

(Q2)

For step 2, we have  $F_{\text{ext}} = 2 \times 10^4 \text{ N}$ . We got  $d_1 = 6.6667 \times 10^{-3} \text{ cm}$ .

For step 2,  $[F_2^{\text{ext}} = 4 \times 10^4]$

$$R^{(0)} = F_2^{\text{ext}} - [F_{\text{ext}} + F_{\text{int}}] = 2 \times 10^4 \text{ N}$$

$K_a, K_b$  calculated on basis of  $F_{\text{internal}}$  in a and b at end of step 1.  
Since, these segments remain elastic at end of step 1, we use  $K_a: A E_e = 10^6 \text{ N/cm}$   
and  $K_b: A E_e = 2 \times 10^6 \text{ N/cm}^2$ . Since we are using modified Newton,

we keep  $k = K_a + K_b = 3 \times 10^6 \text{ N/cm}^2$  constant throughout the step.

$$(K_a + K_b), \Delta d^{(0)}, R^{(0)} \rightarrow \Delta d^{(0)} = 6.667 \times 10^{-3}$$

Iteration 1:-  $\rightarrow d_2^{(1)} = d_2^{(0)} + \Delta d_2^{(0)} = [1.333 \times 10^{-2} \text{ cm}]$

$$\|R^{(1)}\| = 6600 \text{ N}$$

$$\Delta d_2^{(1)} = 2.2 \times 10^{-3} \text{ cm}$$

Iteration 2:-

$$d_2^{(2)} = d_2^{(1)} + \Delta d_2^{(1)} = [1.5533 \times 10^{-2} \text{ cm}]$$

$$\|R^{(2)}\| = 4356 \text{ N}$$

Residual check.

$$\|R^{(2)}\| = 4356 \text{ N}, \quad \epsilon \|R^{(1)}\| = 0.3 \times 6600 \text{ N} = 660 \text{ N}$$

since  $\|R^{(2)}\| \neq \epsilon \|R^{(1)}\| \rightarrow$  convergence not satisfied.

[Note:- in previous notes, prof. had used  $\|R^{(i+1)}\| < \epsilon \|R^{(i)}\|$ , to calculate  $\Delta d_2^{(i)}$ , to define the convergence check, however in this example he used  $\epsilon \|R^{(i)}\|$  to define convergence condition and the same has been used for this example.]

$$\Delta d_2^{(2)} = 1.4521 \times 10^{-3} \text{ cm}$$

The above iterations were completed in class, ~~the~~ detailed working is now provided from iteration 3.

### Iteration 3.

$$d_2^{(3)} = d_2^{(2)} + \Delta d_2^{(2)} = 1.5533 \times 10^{-2} + 1.4521 \times 10^{-3} = 1.6985 \times 10^{-2}$$

Note:  $\varepsilon_{b_2}^{(3)}$  is magnitude of compressive strain

$$\text{strain: } \varepsilon_{a_2}^{(3)} = \frac{d_2^{(3)}}{L_a} = \frac{1.6985 \times 10^{-2}}{10} = 1.6985 \times 10^{-3} < \varepsilon_y [\text{elastic}] [\text{Tensile}]$$

$$\varepsilon_{b_2}^{(3)} = \frac{d_2^{(3)}}{L_b} = \frac{1.6985 \times 10^{-2}}{5} = 3.3971 \times 10^{-3} > \varepsilon_y [\text{plastic}] [\text{Compressive}]$$

Note:  $F_{b_2}^{int(3)}$  is magnitude of compressive internal force.

$$\text{Force: } F_{a_2}^{int(3)} = A E_e \varepsilon_{a_2}^{(3)} = 1 \times 10^7 \times 1.6985 \times 10^{-3} = 1.6985 \times 10^4 N \cdot [\text{Tensile}]$$

$$F_{b_2}^{int(3)} = [E_p (\varepsilon_{b_2}^{(3)} - \varepsilon_y) + \sigma_y] A \cdot [\text{since it is plastic}]$$

$$= [105 (3.3971 \times 10^{-3} - 2 \times 10^{-3}) + 2 \times 10^4] = 2.01397 \times 10^4 N$$

$$[\text{Compressive}]$$

### Residual check.

$$\|R^{(3)}\| = F_2^{ext} - [F_{a_2}^{int(3)} + F_{b_2}^{int(3)}]$$

In reality, it should be  $-F_{b_2}^{int(3)}$ , but since we are considering only algebraic values, we write  $+F_{b_2}^{int(3)}$

$$= 4 \times 10^4 - [1.6985 \times 10^4 + 2.01397 \times 10^4]$$

$$= 2874.96 N$$

$$\|R^{(3)}\| = 660 N$$

$\|R^{(3)}\| \neq \|R^{(1)}\|$  [Residual check not satisfied]

