

EE 204-2018-2 Analog Circuits

Homework #3 Solution

Question 1:

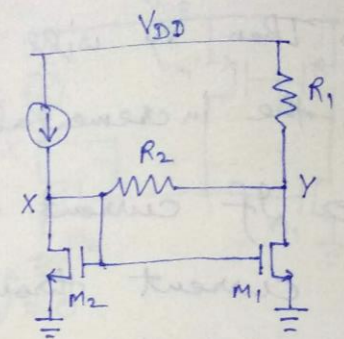
For each circuit shown below, sketch V_X and V_Y as a function of I_{REF} .

Q1 (a)

Here,

If we apply KCL at node X and node Y, then

At node X,



$$-I_{REF} + \frac{K}{2} (V_{GS2} - V_T)^2 + \frac{V_X - V_Y}{R_2} = 0$$

$$-I_{REF} + \frac{K}{2} (V_X - V_T)^2 + \frac{V_X - V_Y}{R_2} = 0 \quad \left[\because V_X = V_{GS2} = V_{GS1} \right] \quad \text{--- (1)}$$

At node Y,

$$\frac{K}{2} (V_X - V_T)^2 + \frac{V_Y - V_X}{R_2} + \frac{V_Y - V_{DD}}{R_1} = 0$$

$$\frac{V_Y}{R_2} + \frac{V_Y}{R_1} = \frac{V_X}{R_2} + \frac{V_{DD}}{R_1} - \frac{K}{2} (V_X - V_T)^2$$

$$V_Y = \frac{R_1 R_2}{R_1 + R_2} \left[\frac{V_{DD}}{R_1} + \frac{V_X}{R_2} - \frac{K}{2} (V_X - V_T)^2 \right] \quad \text{--- (2)}$$

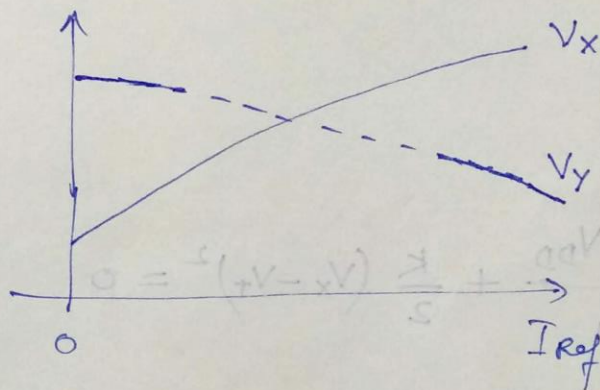
Put equation (2) in (1), then

$$-I_{REF} + \frac{K}{2} (V_X - V_T)^2 + \frac{V_X}{R_2} - \frac{R_1}{R_1 + R_2} \left[\frac{V_{DD}}{R_1} + \frac{V_X}{R_2} - \frac{K}{2} (V_X - V_T)^2 \right] = 0$$

$$\frac{K}{2} (V_X - V_T)^2 \left(1 + \frac{R_1}{R_1 + R_2} \right) + V_X \left[\frac{1}{R_2} - \frac{R_1}{R_2(R_1 + R_2)} \right]$$

$$= \frac{V_{DD}}{R_1 + R_2} + I_{Ref} \quad \text{--- (3)}$$

from equation (2) and (3), we can conclude that if I_{Ref} increases, then V_X also increases. And if V_X increases, then V_Y decreases effectively.



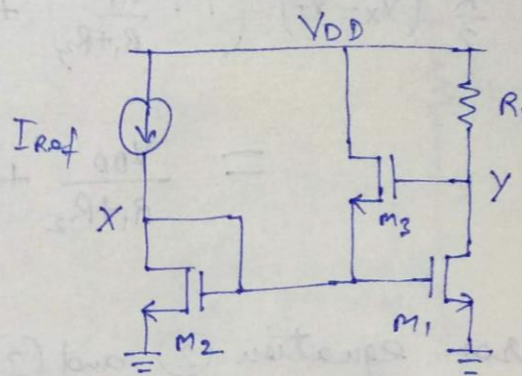
Note \rightarrow If ~~we~~ we see the circuit intuitively,

- ~~\rightarrow If I_{Ref} increases,~~
- \rightarrow It is a current mirror circuit.
- \rightarrow If I_{Ref} increases, it will increase the voltage at node X.
- \rightarrow $V_X = V_{gs1}$, so current through M_1 will also increase due to V_X .
- \rightarrow To maintain the incremental current through M_1 , V_Y should decrease.

Q1 (b)

Here,

We are applying
KCL at node X and
node Y.



