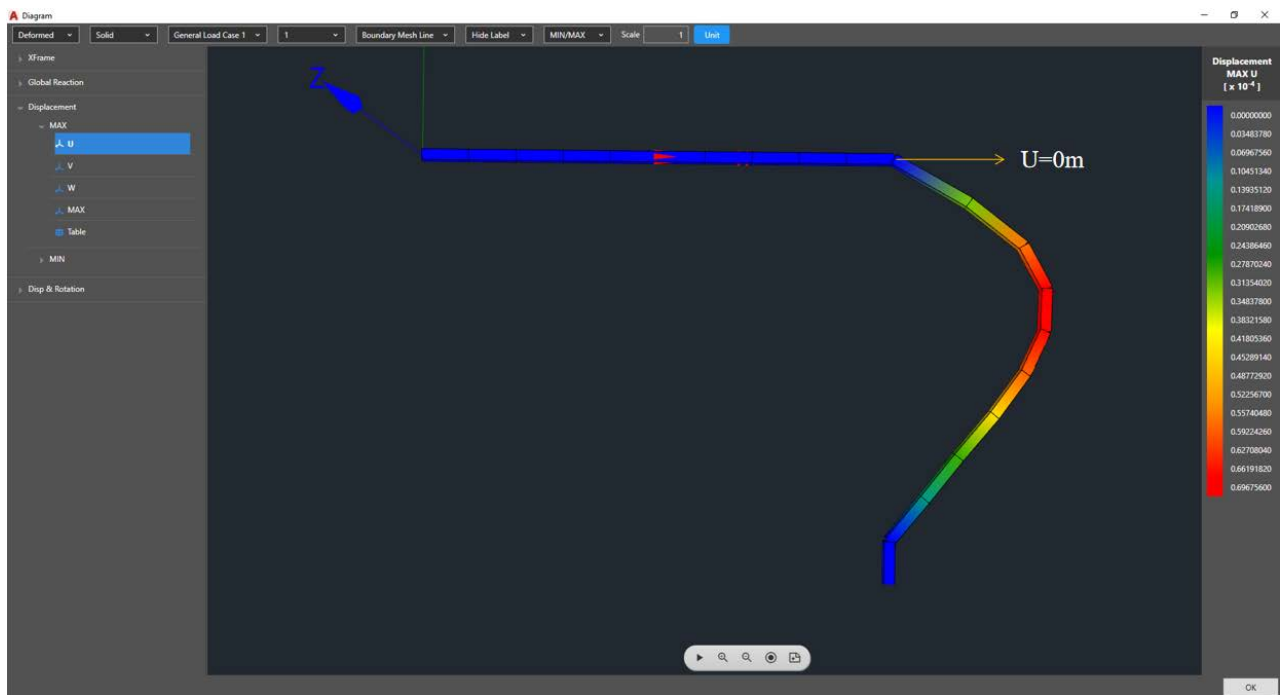


Fig.17.2 Displacement of beam in X direction (20Elements, XFrame)

