

**TOPIC COVERED AT A GLANCE**

1. PROOF FOR THE STATEMENT INFINTESIMAL ROTATION ,DEFINED AS A INFINITESIMALLY SMALL AMOUNT OF ANGLE OF ROTATION IS A VECTOR QUANTITY BUT FINITE ROTATION IS NOT A VECTOR QUANTITY BECAUSE IT DO NOT OBEY THE COMMUNICATIVE LAW OF ADDITION, ALTHOUGH POSSEESSING MAGNITUDE , DIRECTIONS AND SENSE.
2. DEFINITION OF ANGULAR VELOCITY AND ANGULAR ACCELERATION.
3. SCHEMATIC REPRESENTATION OF ANGULAR VELOCITY AND ACCELERATION.
4. REPRESENTATION OF DIFFERENT COORDINATE SYSTEMS.
5. SOME VECTOR OPERATIONS.
6. SOME VECTOR OPERATIONS IN DIFFERENT COORDINATE SYSTEMS.
7. LAWS OF MOTIONS IN LINEAR AND PLANE CURVILINEAR MOTION.
8. DERIVATIVES OF UNIT VECTORS.

### Infinitesimal Rotation

Infinitesimal rotation  $d\theta$ , defined as a infinitesimally small amount of the angle of rotation, is a vector quantity.) It is important to note here that finite rotation ' $\theta$ ' is not a vector quantity.) The reason is that the finite rotations  $\theta_1$ , and  $\theta_2$ , although possessing magnitudes, directions and sense, do not obey the commutative law of addition, i.e., )

$$\theta_1 + \theta_2 \neq \theta_2 + \theta_1 \quad (\text{R2.41})$$

This has been demonstrated in Fig. R2.12 where a foot rule is shown subjected to rotations about the  $x$  and  $y$  axes respectively. An initial rotation  $\theta_1 = \pi/2 \mathbf{i}$  about the  $x$ -axis and a subsequent rotation  $\theta_2 = \pi/2 \mathbf{j}$  about the  $y$ -axis bring the sheet into positions (Aa) and (Aab). On the other hand, an initial rotation  $\theta_2 = \pi/2 \mathbf{j}$  about the  $y$ -axis and a subsequent rotation  $\theta_1 = \pi/2 \mathbf{i}$  about the  $x$ -axis result in positions (Ab) and (Aba) as shown. Obviously, the final positions (Aab) and (Aba) are not the

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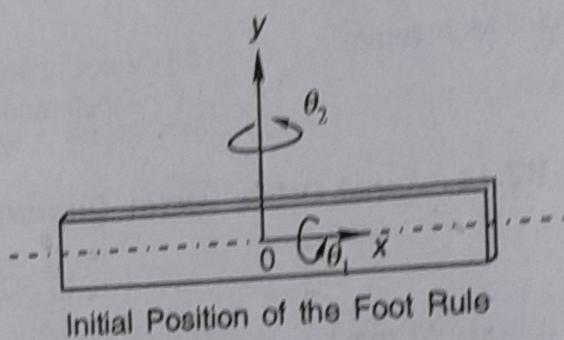
same showing that the commutative law for finite rotations fails; admission disqualifying them from being put under the category of vector quantities.

The case of addition of infinitesimal rotations  $d\theta_1$  and  $d\theta_2$  is also shown in Fig. R2.12. The position of the foot rule after an initial rotation  $d\theta_1$  is shown as (Ba) whereas that after an initial rotation  $d\theta_2$  is shown as (Bb). The final orientation of the foot rule after both  $d\theta_1$  and  $d\theta_2$  have been imparted, in either order, is approximately the same in the limiting case shown in the same figure. Hence,

$$\Delta\theta_1 + \Delta\theta_2 \approx \Delta\theta_2 + \Delta\theta_1 \quad (\text{R2.42})$$

