

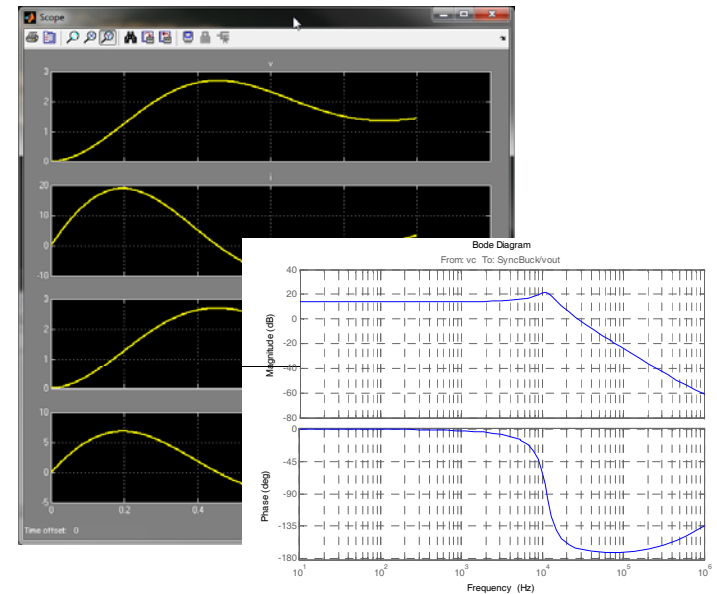
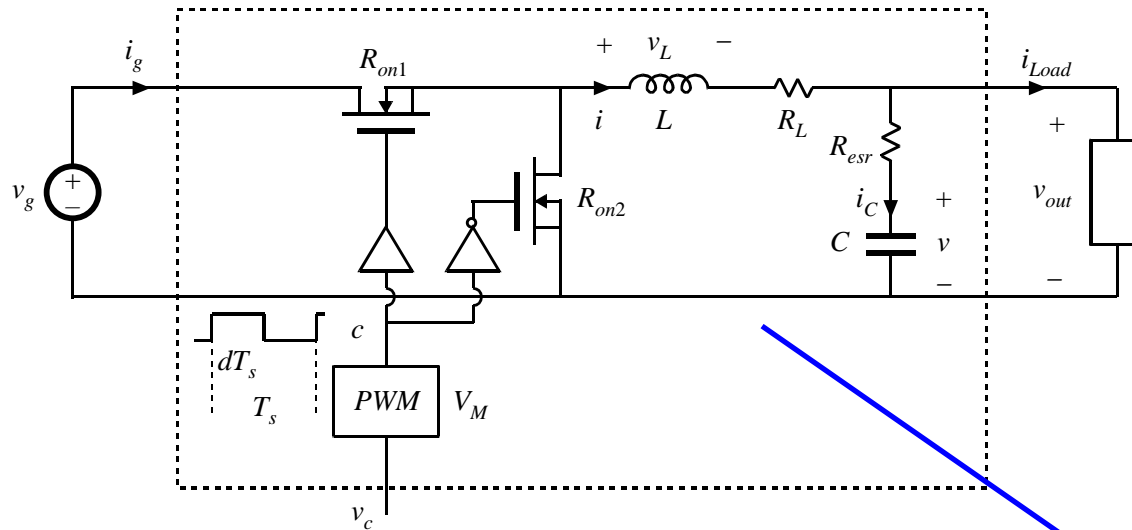
Introduction to Switched-Mode Converter Modeling using MATLAB/Simulink

- MATLAB: programming and scripting environment
- Simulink: block-diagram modeling environment inside MATLAB
- Motivation:
 - Powerful environment for system modeling and simulation
 - More sophisticated controller models, analysis and design tools
- But*:
 - Block-diagram based Simulink models, unidirectional signals
 - Not a traditional circuit simulator; specialized physics-based Spice device models or component libraries are not readily available

*Various add-ons to Simulink are available to allow traditional circuit diagram entry and circuit simulations (e.g. SimPowerSystems, PLECS), or to embed Spice within MATLAB/Simulink environment. These add-ons are not required and will not be used in ECEN5807.

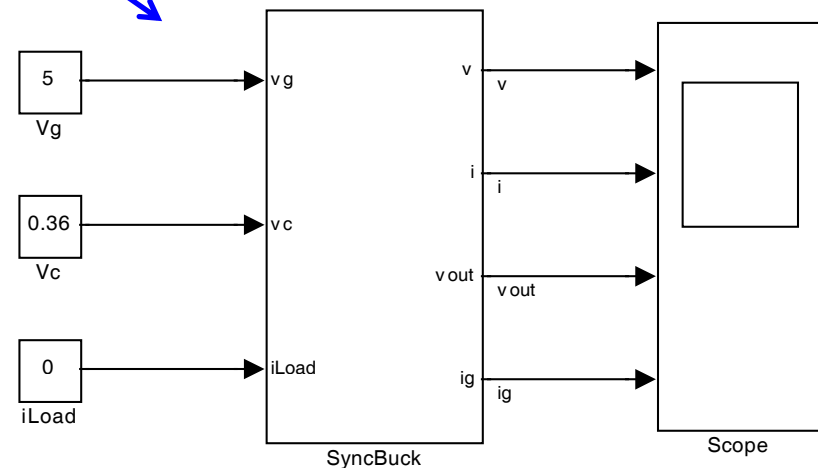
Introduction through an example

Synchronous buck converter



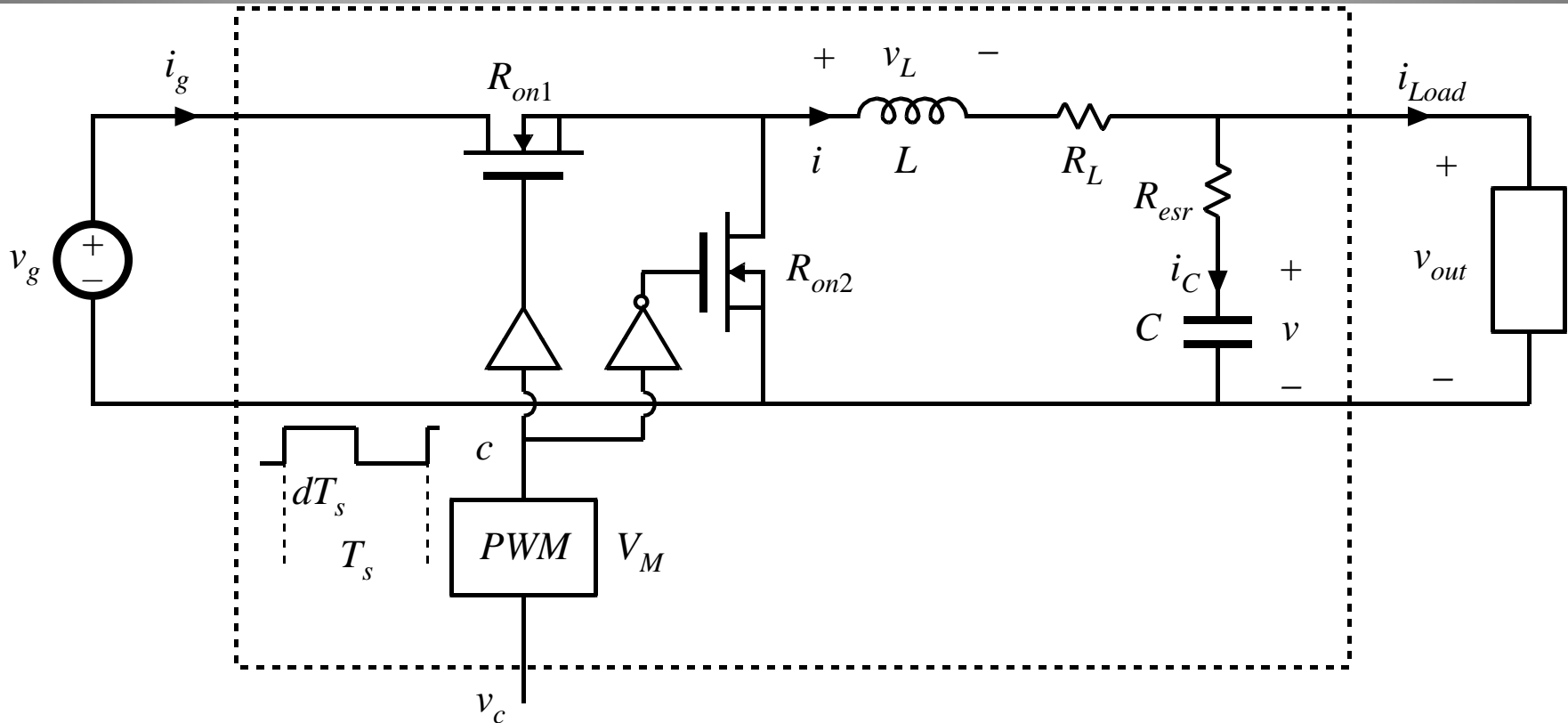
- Switching model
- Averaged model
- Small-signal linearization and frequency responses

See MATLAB/Simulink page on the course website (“Materials” page) for complete step-by-step details, and to download the example files



Simulink model: [syncbuck_OL.mdl](#)

Synchronous Buck Converter

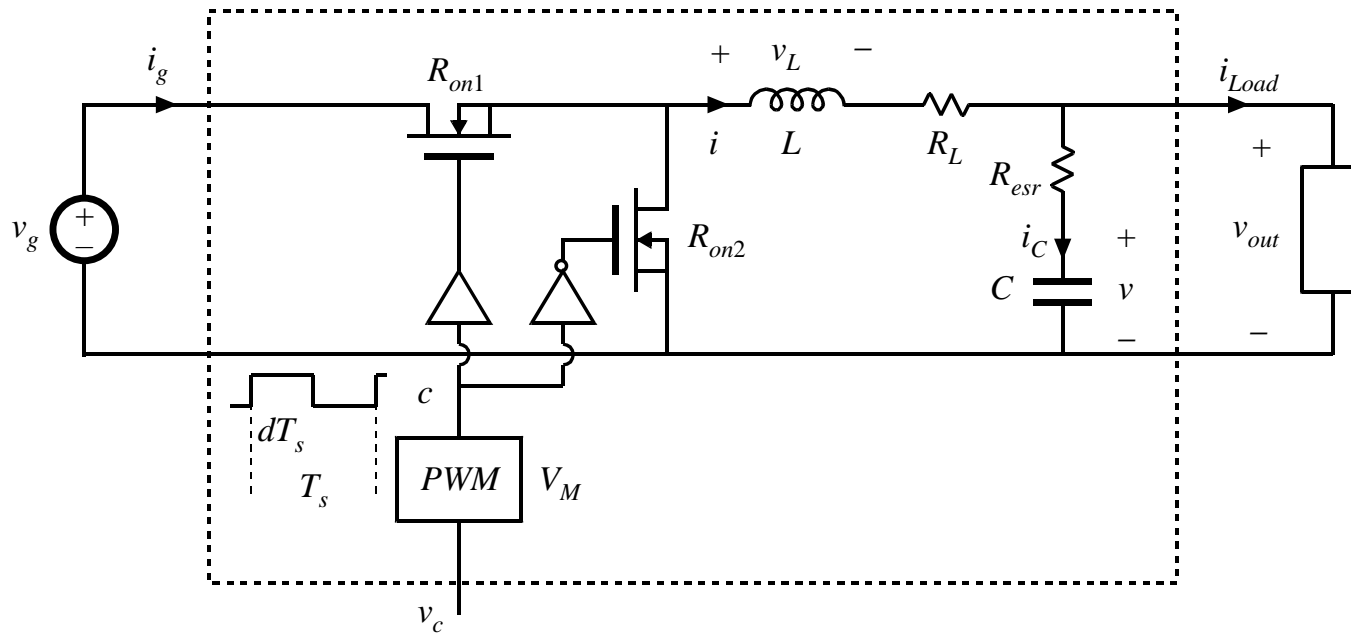


Inputs: v_g , i_{Load} , v_c

Outputs: v_{out} , i_g

State variables: v , i

Converter state equations



State equations

$$v_L = L \frac{di}{dt} = \begin{cases} v_g - (R_{on1} + R_L)i - v_{out} & (c = 1) \\ -(R_{on2} + R_L)i - v_{out} & (c = 0) \end{cases}$$

$$i_C = C \frac{dv}{dt} = i - i_{Load}$$

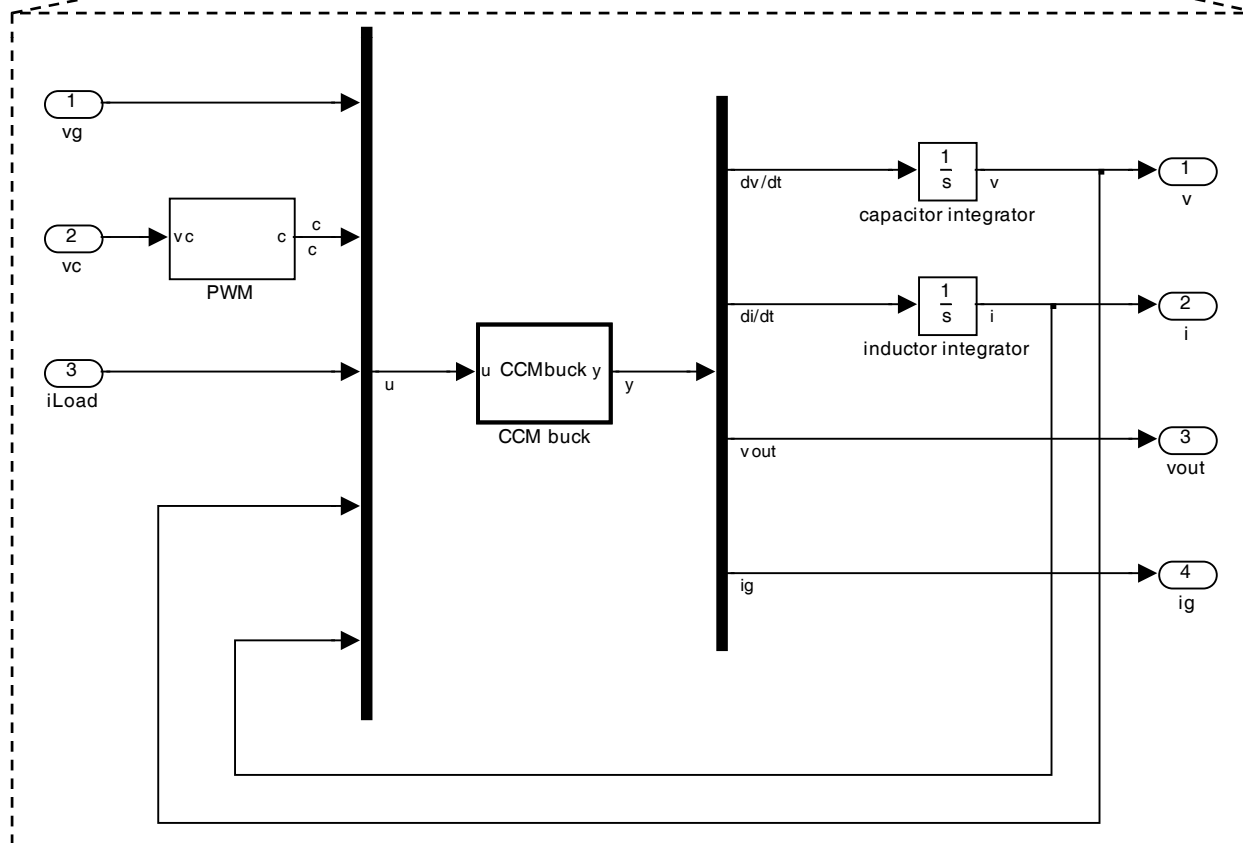
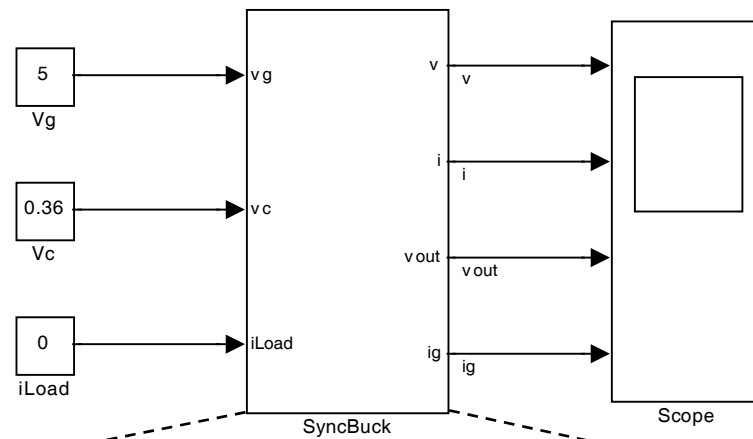
Output equations

