

# Example Homework Assignment

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## 1 Problem 20.2-1

Solute A is diffusing at unsteady state into a semi-infinite medium of pure B and undergoes a first-order reaction with B. Solute A is dilute. Calculate the concentration  $c_A$  at points  $z = 0, 4$ , and  $10$  mm from the surface for  $t = 1 \times 10^5$  s. Physical property data are  $D_{AB} = 1 \times 10^{-9}$  m<sup>2</sup>/s,  $k' = 1 \times 10^{-4}$  s<sup>-1</sup>,  $c_{A0} = 1.0$  kg mol/m<sup>3</sup>. Also calculate the kg mol absorbed/m<sup>2</sup>. The concentration of A at point  $z$  is given by equation (1) (corrected version),

$$\begin{aligned} \frac{C_A}{C_{A0}} = & \frac{1}{2} \exp(-z\sqrt{k'/D_{AB}}) * \operatorname{erfc}\left(\frac{z}{2\sqrt{tD_{AB}}} - \sqrt{k't}\right) \\ & + \frac{1}{2} \exp(z\sqrt{k'/D_{AB}}) * \operatorname{erfc}\left(\frac{z}{2\sqrt{tD_{AB}}} + \sqrt{k't}\right) \end{aligned} \quad (1)$$

Equation (1) was incorrect in the textbook, and has been modified according to the instructor's email.

```
u = symunit;
t = 1e5 * u.s;
D_AB = 1e-9 * u.m^2 / u.s;
k_prime = 1e-4 * u.s^-1;
```

```

C_A0 = 1.0 * (u.kg * u.mol) / (u.m^3);
C_A = @(z) C_A0 * ...
    (0.5*exp(-z*sqrt(k_prime/D_AB))*erfc((z/(2*sqrt(t*D_AB))) - sqrt(k_prime*t)) + ...
    0.5*(exp(z*sqrt(k_prime/D_AB))*erfc((z/(2*sqrt(t*D_AB))) + sqrt(k_prime*t))));
disp(unitString(C_A(0), 'C_A (0 mm)'))
disp(unitString(C_A(0.004 * u.m), 'C_A (4 mm)'))
disp(unitString(C_A(0.010 * u.m), 'C_A (10 mm)'))

C_A (0 mm): 1 (kg*mol)/m^3
C_A (4 mm): 0.28226 (kg*mol)/m^3
C_A (10 mm): 0.042328 (kg*mol)/m^3

```

The amount of A absorbed per square meter is given by equation (2) (corrected version),

$$Q = C_{A0} \sqrt{D_{AB}/k'} \left[ \left( k't + \frac{1}{2} \right) \operatorname{erf} \sqrt{k't} + \sqrt{k't/\pi} e^{-k't} \right] \quad (2)$$

```

Q = C_A0*sqrt(D_AB/k_prime)*((k_prime*t+0.5)*erf(sqrt(k_prime*t)) + ...
    sqrt((k_prime*t)/pi)*exp(-k_prime*t));
disp(unitString(Q))

Q: 0.033204 (kg*mol)/m^2

```

## 2 Problem 21.1-2

Prove or show the following relationships, starting with the flux equations:

### 2.1 Part a

Convert  $k'_c$  to  $k_y$  and  $k_G$ .

The flux equations involving these coefficients are,

$$N_A = k_c(C_{A1} - C_{A2}) = k_G(p_{A1} - p_{A2}) = k_y(y_{A1} - y_{A2})$$

the conversion between  $k'_c$  and  $k_c$  is given in the flux equation for A diffusing through stagnant, non-diffusing B,

$$\begin{aligned}
 N_A &= \frac{k'_c}{x_{BM}} (C_{A1} - C_{A2}) = k_c (C_{A1} - C_{A2}) \\
 k_c &= \frac{k'_c}{x_{BM}} = \frac{k'_c P}{p_{BM}} \\
 k_y &= \frac{k'_c P}{p_{BM}} \cdot \frac{C_{A1} - C_{A2}}{y_{A1} - y_{A2}} = \frac{k'_c P}{RT \cdot y_{BM}} \\
 k_G &= \frac{k'_c P}{p_{BM}} \cdot \frac{C_{A1} - C_{A2}}{p_{A1} - p_{A2}} = \frac{k'_c P}{RT \cdot p_{BM}}
 \end{aligned}$$

## 2.2 Part b

Convert  $k_L$  to  $k_x$  and  $k'_x$ .