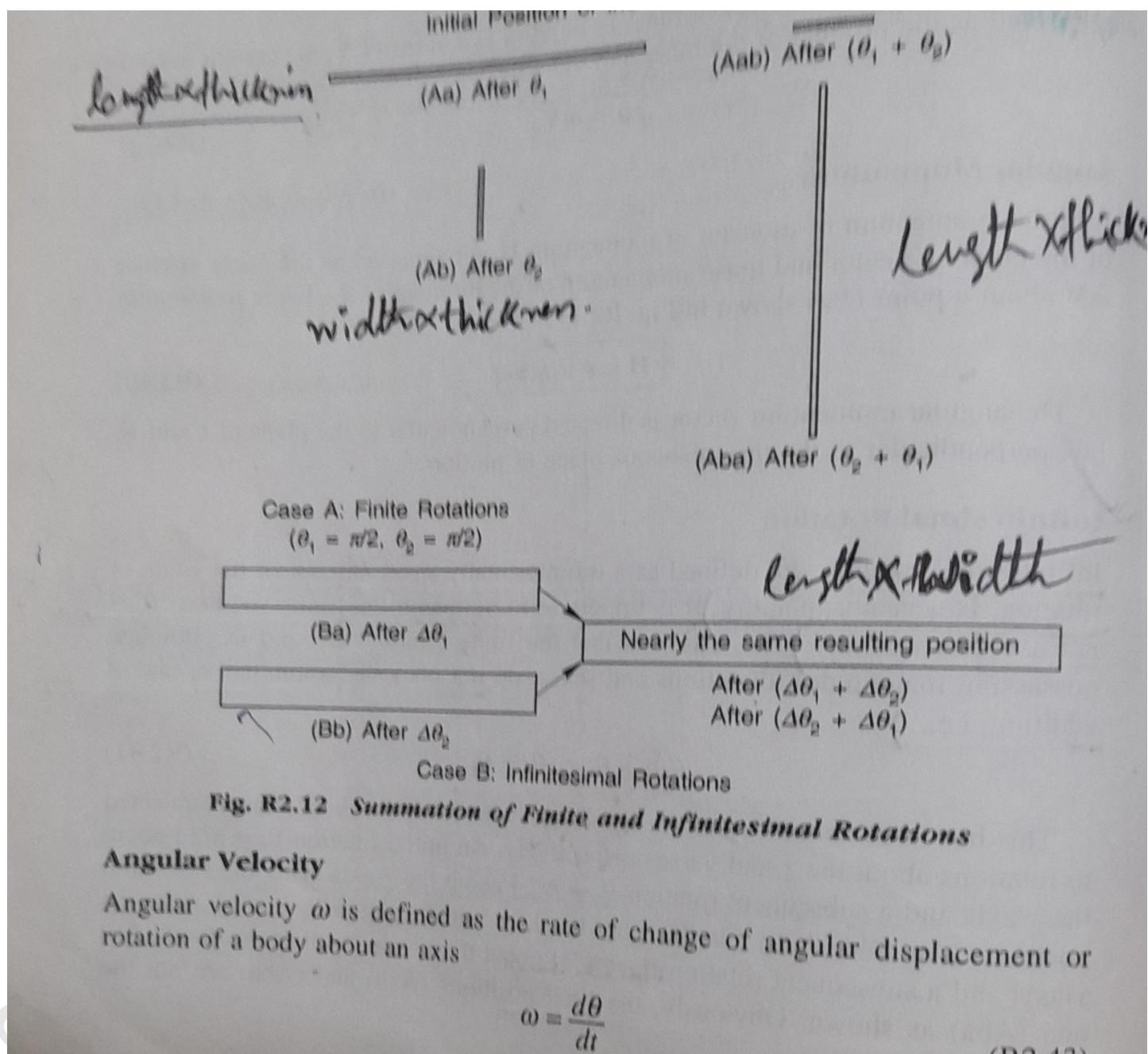
$$d\theta_1 + d\theta_2 = d\theta_2 + d\theta_1$$

and in the limit,



with a thick

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It follows from the vector nature of infinitesimal rotation  $d\theta$  and the scalar nature of time interval  $dt$  that the angular velocity must be a vector quantity.

If a point is located with a position vector  $\mathbf{r}$  with respect to an origin  $O$  on the axis of rotation, the linear velocity  $\mathbf{V}$  of the point is given by

$$\mathbf{V} = \omega \times \mathbf{r} \quad (\text{R2.44})$$

as shown in Fig. R2.11(b).

