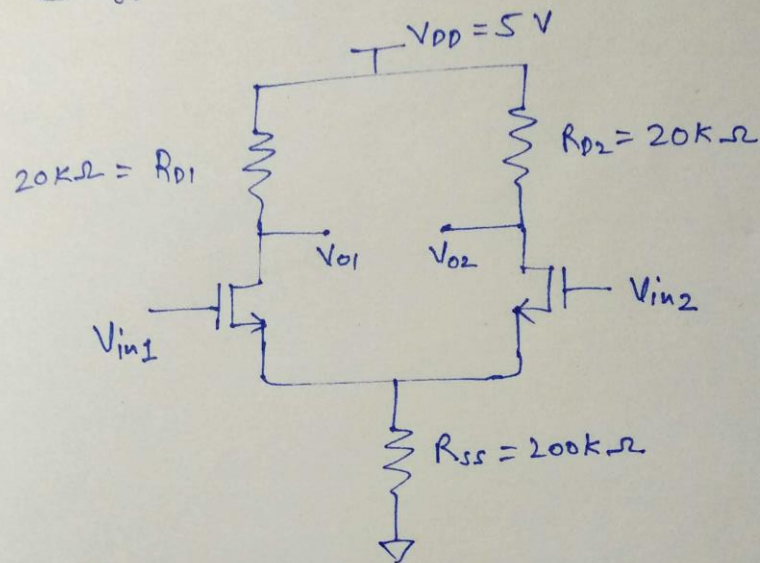


EE 204-2018-2 Analog Circuits
Homework #2 Solution

Question 1A-I

Qus. 1 A

(1) Differential amplifier



Here $g_{m1} = g_{m2} = 2\text{ mS}$, $R_{D1} = R_{D2} = 20k\Omega$

$$(V_{o1} - V_{o2}) = -g_{m1} (V_{in1} - V_{in2}) R_{D1}$$

$$\frac{(V_{o1} - V_{o2})}{(V_{in1} - V_{in2})} = -g_{m1} R_{D1}$$

$$= -2 \times 10^{-3} \times 20 \times 10^3$$

Differential
gain

$$\boxed{A_v = -40}$$

Question 1A-II (a)

Homework-2

1A.

II. (a) $g_{m1} = g_{m0} + \frac{\Delta g_m}{2}$

$g_{m2} = g_{m0} - \frac{\Delta g_m}{2}$

$g_{m0} = 2 \text{ mS}$ and $\Delta g_m = 0.2 \text{ mS}$

$R_{d1} = 20 \text{ k}\Omega$

$R_{d2} = 20 \text{ k}\Omega$

$R_{ss} = 200 \text{ k}\Omega$

$r_{o1} = r_{o2} = \infty$

$$A_{CM-DM} = - \left[\frac{R_d \Delta g_m}{1 + 2g_{m0}R_{ss}} \right] = - \left[\frac{20 \times 10^3 \times 0.2 \times 10^{-3}}{1 + 2 \times 2 \times 10^{-3} \times 200 \times 10^3} \right]$$

$$= -4.993 \times 10^{-3}$$

$$CMRR = \frac{1}{2} \left| \frac{(g_{m1}R_{d1} + g_{m2}R_{d2}) + 2g_{m1}g_{m2}R_{ss}(R_{d1} + R_{d2})}{g_{m1}R_{d1} - g_{m2}R_{d2}} \right|$$

$$= \frac{1}{2} \left| \frac{(2.1 \times 20 + 1.9 \times 20) + 2 \times 2.1 \times 1.9 \times 200 \times 10^3 (20 + 20) \times 10^3}{2.1 \times 20 - 1.9 \times 20} \right|$$

$$= 7990$$

$$= 78.05 \text{ dB}$$

Question 1A-II (b)

A II (b)

$R_{D1} = R_{D0} + \frac{\Delta R_D}{2}$
 $R_{D2} = R_{D0} - \frac{\Delta R_D}{2}$
 $\Delta R_D = R_{D1} - R_{D2}$
 $\therefore R_{D1} + R_{D2} = 2R_{D0}$

Let, $V_{cm} = v_i$

Considering one transistor with small signal analysis,

Now, $V_g = V_i$ & $V_s = V_p = g_m V_{gs} R_{ss}$

$\therefore V_{gs} = V_g - V_s = V_i - g_m V_{gs} R_{ss} \Rightarrow V_{gs} = \frac{V_i}{1 + g_m R_{ss}}$

