

PyTTE: The Technical Document

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1 Introduction

PyTTE (pronounced *pie-tee-tee-ee*) is a Python package for solving X-ray diffraction curves of bent crystals in reflection and transmission geometries. The computation of the diffraction curves is based on the numerical integration of 1D Takagi-Taupin equation (TTE) which is derived from a more general Takagi-Taupin theory describing the propagation of electromagnetic waves in a (quasi)periodic medium. Both energy and angle scans are supported. This document describes the theoretical basis behind PyTTE.

2 Takagi-Taupin equation

In the typical two-beam case, the Takagi-Taupin equations are can be written as

$$\begin{cases} \frac{\partial D_0}{\partial s_0} = ic_0 D_0 + ic_{\bar{h}} D_h \\ \frac{\partial D_h}{\partial s_h} = i \left(c_0 + \beta + \frac{\partial(\mathbf{h} \cdot \mathbf{u})}{\partial s_h} \right) D_h + ic_h D_0, \end{cases} \quad (1a)$$

$$(1b)$$

where D_0 and D_h are the pseudoamplitudes of the incident and diffracted waves, and s_0 and s_h coordinates along their direction of propagation, respectively. The deformation of the crystal is contained in $\mathbf{h} \cdot \mathbf{u}$ which will be considered in detail later. The coefficients $c_{0,h,\bar{h}}$ are given by

$$c_0 = \frac{k\chi_0}{2} \quad c_{h,\bar{h}} = \frac{kC\chi_{h,\bar{h}}}{2}, \quad (2)$$

where $k = 2\pi/\lambda$ and $C = 1$ for σ -polarization and $\cos 2\theta_B$ for π -polarization. The deviation parameter $\beta = (k_h^2 - k_0^2)/2k_h$ is quite often approximated by $\beta \approx k\Delta\theta \sin 2\theta_B$, where $\Delta\theta$ is the deviation from the Bragg angle. However, since this approximation ceases to be valid near the backscattering condition, PyTTE uses a more general form

$$\beta = \frac{2\pi}{d_h} \left(\frac{\lambda}{2d_h} - \sin \theta \right) = h \left(\frac{\lambda}{2d_h} - \sin \theta \right), \quad (3)$$

where d_h is the interplanar separation of the diffractive planes corresponding to the reciprocal vector \mathbf{h} and θ is the incidence angle relative to the aforementioned planes.

The partial derivatives with respect to s_0 and s_h can be written in Cartesian coordinates as

$$\frac{\partial}{\partial s_0} = \cos \alpha_0 \frac{\partial}{\partial x} - \sin \alpha_0 \frac{\partial}{\partial z} \quad \frac{\partial}{\partial s_h} = \cos \alpha_h \frac{\partial}{\partial x} + \sin \alpha_h \frac{\partial}{\partial z}. \quad (4)$$

The incidence and exit angles α_0 and α_h with respect to the crystal surface are related to θ by $\alpha_0 = \theta + \varphi$ and $\alpha_h = \theta - \varphi$, where φ is the asymmetry angle (positive clockwise). When seeking a solely depth-dependent solution for D_0 and D_h , we may drop the x -derivatives and thus obtain

$$\begin{cases} \frac{dD_0}{dz} = -i\gamma_0 c_0 D_0 - i\gamma_0 c_{\bar{h}} D_h \\ \frac{dD_h}{dz} = i\gamma_h \left(c_0 + \beta + \frac{\partial(\mathbf{h} \cdot \mathbf{u})}{\partial s_h} \right) D_h + i\gamma_h c_h D_0, \end{cases} \quad (5a)$$

where $\gamma_0 = 1/\sin \alpha_0$ and $\gamma_h = 1/\sin \alpha_h$. By defining $\xi = D_h/D_0$, the equations can be written as a single ordinary differential equation

$$\frac{d\xi}{dz} = i\gamma_0 c_{\bar{h}} \xi^2 + i \left[(\gamma_0 + \gamma_h) c_0 + \gamma_h \beta + \gamma_h \frac{\partial(\mathbf{h} \cdot \mathbf{u})}{\partial s_h} \right] \xi + i\gamma_h c_h \quad (6)$$

In the reflection geometry (*i.e.* the Bragg case), the reflectivity R of the crystal with thickness t can be solved by integrating Equation (6) from the bottom of the crystal $z = -t$ to the top surface $z = 0$. The initial condition is set $\xi(-t) = 0$. The reflectivity, which is defined in the terms of integrated intensity, is then computed $R = \gamma_0/\gamma_h |\xi(0)|^2$ where γ_0/γ_h takes care of different footprint sizes in the asymmetric case. Using the solved ξ and Equation (5a), the transmission $T = |D_0(-t)/D_0(0)|^2$ can be then solved from

$$\frac{dD_0}{dz} = -i(\gamma_0 c_0 + \gamma_0 c_{\bar{h}} \xi) D_0 \quad (7)$$

by integrating from $z = 0$ to $z = -t$. The transmission geometry (the Laue case) is more straightforward, as the ODEs for ξ and D_0 can be integrated simultaneously from $z = 0$ to $z = -t$. With the initial conditions are set $\xi(0) = 0$ and $D_0(0) = 1$, the forward-diffracted intensity at the exit surface is $|D_0(-t)|^2$ and the diffracted intensity is $|D_h(-t)|^2 = |\xi(-t)D_0(-t)|^2$.