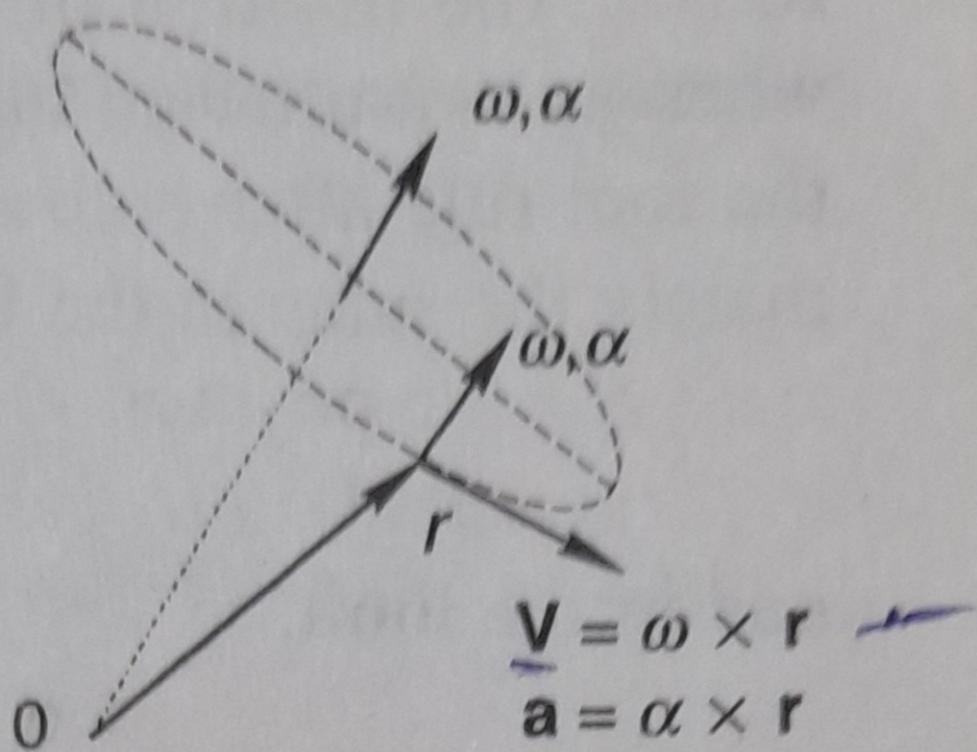
### Angular Acceleration

Angular acceleration  $\alpha$  is defined as the rate of change of angular velocity, i.e.,

$$\alpha = \frac{d\omega}{dt} = \frac{d^2\theta}{dt^2} \quad (\text{R2.45})$$

The linear acceleration  $\mathbf{a}$  of a point with a positive vector  $\mathbf{r}$  with respect to an origin  $O$  on the axis of rotation is given by