$$i_g = \begin{cases} i & (c = 1) \\ 0 & (c = 0) \end{cases}$$

$$v_{out} = v + R_{esr}(i - i_{Load})$$

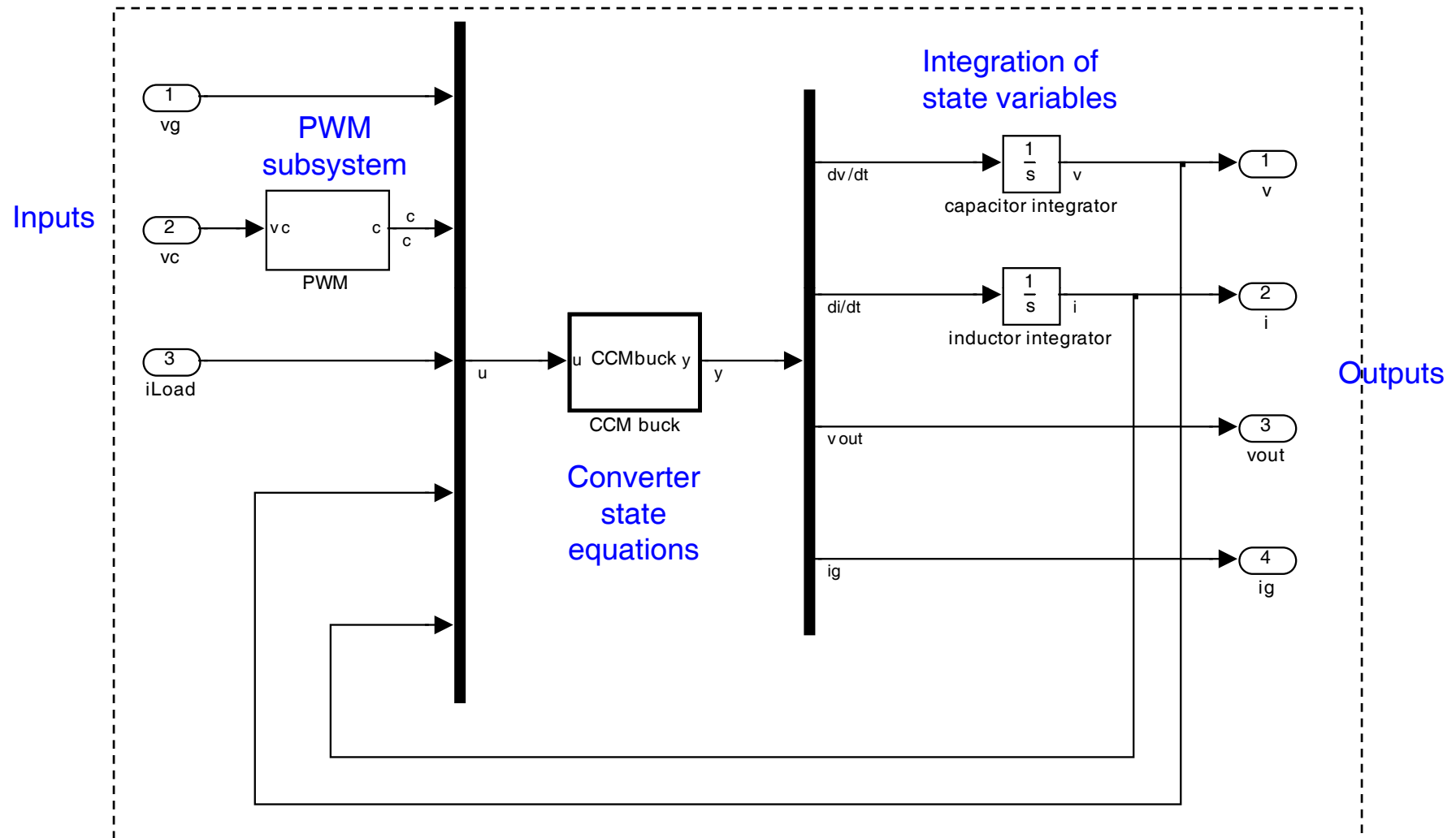
Simulink model

SyncBuck subsystem block

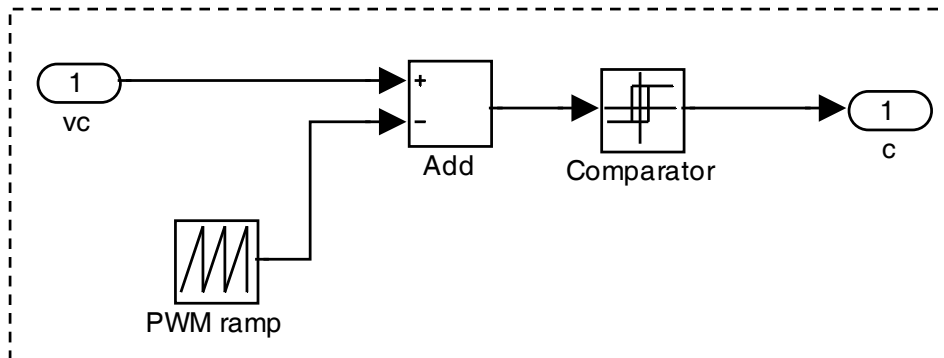
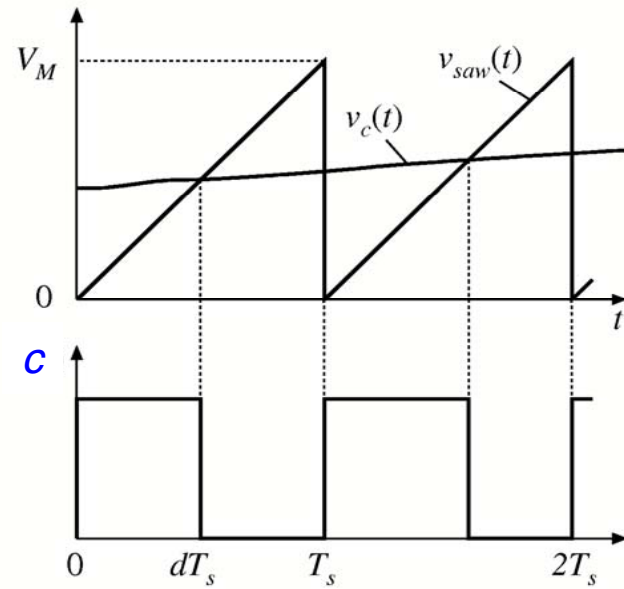
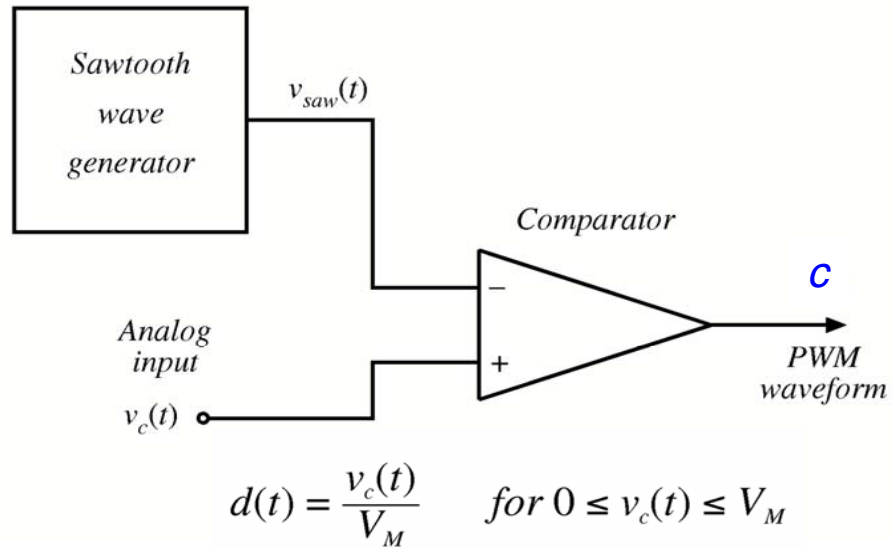


SyncBuck subsystem block internals

Synchronous buck (SyncBuck) subsystem

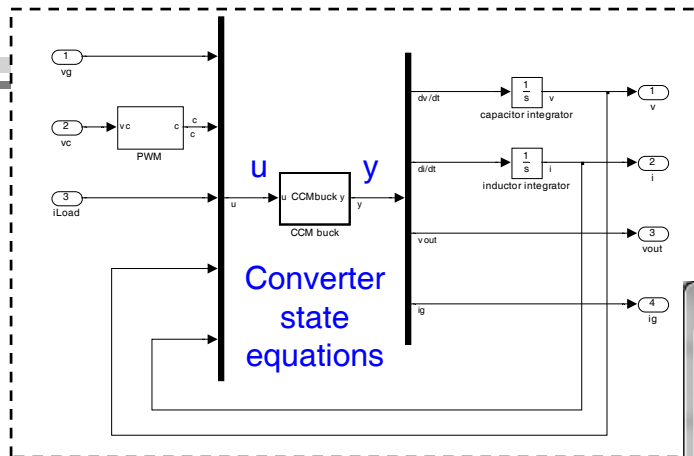


PWM operation and model



Simulink PWM model

Converter state equations: embedded MATLAB script



$u = \text{inputs} = [v_g \ c \ i_{\text{Load}} \ v \ i]$
 $y = \text{outputs} = [i_c/C \ v_L/L \ v_{\text{out}} \ i_g]$

```

Embedded MATLAB Editor - Block: syncbuck_OL/SyncBuck/CCM buck
File Edit Text Debug Tools Window Help
[Icons]
1 function y = CCMbuck(u,L,C,RL,Ron1,Ron2,Resr)
2 % State equations of a synchronous buck converter
3 % Conduction losses due to RL, Ron1, Ron2, Resr are included
4 % Inputs: u = [vg d iLoad v i]
5 % Outputs: y = [iC/C vL/L vout ig]
6 % Parameters: L, C, RL, Ron1, Ron2, Resr
7 %
8 % variables
9 - vg = u(1); % input voltage
10 - d = u(2); % switch control d=c (in the switching model), d in the averaged model
11 - iLoad = u(3); % load current
12 - v = u(4); % capacitor voltage
13 - i = u(5); % inductor current
14 %
15 % state equations
16 - vout = v + Resr*(i-iLoad); % output voltage
17 - ig = d*i; % input current
18 - iC = i - iLoad; % capacitor current
19 - vL = d*(vg - (Ron1+RL)*i - vout) + (1-d)*(-(Ron2+RL)*i - vout); % inductor voltage
20 %
21 % output
22 - y = [iC/C vL/L vout ig];
    
```

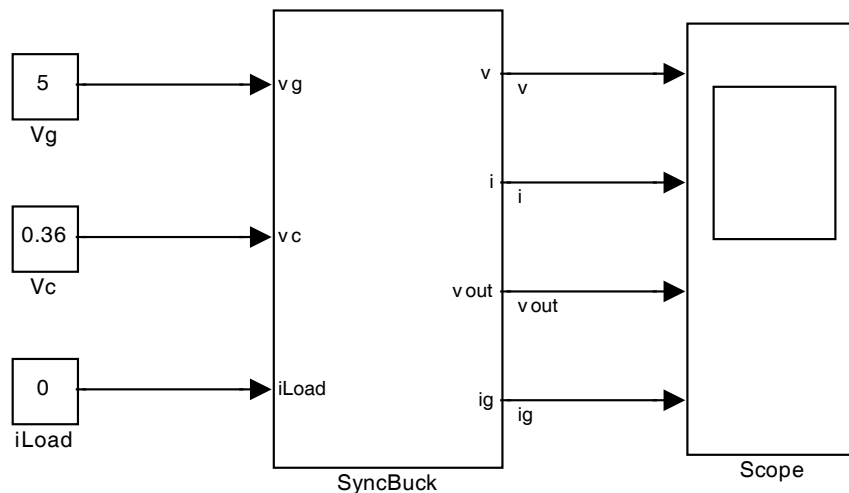
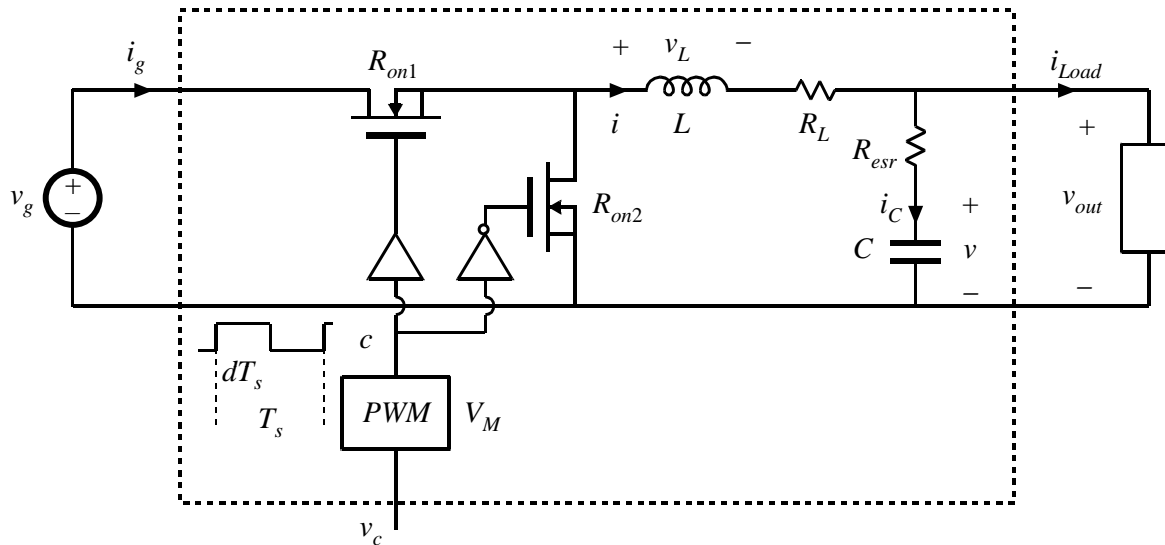
$$v_{out} = v + R_{esr} (i - i_{Load})$$

$$i_g = \begin{cases} i & (c=1) \\ 0 & (c=0) \end{cases}$$

$$i_C = C \frac{dv}{dt} = i - i_{Load}$$

$$v_L = L \frac{di}{dt} = \begin{cases} v_g - (R_{on1} + R_L)i - v_{out} & (c=1) \\ -(R_{on2} + R_L)i - v_{out} & (c=0) \end{cases}$$