The flux equations involving these coefficients are,

$$N_A = k_L(c_{A1} - c_{A2}) = k_x(x_{A1} - x_{A2})$$

A relationship for  $k_x$  can be found by substituting  $x = c_A/c$ ,

$$k_x = k_L \frac{c_{A1} - c_{A2}}{x_{A1} - x_{A2}} = k_L \frac{c_{A1} - c_{A2}}{\frac{c_{A1}}{c} - \frac{c_{A2}}{c}} = k_L \cdot c$$

$$k'_x = k_x \cdot x_{BM} = k_L \cdot c \cdot x_{BM}$$

## 2.3 Part c

Convert  $k_G$  to  $k_y$  and  $k_c$ .

The flux equations involving these coefficients are,

$$N_A = k_G(p_{A1} - p_{A2}) = k_y(y_{A1} - y_{A2}) = k_c(C_{A1} - C_{A2})$$

By substituting  $p_A = y_A P$ ,

$$k_y = k_G \frac{p_{A1} - p_{A2}}{y_{A1} - y_{A2}} = k_G \frac{y_{A1}P - y_{A2}P}{y_{A1} - y_{A2}} = k_G \cdot P$$

Finally, substituting  $C = P/RT$ ,

$$k_c = k_G \frac{p_{A1} - p_{A2}}{C_{A1} - C_{A2}} = k_G \frac{p_{A1} - p_{A2}}{(p_{A1} - p_{A2})/RT} = k_G \cdot RT$$

## 3 Problem 21.1-3

In a wetted-wall tower an air-  $\text{H}_2\text{S}$  mixture is flowing by a film of water that is flowing as a thin film down a vertical plate. The  $\text{H}_2\text{S}$  is being absorbed from the air to the water at a total pressure of 1.50 atm abs and 30 C. A value for  $k'_c$  of  $9.567 \times 10^{-4}$  m/s has been predicted for the gas-phase mass-transfer coefficient. At a given point, the mole fraction of  $\text{H}_2\text{S}$  in the liquid at the liquid-gas interface is  $2.0(10^{-5})$  and  $p_A$  of  $\text{H}_2\text{S}$  in the gas is 0.05 atm. The Henry's law equilibrium relation is  $p_A(\text{atm}) = 609x_A$  (mole fraction in liquid). Calculate the rate of absorption of  $\text{H}_2\text{S}$ . (Hint: Call point 1 the interface and point 2 the gas phase. Then, calculate  $p_{A1}$  from Henry's law and the given  $x_A$ . The value of  $p_{A2}$  is 0.05 atm.)

The mass transfer coefficient given is  $k'_c$ , which can be converted to  $k_G$  for a flux equation based on partial pressures.

$$k_G = \frac{k'_c P}{RT \cdot p_{BM}}$$

$$N_A = k_G(p_{A1} - p_{A2})$$

```

u = symunit;
P = 1.5 * u.atm;
T = rewrite(30 * u.Celsius, u.K, 'Temperature', 'absolute');
k_c_prime = 9.567e-4 * u.m / u.s;
x_A1 = 2.0e-5;
p_A1 = 609 * x_A1 * u.atm;
p_A2 = 0.05 * u.atm;
p1 = separateUnits(p_A1); p2 = separateUnits(p_A2); p = separateUnits(P);
p_BM = ((p-p1)-(p-p2))/log((p-p1)/(p-p2)) * u.atm;
R = 8.2057338e-5 * (u.m^3 * u.atm) / (u.mol * u.K);
k_G = (k_c_prime * P) / (R * T * p_BM);
N_A = k_G * (p_A1 - p_A2) * 1e-3 * u.kg; % convert to kg-mol
disp(unitString(N_A))

```

```
N_A: -1.4854e-06 (kg*mol)/(m^2*s)
```

## 4 Problem 21.2-1

A fluid is flowing in a vertical pipe and mass transfer is occurring from the pipe wall to the fluid. Relate the convective mass-transfer coefficient  $k'_c$  to the variables  $D$ ,  $\rho$ ,  $\mu$ ,  $v$ ,  $D_{AB}$ ,  $g$ , and  $\Delta\rho$ , where  $D$  is pipe diameter,  $L$  is pipe length, and  $\Delta\rho$  is the density difference.

According to Buckingham's pi theorem, given nine independent variables in three physical dimensions, there are six  $\pi$ -groups to construct.