$$\mathbf{a} = \alpha \times \mathbf{r} \quad (\text{R2.46})$$



- (b) Velocity and Angular Velocity ✓  
Acceleration and Angular Acceleration ✓

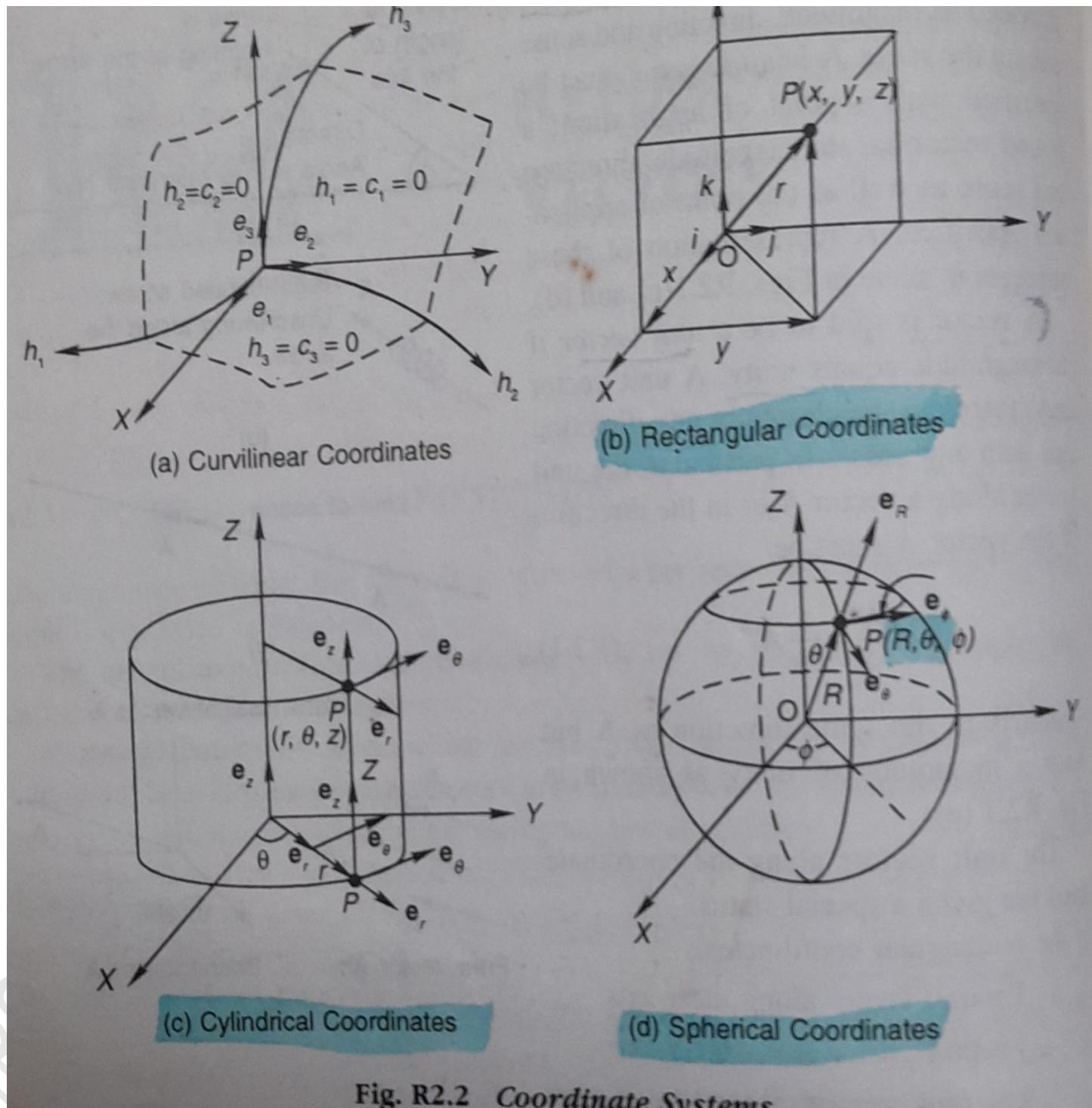


Fig. R2.2 *Coordinate Systems*

## DIFFERENT COORDINATE SYSTEMS

**R2.7 SOME VECTOR OPERATIONS**

Some of the useful results in vector algebra and calculus commonly referred to by the engineering students are summarized in Table R2.1.

$$\mathbf{i} \cdot \mathbf{i} = \mathbf{j} \cdot \mathbf{j} = \mathbf{k} \cdot \mathbf{k} = \mathbf{e}_r \cdot \mathbf{e}_r = \mathbf{e}_\theta \cdot \mathbf{e}_\theta = \dots = 1$$

$$\mathbf{i} \cdot \mathbf{j} = \mathbf{j} \cdot \mathbf{k} = \mathbf{k} \cdot \mathbf{i} = \mathbf{e}_r \cdot \mathbf{e}_\theta = \mathbf{e}_\theta \cdot \mathbf{e}_\phi = \dots = 0$$

$$\mathbf{i} \times \mathbf{i} = \mathbf{j} \times \mathbf{j} = \mathbf{k} \times \mathbf{k} = \mathbf{e}_r \times \mathbf{e}_r = \mathbf{e}_\theta \times \mathbf{e}_\theta = \dots = 0$$

$$\mathbf{i} \times \mathbf{j} = \mathbf{k} = -\mathbf{j} \times \mathbf{i}, \mathbf{j} \times \mathbf{k} = \mathbf{i}, \mathbf{k} \times \mathbf{i} = \mathbf{j}$$

$$\mathbf{e}_r \times \mathbf{e}_\theta = \mathbf{e}_z, \mathbf{e}_\theta \times \mathbf{e}_z = \mathbf{e}_r, \mathbf{e}_z \times \mathbf{e}_r = \mathbf{e}_\theta$$

$$\mathbf{A} \times \mathbf{B} = -\mathbf{B} \times \mathbf{A}, (\mathbf{A} \times \mathbf{B}) \times \mathbf{C} = (\mathbf{A} \cdot \mathbf{C})\mathbf{B} - (\mathbf{B} \cdot \mathbf{C})\mathbf{A}$$

$$\frac{d\mathbf{A}}{du} = \frac{dA_x}{du} \mathbf{i} + \frac{dA_y}{du} \mathbf{j} + \frac{dA_z}{du} \mathbf{k}$$

If  $F = f(x, y)$  where  $x = x(t), y = y(t)$

$$\frac{dF}{dt} = \frac{\partial F}{\partial x} \frac{dx}{dt} + \frac{\partial F}{\partial y} \frac{dy}{dt}$$

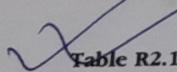
**SOME VECTOR OPERATIONS IN DIFFERENT COORDINATES**