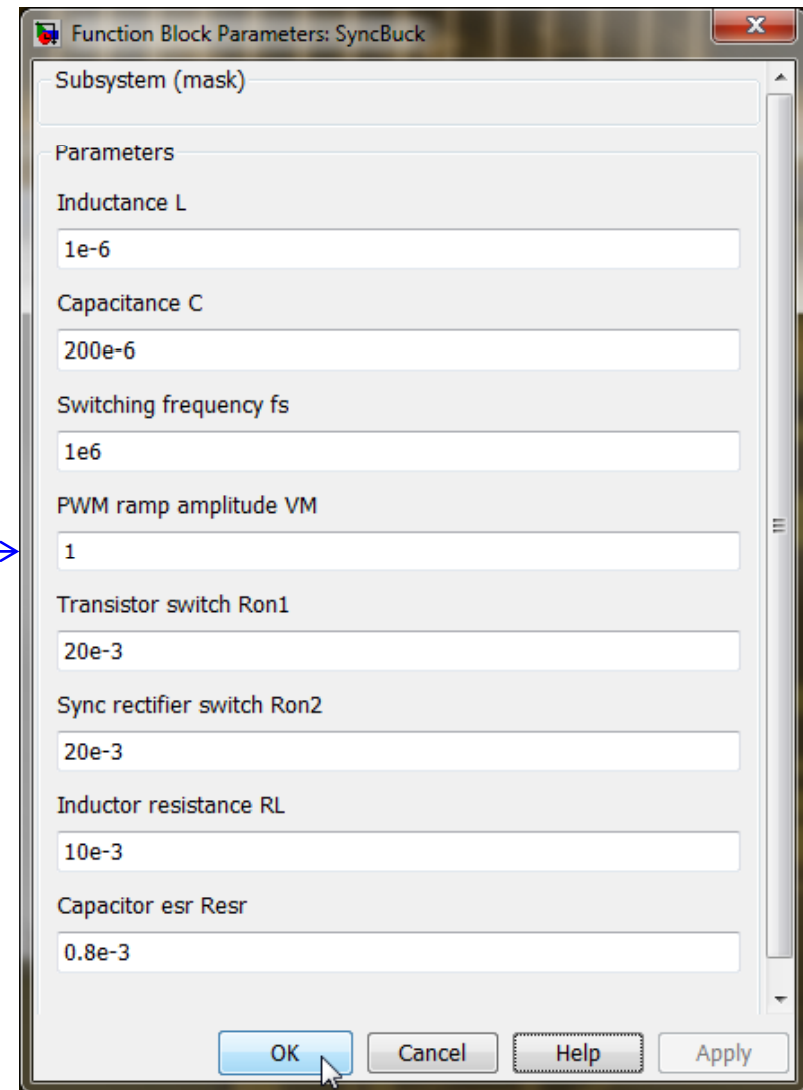
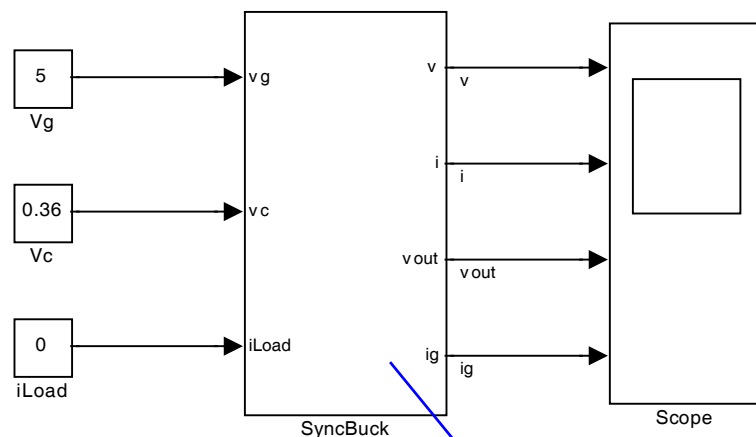
Numerical example



Simulink model: [syncbuck_OL.mdl](#)

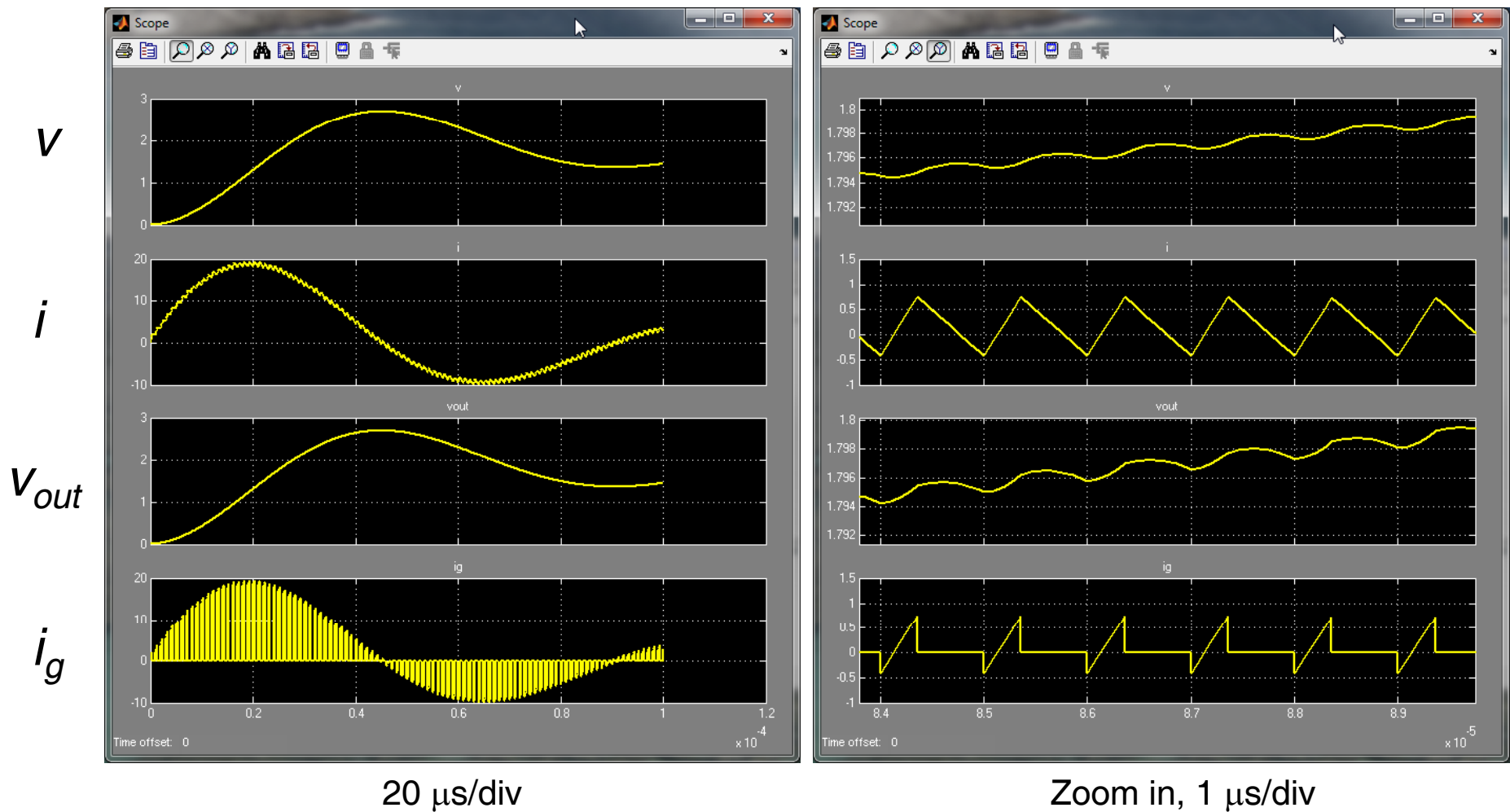
- Switching frequency:
 $f_s = 1\text{ MHz}$
- $I_{out} = 0$
- $V_g = 5\text{ V}$
- $L = 1\text{ }\mu\text{H}$
- $R_L = 10\text{ m}\Omega$
- $R_{on1} = R_{on2} = 20\text{ m}\Omega$
- $C = 200\text{ }\mu\text{F}$
- $R_{esr} = 0.8\text{ m}\Omega$
- PWM ramp amplitude
 $V_M = 1\text{ V}$
- $V_c = 0.36$, $D = 0.36$

Numerical example: synchronous buck converter model



- “Masking” a Simulink subsystem allows parameterization
- Same subsystem model can be re-used
- Models and MATLAB scripts can be collected in a library

Switching simulation: open-loop start-up transient



Averaged model

$$v_L = L \frac{di}{dt} = \begin{cases} v_g - (R_{on1} + R_L)i - v_{out} & (c = 1) \\ -(R_{on2} + R_L)i - v_{out} & (c = 0) \end{cases}$$

$$i_C = C \frac{dv}{dt} = i - i_{Load}$$

$$i_g = \begin{cases} i & (c = 1) \\ 0 & (c = 0) \end{cases}$$

$$v_{out} = v + R_{esr}(i - i_{Load})$$

Switching model

State-space averaging (review Textbook Sections 7.1-7.3)

$$\langle v_L \rangle_{T_s} = L \frac{d\langle i \rangle_{T_s}}{dt} = d \left(\langle v_g \rangle_{T_s} - (R_{on1} + R_L) \langle i \rangle_{T_s} - \langle v_{out} \rangle_{T_s} \right) + (1-d) \left(- (R_{on2} + R_L) \langle i \rangle_{T_s} - \langle v_{out} \rangle_{T_s} \right)$$

$$\langle i_C \rangle_{T_s} = C \frac{d\langle v \rangle_{T_s}}{dt} = \langle i \rangle_{T_s} - \langle i_{Load} \rangle_{T_s}$$

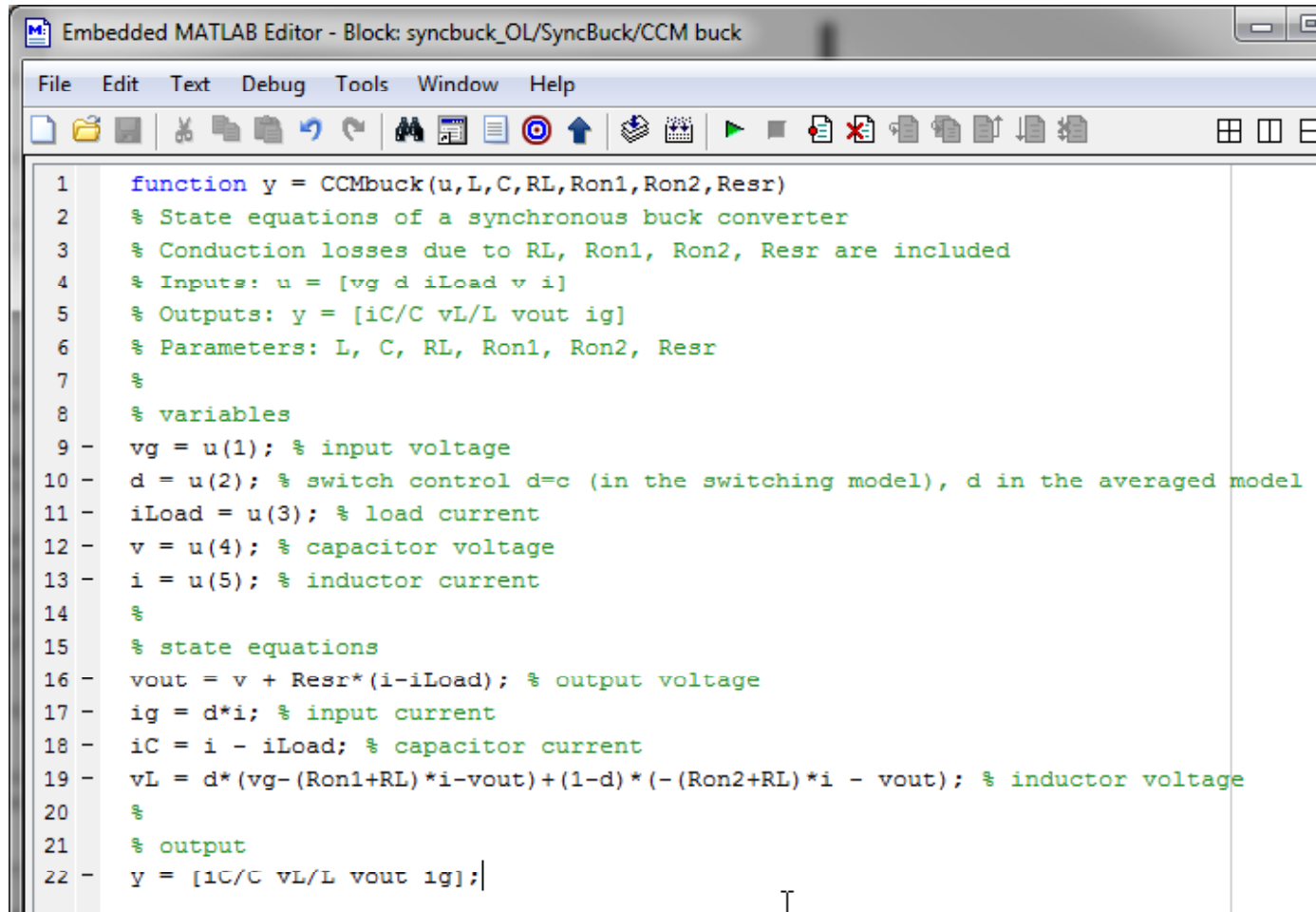
$$\langle i_g \rangle_{T_s} = d \langle i \rangle_{T_s}$$

$$\langle v_{out} \rangle_{T_s} = \langle v \rangle_{T_s} + R_{esr} (\langle i \rangle_{T_s} - \langle i_{Load} \rangle_{T_s})$$

