Implementing of a simple Heat-Convection Model

Florian Nikos Kitzka

June 6, 2020

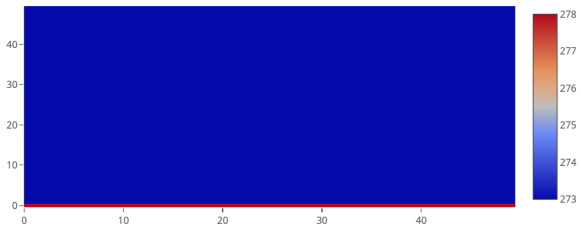
Abstract

The aim of this document is to provide a simple guide how to create and implement a model for a heat-convection problem. Our approach is to start from underlying physics to pose the model-equations and then to explain difficulties arising during implementation. The full implemented result is provided by an external link, which deems to encourage the reader to extend and play with it. We assume basic knowledge of Analysis and Linear Algebra as well as some understanding of Fluid Dynamics. Chapters are written quite independent of each other so that the reader can skip parts in which no interest exist. This all deems as an introduction into the subject. Numerical treatment of Fluid Dynamic belongs to one of the most challenging tasks in numerical mathematics. For the given problem, which is quite easy in each nature our chosen method might work quite satisfactory, but be aware that for other problems much more sophisticated methods are to be taken into consideration.

Contents

1 Simulation Target

We consider a room of cubical shape.
We assume all walls except the bottom to allow transfer of air (open walls).
The bottom is assumed to be heated by the sun-light through radiation.
Our goal is to simulate how this heat is being transferred through the room over time.



2 Creation of Model

There are two main mechanism of heat transfer in nature. One is diffusion the other is advection. We will shortly explain these two mechanisms and how to incorporate this into a model. For a detailed account on this, the reader is referred to standard literature on Fluid Dynamics.

2.1 Heat Diffusion

Consider a volume V with edge length Δx. We denote the temperature at the left surface by T_L and at the right surface by T_R. Then Fourier's law states the heat-flux through left surface is

$$I(x_0) = -\lambda \frac{\partial T}{\partial x}(x_0) \tag{1}$$

and through right surface is

$$I(x_1) = -\lambda \frac{\partial T}{\partial x}(x_1) \tag{2}$$

I is the amount of heat-energy passing per unit of time through unit of area. The coefficient λ depends on the material. Furthermore each material which is

added heat-energy is changing its temperature according to

$$c_p \Delta T = \Delta q$$

q denotes the heat-energy per unit of mass and c_p the specific heat capacity. The later depends on the material. By using the density ρ we can rewrite this as

$$c_p \Delta T = \frac{1}{\rho V} \Delta Q \tag{3}$$

Q denotes the total heat energy added to the volume V. Analogous consideration as done in (1) and (2) can be made for all other surfaces. That is, each surface contributes either positive or negative depending on the direction of flow to the internal change of heat energy per unit of time. We can formulate this by

$$\Delta Q = A \Delta t \sum_j -I_j(x_j + \Delta x) + I_j(x_j)$$

where A denotes the area of a surface, $I_j(x_j)$ the heat-flux through surface S_j and $I_j(x_j + \Delta x)$ the heat-flux through the opposite surface in V. Summation is carried out only over the three surfaces which span the volume. By setting $A = V/\Delta x$ and using equations (1), (2), (3) in the left and right side correspondingly we obtain

$$\rho c_p V \Delta T = \lambda A \Delta t \sum_j \frac{\partial T}{\partial x_j}(x_j + \Delta x) - \frac{\partial T}{\partial x_j}(x_j)$$

By using $V/A = \Delta x$ this equation is equivalent to

$$\rho c_p \frac{\Delta T}{\Delta t} = \frac{\lambda}{\Delta x} \sum_j \frac{\partial T}{\partial x_j}(x_j + \Delta x) - \frac{\partial T}{\partial x_j}(x_j)$$

At the end we can consider the limit $\Delta x \to 0$ to find the heat-diffusion equation

$$\frac{\partial T}{\partial t} = \frac{\lambda}{\rho \alpha} \Delta T \tag{4}$$

Note, ΔT refers to the Laplace operator here ($\Delta T = \nabla \cdot \nabla T$).