Table R2.1 VECTOR OPERATIONS IN DIFFERENT COORDINATE SYSTEMS

	Cartesian	Cylindrical	Spherical
Vector $\mathbf{A}$	$A_x \mathbf{i} + A_y \mathbf{j} + A_z \mathbf{k}$	$A_r \mathbf{e}_r + A_\theta \mathbf{e}_\theta + A_z \mathbf{e}_z$	$A_R \mathbf{e}_R + A_\theta \mathbf{e}_\theta + A_\phi \mathbf{e}_\phi$
$A =  \mathbf{A} $	$(A_x^2 + A_y^2 + A_z^2)^{1/2}$	$(A_r^2 + A_\theta^2 + A_z^2)^{1/2}$	$(A_R^2 + A_\theta^2 + A_\phi^2)^{1/2}$
$\mathbf{A} \cdot \mathbf{B} = AB \cos \alpha$	$A_x B_x + A_y B_y + A_z B_z$	$A_r B_r + A_\theta B_\theta + A_z B_z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
$\mathbf{A} \times \mathbf{B} = AB \sin \alpha \mathbf{n}$	$\begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \mathbf{e}_r & \mathbf{e}_\theta & \mathbf{e}_z \\ A_r & A_\theta & A_z \\ B_r & B_\theta & B_z \end{vmatrix}$	$\begin{vmatrix} \mathbf{e}_R & \mathbf{e}_\theta & \mathbf{e}_\phi \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
$(\mathbf{ABC}) = \mathbf{A} \cdot (\mathbf{B} \times \mathbf{C})$	$\begin{vmatrix} A_x & A_y & A_z \\ B_x & B_y & B_z \\ C_x & C_y & C_z \end{vmatrix}$	$\begin{vmatrix} A_r & A_\theta & A_z \\ B_r & B_\theta & B_z \\ C_r & C_\theta & C_z \end{vmatrix}$	$\begin{vmatrix} A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \\ C_R & C_\theta & C_\phi \end{vmatrix}$
Operator $\nabla =$	$i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z}$	$\mathbf{e}_r \frac{\partial}{\partial r} + \mathbf{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \mathbf{e}_z \frac{\partial}{\partial z}$	$\mathbf{e}_R \frac{\partial}{\partial R} + \mathbf{e}_\theta \frac{1}{R} \frac{\partial}{\partial \theta} + \mathbf{e}_\phi \frac{1}{R \sin \theta} \frac{\partial}{\partial \phi}$
$\text{grad } p = \nabla p =$	$\frac{\partial p}{\partial x} \mathbf{i} + \frac{\partial p}{\partial y} \mathbf{j} + \frac{\partial p}{\partial z} \mathbf{k}$	$\frac{\partial p}{\partial r} \mathbf{e}_r + \frac{1}{r} \frac{\partial p}{\partial \theta} \mathbf{e}_\theta + \frac{\partial p}{\partial z} \mathbf{e}_z$	$\frac{\partial p}{\partial R} \mathbf{e}_R + \frac{1}{R} \frac{\partial p}{\partial \theta} \mathbf{e}_\theta + \frac{1}{R \sin \theta} \frac{\partial p}{\partial \phi} \mathbf{e}_\phi$
$\text{div} \cdot \mathbf{A} = \nabla \cdot \mathbf{A}$	$\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$	$\frac{1}{r} \frac{\partial}{\partial r} (r A_r) + \frac{1}{r} \frac{\partial A_\theta}{\partial \theta} + \frac{\partial A_z}{\partial z}$	$\frac{1}{R^2} \frac{\partial}{\partial R} (R^2 A_R) + \frac{1}{R \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_\theta) + \frac{1}{R \sin \theta} \frac{\partial A_\phi}{\partial \phi}$
$\text{curl } \mathbf{A} = \nabla \times \mathbf{A}$	$\begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$	$\frac{1}{r} \begin{vmatrix} \mathbf{e}_r & r \mathbf{e}_\theta & \mathbf{e}_z \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ A_r & r A_\theta & A_z \end{vmatrix}$	$\frac{1}{R^2 \sin \theta} \begin{vmatrix} e_R & R e_\theta & R \sin \theta e_\phi \\ \frac{\partial}{\partial R} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_R & A_\theta & R \sin \theta A_\phi \end{vmatrix}$

(Contd.)