Large-signal
averaged model

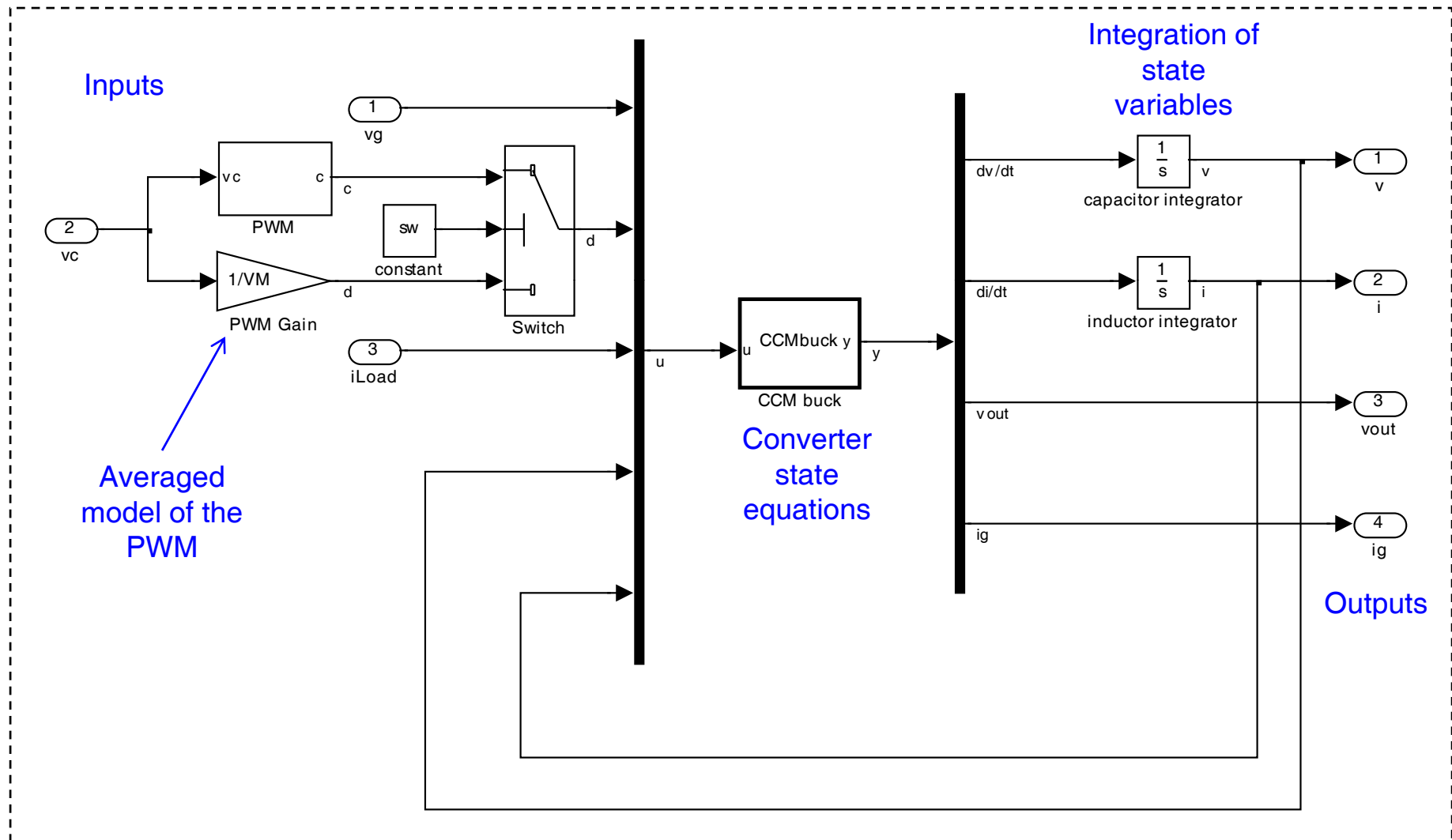
Converter averaged state equations: MATLAB

The MATLAB function stays exactly the same, except d (duty-cycle) replaces c (switch control)

The image shows a screenshot of the 'Embedded MATLAB Editor' window. The title bar reads 'Embedded MATLAB Editor - Block: syncbuck_OL/SyncBuck/CCM buck'. The menu bar includes 'File', 'Edit', 'Text', 'Debug', 'Tools', 'Window', and 'Help'. Below the menu is a toolbar with various icons for file operations, editing, and execution. The main editor area displays the MATLAB function 'function y = CCMbuck(u,L,C,RL,Ron1,Ron2,Resr)'. The code includes comments for state equations, conduction losses, inputs, outputs, and parameters. It defines variables for input voltage, switch control, load current, capacitor voltage, and inductor current. The state equations for output voltage, input current, capacitor current, and inductor voltage are calculated. Finally, the output vector 'y' is defined as [iC/C vL/L vout ig].

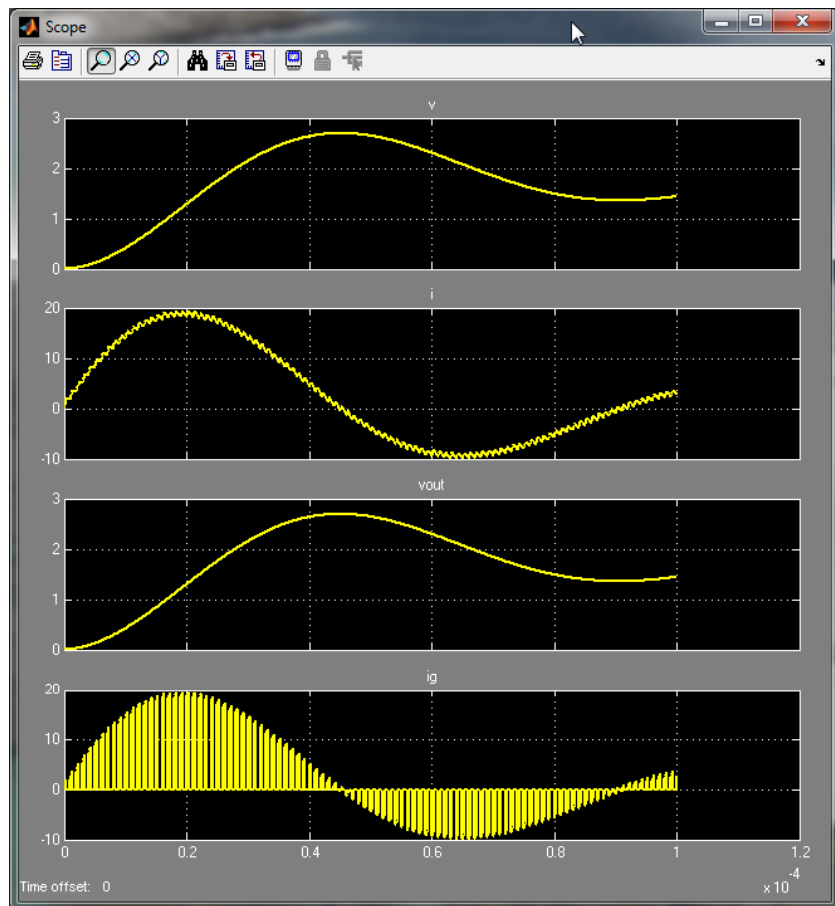
```
1 function y = CCMbuck(u,L,C,RL,Ron1,Ron2,Resr)
2 % State equations of a synchronous buck converter
3 % Conduction losses due to RL, Ron1, Ron2, Resr are included
4 % Inputs: u = [vg d iLoad v i]
5 % Outputs: y = [iC/C vL/L vout ig]
6 % Parameters: L, C, RL, Ron1, Ron2, Resr
7 %
8 % variables
9 - vg = u(1); % input voltage
10 - d = u(2); % switch control d=c (in the switching model), d in the averaged model
11 - iLoad = u(3); % load current
12 - v = u(4); % capacitor voltage
13 - i = u(5); % inductor current
14 %
15 % state equations
16 - vout = v + Resr*(i-iLoad); % output voltage
17 - ig = d*i; % input current
18 - iC = i - iLoad; % capacitor current
19 - vL = d*(vg-(Ron1+RL)*i-vout)+(1-d)*(-(Ron2+RL)*i - vout); % inductor voltage
20 %
21 % output
22 - y = [iC/C vL/L vout ig];
```

Synchronous buck (SyncBuck) subsystem: switching or averaged model



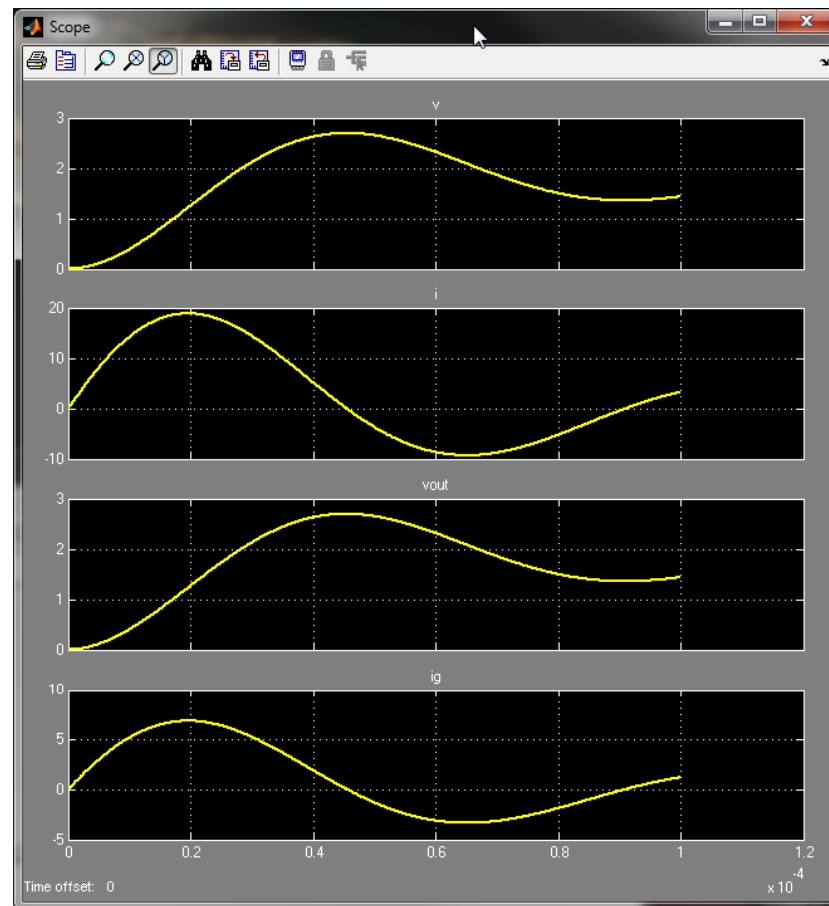
Start-up transient simulations

Switching model



v
 i
 V_{out}
 i_g

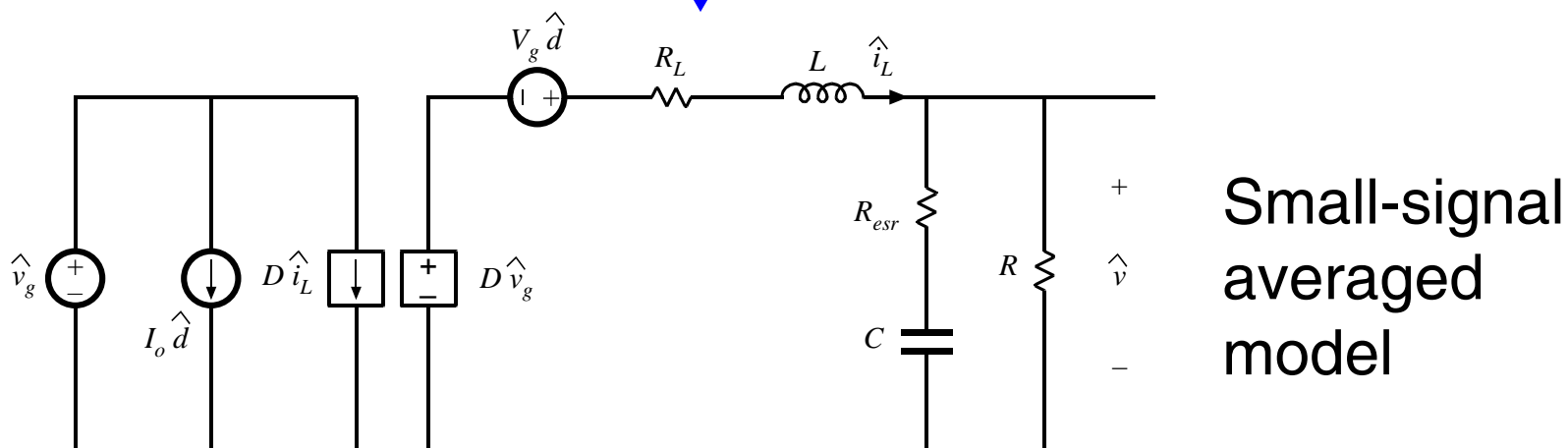
Averaged model



Linearization of the large-signal averaged model

Large-signal (nonlinear) averaged model

Linearization at an operating point



Small-signal
averaged
model

The small-signal model can be solved for all important converter transfer functions:

$$G_{vd}(s) = \frac{\hat{v}}{\hat{d}}$$

Control-to-output

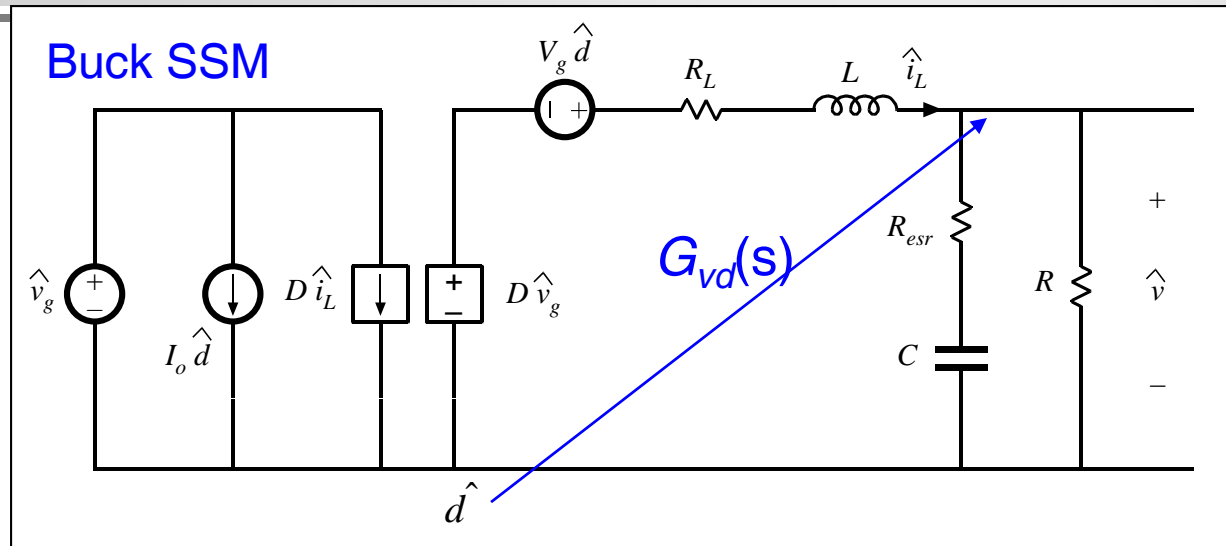
$$G_{vg}(s) = \frac{\hat{v}}{\hat{v}_g}$$