& $\therefore \frac{V_p}{V_i} = \frac{g_m R_{ss}}{1 + g_m R_{ss}}$

\therefore Two transistors are sending current through R_{ss} . In mismatch

$\Delta V_p = \frac{2R_{ss} g_m}{1 + 2g_m R_{ss}} \Delta V_{i,cm}$ & $\Delta I_{ss} = \frac{\Delta V_p}{R_{ss}}$

Also, $\Delta I_{D1} = \Delta I_{D2} = \frac{\Delta I_{ss}}{2} = \frac{g_m}{1 + 2g_m R_{ss}} \Delta V_{i,cm}$

Hence, $\Delta V_{o,cm-dm} = (-\Delta I_{D1} R_{D1}) - (-\Delta I_{D2} R_{D2}) = \left(\frac{\Delta I_{ss}}{2}\right) \Delta R_D$

or $\Delta V_{o,cm-dm} = -\frac{g_m \Delta R_D}{1 + 2g_m R_{ss}} \Delta V_{i,cm}$ & $A_{cm-dm} = \frac{\Delta V_{o,cm-dm}}{\Delta V_{i,cm}}$

$\Rightarrow A_{cm-dm} = -\frac{g_m \Delta R_D}{1 + 2g_m R_{ss}}$

\therefore In Differential mode, $V_p \approx 0$ virtual ground.

& $A_{dm} = -g_m R_{D0}$ {check. }

given $R_{ss} = 200k\Omega$
 $R_D = 20k\Omega$
 $\Delta R_D = 2k\Omega$
 $g_m = 2mS$

$$So, A_{dm} = -(2 \times 10^{-3}) \cdot (20 \times 10^3)$$

$$or A_{dm} = -40$$

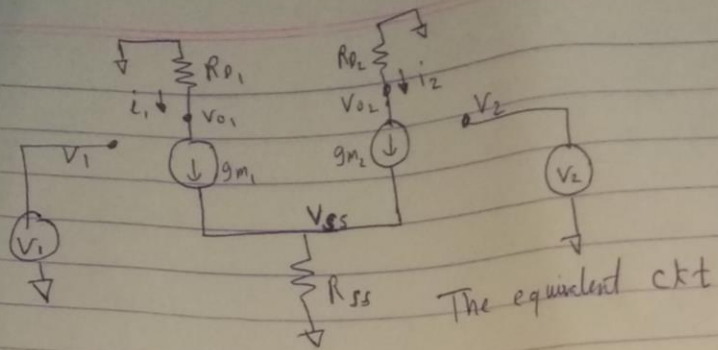
$$\Delta A_{cm-dm} = \frac{-(2 \times 10^{-3})(2 \times 10^3)}{1 + (2 \times 2 \times 10^{-3} \times 200 \times 10^3)}$$

$$A_{cm-dm} = \frac{-4}{1 + 800} \approx \frac{-4}{800} = -5 \times 10^{-3}$$

$$\frac{A_{cm-dm}}{A_{dm}} = \frac{+5 \times 10^{-3}}{+40} = \frac{1}{8000}$$

$$\therefore CMRR = 20 \log \left| \frac{A_{dm}}{A_{cm-dm}} \right| = 78.0618 \text{ dB}$$

Question 1A-II(c)



The equivalent ckt

$$V_{SS} = (i_1 + i_2) R_{SS} \quad (1)$$

$$i_1 = (V_1 - V_{SS}) g_{m1}, \quad i_2 = (V_2 - V_{SS}) g_{m2} \quad (2)$$

for Common mode ,

$$V_1 = V_2 = V_C$$

Solving for V_{SS} using above equations

$$V_{SS} = (g_{m1} + g_{m2}) / (1/R_{SS} + g_{m1} + g_{m2})$$

now $V_{O1} = R_{D1} g_{m1} (V_C - V_{SS})$, $V_{O2} = R_{D2} g_{m2} (V_C - V_{SS})$

$$\Rightarrow V_O = V_{O1} - V_{O2} = (R_{D1} g_{m1} - R_{D2} g_{m2}) (V_C - V_{SS})$$

$$= (R_{D1} g_{m1} - R_{D2} g_{m2}) V_C / (1 + (g_{m1} + g_{m2}) R_{SS})$$

$$\Rightarrow A_{cm} = (R_{D1} g_{m1} - R_{D2} g_{m2}) / (1 + (g_{m1} + g_{m2}) R_{SS})$$