∴ calculate  $\Delta d_2^{(3)}$ ,

$$(k_a + k_b) \Delta d_2^{(3)} = \|R\|$$

$$\therefore 3 \times 10^6 \Delta d_2^{(3)} = 2874.96$$

$$\therefore \Delta d_2^{(3)} = 9.5832 \times 10^{-4} \text{ cm.}$$

Iteration 4:

$$d_2^{(4)} = d_2^{(3)} + \Delta d_2^{(3)} = 1.6985 \times 10^{-2} + 9.5832 \times 10^{-4} = \boxed{1.7944 \times 10^{-2} \text{ cm}}$$

strain:  $\epsilon_{a_2}^{(4)} = \frac{d_2^{(4)}}{L_a} = \frac{1.7944 \times 10^{-2}}{10} = 1.7944 \times 10^{-3} < \epsilon_y [\text{elastic}]$

$$\epsilon_{b_2}^{(4)} = \frac{d_2^{(4)}}{L_b} = \frac{1.7944 \times 10^{-2}}{5} = 3.5887 \times 10^{-3} > \epsilon_y [\text{plastic}]$$

$F_{\text{int}} := F_{a_2}^{\text{int}(4)} = A E_c \epsilon_{a_2}^{(4)} = 1 \times 10^7 \times 1.7944 \times 10^{-3} = 1.7944 \times 10^4 \text{ N}$

$$\begin{aligned} F_{b_2}^{\text{int}(4)} &= [E_p (\epsilon_{b_2}^{(4)} - \epsilon_y) + \sigma_y] A \quad [\text{since it is plastic}] \\ &\cdot [10^5 (3.5887 \times 10^{-3} - 2 \times 10^{-3}) + 2 \times 10^4] \times 1 \\ &\cdot 2.015887 \times 10^4 \text{ N} \end{aligned}$$

Residual check.

$$\begin{aligned} \|R^{(4)}\| &= F_2^{\text{ext}} - [F_{a_2}^{\text{int}(4)} + F_{b_2}^{\text{int}(4)}] \\ &= 4 \times 10^4 - [1.7944 \times 10^4 + 2.015887 \times 10^4] \\ &= \underline{1897.474 \text{ N}}. \end{aligned}$$

$$\epsilon \|R^{(4)}\| = 660 \text{ N.}$$

$\|R^{(4)}\| \neq \epsilon \|R^{(1)}\|$  [Residual check not satisfied].

$\therefore$  calculate  $\Delta d_2^{(4)}$ .

$$(k_a + k_b)_2 \Delta d_2^{(4)} = \|R^{(4)}\|.$$

$$3 \times 10^6 \Delta d_2^{(4)} = 1897.474$$

$$\Delta d_2^{(4)} = 6.3249 \times 10^{-4} \text{ cm.}$$

### Iteration 5.

$$d_2^{(5)} = d_2^{(4)} + \Delta d_2^{(4)} = 1.7944 \times 10^{-2} + 6.3249 \times 10^{-4}, \boxed{1.8576 \times 10^{-2}}$$

strain:  $\epsilon_{a_2}^{(5)} = \frac{d_2^{(5)}}{L_a} = \frac{1.8576 \times 10^{-2}}{10} = 1.8576 \times 10^{-3} < \epsilon_y [\text{elastic}]$

$$\epsilon_{b_2}^{(5)} = \frac{d_2^{(5)}}{L_b} = \frac{1.8576 \times 10^{-2}}{5} = 3.7152 \times 10^{-3} > \epsilon_y [\text{plastic}]$$