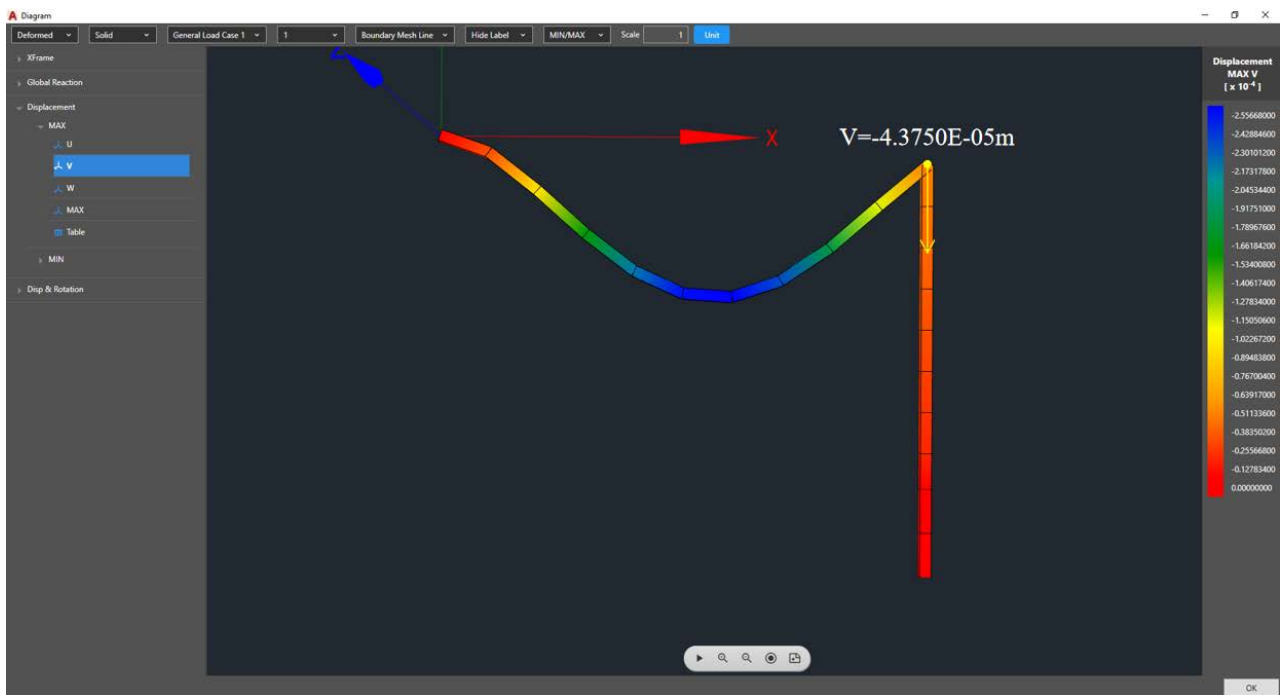


Fig.17.3 Displacement of beam in Y direction (20Elements, XFrame)

Table 17.1 Displacement at node 2

Element type	U (in (m))	V (in (m))	Rz (rad)
Reference	-0.2845E-03	-0.16359E-02	0.17815E-03
XSEA	0	-0.1722E-02 (-4.3750E-05)	0.18758E-03

Table 17.2 Reaction at node 1 and 3

Element type	Node 1			Node 3		
	F _x (lbf) (N)	F _y (lbf) (N)	M _z (lbf·in) (N·m)	F _x (lbf) (N)	F _y (lbf) (N)	M _z (lbf·in) (N·m)
Reference	0.5443E+03	0.4524E+04	0.1024E+06	-0.5443E+03	0.3476E+04	0.1930E+05
XSEA	0.5540E+03 (2.4643E+03)	0.4605E+04 (2.0483E+04)	0.1042E+06 (1.1770E+04)	-0.5540E+03 (-2.4643E+03)	0.3538E+04 (1.5740E+04)	0.1964E+05 (2.2190E+03)

Title: Frame Element Numerical Examples-8

Problem Description

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

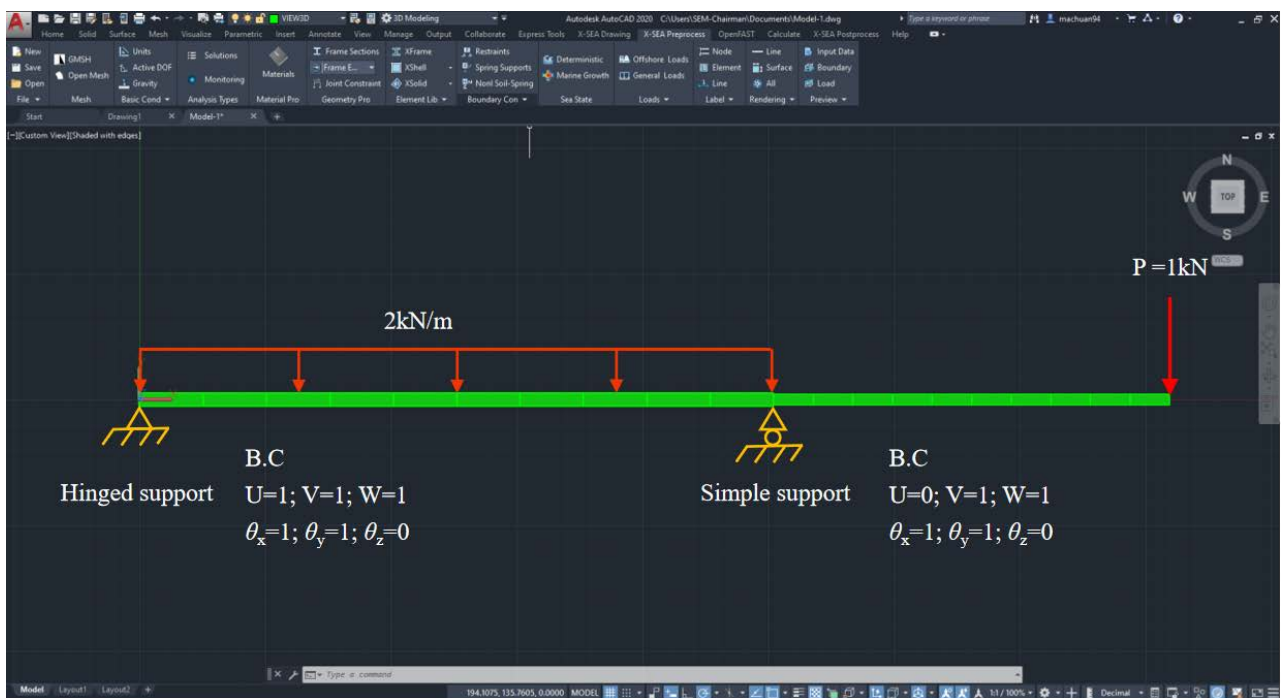
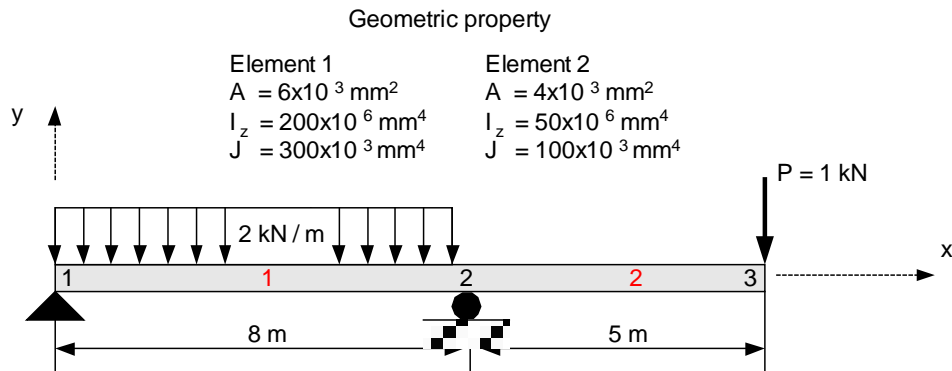