(putting values) = 0.1

for Diff Mode

$$V_1 = +V_d/2, \quad V_2 = -V_d/2$$

$$V_O = V_{O1} - V_{O2} = R_{D1} g_{m1} \left(\frac{V_d}{2} - V_{SS} \right) - R_{D2} g_{m2} \left(\frac{-V_d}{2} - V_{SS} \right)$$

$V_{SS} = 0$ for diff mode

$$\Rightarrow A_{dm} = \frac{R_{D1} g_{m1} + R_{D2} g_{m2}}{2}$$

putting values $A_{dm} \approx 40$

$$\Rightarrow CMRR \approx 4000$$

Question 1A-II(d)

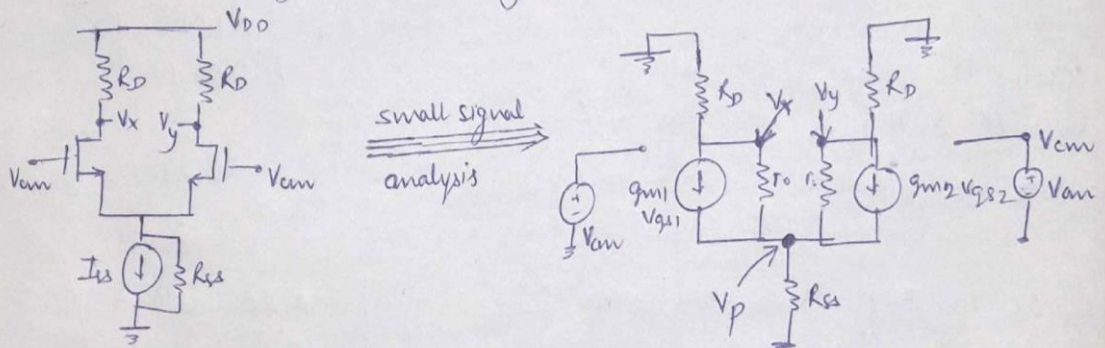
Ques 1A II. (d)

Repeating part (a). Given $r_{o1} = r_{o2} = 50k\Omega$, $R_{D1} = R_{D2} = 20k\Omega$
 $R_{SS} = 200k\Omega$, $g_{m1} = g_{m0} + \frac{\Delta g_m}{2}$
 $= 2m + \frac{0.2m}{2} = 2.1mS$

$$g_{m2} = g_{m0} - \frac{\Delta g_m}{2}$$

$$= 2m - \frac{0.2m}{2} = 1.9mS.$$

When r_o comes into effect, we need to apply exact analysis using small signal model of ckt.



Due to mismatch there would be Acm-dm. and we need to find $\frac{V_x - V_y}{V_{cm}}$ i.e. differential o/p due to common mode inputs

Applying KCL at node V_p .

$$\Rightarrow \frac{V_p}{R_{SS}} + \frac{V_p - V_x}{r_o} + \frac{V_p - V_y}{r_o} = g_{m1}(V_{gs1}) + g_{m2}(V_{gs2})$$

$$\Rightarrow \frac{V_p}{200k} + \frac{V_p - V_x}{50k} + \frac{V_p - V_y}{50k} = 2.1m(V_{cm} - V_p) + 1.9m(V_{cm} - V_p)$$

$$\Rightarrow \frac{V_p}{200k} + \frac{V_p - V_x}{50k} + \frac{V_p - V_y}{50k} = 4m(V_{cm} - V_p)$$

$$\left[\begin{aligned} V_{gs} &= V_{gate} - V_{source} \\ &= V_{cm} - V_p \end{aligned} \right]$$

$$\Rightarrow V_p \left[\frac{1}{200k} + \frac{1}{50k} + \frac{1}{50k} + 4m \right] = 4m V_{cm} + \frac{V_x}{50k} + \frac{V_y}{50k}$$

$$\Rightarrow \boxed{809V_p = 800V_{cm} + 4V_x + 4V_y} \quad \text{--- (1)}$$

Now applying KCL at node V_x .