At node X,

$$-I_{ref} + \frac{K}{2} (V_X - V_T)^2 - \frac{K}{2} (V_Y - V_X)^2 = 0 \quad \text{--- (1)}$$

At node Y,

$$\frac{V_Y - V_{DD}}{R_1} + \frac{K}{2} (V_X - V_T)^2 = 0$$

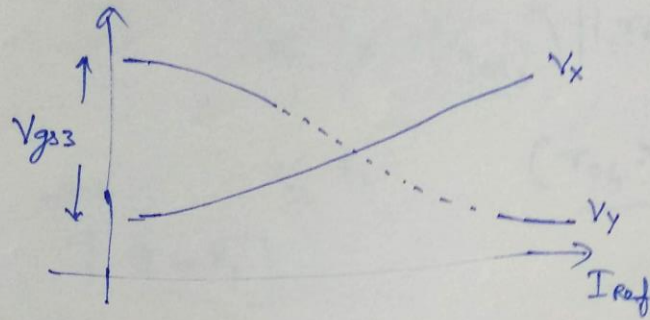
$$V_Y = V_{DD} - \frac{KR_1}{2} (V_X - V_T)^2 \quad \text{--- (2)}$$

Put equation (2) ~~at node~~ in (1), then we get

$$I_{ref} = \frac{K}{2} (V_X - V_T)^2 - \frac{K}{2} \left[V_{DD} - \frac{KR_1}{2} (V_X - V_T)^2 - V_X \right]^2 \quad \text{--- (3)}$$

In equation (3), if I_{ref} is increasing, then to maintain the equality, V_X should increase.

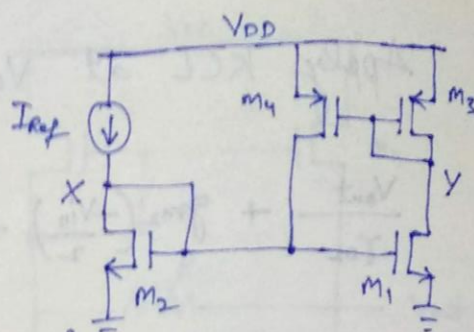
In equation (2), if V_x increases, then V_y will decrease.



→ Here, you can apply same intuition as Q 1(a).

Q1(c)

Apply KCL at X,



$$-I_{ref} + \frac{k}{2} (V_X - V_T)^2 - \frac{k}{2} (V_{DD} - V_Y - V_T)^2 = 0$$

$$I_{ref} = \frac{k}{2} (V_{DD} - V_Y - V_T)^2 - \frac{k}{2} (V_X - V_T)^2 \quad \text{--- (1)}$$

Apply KCL at Y,

$$-\frac{k}{2} (V_{DD} - V_Y - V_T)^2 + \frac{k}{2} (V_X - V_T)^2 = 0$$

$$(V_{DD} - V_Y - V_T)^2 = (V_X - V_T)^2 \quad \text{--- (2)}$$

Put equation (2) in (1),

$$I_{ref} = \frac{k}{2} (V_X - V_T)^2 - \frac{k}{2} (V_X - V_T)^2 = 0$$

⇒ Now we will solve this circuit by intuition.

↳ This is the positive feedback circuit with back to back current mirror.

→ If I_{ref} increases, V_X will increase.

→ V_X will increase the current through M_1 .

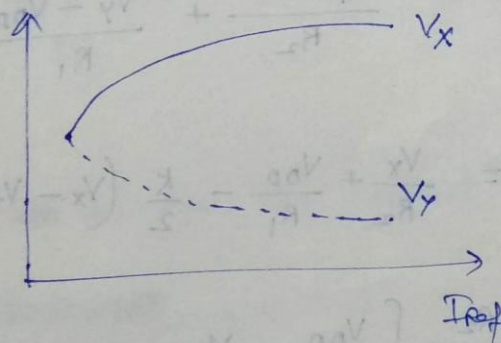
and some ~~more~~ increase in M_3 due to same branch.

→ Then V_Y will decrease slightly to maintain the incremental current.

→ If current through M_3 increases, then current through M_4 increases and it will increase the voltage at node X .

→ Voltage at node Y will start decrease again and so on.