Fig.18.1 Frame model-8 (20Elements, XFrame)

Results

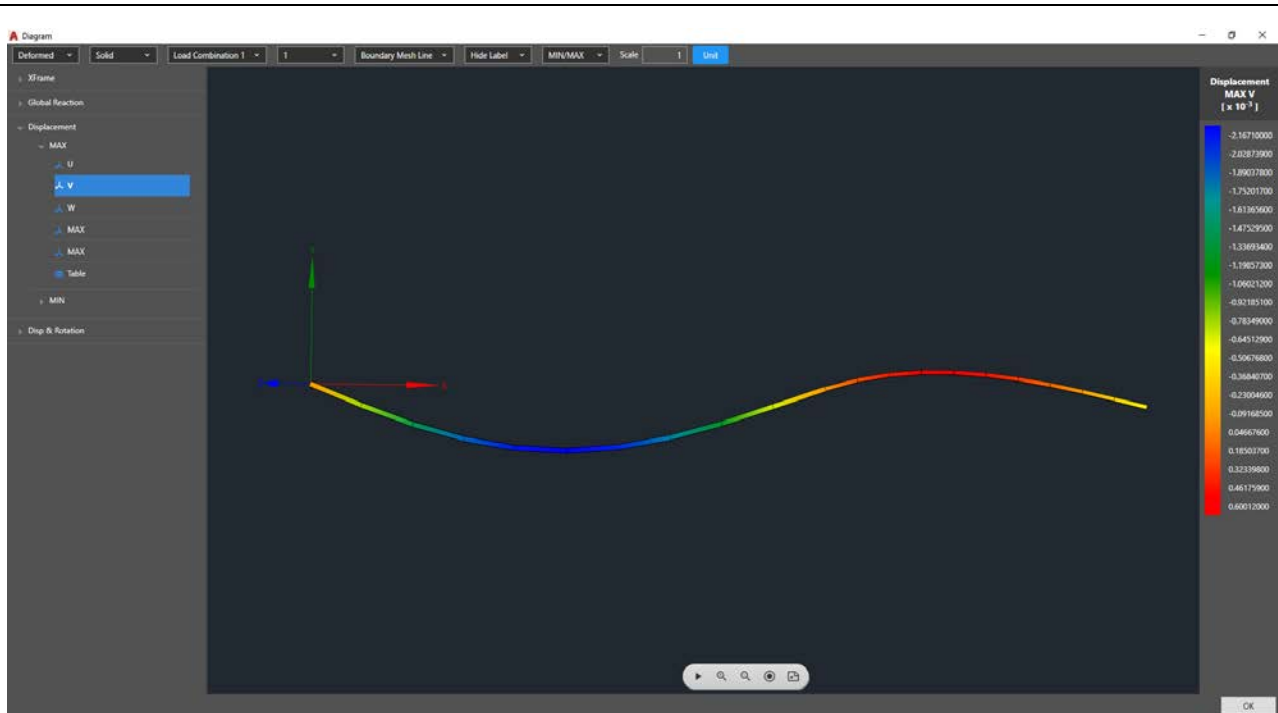


Fig.18.2 Displacement of beam in Y direction (20Elements, XFrame)