$$\Rightarrow \frac{V_x}{R_D} + \frac{V_x - V_p}{r_o} + g_{m1}(V_{gs1}) = 0$$

$$\Rightarrow \frac{V_x}{20k} + \frac{V_x - V_p}{50k} + 2.1m(V_{cm} - V_p) = 0$$

$$\Rightarrow \boxed{V_x = 30.29V_p - 30V_{cm}} \quad \text{--- (2)}$$

Applying KCL at node V_y

$$\Rightarrow \frac{V_y}{R_D} + \frac{V_y - V_p}{r_o} + g_{m2}V_{gs2} = 0$$

$$\Rightarrow \frac{V_y}{20k} + \frac{V_y - V_p}{50k} + 1.9m(V_{cm} - V_p) = 0$$

$$\Rightarrow \boxed{V_y = 27.43V_p - 27.14V_{cm}} \quad \text{--- (3)}$$

Putting the values of V_x and V_y from eqn (2) and (3) into eqn (1)

$$\Rightarrow 809V_p = 800V_{cm} + 4(30.29V_p - 30V_{cm}) + 4(27.43V_p - 27.14V_{cm})$$

$$\Rightarrow 809V_p = 571.44V_{cm} + 230.88V_p$$

$$\Rightarrow 578.12V_p = 571.44V_{cm}$$

$$\boxed{V_p = 0.988V_{cm}} \quad \text{--- (4)}$$

from eqn (2) and (3)

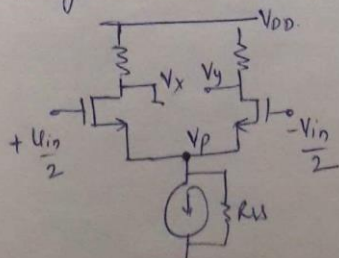
$$V_x - V_y = 2.86V_p - 2.86V_{cm}$$

putting V_p from eqn (4)

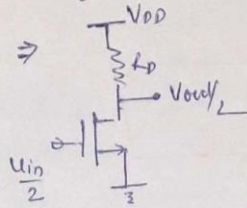
$$V_x - V_y = 2.86 \times (0.988)V_{cm} - 2.86V_{cm}$$

$$\boxed{\frac{V_x - V_y}{V_{cm}} = -0.034 \Rightarrow A_{CM-DM}} \quad \text{Ans}$$

To calculate CMRR we need to find out A_{DM} .



Applying half ckt. analysis



$$\Rightarrow A_{DM} = -g_m R_{out}$$

$$\Rightarrow = -g_m (R_D || r_o)$$

$$= -2m [20k || 50k]$$

$$\boxed{A_{DM} = -28.57}$$

$$CMRR = \left| \frac{A_{DM}}{A_{CM-DM}} \right|$$

$$= \frac{28.57}{0.034} = 840.3$$

$$\boxed{CMRR = 840.3}$$

In previous case, when $r_{o1} = r_{o2} = \infty$

$$A_{DM} = 40, A_{CM-DM} = \frac{0.0005}{0.005}$$

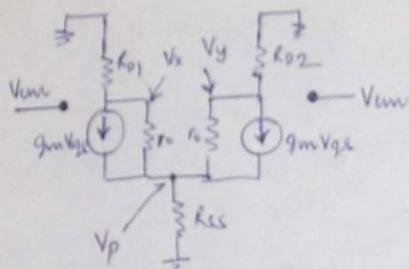
$$CMRR = \frac{40}{0.005} = 8000$$

Repeating part (b)

Given $r_{o1} = r_{o2} = 50k$, $R_{D1} = R_{D2} = 21k\Omega$, $g_{m1} = g_{m2} = 2mS$

$$R_{SS} = 200k\Omega \quad R_{D1} = R_{D0} + \frac{\Delta R_D}{2} = 21k\Omega$$

$$R_{D2} = R_{D0} - \frac{\Delta R_D}{2} = 19k\Omega$$



applying KCL at node V_p .

$$\frac{V_p}{R_{SS}} + \frac{V_p - V_x}{r_{o1}} + \frac{V_p - V_y}{r_{o2}} = 2g_m V_{gs}$$

$$V_p \left(\frac{1}{R_{SS}} + \frac{2}{r_o} \right) = \frac{V_x}{r_o} + \frac{V_y}{r_o} + 2g_m (V_{cm} - V_p)$$

$$V_p \left(\frac{1}{R_{SS}} + \frac{2}{r_o} + 2g_m \right) = \frac{V_x}{r_o} + \frac{V_y}{r_o} + 2g_m V_{cm}$$

$$V_p \left(\frac{1}{200k} + \frac{2}{50k} + 2 \cdot 2m \right) = \frac{V_x}{50k} + \frac{V_y}{50k} + 4m V_{cm}$$