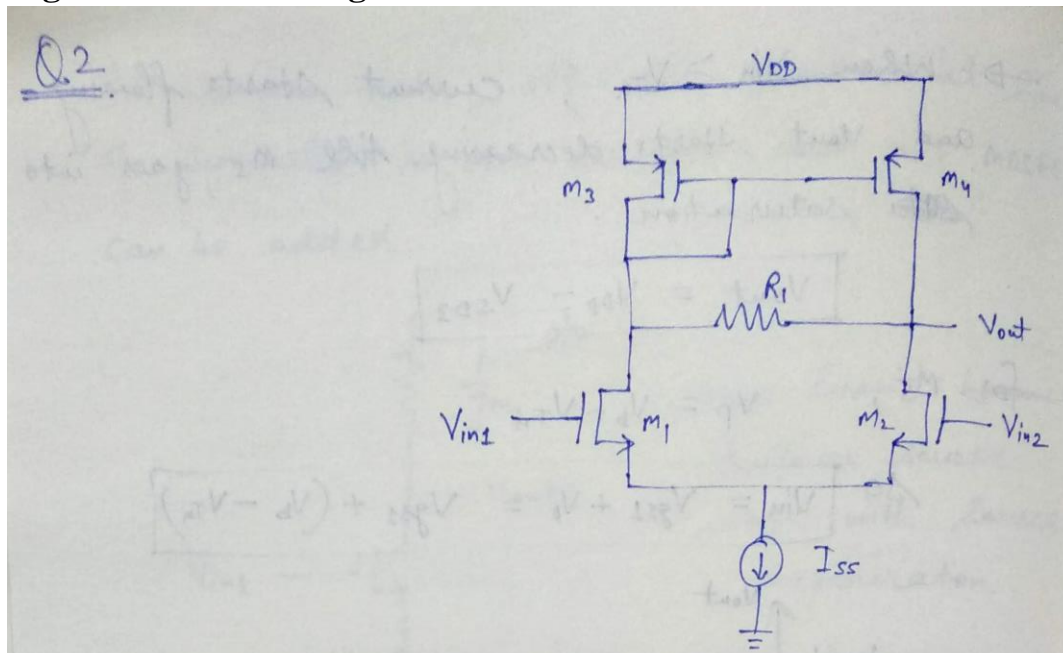
→ If V_X becomes so high, then M_1 & M_4 go in triode region.



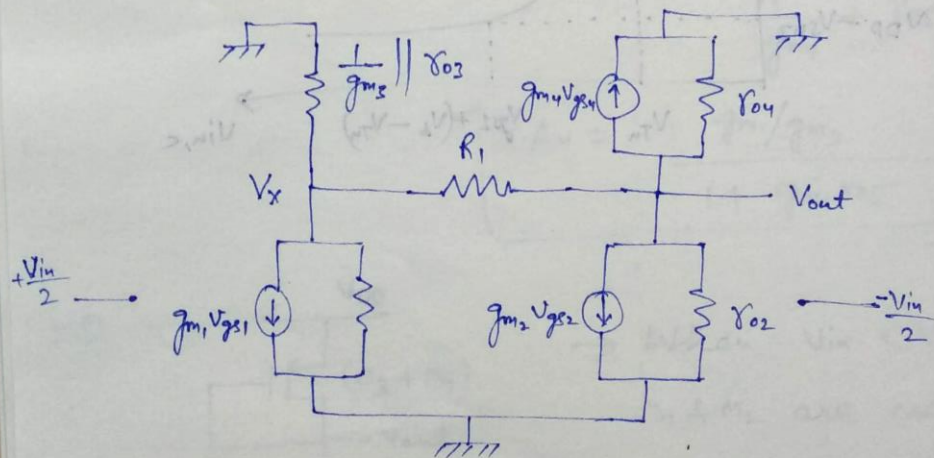
If V_X and V_Y are initially same.

Question 2:

Calculate the gain of the following circuit.



Small signal equivalent circuit



Apply KCL at V_x ,

$$\frac{V_x}{\frac{1}{g_{m3}} \parallel r_{o3}} + \frac{V_x - V_{out}}{R_1} + \frac{V_x}{r_{o1}} + g_{m1} \frac{V_{in}}{2} = 0$$

$$V_x = \frac{-g_{m1} \frac{V_{in}}{2} + \frac{V_{out}}{R_1}}{\frac{1}{R_1} + \frac{1}{r_{o1}} + \left(\frac{1}{g_{m3}} \parallel r_{o3} \right)} \quad \text{--- (1)}$$

Apply KCL at V_{out} ,

$$\frac{V_{out}}{r_{o2}} + g_{m2} \left(-\frac{V_{in}}{2} \right) + \frac{V_{out} - V_X}{R_1} + \frac{V_{out}}{r_{o4}} + g_{m4} V_X = 0$$

$$V_{out} \left[\frac{1}{r_{o2}} + \frac{1}{R_1} + \frac{1}{r_{o4}} \right] = g_{m2} \frac{V_{in}}{2} + V_X \left[\frac{1}{R_1} - g_{m4} \right] \quad \text{--- (2)}$$

Put equation (1) in (2), then we get

$$V_{out} \left[\frac{1}{r_{o2}} + \frac{1}{R_1} + \frac{1}{r_{o4}} \right] = g_{m2} \frac{V_{in}}{2} + \left[\frac{1}{R_1} - g_{m4} \right] \left[\frac{-g_{m1} \frac{V_{in}}{2} + \frac{V_{out}}{R_1}}{\frac{1}{R_1} + \frac{1}{r_{o1}} + \left(\frac{1}{g_{m3}} \parallel r_{o3} \right)} \right]$$