Line-to-output

$$Z_{out}(s) = \frac{\hat{v}}{\hat{i}_{load}}$$

Output impedance

Synchronous buck converter example



$$G_{vd}(s) = \frac{\hat{v}_o}{\hat{d}}$$

$$G_{vd}(s) = V_g \frac{1 + \frac{s}{\omega_{esr}}}{1 + \frac{1}{Q} \frac{s}{\omega_o} + \left(\frac{s}{\omega_o} \right)^2}$$

Pair of poles:

$$f_o = \frac{1}{2\pi\sqrt{CL}} = 11 \text{ kHz}$$

$$Q_{loss} = \frac{\sqrt{L/C}}{R_{esr} + R_L} = 2.3 \rightarrow 7.2 \text{ dB} \quad Q_{load} = \frac{R}{\sqrt{L/C}} > 5$$

$$Q = Q_{loss} \parallel Q_{load} = \frac{Q_{loss} Q_{load}}{Q_{loss} + Q_{load}} < 2.3 \rightarrow 7.2 \text{ dB}$$

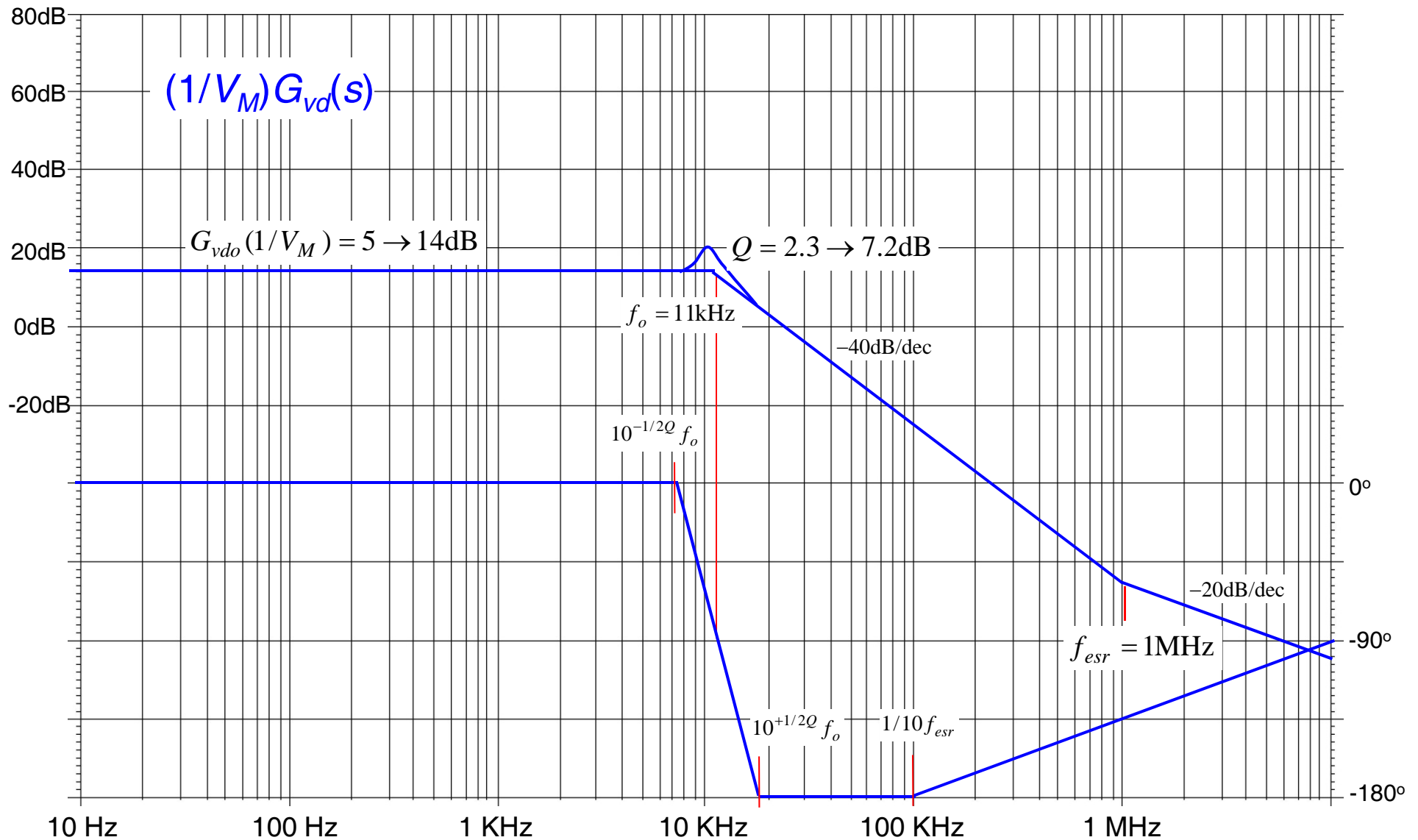
Low-frequency gain:

$$G_{vdo} = 5\text{V} \rightarrow 14\text{dBV}$$

ESR zero:

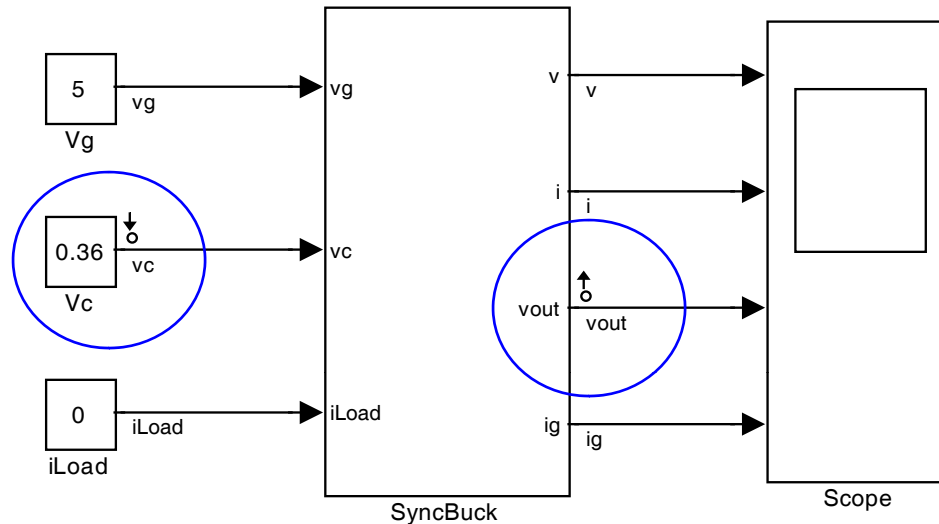
$$f_{esr} = \frac{1}{2\pi C R_{esr}} = 1 \text{ MHz}$$

Magnitude and phase Bode plots of G_{vd}



Linearization and frequency responses in MATLAB/Simulink

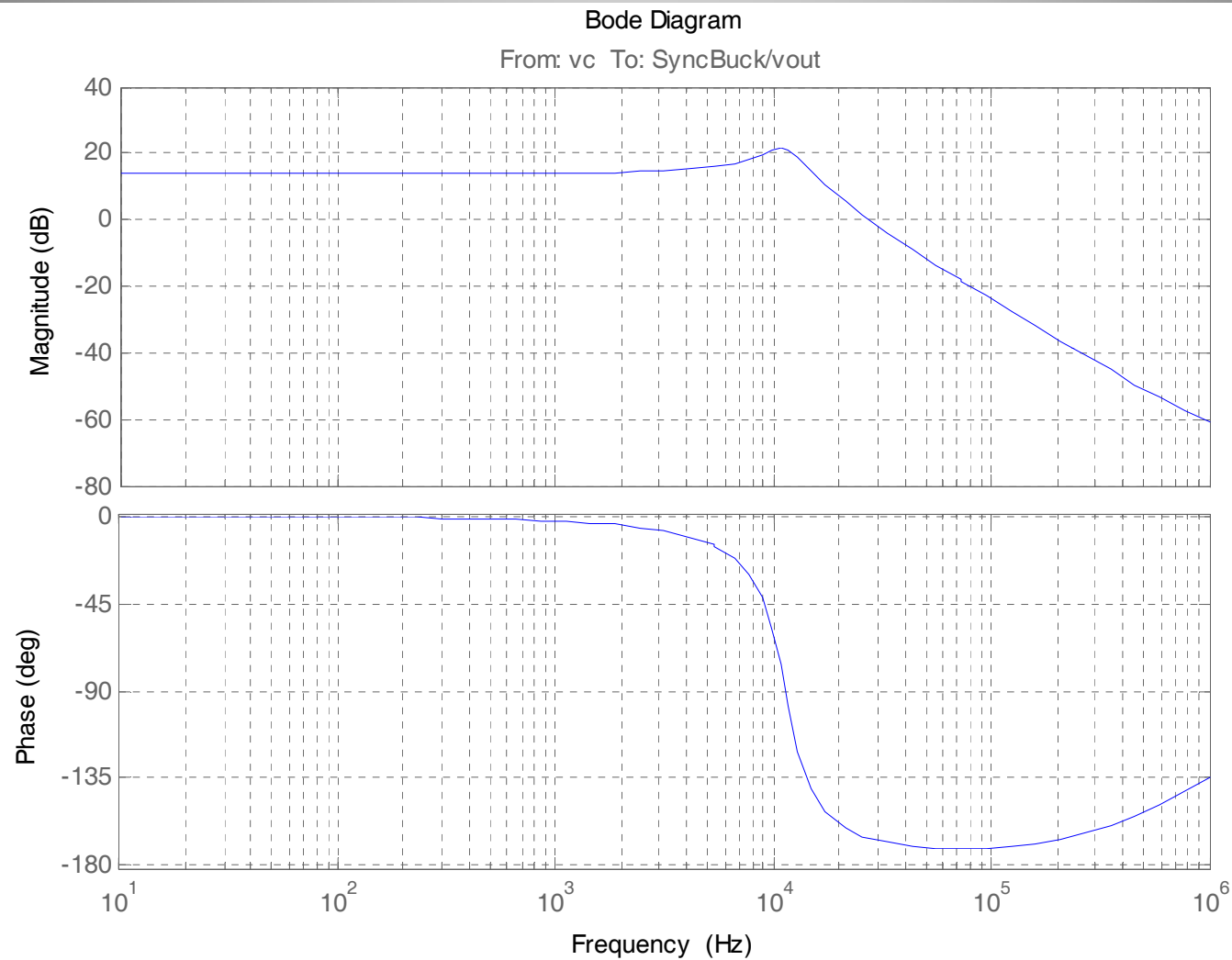
1. Set transfer function input and output points



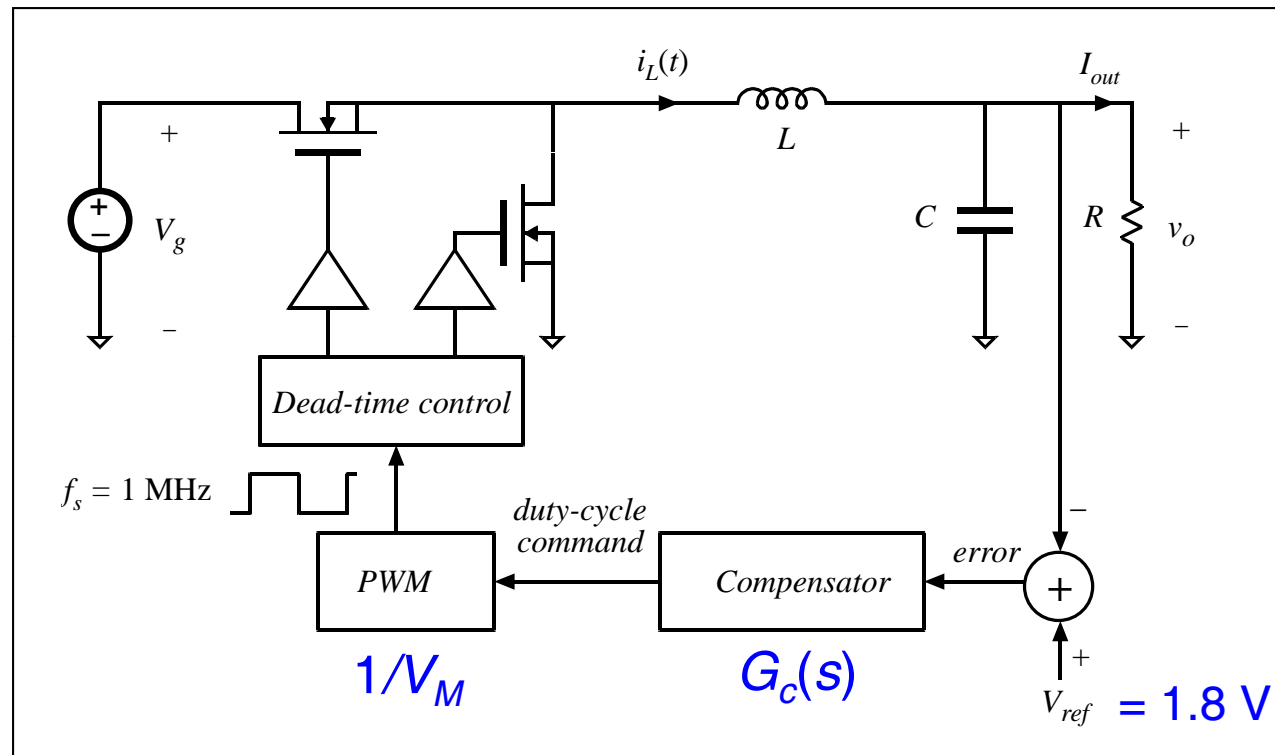
2. MATLAB script (BodePlotter_script.m) computes DC operating point, linearizes the model, computes and plots the transfer function magnitude and phase responses

```
1 %% Bode plotter using linearization tool
2 % requires Simulink Control Design toolbox
3 %
4 %
5 model = 'syncbuck_OL'; % set to file name of simulink model. Must have i/o points set within this model
6 io = getlinio(model) % get i/o signals of model
7 op = operspec(model)
8 op = findop(model,op) % calculate model operating point
9 ssm = linearize(model,op,io) % compute state space model of linearized system
10 %
11 %
12 ltiview('bode',ssm) % send linearized model to LTI Viewer tool
13 %
```