$$809V_p = 800V_{cm} + 4V_x + 4V_y \quad \text{--- (1)}$$

applying KCL at node V_x

$$\frac{V_x}{R_{D1}} + \frac{V_x - V_p}{r_o} + g_m V_{gs} = 0$$

$$\frac{V_x}{21k} + \frac{V_x - V_p}{50k} + 2m(V_{cm} - V_p) = 0$$

$$V_x = -29.41V_{cm} + 29.71V_p \quad \text{--- (2)}$$

Similarly, at node V_y

$$V_y = -27.40V_{cm} + 27.67V_p \quad \text{--- (3)}$$

putting the values of (2) and (3) into (1)

$$V_p = 0.988V_{cm} \quad \text{--- (4)}$$

from eqn (2) and eqn (3)

$$V_x - V_y = -2.01V_{cm} + 2.04V_p$$

$$= -2.01V_{cm} + 2.04 \times 0.988V_{cm}$$

$$\frac{V_x - V_y}{V_{cm}} = 0.0055 = A_{CM-DM}$$

$$CMRR = \frac{A_{DM}}{A_{CM-DM}} = \frac{28.57}{0.0055}$$

$$CMRR = 5194.5$$

In previous case, when $r_{o1} = r_{o2} = \infty$, then

$$A_{DM} = 40$$

$$A_{CM-DM} = 0.005$$

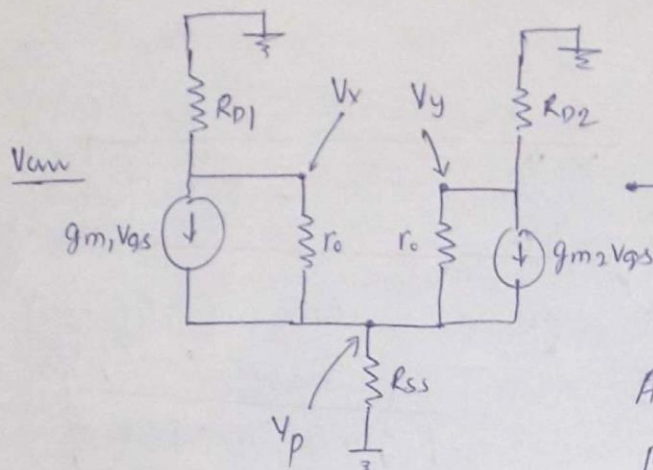
$$CMRR = 8000$$

Repeating part c

Given $r_{o1} = r_{o2} = 50 \text{ k}\Omega$, $R_{SS} = 200 \text{ k}\Omega$

$$R_{D1} = 210 \text{ k}\Omega \quad g_{m1} = 2.1 \text{ mS}$$

$$R_{D2} = 19 \text{ k}\Omega \quad g_{m2} = 1.9 \text{ mS}$$



In this case we need to find $\frac{V_x - V_y}{V_{cm}}$ when

V_{cm} the mismatch is present in r_o and g_m both.

Applying KCL analysis like previous case. i.e. at node V_x , V_y & V_p .

$$809V_p = 800V_c + 4V_x + 4V_y$$

$$V_x = 31.36V_p - 31.06V_{cm}$$

$$V_y = 26.45V_p - 26.17V_{cm}$$

$$V_p = 0.988V_{cm}$$

$$V_x - V_y = -0.04V_{cm}$$

$$\frac{V_x - V_y}{V_{cm}} = -0.04 = A_{CM-DM}$$

$$CMRR = \left| \frac{-2857}{-0.04} \right| = 714.25$$

With $r_{o1} = r_{o2} = \infty$

$$\frac{V_x - V_y}{V_{cm}} = A_{CM-DM} = 0.01$$

$$CMRR = \frac{40}{0.01} = 4000$$

Question 1A-II(e)

According to the electrical circuit given in d) part we apply KCL at x,y and p nodes to get the following equations

$$V_p \left(\frac{1}{R_{ss}} + \frac{2}{r_o} \right) - \left(\frac{V_x + V_y}{r_o} \right) - (g_{m1} + g_{m2}) (V_{cm} - V_p) = 0 \quad (1)$$

$$V_x \left(\frac{1}{r_o} + \frac{1}{R_{D1}} \right) + g_{m1} (V_{cm} - V_p) - \frac{V_p}{r_o} = 0 \quad (2)$$

$$V_y \left(\frac{1}{r_o} + \frac{1}{R_{D2}} \right) + g_{m2} (V_{cm} - V_p) - \frac{V_p}{r_o} = 0 \quad (3)$$