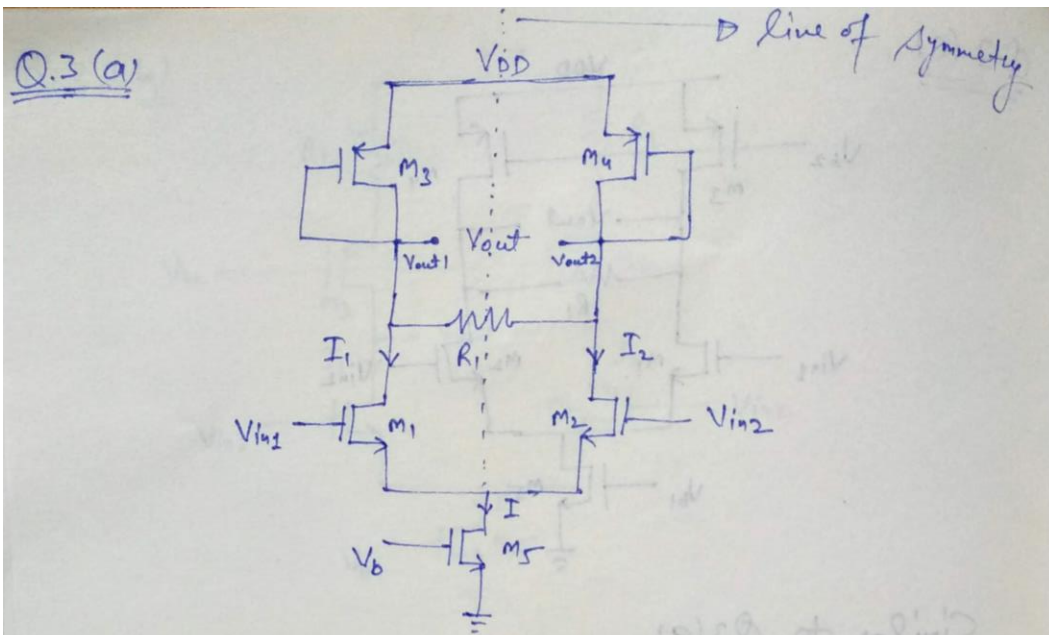
By simplification,

$$V_{out} \left[\frac{1}{r_{o2}} + \frac{1}{R_1} + \frac{1}{r_{o4}} - \frac{\frac{1}{R_1} (\frac{1}{R_1} - g_{m4})}{\frac{1}{R_1} + \frac{1}{r_{o1}} + \left(\frac{1}{g_{m3}} \parallel r_{o3} \right)} \right] = V_{in} \left[\frac{\frac{g_{m2}}{2} - \frac{g_{m1}}{2} \left[\frac{1}{R_1} - g_{m4} \right]}{\frac{1}{R_1} + \frac{1}{r_{o1}} + \left(\frac{1}{g_{m3}} \parallel r_{o3} \right)} \right]$$

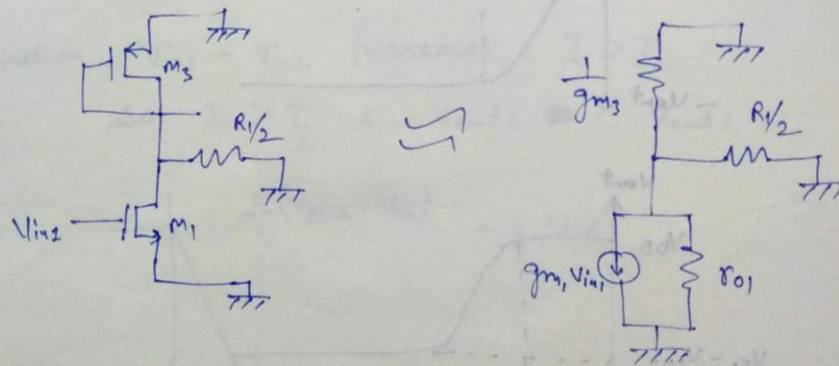
$$A_v = \frac{V_{out}}{V_{in}} = \frac{\frac{\frac{g_{m2}}{2} - \frac{g_{m1}}{2} \left(\frac{1}{R_1} - g_{m4} \right)}{\frac{1}{R_1} + \frac{1}{r_{o1}} + \left(\frac{1}{g_{m3}} \parallel r_{o3} \right)}}{\frac{1}{r_{o2}} + \frac{1}{R_1} + \frac{1}{r_{o4}} - \frac{\frac{1}{R_1} (\frac{1}{R_1} - g_{m4})}{\frac{1}{R_1} + \frac{1}{r_{o1}} + \left(\frac{1}{g_{m3}} \parallel r_{o3} \right)}}$$

Question 3:

Assuming all of the circuits shown in figure below are symmetric, sketch V_{out} as (a) V_{in1} and V_{in2} vary differentially from zero to V_{DD} , and (b) V_{in1} and V_{in2} are equal and they vary from zero to V_{DD} .