Magnitude and phase Bode plots of G_{vd}

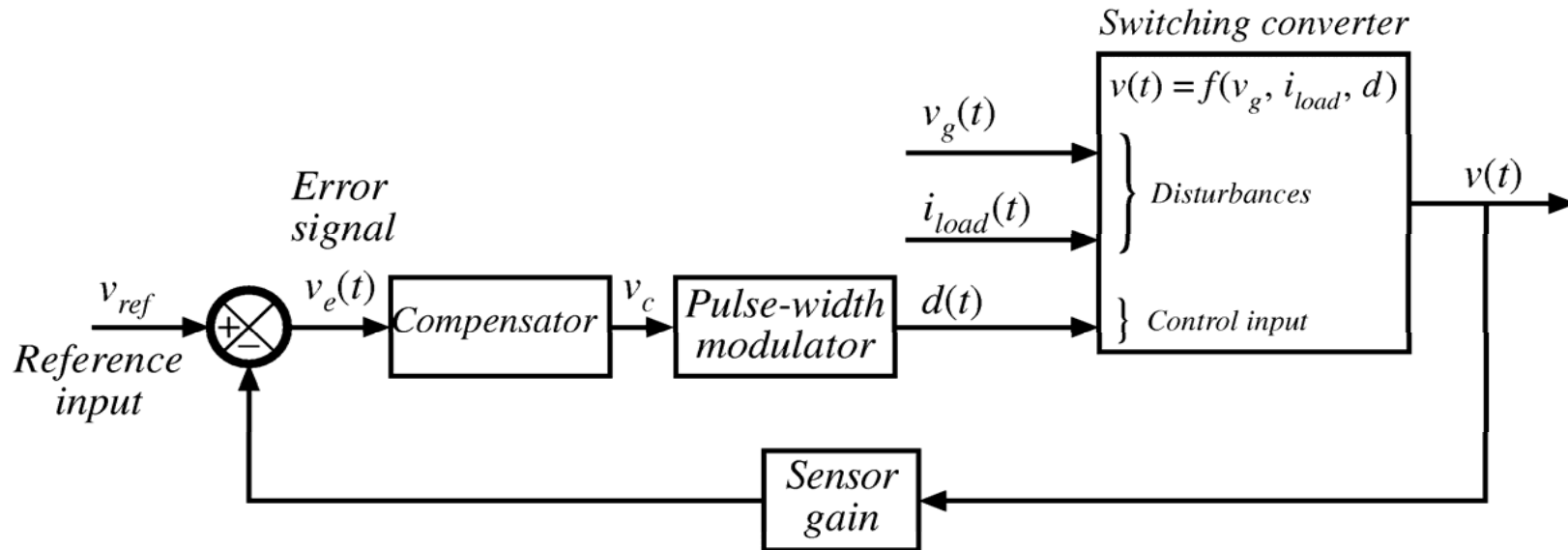


Closed-loop (voltage-mode) control



Point-of-Load (POL) Synchronous Buck Regulator

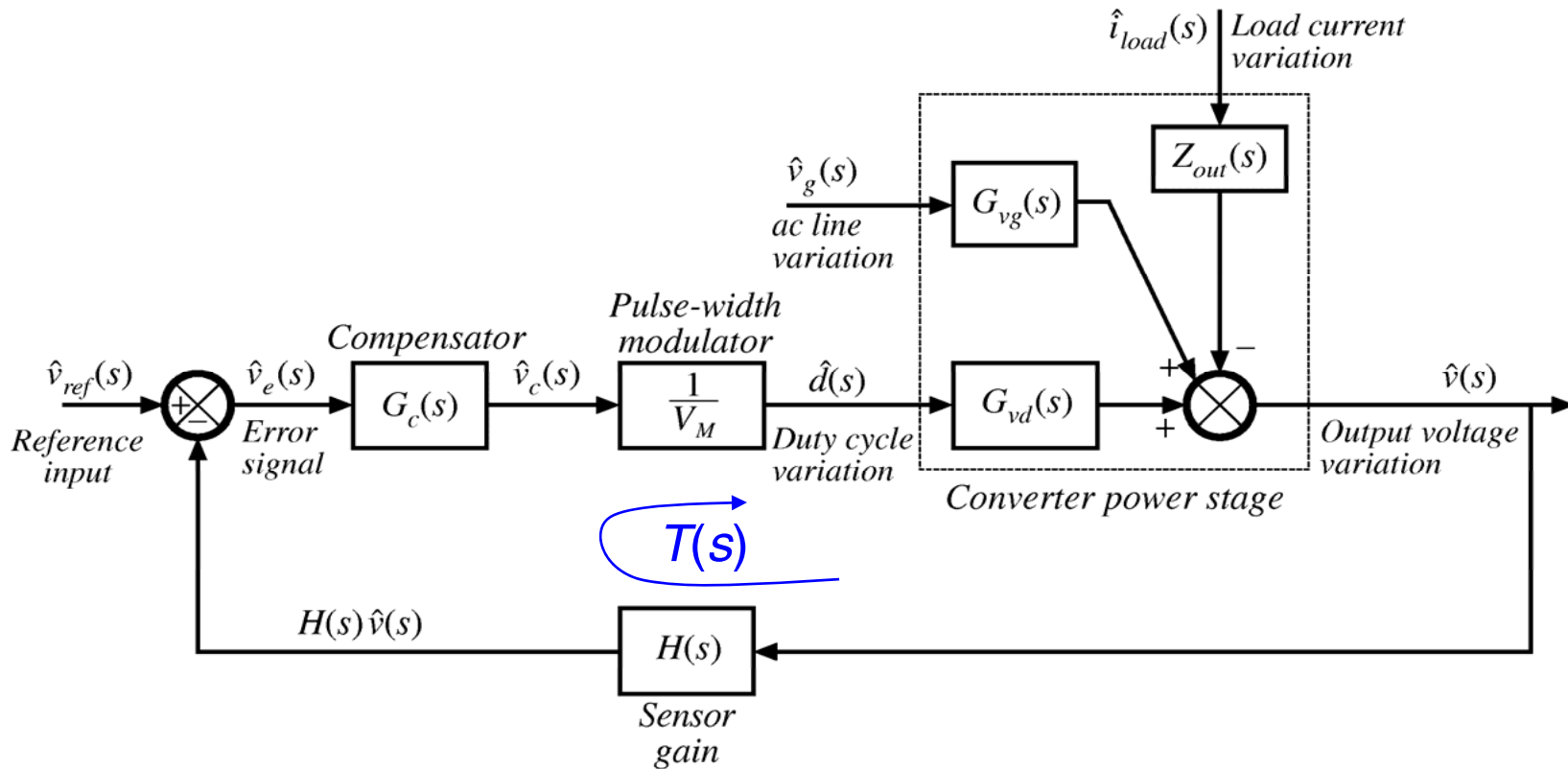
Closed-loop SMPS block diagram



Control objectives: tight output voltage regulation

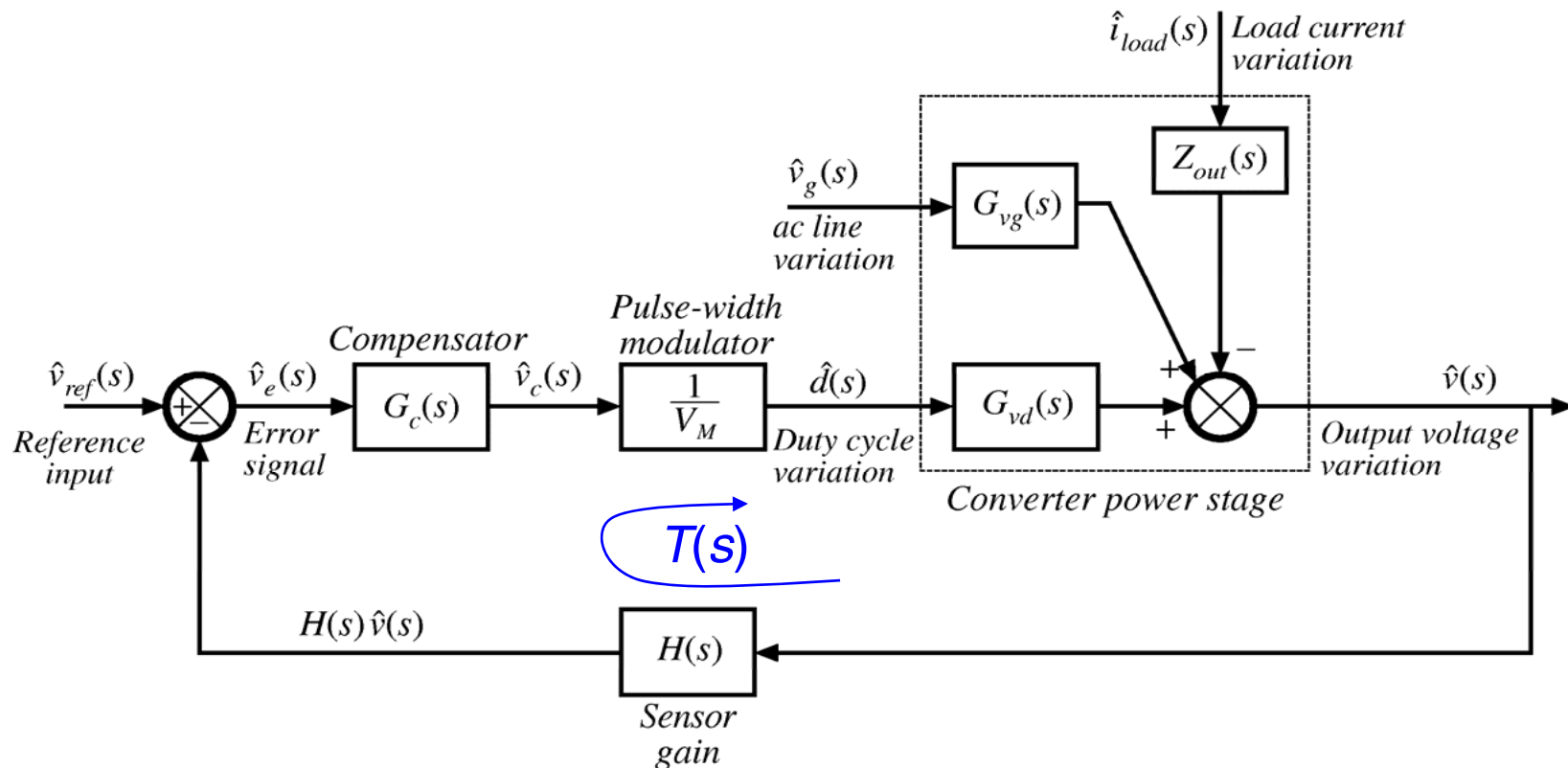
- Static or dynamic disturbances
 - Input (line) voltage v_g
 - Load current i_{load}
- Component tolerances

Small-signal model: loop gain T



Loop gain:
$$T(s) = H(s)G_c(s)(1/V_M)G_{vd}(s)$$

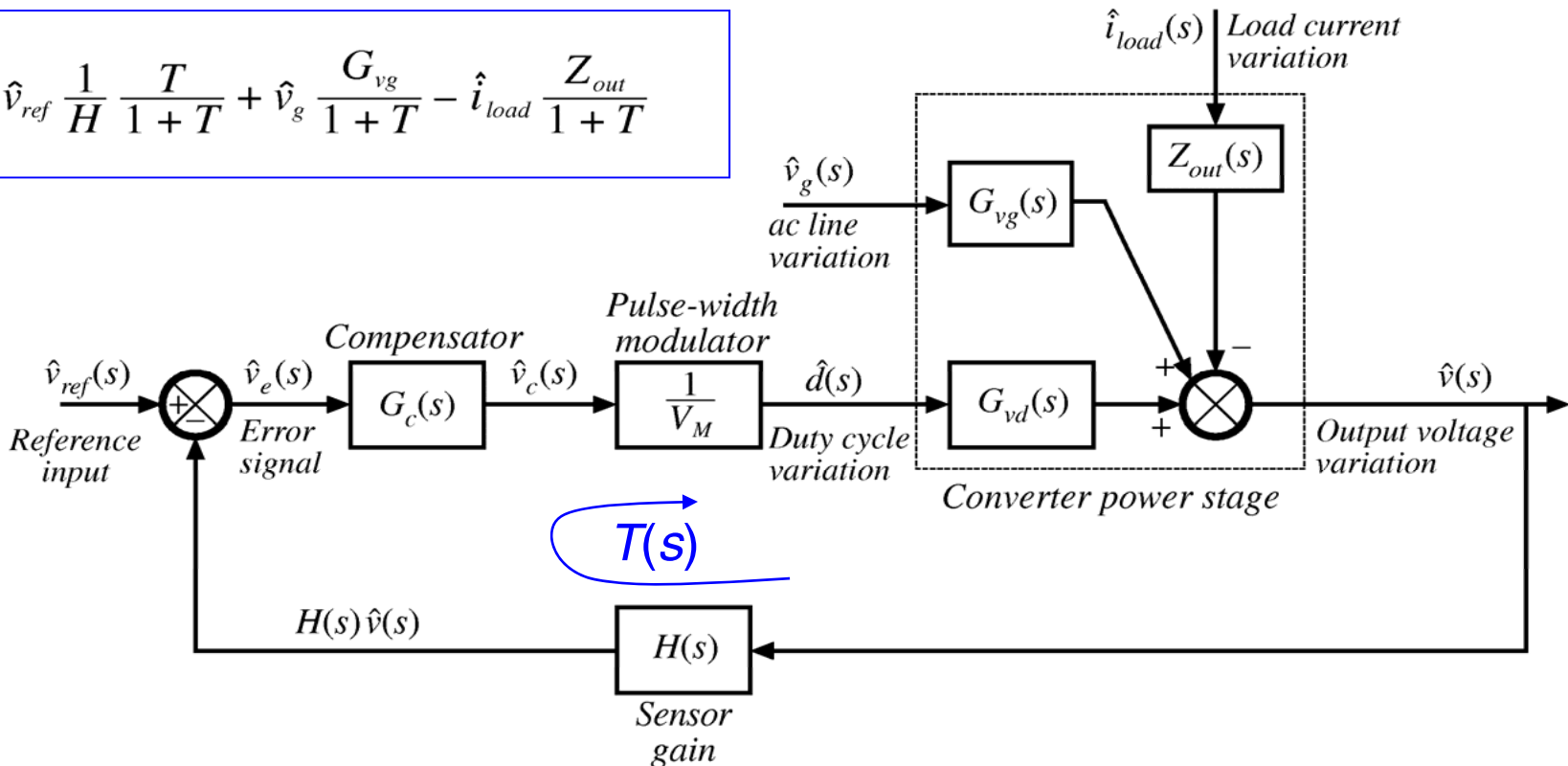
Small-signal model: closed-loop responses



$$\hat{v} = \hat{v}_{ref} \frac{1}{H} \frac{T}{1+T} + \hat{v}_g \frac{G_{vg}}{1+T} - \hat{i}_{load} \frac{Z_{out}}{1+T}$$