Solving the above equations gives us the following result

$$V_p = \frac{r_o (g_{m2} (R_{D1} + r_o) + g_{m1} (R_{D2} + r_o)) R_{SS} V_{cm}}{(R_{D1} + r_o) (R_{D2} + r_o) + (R_{D1} + R_{D2} + g_{m2} R_{D1} r_o + g_{m1} R_{D2} r_o + r_o (2 + (g_{m1} + g_{m2}) r_o)) R_{SS}} \quad (4)$$

$$V_x = - \frac{R_{D1} r_o (-g_{m2} R_{SS} + g_{m1} (R_{D2} + r_o + R_{SS})) V_{cm}}{(R_{D1} + r_o) (R_{D2} + r_o) + (R_{D1} + R_{D2} + g_{m2} R_{D1} r_o + g_{m1} R_{D2} r_o + r_o (2 + (g_{m1} + g_{m2}) r_o)) R_{SS}} \quad (5)$$

$$V_y = - \frac{R_{D2} r_o (-g_{m1} R_{SS} + g_{m2} (R_{D1} + r_o + R_{SS})) V_{cm}}{(R_{D1} + r_o) (R_{D2} + r_o) + (R_{D1} + R_{D2} + g_{m2} R_{D1} r_o + g_{m1} R_{D2} r_o + r_o (2 + (g_{m1} + g_{m2}) r_o)) R_{SS}} \quad (6)$$

1.1 Sensitivity with only g_m mismatch

After substituting $R_{D1} = R_{D2} = R_D$, $g_{m1} = g_m + \Delta g_m/2$, $g_{m2} = g_m - \Delta g_m/2$, $r_o = 50k$ and $R_{SS} = 200k$. We get the following values

$$A_{CM-DM} = - \frac{50 \times 10^3 \Delta g_m R_D (450 \times 10^3 + R_D)}{(50 \times 10^3 + R_D) (50 \times 10^3 (9 + 400 \times 10^3 g_m) + R_D)} \quad (7)$$

Now the sensitivity is found as

$$Sensitivity_{g_m} = \frac{\partial A_{CM-DM}}{\partial g_m} \frac{g_m}{A_{CM-DM}} = - \frac{2 \times 10^{10} g_m}{50 \times 10^3 (9 + 4 \times 10^5 g_m) + R_D} \quad (8)$$

Therefore the value turns out to be **-0.988386**

1.2 Sensitivity with only R_D mismatch

After substituting $g_{m1} = g_{m2} = g_m$, $R_{D1} = R_D + \Delta R_D/2$, $R_{D2} = R_D - \Delta R_D/2$, $r_o = 50k$ and $R_{SS} = 200k$. We get the following values

$$A_{CM-DM} = -\frac{10^{10} \Delta R_D g_m}{\Delta R_D^2 - 4(50 \times 10^3 + R_D)(50 \times 10^3(9 + 400 \times 10^3 g_m) + R_D)} \quad (9)$$

Now the sensitivity is found as

$$Sensitivity_{RD} = \frac{\partial A_{CM-DM}}{\partial R_D} \frac{R_D}{A_{CM-DM}} = -\frac{R_D(-4(50 \times 10^3 + R_D) - 4(50 \times 10^3(9 + 400 \times 10^3 g_m) + R_D))}{\Delta R_D^2 - 4(50 \times 10^3 + R_D)(50 \times 10^3(9 + 400 \times 10^3 g_m) + R_D)} \quad (10)$$

Therefore the value turns out to be **-0.286209**

1.3 Sensitivity with R_D and g_m mismatch

After substituting $g_{m1} = g_m + \Delta g_m/2$, $g_{m2} = g_m - \Delta g_m/2$, $R_{D1} = R_D + \Delta R_D/2$, $R_{D2} = R_D - \Delta R_D/2$, $r_o = 50k$ and $R_{SS} = 200k$. We get the following values

$$A_{CM-DM} = -\frac{50 \times 10^3(-200 \times 10^3 \Delta R_D g_m + \Delta g_m(\Delta R_D^2 - 4R_D(450 \times 10^3 + R_D)))}{20 \times 10^9 \Delta g_m \Delta R_D + \Delta R_D^2 - 4(50 \times 10^3 + R_D)(50 \times 10^3(9 + 400 \times 10^3) + R_D)} \quad (11)$$

Now the sensitivity is found as

$$Sensitivity_{RD} = \frac{\partial A_{CM-DM}}{\partial R_D} \frac{R_D}{A_{CM-DM}} = 0.656071 \quad (12)$$

$$Sensitivity_{gm} = \frac{\partial A_{CM-DM}}{\partial g_m} \frac{g_m}{A_{CM-DM}} = -0.892405 \quad (13)$$

Note the change in signs in sensitivity of R_D .

