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% Linear Finite Element Program for 2-D Elasticity
%
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%
% This program computes a numerical solution to a finite element model
% using input on the geometry and physical properties of a mesh, and on the
% boundary conditions and applied loads. The routine assembles element
% quantities into the stiffness matrix and force vector to create a system
% of equations which is then solved for the nodal values of the
% displacement field. Boundary conditions are applied to constrain the
% stiffness matrix and to augment the force vector. The output is a list of
% the displacements printed on screen, contour plots of the displacement
% fields, and a plot of the deformed configuration of the mesh.
%
% Mesh input should be uploaded by running an input .m file before
% executing this program.
%
% Format of required input:
%
%   numnp:           = number of nodes in the mesh (length(NodeTable))
%
%   numel:           = number of elements in the mesh
%
%   nen:             = maximum number of nodes per element (4)
%
%   PSPS:            = flag for plane stress ('s') or plane strain ('n')
%
%   NodeTable:       = table of mesh nodal coordinates defining the
%                     geometry of the mesh; format of the table is as
%                     follows:
%
%                     Nodes |           x-coord  y-coord
%                     n1   |   NodeTable = [x1      y1
%                     n2   |                   x2      y2
%                     ...   |                   ..      ..
%                     nnumnp |                   xnumnp ynumnp];
%
%   ix:              = table of mesh connectivity information, specifying
%                     how nodes are attached to elements and how materials
%                     are assigned to elements; entries in the first nen
%                     columns correspond to the rows of NodeTable
%                     representing the nodes attached to element e;
%                     entries in the last nen+1 column are rows from MateT
%                     signifying the material properties assigned to
%                     element e; format of the table is as follows:
%
%                     Elements |           n1    n2    n3    n4    mat
%                     e1      |   ix = [eln1  eln2  eln3  eln4  elmat
%                     e2      |           e2n1  e2n2  e2n3  e2n4  e2mat
%                     ...      |           ..    ..    ..    ..    ..
%                     numel    |   values for element numel  ];
%
%   MateT:           = table of mesh material properties for each distinct
%                     set of material properties; these sets are

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% referenced by element e by setting the value of
% ix(e,nen+1) to the row number of the desired
% material set; format of the table is as follows:
%
%      Materials |      E      v      t
%      mat1      |      E1     v1     t1
%      mat2      |      E2     v2     t2
%      ...       |      ..     ..     ..];
%
% BCLIndex:      = list of the number of boundary conditions and loads
%                applied to the mesh; first entry is the number of
%                prescribed displacements at nodes; second entry is
%                the number of nodal forces
%
% NodeBC:        = table of prescribed nodal displacement boundary
%                conditions; it contains lists of nodes, the
%                direction of the displacement prescribed (x=1, y=2),
%                and the value of the displacement (set 0 for fixed
%                boundary); the length of the table must match the
%                entry in BCLIndex(1), otherwise an error will result
%                if too few conditions are given or extra BCs will be
%                ignored in the model input module; format of the
%                table is as follows:
%
%      BCs      |      nodes direction value
%      bc1      |      NodeBC = [bc1n     bc1dir     bc1u
%      bc2      |      bc2n     bc2dir     bc2u
%      ...      |      ..      ..      .. ];
%
% NodeLoad:      = table of prescribed nodal forces; it contains lists
%                of nodes, the direction of the force prescribed
%                (x=1, y=2), and the value of the force; the length
%                of the table must match the entry in BCLIndex(2),
%                otherwise an error will result if too few conditions
%                are given or extra loads will be ignored in the
%                model input module; format of the table is as
%                follows:
%
%      Loads    |      nodes direction value
%      P1       |      NodeLoad = [ P1n     P1dir     P1P
%      P2       |      P2n     P2dir     P2P
%      ...      |      ..      ..      .. ];
%
% The following numbering convention is used for 4-node quadrilateral
% elements:
%
%
%      4 ----- 3
%      |           |
%      |           |
%      |           |
%      |           |
%      |           |
%      |           |
%      1 ----- 2
%
%      2
%      | \
%      |  \
%      |   \
%      |    \
%      |     \
%      |      \
%      3-----1

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format compact

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% Updating the NodeTable to match initial displacement :
NodeTable = [0          0
              L          0
              L+dis(1,storej) H+dis(2,storej)
              dis(3,storej) H+dis(4,storej)];

% Calling FormFE to make one-pass through the Algorithm :
FormFE
%

% Storing the Computed Acceleration iterates :
acc(:,storej) = -(1+alpha)*Mdd\F_bar_int;
an(:,1) = acc(:,1);

% Optional Parameter to include any tractions :
Fext = 0*linspace(0,1,tSteps);

% dn3x(:,1) = 0;
% dn3y(:,1) = do;
% dn4x(:,1) = 0;
% dn4y(:,1) = do;

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% Major Modification in the Code %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

for n=1:tSteps-1

    if n==1
        FEXT(:,n+1) = Fd;
    else
        FEXT(:,n+1) = Fdtilda;
    end

    IntF_store(:,n) = F_bar_int;
    res = 1;Res_0 = res;
    iter = 1;

    % Initializing the Predictors for the Newton Step (iteration in Multi-Corrector)
    dis(:,storej) = dn(:,n) + delt*vn(:,n) + delt^2/2*(1-2*beta)*an(:,n);
    vel(:,storej) = vn(:,n) + delt*(1-gamma)*an(:,n);
    acc(:,storej) = an(:,n);

    while (res>tol*Res_0) && iter < maxiter

        % Form and Solve Matrix System for current iterate :
        FormFE

        % Calling SolveFE for the solution to the linearized system :
        SolveFE

        % Store the Initial Residual (Res_0) :

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        if iter==1
            Res_0=res;
        end

        % Update the Node Table to include the displacement iterate :
        NodeTable = [0          0
                    L          0
                    L+dis(1,storej+1) H+dis(2,storej+1)
                    dis(3,storej+1) H+dis(4,storej+1)];

        residual(n,iter) = res;
        iter=iter+1;           % Update the iteration counter
        storej=storej+1;
    end
    n=n+1;
    %     if norm(Mstar) > 1e7
    %         break
    %     end
    %     Updating the last converged iterate :
    dn(:,n) = dis(:,storej);    vn(:,n) = vel(:,storej);    an(:,n) = acc(:,storej);

    % Store the Displacement from the last converged iterate (plotting) :
    %     Disp(:,n) = dn;
    %     Vel(:,n) = vn;
    %     Acc(:,n) = an;

    Stress(n,:)=stress(4,:);    % We define the Integration Point counterclockwise
    Strain(n,:)=strain(4,:);
end

% Output Results

Node_U_V = zeros(numnp,2*ndf);

for node = 1:numnp
    for dir = 1:ndf
        gDOF = NDOFT(node, dir);
        if gDOF <= neq
            Node_U_V(node, dir) = dn(gDOF,n);
        else
            Node_U_V(node, dir) = ModelDc(gDOF - neq);
        end
    end
end

Node_U_V;
maxuvw = zeros(ndm,1);
maxxyz = zeros(ndm,1);

for i = 1:ndm
    maxuvw(i) = max(abs(Node_U_V(:,i)));
    maxxyz(i) = max(NodeTable(:,i));
end

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len = sqrt(maxxyz'*maxxyz);
perc = 5/100;
factor = len/max(maxuvw)*perc;
NodeTable2 = NodeTable;

for i = 1:ndm
    NodeTable2(:,i) = NodeTable2(:,i) + Node_U_V(:,i)*factor;
end

dn=dn';vn = vn';an=an';

% Producing the Output for Plotting :
Output
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