3 Deformation

As stated in the previous section, the deformation is introduced through $\partial_h(\mathbf{h} \cdot \mathbf{u})$ term where \mathbf{u} is the displacement vector field. Taking the asymmetry into account, the reciprocal vector is given by $\mathbf{h} = h \sin \varphi \hat{\mathbf{x}} + h \cos \varphi \hat{\mathbf{z}}$. Thus

$$\frac{\partial(\mathbf{h} \cdot \mathbf{u})}{\partial s_h} = h \sin \varphi \frac{\partial u_x}{\partial s_h} + h \cos \varphi \frac{\partial u_z}{\partial s_h}. \quad (8)$$

Again we write the partial derivatives in terms of x and z . In this case, however, neither x - or z -derivatives can be dropped as they both contain physical information about the rotation and the separation of the diffractive planes. Since the beam propagates also in the x -direction, the situation is not strictly speaking one dimensional. However, since the x -coordinate is geometrically related to z , the problem can be treated as such. Therefore the deformation term becomes

$$\frac{\partial(\mathbf{h} \cdot \mathbf{u})}{\partial s_h} = h \left(\sin \varphi \cos \alpha' \frac{\partial u_x}{\partial x} + \sin \varphi \sin \alpha' \frac{\partial u_x}{\partial z} + \cos \varphi \cos \alpha' \frac{\partial u_z}{\partial x} + \cos \varphi \sin \alpha' \frac{\partial u_z}{\partial z} \right), \quad (9)$$

where the derivatives, that are functions of x and z , are made only z -dependent with $x(z) = -z \cot \alpha$. PyTTE computes the strain term from the Jacobian of \mathbf{u} .

3.1 Anisotropic plate

According to [1], the components of the displacement field for an anisotropic plate bent by two (scaled) torques m_x and m_y are

$$u_x = (S_{11}m_x + S_{12}m_y)xz + (S_{51}m_x + S_{52}m_y)\frac{z^2}{2} + (S_{61}m_x + S_{62}m_y)\frac{yz}{2} \quad (10)$$

$$u_y = (S_{21}m_x + S_{22}m_y)yz + (S_{41}m_x + S_{42}m_y)\frac{z^2}{2} + (S_{61}m_x + S_{62}m_y)\frac{xz}{2} \quad (11)$$

$$u_z = -(S_{11}m_x + S_{12}m_y)\frac{x^2}{2} - (S_{21}m_x + S_{22}m_y)\frac{y^2}{2} - (S_{61}m_x + S_{62}m_y)\frac{xy}{2} + (S_{31}m_x + S_{32}m_y)\frac{z^2}{2}, \quad (12)$$

where S_{ij} are the components of the compliance matrix. Thus we find the partial derivatives:

$$\frac{\partial u_x}{\partial x} = (S_{11}m_x + S_{12}m_y)z \quad (13)$$

$$\frac{\partial u_x}{\partial z} = (S_{11}m_x + S_{12}m_y)x + (S_{51}m_x + S_{52}m_y)z + (S_{61}m_x + S_{62}m_y)\frac{y}{2} \quad (14)$$

$$\frac{\partial u_z}{\partial x} = -(S_{11}m_x + S_{12}m_y)x - (S_{61}m_x + S_{62}m_y)\frac{y}{2} \quad (15)$$

$$\frac{\partial u_z}{\partial z} = (S_{31}m_x + S_{32}m_y)z \quad (16)$$

The torques are related to the bending radii R_i by¹

$$\frac{1}{R_x} = -S_{11}m_x - S_{12}m_y, \quad \frac{1}{R_y} = -S_{21}m_x - S_{22}m_y. \quad (17)$$

Thus

$$m_x = \frac{1}{S_{11}S_{22} - S_{12}S_{21}} \left(\frac{S_{12}}{R_y} - \frac{S_{22}}{R_x} \right), \quad m_y = \frac{1}{S_{11}S_{22} - S_{12}S_{21}} \left(\frac{S_{21}}{R_x} - \frac{S_{11}}{R_y} \right). \quad (18)$$

3.2 Isotropic plate

The general anisotropic equations simplify considerably when assuming the plate to be isotropic. The isotropic compliance matrix is given by

$$S = \frac{1}{E} \begin{bmatrix} 1 & -\nu & -\nu & 0 & 0 & 0 \\ -\nu & 1 & -\nu & 0 & 0 & 0 \\ -\nu & -\nu & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 2(1+\nu) & 0 & 0 \\ 0 & 0 & 0 & 0 & 2(1+\nu) & 0 \\ 0 & 0 & 0 & 0 & 0 & 2(1+\nu) \end{bmatrix}, \quad (19)$$

where E is Young's modulus and ν is the Poisson ratio. Plugging these into (18), we obtain

$$m_x = -\frac{E}{1-\nu^2} \left(\frac{1}{R_x} + \frac{\nu}{R_y} \right), \quad m_y = -\frac{E}{1-\nu^2} \left(\frac{1}{R_y} + \frac{\nu}{R_x} \right) \quad (20)$$

and thus

$$\frac{\partial u_x}{\partial x} = -\frac{z}{R_x}, \quad \frac{\partial u_x}{\partial z} = -\frac{x}{R_x}, \quad \frac{\partial u_z}{\partial x} = \frac{x}{R_x}, \quad \frac{\partial u_z}{\partial z} = \frac{\nu}{1-\nu} \left(\frac{1}{R_x} + \frac{1}{R_y} \right) z. \quad (21)$$

Finally, since PyTTE assumes the top surface is at $z = 0$, we need to shift the z -axis $z \rightarrow z + t/2$

¹In this work the signs of R_i is the opposite to that of [1]

References

- [1] Manuel Sanchez del Rio, Nicolas Perez-Bocanegra, Xianbo Shi, Veijo Honkimäki, and Lin Zhang. Simulation of x-ray diffraction profiles for bent anisotropic crystals. *Journal of Applied Crystallography*, 48(2):477–491, mar 2015.