This circuit is symmetrical, so AC potential at line of symmetry would be zero.



Differential gain is

$$A_v = g_{m1} \left(\frac{1}{g_{m3}} \parallel R_{01} \parallel R_{1/2} \right)$$

To plot the graph, initially we take $V_{in1} = V_{in2}$

$$V_{id} = V_{in1} - V_{in2} = 0$$

If $V_{in1} = V_{in2}$, then $I_1 = I_2 = \frac{I}{2}$

→ $V_{out} = 0$ because $V_{out1} = V_{out2}$

⇒ As $V_{in1} - V_{in2}$ increases, $I_1 > I_2$

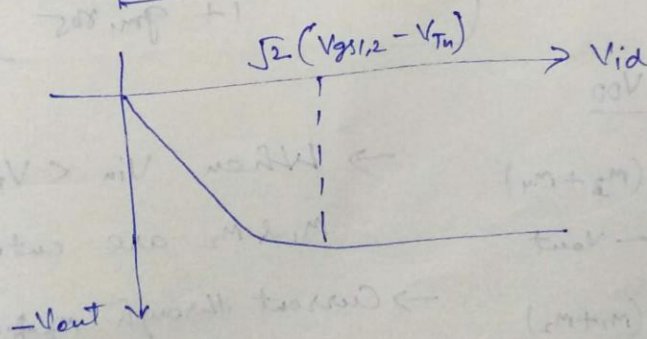
So $I_1 > \frac{I}{2}$

and $V_{out1} < V_{out2}$

then V_{out} will start decreasing.

→ After certain point, $I_2 = 0$ & M_2 goes in cut-off region. Now

$I_1 = I$ and V_{out} becomes constant



⇒ When $V_{in1} = V_{in2}$, $I_1 = I_2 = \frac{I}{2}$

$$\frac{I}{2} = \frac{k}{2} (V_{gs1,2} - V_{tn})^2$$

$$V_{gs1,2} - V_{tn} = \sqrt{\frac{I}{k}}$$

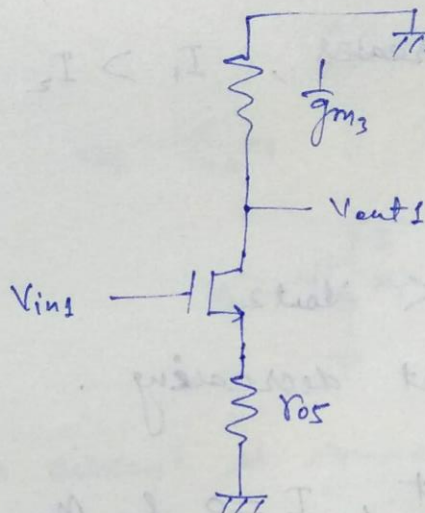
When $I_1 = I$

$$I = \frac{k}{2} (V_{gs1} - V_{tn})^2$$

$$V_{gs1} - V_{tn} = \sqrt{\frac{2I}{k}}$$

$$V_{gs1} - V_{tn} = \sqrt{2} (V_{gs1,2} - V_{tn})$$

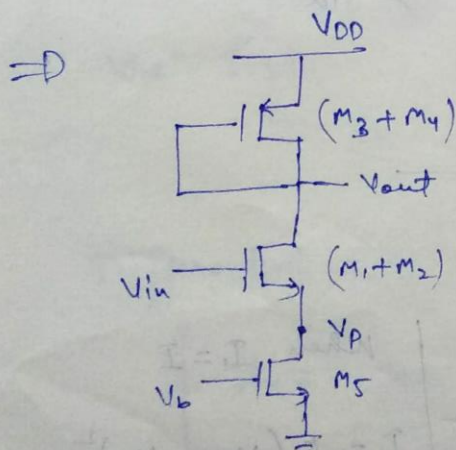
In common mode, all node potentials at line of symmetry is open circuit and all MOSFETs can be added.



New circuit becomes common source stage with source degeneration.

$$A_v = \frac{\frac{1}{g_{m3}}}{\frac{1}{g_{m1}} + r_{OS}}$$

$$A_v = \left[\frac{g_{m1}/g_{m3}}{1 + g_{m1} r_{OS}} \right]$$



\rightarrow When $V_{in} < V_{Tn}$
 M_1 & M_2 are cutoff.