2.2 Advection

Advection describes the mechanism a physical property to be transported by a bulk movement. In our example the bulk movement is presented by the wind and the physical property is either momentum or heat.
We consider the same volume V as in previous section and denote the physical (scalar) property by ϕ. Here ϕ shall be given per unit of mass. In addition we denote by $\mathbf{v}$ the current velocity field. At the left surface let us consider the normal directed velocity component v_x. During the interval Δt we have a displacement of mass by

$$\xi_x = v_x \Delta t \tag{5}$$

Thus the net balance of mass flowing into and out of V through the left and right surface is

$$-\rho A \cdot \xi_x \cdot \phi(x + \Delta x) + \rho A \cdot \xi_x \cdot \phi(x) \tag{6}$$

By using (5) and $A = V/\Delta x$ we can write this as

$$\rho v_x \Delta t \cdot V \frac{\phi(x) - \phi(x + \Delta x)}{\Delta x}$$

By letting $\Delta x \to 0$ we obtain

$$-\rho v_x \Delta t \cdot V \frac{\partial \phi}{\partial x}(x)$$

The same consideration can be done in y and z direction to obtain as net change of phi

$$\rho V \Delta \phi = -\rho V \Delta t \left(v_x \frac{\partial \phi}{\partial x} + v_y \frac{\partial \phi}{\partial y} + + v_z \frac{\partial \phi}{\partial z} \right)$$

Dividing by $\rho V \Delta t$ and letting $\Delta t \to 0$, we obtain

$$\frac{\partial \phi}{\partial t} = -\mathbf{v} \cdot \nabla \phi \tag{7}$$

We can now use this equation to express transport of heat-energy. Heat-energy and temperature are related by $c_p T = u$ where u denotes the inner energy. So what in fact is transported is u and be inserting we get

$$\frac{\partial T}{\partial t} = -\mathbf{v} \cdot \nabla T \tag{8}$$

As for the moment we can do similar considerations but things are little more involved since the velocity is transported so to say by itself. More in detail, when posing the net balance in (6) we instead have to take into account that the moved distance ξ depends on its location. For the left surface we would have $\xi_x = v_x \Delta t$ and for the right one $\xi_{x+\Delta x} = v_{x+\Delta x} \Delta t$. Putting this into equation yields

$$-\rho A \cdot v_{x+\Delta x} \cdot \Delta t \cdot \phi(x + \Delta x) + \rho A \cdot v_x \cdot \Delta t \cdot \phi(x)$$

We can apply a trick and rewrite this as

$$\begin{aligned} &- \rho A \cdot v_{x+\Delta x} \cdot \Delta t \cdot \phi(x + \Delta x) \\ &+ \rho A \cdot v_x \cdot \Delta t \cdot \phi(x + \Delta x) - \rho A \cdot v_x \cdot \Delta t \cdot \phi(x + \Delta x) \\ &+ \rho A \cdot v_x \cdot \Delta t \cdot \phi(x) \end{aligned}$$

Further by putting terms together as

$$\begin{aligned} &\rho A \cdot (v_x - v_{x+\Delta x}) \cdot \Delta t \cdot \phi(x + \Delta x) \\ &+ \rho A \cdot v_x \cdot \Delta t \cdot (\phi(x) - \phi(x + \Delta x)) \end{aligned}$$

By doing analogous reformulation as done to obtain equation (7) we arrive at

$$\frac{\partial \phi}{\partial t} = -\mathbf{v} \cdot \nabla \phi - \phi \nabla \cdot \mathbf{v}$$