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**Table R2.1 (Contd.) VECTOR OPERATIONS IN DIFFERENT COORDINATE SYSTEMS**

	<i>Cartesian</i>	<i>Cylindrical</i>	<i>Spherical</i>
Operator $\nabla^2 \equiv$ (Laplacian)	$\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$	$\frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} + \frac{\partial^2}{\partial z^2}$	$\frac{1}{R^2} \frac{\partial}{\partial R} \left( R^2 \frac{\partial}{\partial R} \right) + \frac{1}{R^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial}{\partial \theta} \right) + \frac{1}{R^2 \sin^2 \theta} \frac{\partial^2}{\partial \phi^2}$
Operator $\frac{D}{Dt} \equiv = (U \cdot \nabla) + \frac{\partial}{\partial t}$	$u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} + w \frac{\partial}{\partial z} + \frac{\partial}{\partial t}$	$u_r \frac{\partial}{\partial r} + \frac{u_\theta}{r} \frac{\partial}{\partial \theta} + u_z \frac{\partial}{\partial z} + \frac{\partial}{\partial t}$	$u_R \frac{\partial}{\partial R} + \frac{u_\theta}{R} \frac{\partial}{\partial \theta} + \frac{u_\phi}{R \sin \theta} \frac{\partial}{\partial \phi} + \frac{\partial}{\partial t}$

Laws of Motions for Linear vs Plane curvilinear motion

**Table 5.1 Linear vs Angular Motion**

	<i>Linear Motion</i>	<i>Angular Motion</i>	<i>Remarks</i>
<i>Displacement</i>	$s$	$\theta$	$ds = r d\theta$
<i>Velocity</i>	$v = \frac{ds}{dt}$	$\omega = \frac{d\theta}{dt}$	$V = r\omega$
<i>Acceleration</i>	$a = \frac{dv}{dt}$	$\alpha = \frac{d\omega}{dt}$	$a = r\alpha$
<i>Initial velocity</i>	$u$	$\omega_0$	
<i>Expressions relating the displacement, velocity, acceleration and time</i>	$V = u + at$ $s = ut + \frac{1}{2}at^2$ $V^2 - u^2 = 2as$ $s = \int V dt + C$ $V = \int a dt + K$	$\omega = \omega_0 + \alpha t$ $\theta = \omega_0 t + \frac{1}{2}\alpha t^2$ $\omega - \omega_0 = 2\alpha\theta$ $\theta = \int \omega dt + C'$ $\omega = \int \alpha dt + K'$	valid only for constant acceleration

## DERIVATIVES OF UNIT VECTOR

### (b) Derivatives of Unit Vectors

Derivatives of the unit vectors  $\mathbf{i}$ ,  $\mathbf{j}$  and  $\mathbf{k}$  along the fixed space coordinates  $x$ ,  $y$  and  $z$  respectively must be zero with respect to any scalar.

$$\frac{d\mathbf{i}}{dt} = 0 = \frac{d\mathbf{j}}{dt} = \frac{d\mathbf{k}}{dt}, \dots$$

Let us consider the derivatives of the unit vectors in radial and tangential direction, i.e., of  $\mathbf{e}_r$  and  $\mathbf{e}_\theta$  as shown in Fig. R2.8(b)

$$\mathbf{e}_r = \cos \theta \mathbf{i} + \sin \theta \mathbf{j}$$

$$\frac{d\mathbf{e}_r}{dt} = (-\sin \theta \mathbf{i} + \cos \theta \mathbf{j}) \frac{d\theta}{dt}$$

Since

$$\mathbf{e}_\theta = -\sin \theta \mathbf{i} + \cos \theta \mathbf{j}$$

and

$$\omega = \frac{d\theta}{dt}$$

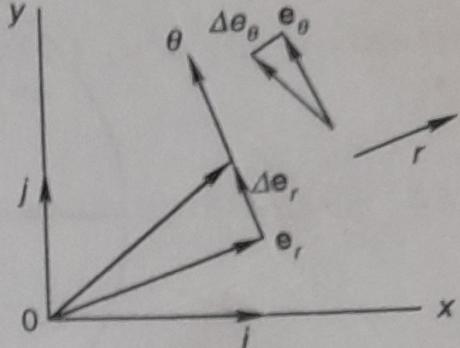


Fig. R2.8(b) Change in Unit Vectors

Similarly,

$$\boxed{\frac{d\mathbf{e}_r}{dt} = \omega \mathbf{e}_\theta}$$

$$\boxed{\frac{d\mathbf{e}_\theta}{dt} = (-\cos \theta \mathbf{i} - \sin \theta \mathbf{j}) \frac{d\theta}{dt}}$$

$$= -\omega \mathbf{e}_r$$