Table 18.1 Reaction at node 1, 2

Element type	Reaction F_y (N)	
	Node1	Node 2
Reference	0.7375E+04	0.9625E+04
XSEA	0.7375E+04	0.9625E+04

Title: Validation of the proposed spring supported boundary element**Problem Description**

Beam is supported and loaded as follows.

$E=199.96\text{GPa}$; $\nu=0.03$.

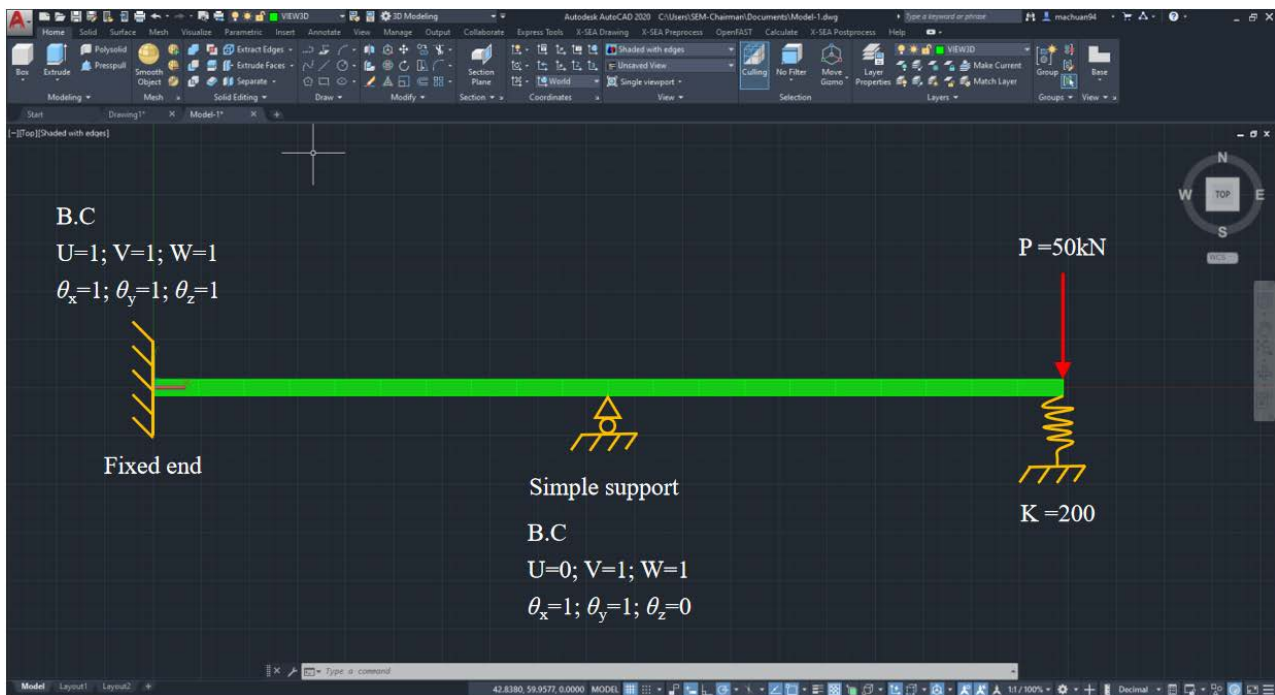
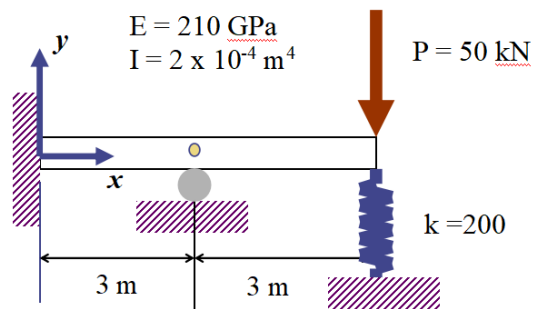


Fig.19.1 Frame model-8 (20Elements, XFrame)

Results



Fig.19.2 Displacement of beam in Y direction (20Elements, XFrame)

Table 19.1 Reaction at end node

Element type	Displacement (m)	Rotation (rad)
Reference	-0.01740	-0.00747
XSEA	-0.01875	-0.00803