Vector order: [Length Mass time]

```

D = [1 0 0];
L = [1 0 0];
rho = [-3 1 0];
mu = [-1 1 -1];
v = [1 0 -1];
D_AB = [2 0 -1];
g = [1 0 -2];
delta_rho = [-3 1 0];
k_c_prime = [1 0 -1];

pi_1 = ([D' rho' mu']\-k_c_prime)

```

```
pi_1 =
```

```
1      1      -1
```

$$\pi_1 = \frac{D\rho k'_c}{\mu}$$

$$\text{pi\_2} = ([D' \text{ rho}' \text{ mu}'] \backslash -v')'$$

$$\text{pi\_2} =$$

$$\begin{matrix} 1 & 1 & -1 \end{matrix}$$

$$\pi_2 = \frac{D\rho v}{\mu}$$

$$\text{pi\_3} = ([D' \text{ rho}' \text{ mu}'] \backslash -D_{AB}')'$$

$$\text{pi\_3} =$$

$$\begin{matrix} 0 & 1 & -1 \end{matrix}$$

$$\pi_3 = \frac{\rho D_{AB}}{\mu}$$

$$\text{pi\_4} = ([D' \text{ rho}' \text{ mu}'] \backslash -g')'$$

$$\text{pi\_4} =$$

$$\begin{matrix} 3 & 2 & -2 \end{matrix}$$

$$\pi_4 = \frac{D^3 \rho^2 g}{\mu^2}$$

$$\text{pi\_5} = ([D' \text{ rho}' \text{ mu}'] \backslash -\text{delta\_rho}')'$$

$$\text{pi\_5} =$$

$$\begin{matrix} 0 & -1 & 0 \end{matrix}$$

$$\pi_5 = \frac{\Delta \rho}{\rho}$$

$$\text{pi\_6} = ([D' \text{ rho}' \text{ mu}'] \backslash -L')'$$

$$\text{pi\_6} =$$

$$\begin{matrix} -1 & 0 & 0 \end{matrix}$$

$$\pi_6 = \frac{L}{D}$$

These dimensionless groups can be combined to describe the system. This combination was done pencil-and-paper with a lot of frustration, and the results are shown here.

$$\frac{\pi_1}{\pi_3} = f(\pi_4 \pi_5 \pi_6^3, \pi_2, \pi_3^{-1})$$

$$\frac{k'_c D}{D_{AB}} = f\left(\frac{gL^3 \rho \Delta \rho}{\mu^2}, \frac{Dv\rho}{\mu}, \frac{\mu}{\rho D_{AB}}\right)$$

## 5 Problem 21.3-1

Using the data and physical properties of Example 21.3-2, calculate the flux for a water velocity of 0.152 m/s and a plate length of  $L = 0.137$  m. Do not assume that  $x_{BM} = 1.0$  but actually calculate its value.

The Schmidt and Reynolds numbers can be calculated from the given quantities,

```
u = symunit;
T = rewrite(26.1 * u.Celsius, u.K, 'Temperature', 'absolute');
L = 0.137 * u.m;
v = 0.152 * u.m / u.s;
solubility = 0.02948 * (u.kg * u.mol) / (u.m^3);
D_AB = 1.245e-9 * u.m^2 / u.s;
mu = 8.71e-4 * u.Pa * u.s;
rho = 996 * u.kg / u.m^3;
N_Sc = simplify(mu / (rho * D_AB));
N_Re = simplify((L * v * rho)/mu);
disp(unitString(N_Sc))
disp(unitString(N_Re))
```

```
N_Sc: 702.408 1
N_Re: 23812.5189 1
```

This value for the Reynolds number corresponds to this equation for mass flux,

$$J_D = 0.99 N_{Re,L}^{-0.5} = \frac{k'_c}{v} (N_{Sc})^{2/3}$$

```
syms k_c_prime;
k_c_prime = solve(0.99*N_Re^-0.5 == (k_c_prime/v)*(N_Sc^(2/3)));
FW_water = 18.02 * u.kg / (u.kg * u.mol);
c = rho / FW_water;
x_A1 = 0;
x_A2 = solubility / (solubility + c);
```

```
x_BM = (1 - (1 - x_A2))/log(1/(1 - x_A2));  
k_c = k_c_prime / x_BM;  
N_A = k_c * solubility;  
disp(unitString(N_A))
```

```
N_A: 3.6391e-07 (kg*mol)/(m^2*s)
```

## 6 Referenced Functions

### 6.1 unitString.m

```
function displayString = unitString(quantity, name)  
%UNITSTRING Display a 1x2 sym with symbolic units  
% USAGE: unitString(some_quantity, name)  
% OUTPUT:  
% - displayString: char vector containing name, scalar, and units  
if nargin < 2  
    n = inputname(1);  
else  
    n = name;  
end  
  
[s, U] = separateUnits(quantity);  
formatSpec = '%s: %s %s';  
displayString = sprintf(formatSpec, n, num2str(double(s)), symunit2str(U));  
end
```