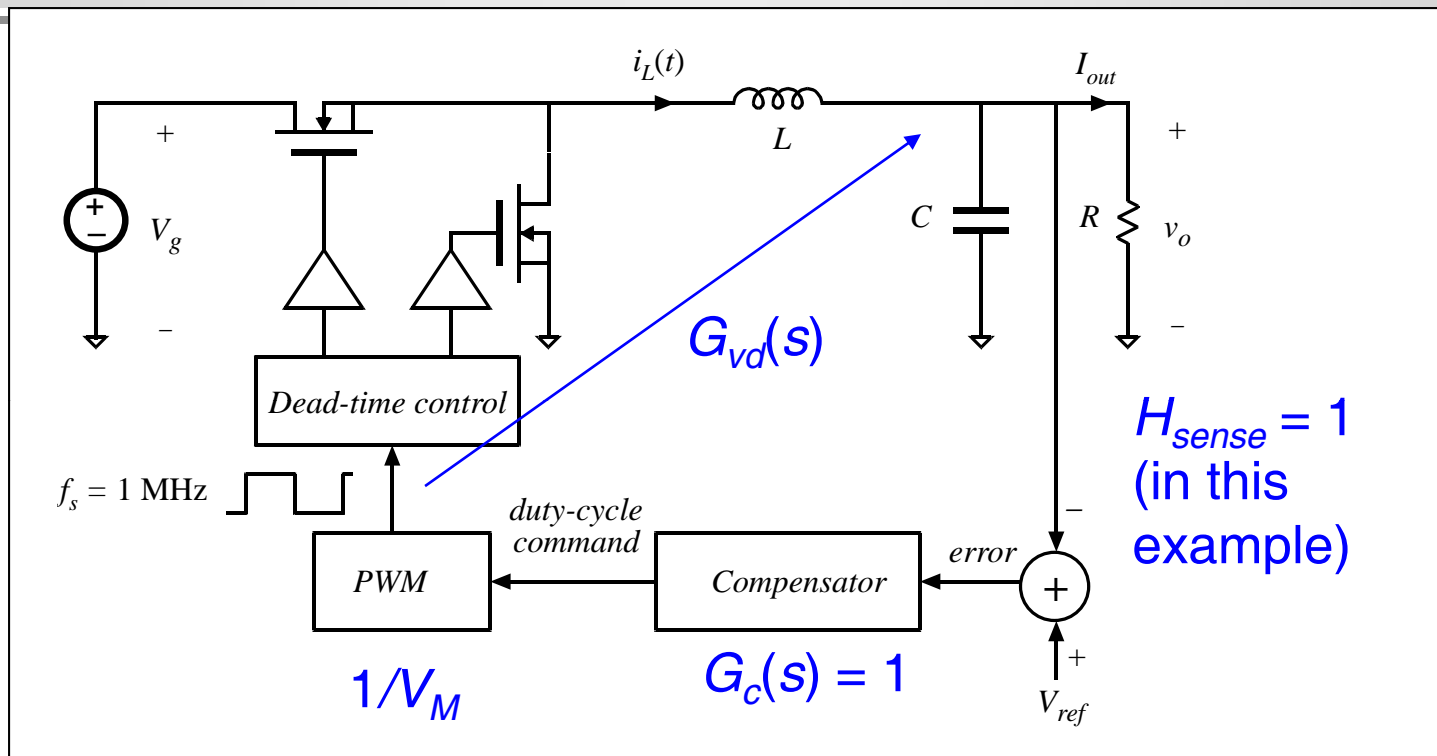
Feedback loop design objectives

$$\hat{v} = \hat{v}_{ref} \frac{1}{H} \frac{T}{1+T} + \hat{v}_g \frac{G_{vg}}{1+T} - \hat{i}_{load} \frac{Z_{out}}{1+T}$$



- To meet the control objectives, design T as large as possible in as wide frequency range as possible, i.e. with as high f_c as possible
- Limitation: stability and quality of closed-loop responses

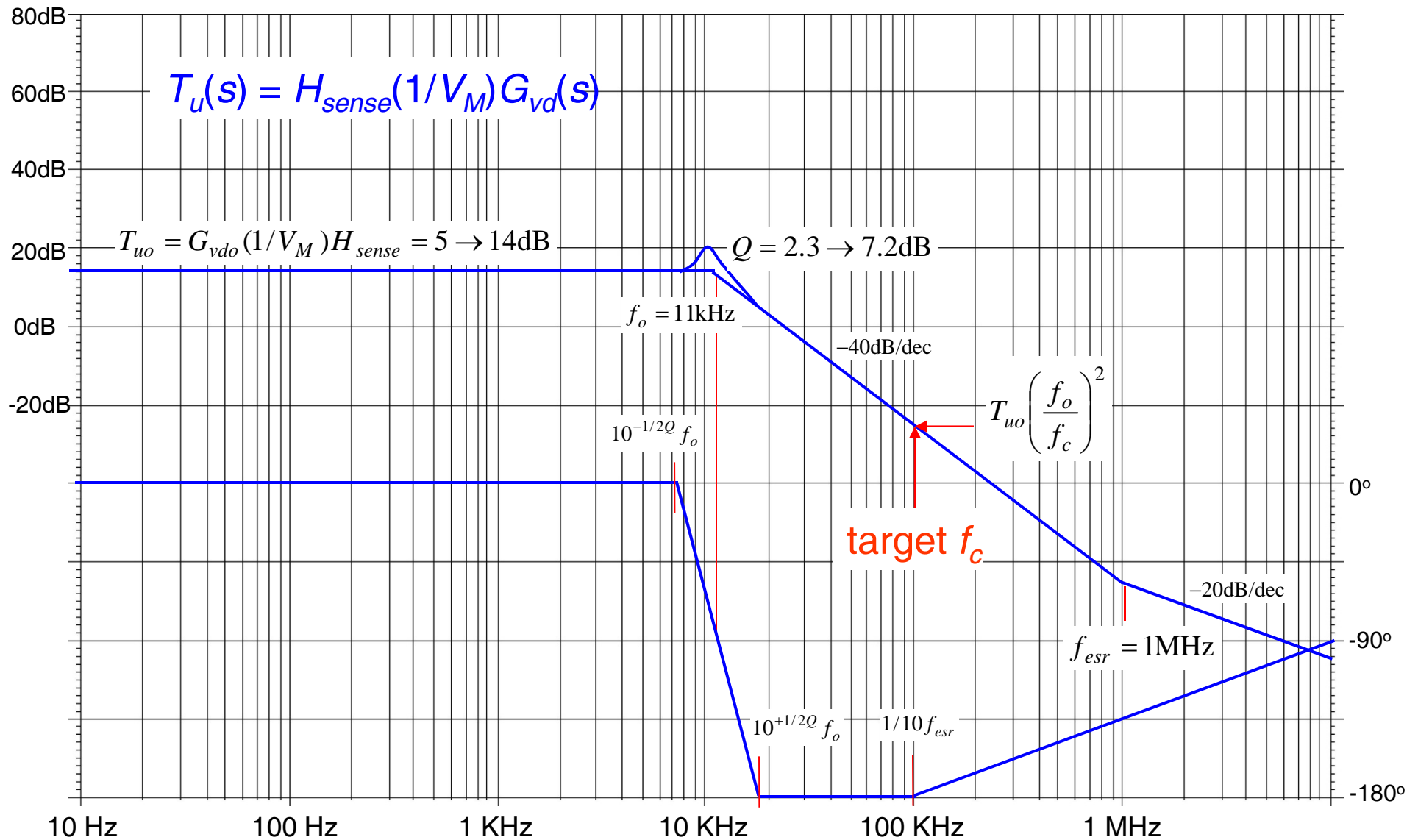
Uncompensated loop gain T_u



$$T_u(s) = H_{sense}(1/V_M)G_{vd}(s)$$

Plot magnitude and phase responses of $T_u(s)$ to plan how to design $G_c(s)$

Magnitude and phase Bode plots of T_u



Lead (PD) compensator design

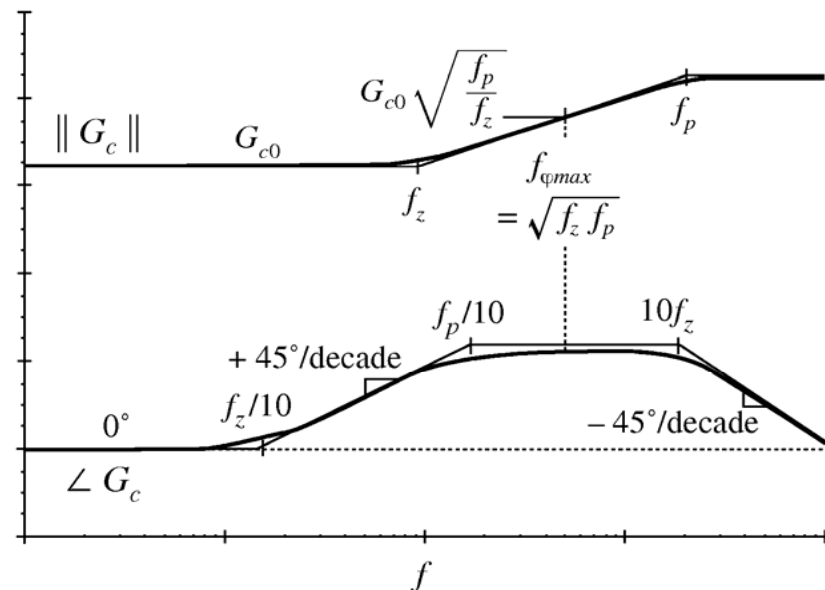
1. Choose: $f_c = 100 \text{ kHz}$

$$\theta = \varphi_m = 53^\circ$$

2. Compute:

$$f_z = f_c \sqrt{\frac{1 - \sin(\theta)}{1 + \sin(\theta)}} = 33 \text{ kHz}$$

$$f_p = f_c \sqrt{\frac{1 + \sin(\theta)}{1 - \sin(\theta)}} = 300 \text{ kHz}$$



3. Find G_{co} to position the crossover frequency:

$$\underbrace{T_{uo} \left(\frac{f_o}{f_c} \right)^2}_{\text{Magnitude of } T_u \text{ at } f_c} \underbrace{G_{co} \sqrt{\frac{f_p}{f_z}}}_{\text{Magnitude of } G_c \text{ at } f_c} = 1 \quad \rightarrow \quad G_{co} = \frac{1}{T_{uo} \left(\frac{f_o}{f_c} \right)^2} \sqrt{\frac{f_z}{f_p}} = 5.45 \rightarrow 15 \text{ dB}$$

Magnitude of T_u at f_c Magnitude of G_c at f_c

Lead (PD) compensator summary

$$G_c(s) = G_{co} \underbrace{\frac{\left(1 + \frac{s}{\omega_z}\right)}{\left(1 + \frac{s}{\omega_{p1}}\right)}}_{\text{Lead compensator}} \underbrace{\frac{1}{\left(1 + \frac{s}{\omega_{p2}}\right)}}_{\text{HF pole}}$$

$$G_{co} = 5.45 \rightarrow 15 \text{ dB}$$

$$f_z = 33 \text{ kHz}$$

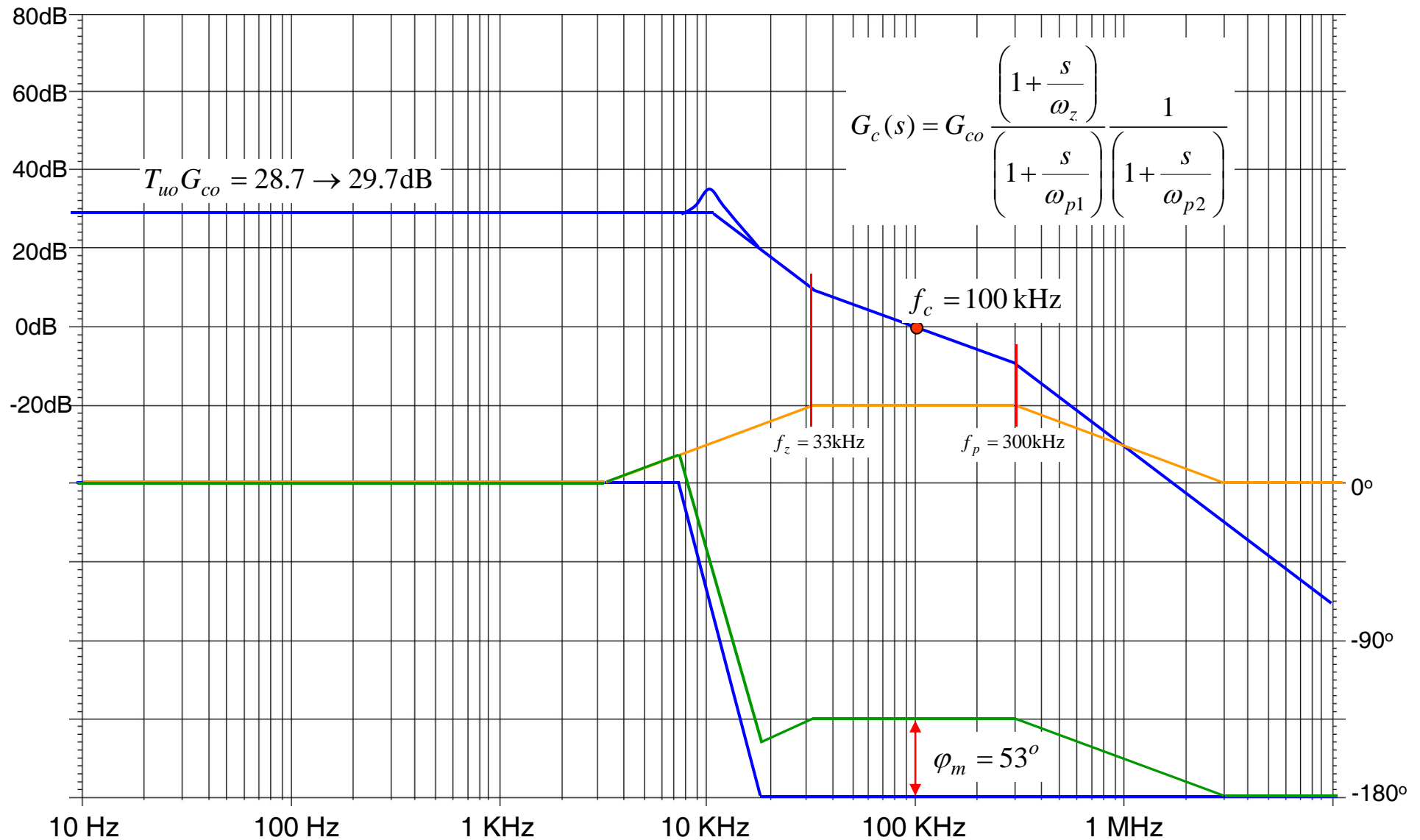
$$f_{p1} = 300 \text{ kHz}$$

$$f_c = 100 \text{ kHz} \quad (=1/10 \text{ of } f_s)$$

High-frequency gain of the lead compensator: $G_{co} f_{p1}/f_z = 49$ (34 dB)