Note, since moment applies in all three directions we have to consider as ϕ all three components, v_x, v_y, v_z of velocity. Hence we obtain the following system of equations

$$\frac{\partial \mathbf{v}}{\partial t} = -\mathbf{v} \cdot \nabla \mathbf{v} - \mathbf{v}(\nabla \cdot \mathbf{v})$$

Note, in very generic contexts one also takes the change of density into account, but here we will assume the density to be global constant. Also for our needs it will suffice to assume incrompressibility , that is, $\nabla \cdot \mathbf{v} = 0$. It expresses in essence that all mass flowing into the volume must flow out somewhere else. Out final equation for the moment becomes

$$\frac{\partial \mathbf{v}}{\partial t} = -\mathbf{v} \cdot \nabla \mathbf{v} \tag{9}$$

2.3 Momentum Sources

The initial velocity is assumed to be 0 everywhere. For changes in moment due to Newton it requires a force. For simplification we assume the pressure is in so called static equilibrium. With these assumptions we can obtain at a force which is called buoyancy. It always arises when a region of warmer fluid is surrounded by colder fluid. It only applies in vertical direction and can be formulated it terms of an acceleration as

$$\mathbf{F}_B = g \frac{T - T_A}{T_A} \mathbf{e}_z \tag{10}$$

Here g denotes the gravity acceleration and T_A the surrounding temperature. For a detailed derivation see standard literature in Fluid Dynamics. Note, in our implementation we will assume this T_A is just given by the temperature above the considered grid-point.

2.4 Final Model

A final very simplified model looks like this

$$\begin{aligned} \frac{\partial T}{\partial t} &= -\mathbf{v} \cdot \nabla T + \frac{k}{\rho \alpha} \Delta T \\ \frac{\partial v_z}{\partial t} &= g \frac{T - T_A}{T_A} - v_z \frac{\partial v_z}{\partial z} \end{aligned} \tag{11}$$

Although we could restrict computation on dimension 1 we will do it for dimension 2 in order to get more inside into the used techniques.

3 Numerical Scheme

In order to solve the model equations (11) numerically we are going to use the so called Finite Difference Method. This requires to lay a fixed grid over our domain (the room) and replace all derivative expressions by discrete approximations.
Moreover, as we have seen in section 2, physical properties like heat and momentum are transported by diffusion and advection processes.
Our goal in this section is to provide a generic scheme for both mechanisms. Hereby we are going to consider both processes independent of each other and restrict attention to the 1-dimensional case. It will turn out later that this treatment is already sufficient for the final implementation.

3.1 Derivative Approximations

The main method to obtain such approximations for derivatives is using Taylor expansion. We give a detailed description for one specific derivative expression but leave the remaining for the reader since they are produced in analogy.
Also, for reasons becoming clear later, we restrict our attention to 1-dimensional functions. Consider the two Taylor expansions,

$$u(x+h) = u(x) + u'(x)h + \frac{1}{2}u''(x)h^2 + o(2)$$

$$u(x-h) = u(x) - u'(x)h + \frac{1}{2}u''(x)h^2 + o(2)$$

By adding both equations we obtain

$$u(x+h) + u(x-h) = 2u(x) + u''(x)h^2$$

By solving the later for $u''(x)$ we get a second-order approximation for the second derivative of u.

$$u''(x) = \frac{1}{h^2}(u(x+h) + u(x-h) - 2u(x)) + o(2)$$

For the numerical treatment we have to consider u discrete in space and time. We define

$$u_i^n = u(t_n, x_i)$$

or in case of 2-dimensions

$$u_{i,j}^n = u(t_n, x_i, y_j)$$

With this we can now easily list the approximations we are going to use, especially the one we just obtained for second-order derivatives.