\rightarrow Current through M_3 & M_4 ,

$$I_D = \frac{k}{2} (V_{SG} - V_{TP})^2 = 0$$

$$V_{SG} = V_{TP}$$

$$V_{DD} - V_{out} = V_{TP}$$

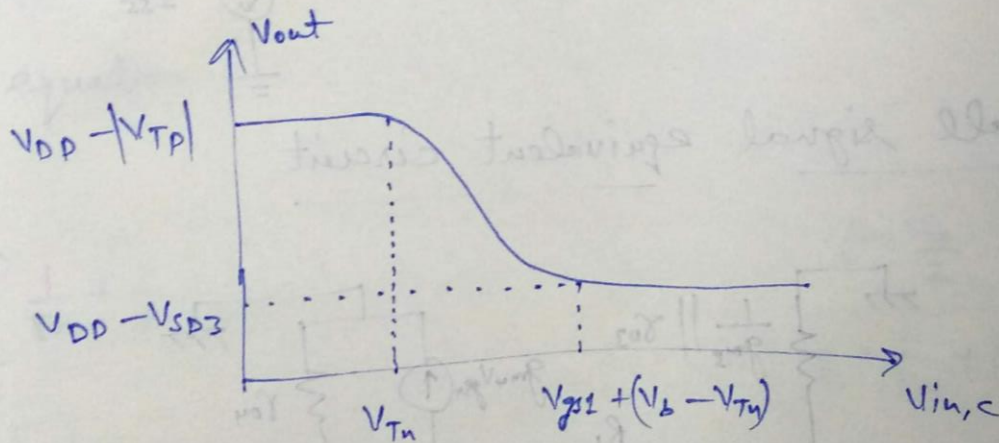
$$V_{out} = V_{DD} - V_{TP}$$

→ When $V_{in} > V_{Tn}$, current starts flowing.
and V_{out} starts decreasing till M_5 goes into
~~the~~ saturation.

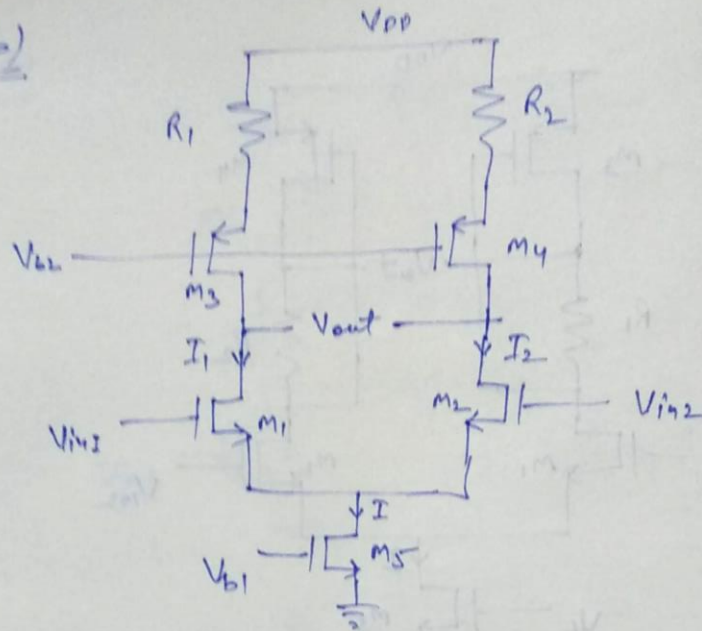
$$V_{out} = V_{DD} - V_{SD3}$$

for M_5 , $V_p = V_b - V_{Tn}$

$$\text{so } V_{in} = V_{gs1} + V_p = V_{gs1} + (V_b - V_{Tn})$$



Q3 (b)

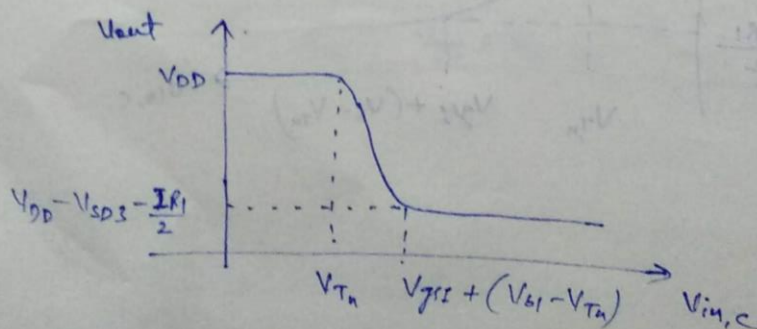
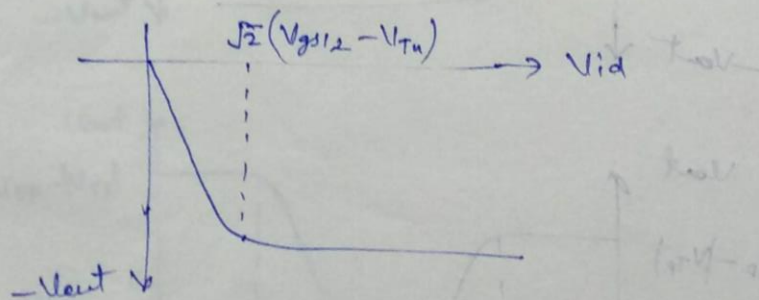