$F_{\text{int}} := F_{a_2}^{\text{int}(5)} \cdot A E_e \epsilon_{a_2}^{(5)} = 1 \times 10^7 \times 1.8576 \times 10^{-3} = 1.8576 \times 10^4 N$

$$\begin{aligned} F_{b_2}^{\text{int}(5)} &= [F_p (\epsilon_{b_2}^{(5)} - \epsilon_y) + c_f] A \quad [\text{since it is plastic}] \\ &= [10^5 (3.7152 \times 10^{-3} - 2 \times 10^{-3}) + 2 \times 10^4] \times 1 \\ &= 2.017152 \times 10^4 N \end{aligned}$$

### Residual check.

$$\begin{aligned} \|R^{(5)}\| &= F_2^{\text{ext}} - [F_{a_2}^{\text{int}(5)} + F_{b_2}^{\text{int}(5)}] \\ &= 4 \times 10^4 - [1.8576 \times 10^4 + 2.017152 \times 10^4] \\ &= \underline{1252.333 N} \end{aligned}$$

$$\epsilon \|R^{(5)}\| = 660 N$$

$\|R^{(5)}\| \neq \epsilon \|R^{(5)}\|$  [Residual check not satisfied].

calculate  $\Delta d_2^{(5)}$

$$(k_a + k_b) \cdot \Delta d_2^{(5)} = \|R^{(5)}\|$$

$$3 \times 10^4 \cdot \Delta d_2^{(5)} = 1252.333$$

$$\Delta d_2^{(5)} = 4.17444 \times 10^{-4} \text{ cm.}$$

Iteration 6

$$d_2^{(6)} = \boxed{1.8994 \times 10^{-2} \text{ cm}}$$

strain:  $\epsilon_{a_2}^{(6)} = 1.8994 \times 10^{-3} < \epsilon_y$  [elastic]  $\epsilon_{b_2}^{(6)} = 3.4987 \times 10^{-3} > \epsilon_y$  [plastic]

Flat:  $F_{a_2}^{int(6)} = 1.8994 \times 10^4 \text{ N}$ ,  $F_{b_2}^{int(6)} = 2.017987 \times 10^4 \text{ N}$

$$\|R^{(6)}\| = 826.5395 \text{ N}$$

$\|R^{(5)}\| \neq \epsilon \|R^{(4)}\|$  [Residual check not satisfied].

$$Ad_2^{(6)} = 2.75513 \times 10^{-4} \text{ cm.}$$

Iteration 7

$$d_2^{(7)} = \boxed{1.9269 \times 10^{-2} \text{ cm}} \quad \text{--- Ans.}$$

strain:  $\epsilon_{a_2}^{(7)} = 1.9269 \times 10^{-3} < \epsilon_y$  [elastic]  $\epsilon_{b_2}^{(7)} = 3.8538 \times 10^{-3} > \epsilon_y$  [plastic]

Flat:  $F_{a_2}^{int(7)} = \cancel{1.9269 \times 10^4 \text{ N}}$ ,  $F_{b_2}^{int(7)} = 2.018538 \times 10^4 \text{ N}$

$$\|R^{(7)}\| = 545.5161 \text{ N}$$

$\|R^{(7)}\| \nearrow < \underbrace{\epsilon \|R^{(6)}\|}_{660 \text{ N}}$  [Residual check satisfied !!]

Step 2.

Iteration no.	$d_2^{(i)}$	$R_2^{(i)}$
0	$6.6667 \times 10^{-3} \text{ cm}$	$2 \times 10^4 \text{ N}$
1	$1.333 \times 10^{-2} \text{ cm}$	6600 N
2	$1.5533 \times 10^{-2} \text{ cm}$	4356 N
3	$1.6985 \times 10^{-2} \text{ cm}$	2874.96 N
4	$1.7944 \times 10^{-2} \text{ cm}$	1897.474 N
5	$1.8576 \times 10^{-2} \text{ cm}$	1252.333 N
6	$1.8944 \times 10^{-2} \text{ cm}$	826.5395 N
7	$1.9269 \times 10^{-2}$	545.5161 N

Ans: For  $\epsilon = 0.1$ , we reach convergence after 7 iterations, with  $d_2 = 1.9269 \times 10^{-2} \text{ cm}$ .

~~Final~~

$< 6600 \times 0.1 \checkmark$