$$\left[\frac{\partial u}{\partial t}\right]_i^n \approx \frac{1}{\Delta t}(u_i^{n+1} - u_i^n)$$

$$\left[\frac{\partial u}{\partial x}\right]_i^n \approx \frac{1}{\Delta x}(u_i^n - u_{i-1}^n) \tag{12}$$

$$\left[\frac{\partial u}{\partial x}\right]_i^n \approx \frac{1}{\Delta x}(u_{i+1}^n - u_i^n) \tag{13}$$

$$\left[\frac{\partial^2 u}{\partial x^2}\right]_i^n \approx \frac{1}{\Delta x^2}(u_{i-1}^n - 2u_i^n + u_{i+1}^n)$$

For first derivative we have provided two approximations, (13) is called forward in space and (12) is called backward in space.

Note, we only present a small selection of possible ways to approximate derivatives. Also, since this article deems as an introduction we only focused on explicit schemes, but the reader should be aware there exists another important category of so called implicit schemes. For a more comprehensive list and treatment the reader is referred to standard literature of finite difference method.

3.2 Advection Scheme

In general advaction processes have the form

$$\frac{\partial u}{\partial t} = -c\frac{\partial u}{\partial x} + S$$

Here S denotes a possible source term for the property u.
By using approximations for derivatives as given in section 3.1 we can formulate the following scheme:

For positive velocity ($c \geq 0$):

$$u_i^{n+1} = u_i^n - c\frac{\Delta t}{\Delta x}(u_i^n - u_{i-1}^n) + S_i^n \tag{14}$$

For negative velocity:

$$u_i^{n+1} = u_i^n - c\frac{\Delta t}{\Delta x}(u_{i+1}^n - u_{i-1}^n) + S_i^n \tag{15}$$

The reason for splitting the scheme based on the direction of velocity becomes clear in section 3.4.

3.3 Diffusion Scheme

Diffusion processes are of the form

$$\frac{\partial u}{\partial t} = \alpha\frac{\partial^2 u}{\partial x^2}$$

and again by using derivative approximations from section 3.1 we formulate the following scheme:

$$u_i^{n+1} = u_i^n + \alpha \frac{\Delta t}{\Delta x^2}(u_{i-1}^n - 2u_i^n + u_{i+1}^n) \tag{16}$$

3.4 Stability

One of the most important things with the use of approximation schemes is to ensure stability. Actually one could argue that since we have justified all our derivative approximations by Taylor-expansions we are ready and can blindly implement the discrete equations into a computer-system. This approach turns out to be too naive.
In general each computation is accompanied with rounding errors. Although these can be very small they can sum-up drastically when we have to repeat calculations iterative. Our scheme has the form

$$u_{n+1} = A(u_n) \tag{17}$$

where A is some linear function.
If we assume the u_n's to be computed without rounding errors (hypothetically), and our 'realistic' calculated values are $\tilde{u}_n$ then we have

$$\tilde{u}_n = u_n + \epsilon_n \tag{18}$$

where ϵ_n denotes the deviation of step n. Therefore instead of (17) we actually deal with

$$u_{n+1} + \epsilon_{n+1} = A(u_n + \epsilon_n) \tag{19}$$

We observe, at step n we obtained a deviated solution which we use to compute step $n+1$. Thus at step $n+1$ we are faced to the rounding error made in this step and the fact that we were actually using the deviated solution, $u_n + \epsilon_n$, as input. So the very important question arises: How does the ϵ_n's evolve over time?
Combining equations (17), (19) and using linearity of A we obtain

$$\epsilon_{n+1} = A(\epsilon_n) \tag{20}$$

This gives us a direct relation between errors at different steps. The striking idea is to formulate a scheme, that is choose A, so that for all n

$$|\epsilon_{n+1}| \leq |\epsilon_n| \tag{21}$$

Note, if above equation holds, then we can be sure that although we still have to face rounding errors, the fact that we use a deviated version, $u_n + \epsilon_n$, as input in step $n+1$ does not impact the overall outcome of the iteration.
In order to show a given scheme to fulfill (21) we use a method invented by John von Neumann.