Similar to Q3(a),

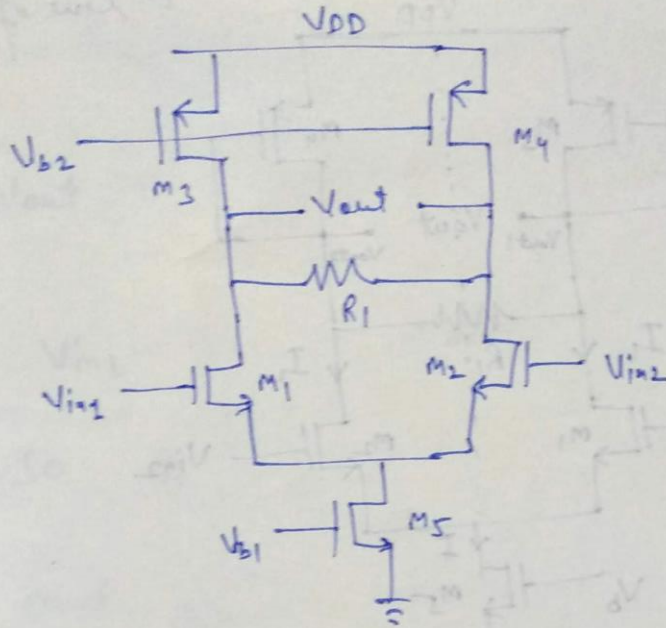
When $V_{in1} = V_{in2}$, then $I_1 = I_2 = \frac{I}{2}$
and $V_{out} = 0$

When $V_{in1} - V_{in2}$ increases, $I_1 > I_2$

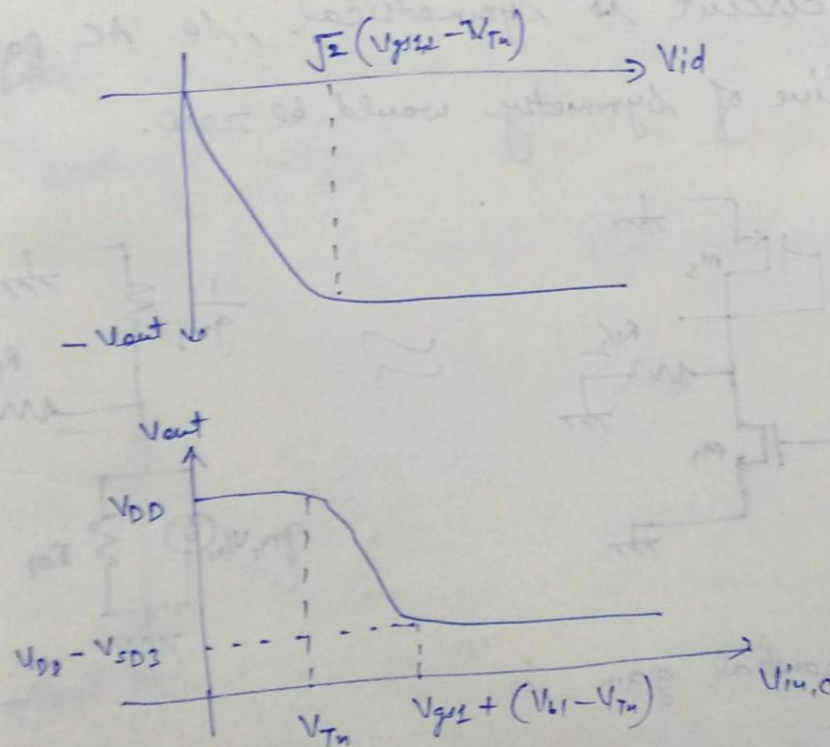
So $I_1 > \frac{I}{2}$ & $V_{out1} < V_{out2}$