Question 1B-I

1B
1

$I_{SS} (8mA)$
 $5V$
 V_{it}
 V_{i-}
 V_{DD}
 $10k\Omega$
 $10k\Omega$
 V_o

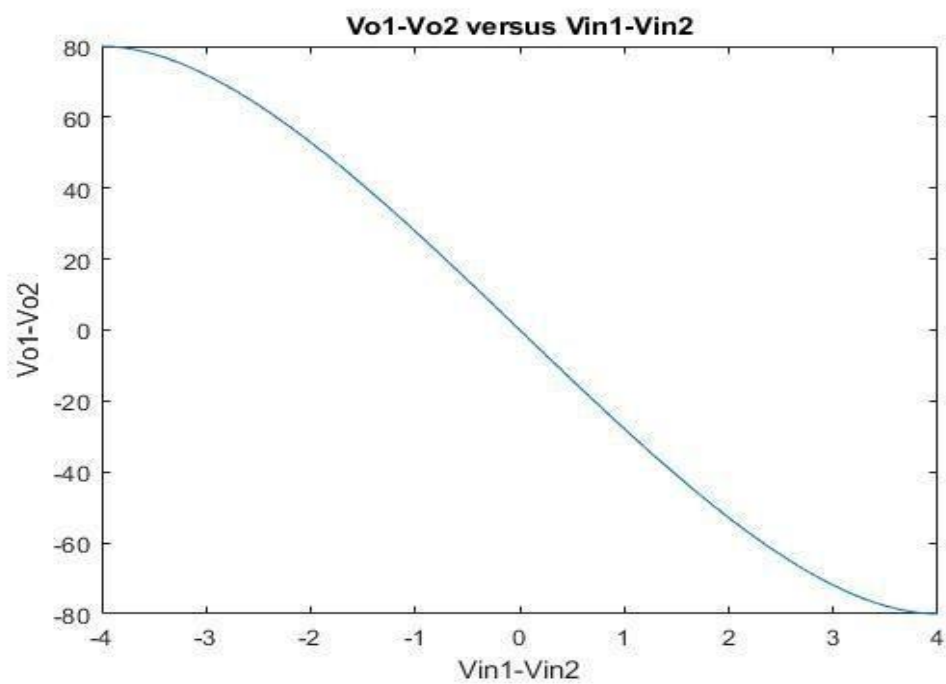
$$8mA = \frac{1}{2} \beta (V_{GS} - V_T)^2$$