The idea behind this is to assume the errors can be approximated (or estimated) by a Fourier-expansion

$$\epsilon(t,x) = e^{at}\sum_k e^{jkx} \tag{22}$$

In other words, some function which decreases or increases exponentially in time. Our aim is to find a scheme A which enforces $a < 0$ in above representation of $\epsilon(t,x)$.

3.4.1 Diffusion Scheme

We replace $\epsilon(t,x)$ in equation (21) by using for A the scheme given in (16). Since A is linear we can restrict attention to one specific index k in (22) to obtain

$$e^{a(t+\Delta t)}e^{jkx_i} = e^{at}e^{jkx_i} + \alpha\frac{\Delta t}{\Delta x^2}\left(e^{at}e^{jk(x_i-\Delta x)} - 2e^{at}e^{jkx_i} + e^{at}e^{jk(x_i+\Delta x)}\right)$$

Note the we have used $x_{i-1} = x_i - \Delta x$, $x_{i+1} = x_i + \Delta x$ and $\epsilon(t_{n+1}, x_i) = \epsilon(t_n + \Delta t, x_i)$.
Further by canceling out factors on both sides we get

$$e^{a\Delta t} = 1 + \alpha\frac{\Delta t}{\Delta x^2}\left(e^{-jk\Delta x} - 2 + e^{jk\Delta x}\right)$$

Further by use of Euler's formula the r.h.s can be combined to get

$$e^{a\Delta t} = 1 + \alpha\frac{\Delta t}{\Delta x^2}\left(2cos(k\Delta x) - 2\right)$$

Since the *cos* always has absolute values below 1 we infer a sufficient condition the l.h.s to be lower 1 is $2\alpha\frac{\Delta t}{\Delta x^2} \leq \frac{1}{2}$ or equivalently,

$$\Delta t \leq \frac{1}{4}\frac{\Delta x^2}{\alpha} \tag{23}$$

In other words, in order to ensure our diffusion-scheme to be stable, we have to impose (23) onto our implementation - we cannot choose arbitrary large time steps Δt for given a grid-width Δx.

3.4.2 Advection Scheme

The same steps as above but by using as A the scheme (14) we obtain

$$e^{at} = 1 - c\frac{\Delta t}{\Delta x}\left(1 - e^{-jk\Delta x}\right)$$

We can use the triangle inequality to estimate

$$e^{at} \leq \left|1 - c\frac{\Delta t}{\Delta x}\right| + c\frac{\Delta t}{\Delta x}$$

Note, we have used the known identity $|e^{jy}| = 1$.
From the we can conclude the r.h.s to be lower 1 if $0 \leq c\Delta t/\Delta x \leq 1$ or equivalent

$$\Delta t \leq \frac{\Delta x}{c} \tag{24}$$

For the case of $c < 0$ above consideration would show scheme (14) to never be stable. But if the same steps as above are applied on scheme (15) instead we find the same stability criterion (24).

3.5 Operator and Term Splitting

You might have wondered that our approximation schemes all were targeted at 1-dimensional problems, but our model is formulated in two dimensions. Moreover we have treated diffusion and advection independent of each other whereas in our model they interact with each other.
The secrete behind this is an elegant trick referred as Operator and Term Splitting which allows us in the final implementation to separate dimensions and transport mechanisms. In other words we can implement for each dimension and each transport mechanism a scheme and then combine these schemes with each other.