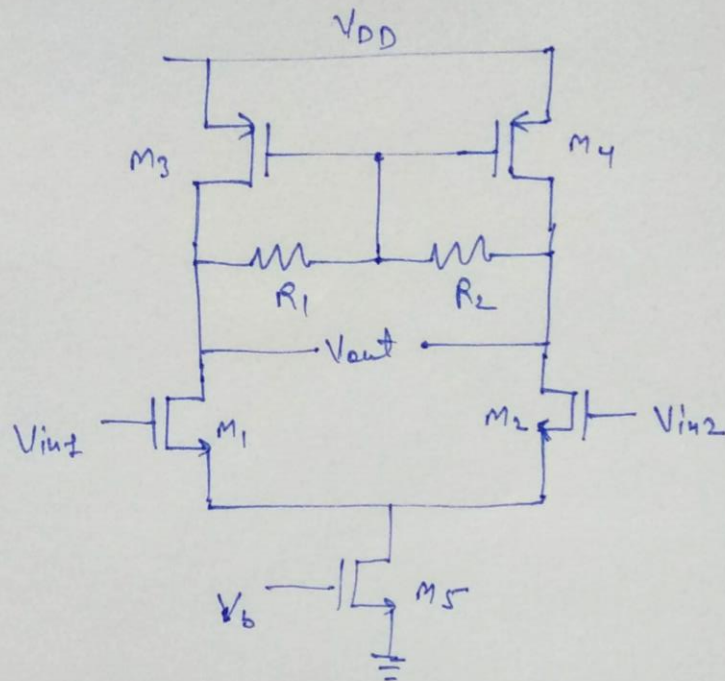
Q3 (c)



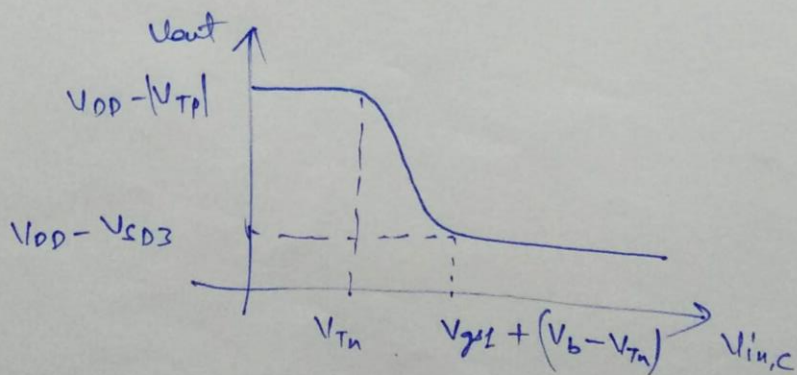
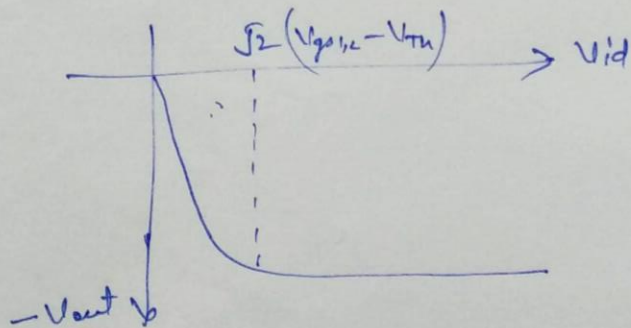
Similar to Q3(a),



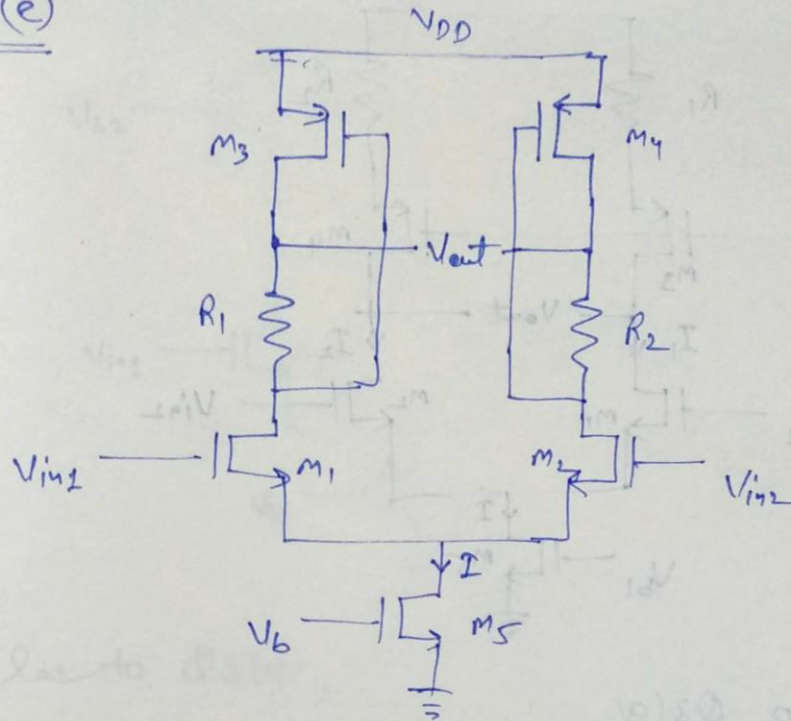
Q3 (d)



Similar to Q3 (a),



Q3 (e)



Similar to Q3(a)