$$8mA = \frac{1}{2} \times 1\mu A (V_{GS} - 1)^2$$

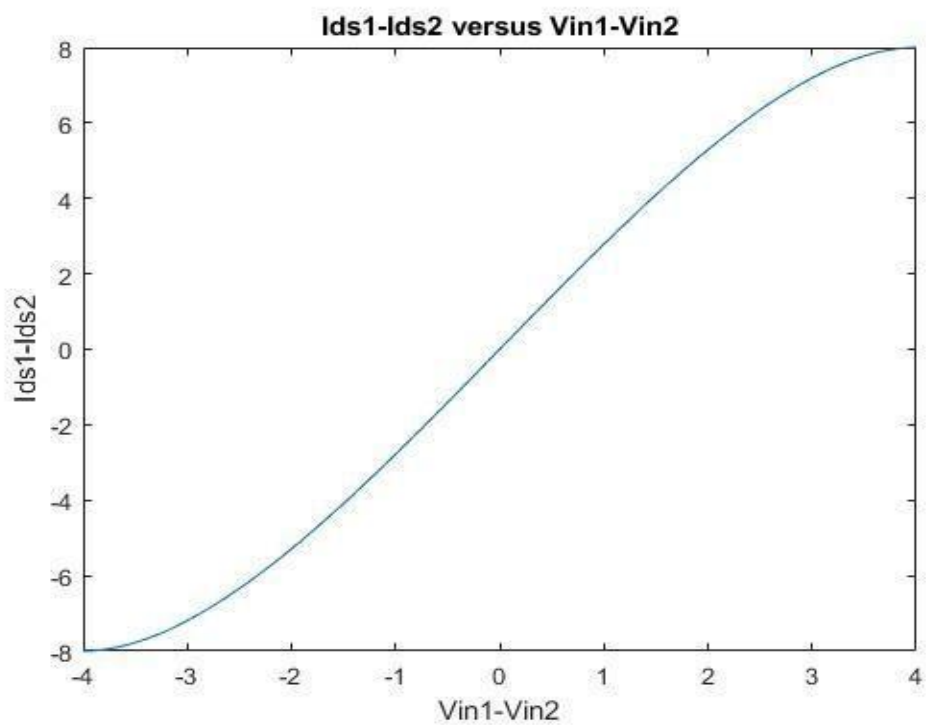
$$16 = (V_{GS} - 1)^2$$

$$\underline{\underline{V_{GS} = 5V}}$$

Question 1B-II



Question 1B-III



Question 1B-IV

1B (5V)

Assuming M_1 & M_2 are in sat region

$$I_D = \frac{k'}{2} (V_{GS} - V_T)^2$$

$$V_{GS} = \sqrt{\frac{2I_D}{k'}} + V_T$$

$$V_{GS1} = \sqrt{\frac{2I_{D1}}{k'}} + V_T$$

$$V_{GS2} = \sqrt{\frac{2I_{D2}}{k'}} + V_T$$

$$V_{GS1} - V_{GS2} = \sqrt{\frac{2I_{D1}}{k'}} - \sqrt{\frac{2I_{D2}}{k'}}$$

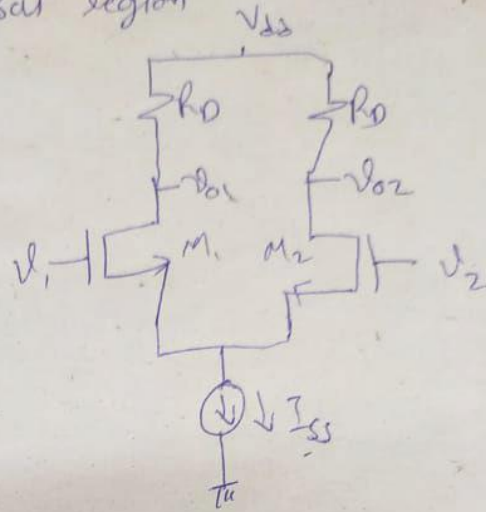
$$V_{GS1} (V_1 - V_S) - (V_2 - V_S) = \sqrt{\frac{2}{k'}} (\sqrt{I_{D1}} - \sqrt{I_{D2}})$$

$$(V_1 - V_2)^2 = \frac{2}{k'} [I_{D1} + I_{D2} - 2\sqrt{I_{D1}I_{D2}}]$$

$$V_d^2 = \frac{2}{k'} \left[I_{SS} - \sqrt{(I_{D1} + I_{D2})^2 - (I_{D1} - I_{D2})^2} \right]$$

$$\frac{k'}{2} V_d^2 - I_{SS} = -\sqrt{I_{SS}^2 - (I_{D1} - I_{D2})^2}$$

$$(I_{D1} - I_{D2})^2 = I_{SS}^2 - \left(I_{SS} - \frac{k'}{2} V_d^2 \right)^2$$



$$I_{d1} - I_{d2} = \sqrt{k' I_{SS} v_d^2 - \left(\frac{k'}{2}\right)^2 v_d^4}$$

$$v_{o1} = v_{d1} - I_{d1} R_D \quad v_{o2} = v_{d2} - I_{d2} R_D$$

$$v_{o1} - v_{o2} = R_D (I_{d2} - I_{d1})$$

$$v_o = -R_D \sqrt{k' I_{SS} v_d^2 - \left(\frac{k'}{2}\right)^2 v_d^4}$$

$$v_o = -R_D \sqrt{k' I_{SS} v_d^2} \left(1 - \frac{k' v_d^2}{4 I_{SS}}\right)^{1/2}$$

For $R_D = 10 \text{ k}\Omega$, $I_{SS} = 8 \text{ mA}$, $k' = 1 \text{ mA/V}^2$

$$v_o = v_d \left[-10 \text{ k} \sqrt{1 \text{ mA} \times 8 \text{ mA}} \left(1 - \frac{1 \text{ mA} v_d^2}{4 \times 8 \text{ mA}}\right)^{1/2} \right]$$

$$v_o = v_d \left[-28.28 \left(1 - \frac{v_d^2}{32}\right)^{1/2} \right]$$

after expanding root with Taylor series we get

→ first ~~order~~ harmonic gain $A_{1m} = -28.28$

Second harmonic gain = 0