3.5.1 Dimensional Split

Let us use the advection-scheme as explanatory example. Once understanding the idea, the reader easily can adapt the techniques to other schemes.
We can write scheme (14) in an operator form

$$L_x := id - c\Delta t\delta_x + S$$

Hereby δ_x stands for an operator which takes a function u as argument and returns the approximated first derivative on a given grid, that is

$$\delta_x(u_i) = \frac{u_i - u_{i-1}}{\Delta x}$$

Further id denotes the identity operator

$$id(u_i) = u_i$$

and S a constant operator

$$S(u_i) = S_i$$

With this definitions our scheme (14) can be written as

$$u_i^{n+1} = L_x(u_i^n)$$

In analogy we can define the operator L_y which applies in y-direction

$$L_y := id - c\Delta t\delta_y + S$$

and compute the composition of both

$$L_x \circ L_y = id - c\Delta t\delta_x - c\Delta t\delta_y + o(2) \tag{25}$$

In the later we have skipped terms of order 2 in Δt. The general advaction-process in dimension 2 has the form,

$$\frac{\partial u}{\partial t} = -c_x \frac{\partial u}{\partial x} - c_y \frac{\partial u}{\partial y}$$

We can use derivative approximations from section 3.1 to obtain a scheme in the form

$$u_{i,j}^{n+1} = u_{i,j}^n - c_x \frac{\Delta t}{\Delta x}(u_{i,j}^n - u_{i-1,j}^n) - c_y \frac{\Delta t}{\Delta x}(u_{i,j}^n - u_{i,j-1}^n) \tag{26}$$

Now it is an easy task to verify that

$$L_x \circ L_y(u_{i,j}) = u_{i,j}^n - c_x \frac{\Delta t}{\Delta x}(u_{i,j}^n - u_{i-1,j}^n) - c_y \frac{\Delta t}{\Delta x}(u_{i,j}^n - u_{i,j-1}^n) + o(2)$$

and by comparing with (26) to see that the 2-dimensional scheme coincides up to order 2 with the composition of the 1-dimensional scheme.
Therefore, in our implementation instead of writing the scheme (26) we will first apply the advection scheme (14) for x-direction and on the result we will again apply (14) but in y-direction.

3.5.2 Term Splitting

The idea of term splitting is quite the same as for dimension splitting. But this times the split is done w.r.t different physical processes, that is diffusion and advection.
Like for the advection scheme we can introduce an operator which describes scheme (16)

$$L_d := id + \alpha\Delta t\delta_{xx}$$

whereas

$$\delta_{xx}(u_i) = \frac{u_{i-1} - 2u_i + u_{i+1}}{\Delta x^2}$$

When we compose L_d with L_x from previous section we obtain

$$L_x \circ L_d = id - c\Delta t\delta_x + \alpha\Delta t\delta_{xx} + o(2)$$

A system containing diffusion and advection has in general the form

$$\frac{\partial u}{\partial t} = -c\frac{\partial u}{\partial x} + \alpha\frac{\partial^2 u}{\partial x^2}$$

Again we can use the derivative approximations from section 3.1 to obtain a scheme

$$u_i^{n+1} = u_i^n - c\Delta t\delta_x(u_i^n) + \alpha\Delta t\delta_{xx}(u_i^n) \tag{27}$$

We observe that the composition $L_x \circ L_d$ coincides up to order 2 with above scheme.
So, in implementation instead of writing (27) we will first apply L_d and on the result L_x.

3.6 Final Scheme

In previous sections we were describing things a little bit more general than they actually are in our specific model. Since buoyancy only acts into y-direction we have only the z-component of velocity to have a positive value. Due to our specific boundary conditions we actually could model the entire system in 1-dimension but for educational reasons we do it in 2-dimensions.
How final scheme can be written by using above operator expressions as

$$u_{i,j}^{n+1} = L_x \circ L_{D,y} \circ L_{D,x}(u_{i,j}^n) \tag{28}$$

$L_{D,x}$, $L_{D,y}$ denote the 1-dimensional diffusion operators applied in x-direction resp. y-direction.
This is an explicit scheme which becomes very handy to implement in this form as we will see next.

4 Implementation

This section will explain the important snippets of code which can be found at `https://github.com/applied-math-coding/basic-diffusion-transport`. Implementation is provided in Typescript (by utilizing the package [TODO lina]) and in Python. An online running example can be found here, `https://applied-math-coding.github.io/basic-diffusion-transport/`. We will give detailed explanations for the Python code only. The Typescript code is similar structured and due to the use of [TODO lina] operator implementation are quite straight forward.

Model parameter are defined in the file 'params.py'. We initialize the temperature and velocity field by using three matrices. Note, the matrices include the boundaries:

```
T = np.empty((params.n_grid, params.n_grid))
T.fill(params.T_c)
v_y = np.zeros((params.n_grid, params.n_grid))
v_x = np.zeros((params.n_grid, params.n_grid))
```

We iterate the application of all operators and ensure the results are directly written into above matrices:

```
def simulate():
  t = 0
  while t <= params.duration:
    utils.adjust_boundary(T, v_x, v_y)
    utils.diffusion_x_op(T, alpha, delta_t, delta_x)
    utils.diffusion_y_op(T, alpha, delta_t, delta_x)
    utils.heat_convection_y_op(T, v_y, delta_t, delta_x)
    utils.mom_convection_y_op(T, v_y, delta_t, delta_x)
    utils.adjust_boundary(T, v_x, v_y)
```

```
    t = t+delta_t
```

Each operator is defined in file 'utils.py'. The boundary conditions are ensured by:

```
def adjust_boundary(T, v_x, v_y):
  T[0, :] = params.T_h
  T[-1, :] = T[-2, :]
  T[:, 0] = T[:, 1]
  T[:, -1] = T[:, -2]
  v_y[0, :] = 0
  v_y[-1, :] = v_y[-2, :]
  v_y[:, 0] = v_y[:, 1]
  v_y[:, -1] = v_y[:, -2]
```

In order to implement the operators, instead of using loops we are element-wise combining (adding, ...) matrices which indexes are shifted correspondingly in order to achieve the specific schemes receipt (note how much the implementation resembles the actual scheme's definition):

```
def diffusion_x_op(T, alpha, delta_t, delta_x):
  T[1:-1, 1:-1] = T[1:-1, 1:-1] + alpha * delta_t / \
  pow(delta_x, 2)
    * (T[1:-1, 0:-2]-2*T[1:-1, 1:-1]+T[1:-1, 2:])


def diffusion_y_op(T, alpha, delta_t, delta_x):
  T_cen = T[1:-1, 1:-1]
  T_down = T[0:-2, 1:-1]
  T_up = T[2:, 1:-1]
  T[1:-1, 1:-1] = T_cen + alpha * delta_t / \
  pow(delta_x, 2) * (T_down-2*T_cen+T_up)


def heat_convection_y_op(T, v_y, delta_t, delta_x):
  T_cen = T[1:-1, 1:-1]
  T_down = T[0:-2, 1:-1]
  v_y_cen = v_y[1:-1, 1:-1]
  T[1:-1, 1:-1] = T_cen - delta_t / delta_x * v_y_cen
    * (T_cen-T_down)


def mom_convection_y_op(T, v_y, delta_t, delta_x):
  T_cen = T[1:-1, 1:-1]
  v_y_cen = v_y[1:-1, 1:-1]
  v_y_down = v_y[0:-2, 1:-1]
  T_up = T[2:, 1:-1]
  b = params.g * np.maximum(np.zeros(T_cen.shape),
```

```
(T_cen-T_up)/T_up)
v_y[1:-1, 1:-1] = v_y_cen + delta_t * b - \
delta_t / delta_x * v_y_cen * (v_y_cen-v_y_down)
```

5 Further Reading

This article intends to give an introduction into all treated areas. There are many good books or only tutorials about numerical treatment of partial differential equations. Or if you are more specialized on fluid dynamics you will many good accounts on this field too. In case your are more interested in the implementation side, be encouraged to clone the entire project from `https://github.com/applied-math-coding/basic-diffusion-transport` and to extend or play around.