Added high-frequency pole: $f_{p2} = 1 \text{ MHz}$ ($= f_{esr} = f_s$ in this example)

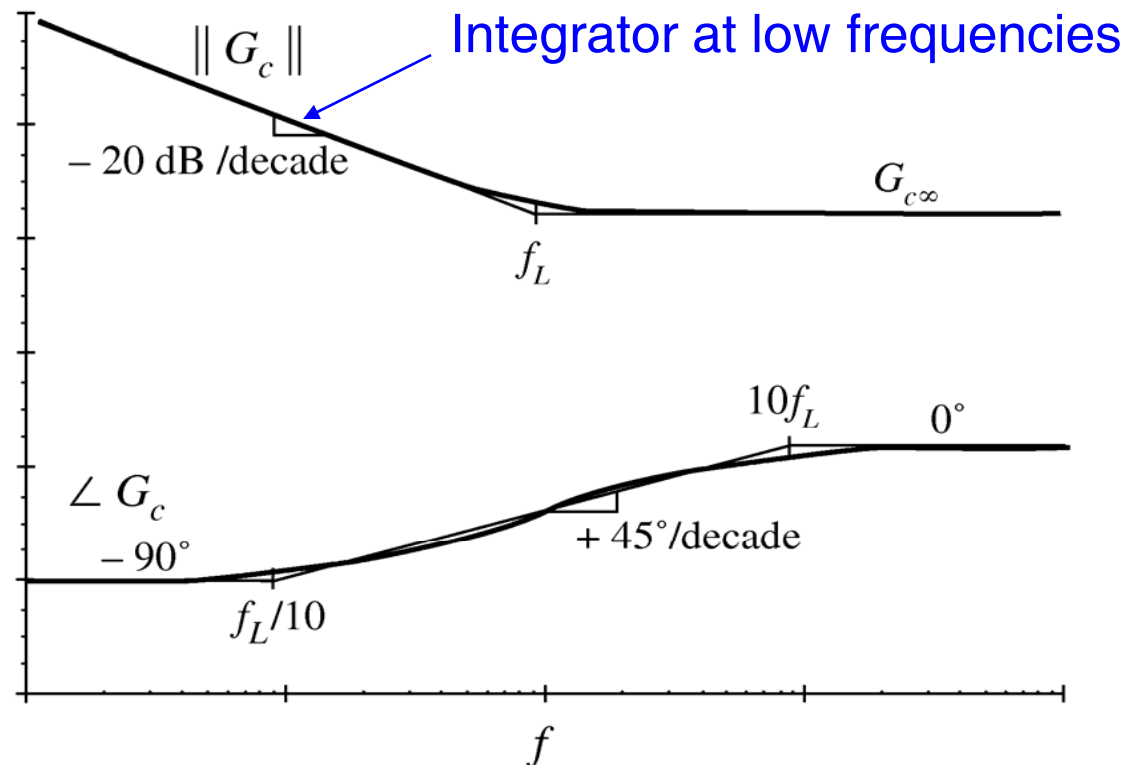
Loop gain with lead (PD) compensator



Add lag (PI) compensator

$$G_c(s) = G_{c\infty} \left(1 + \frac{\omega_L}{s} \right)$$

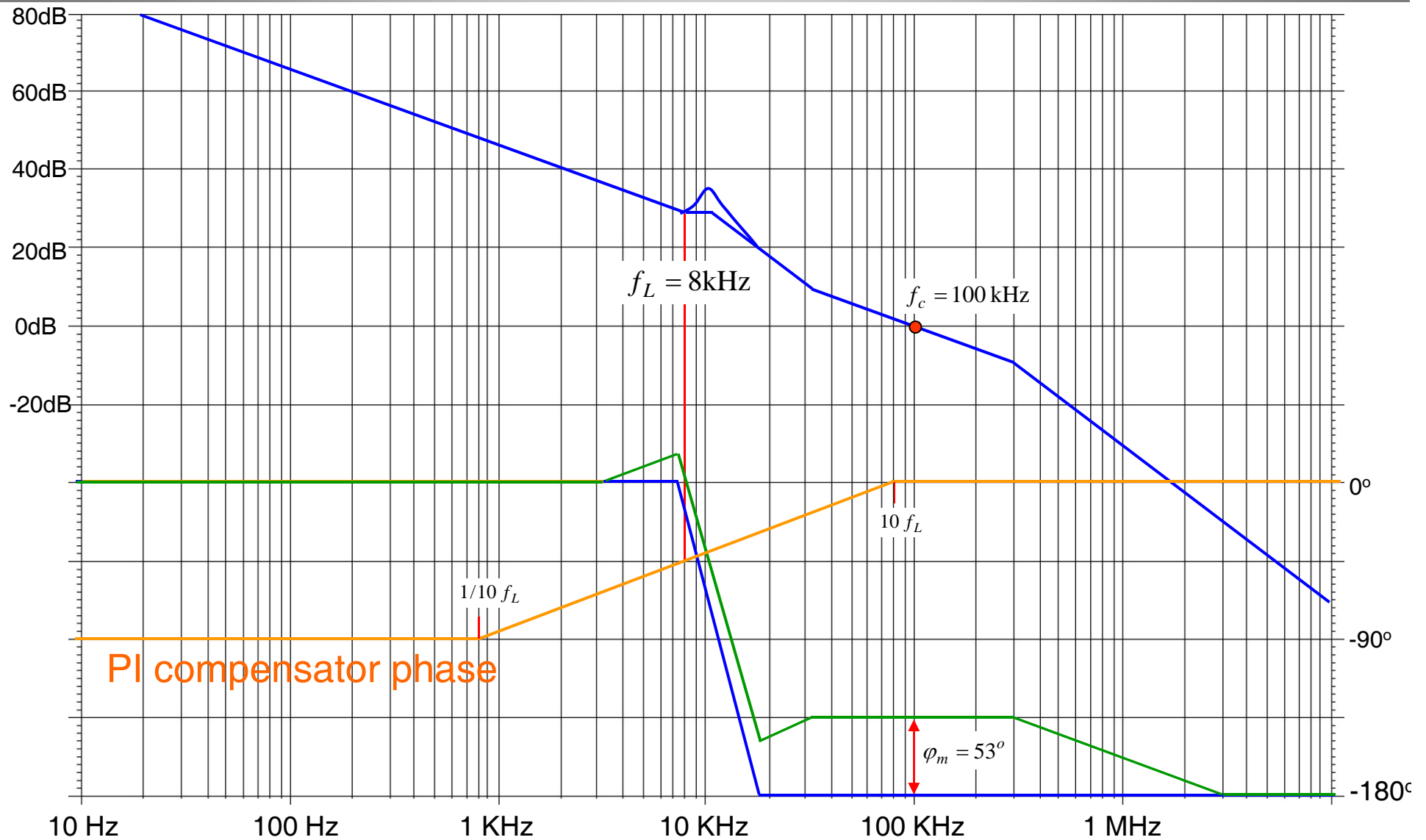
Improves low-frequency loop gain and regulation



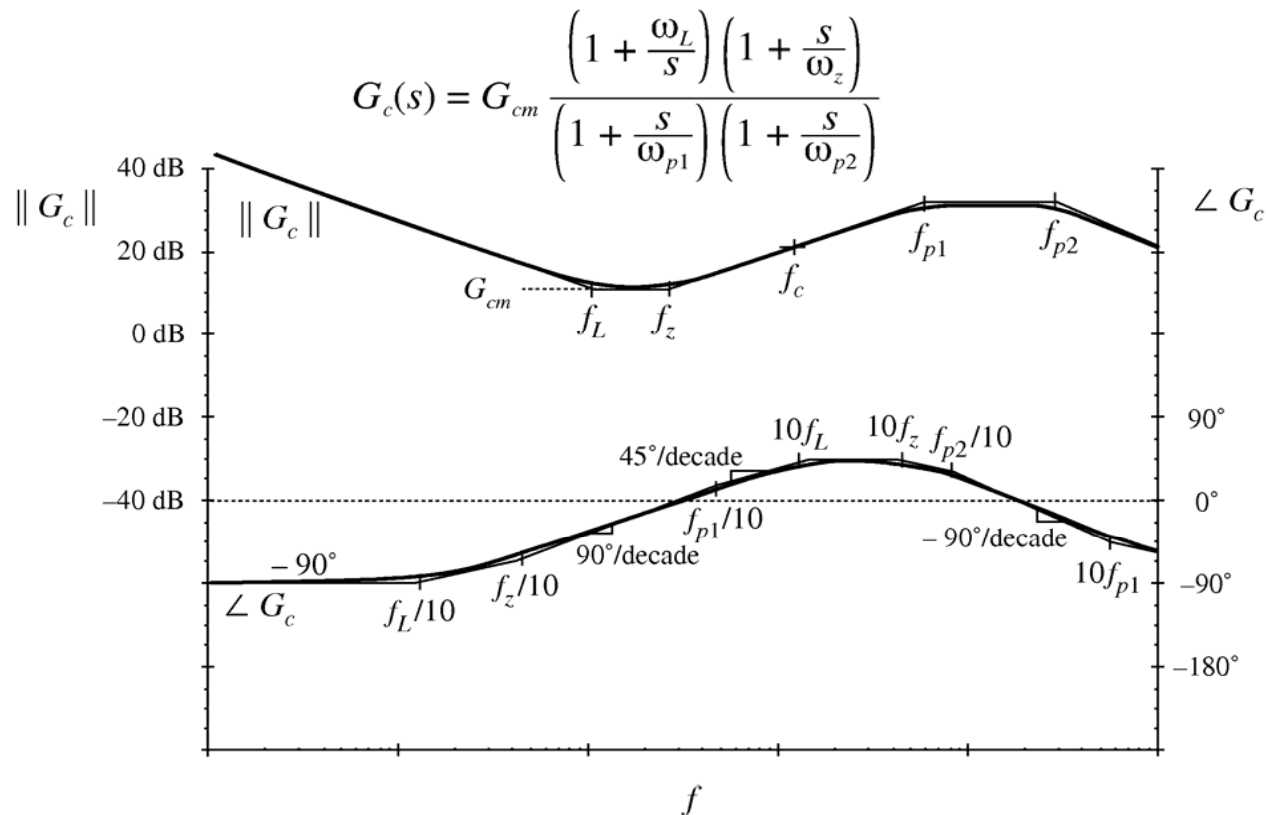
Choose $10f_L < f_c$ so that phase margin stays approximately the same: $f_L = 8$ kHz

Keep the same cross-over frequency: $G_{c\infty} = G_{co} = G_{cm} = 5.45 \rightarrow 15$ dB

Adding PI Compensator



Complete PID compensator: summary



$$G_{cm} = 5.45 \rightarrow 15 \text{ dB}$$

$$f_L = 8 \text{ kHz}$$

$$f_z = 33 \text{ kHz}$$

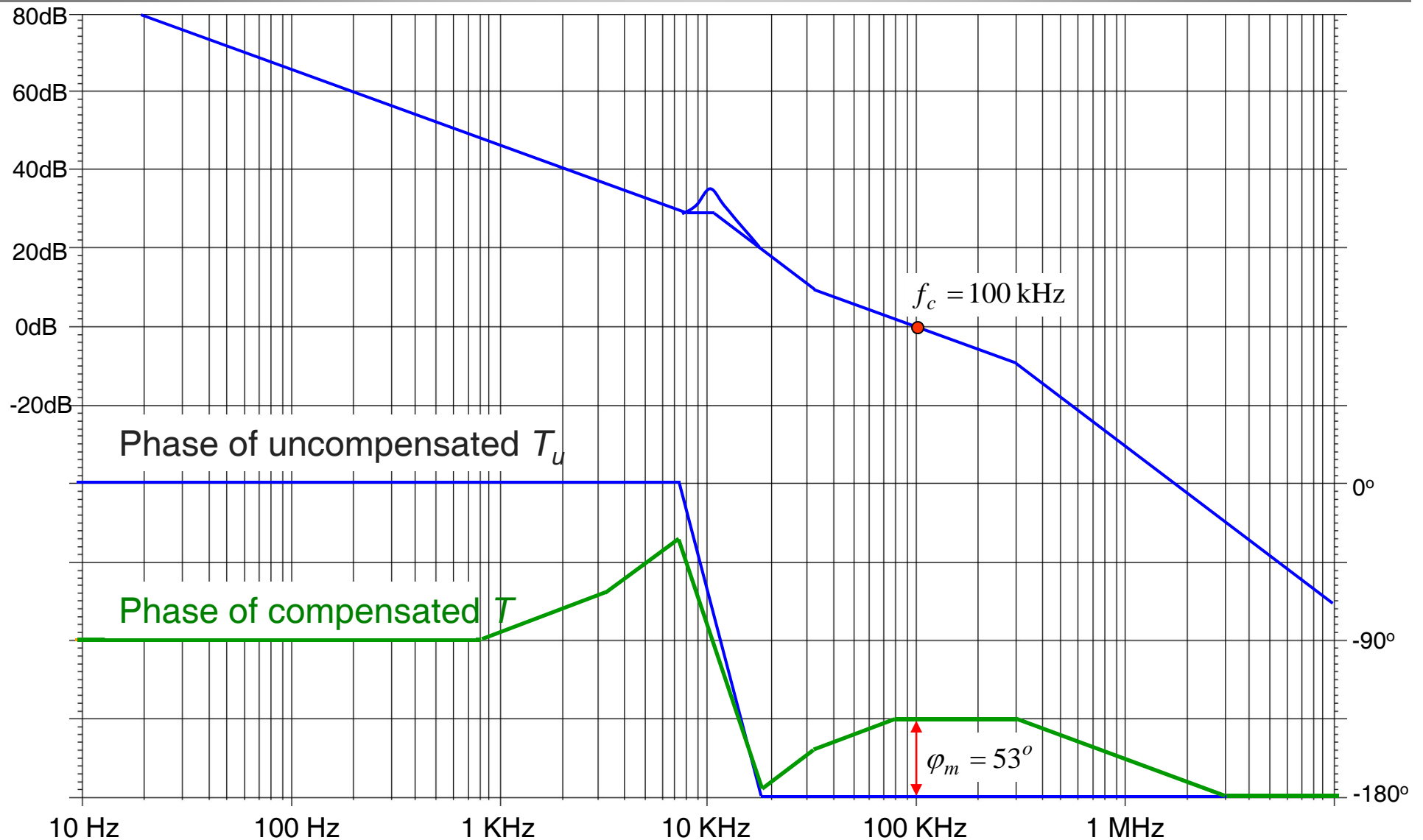
$$f_{p1} = 300 \text{ kHz}$$

$$f_{p2} = 1 \text{ MHz}$$

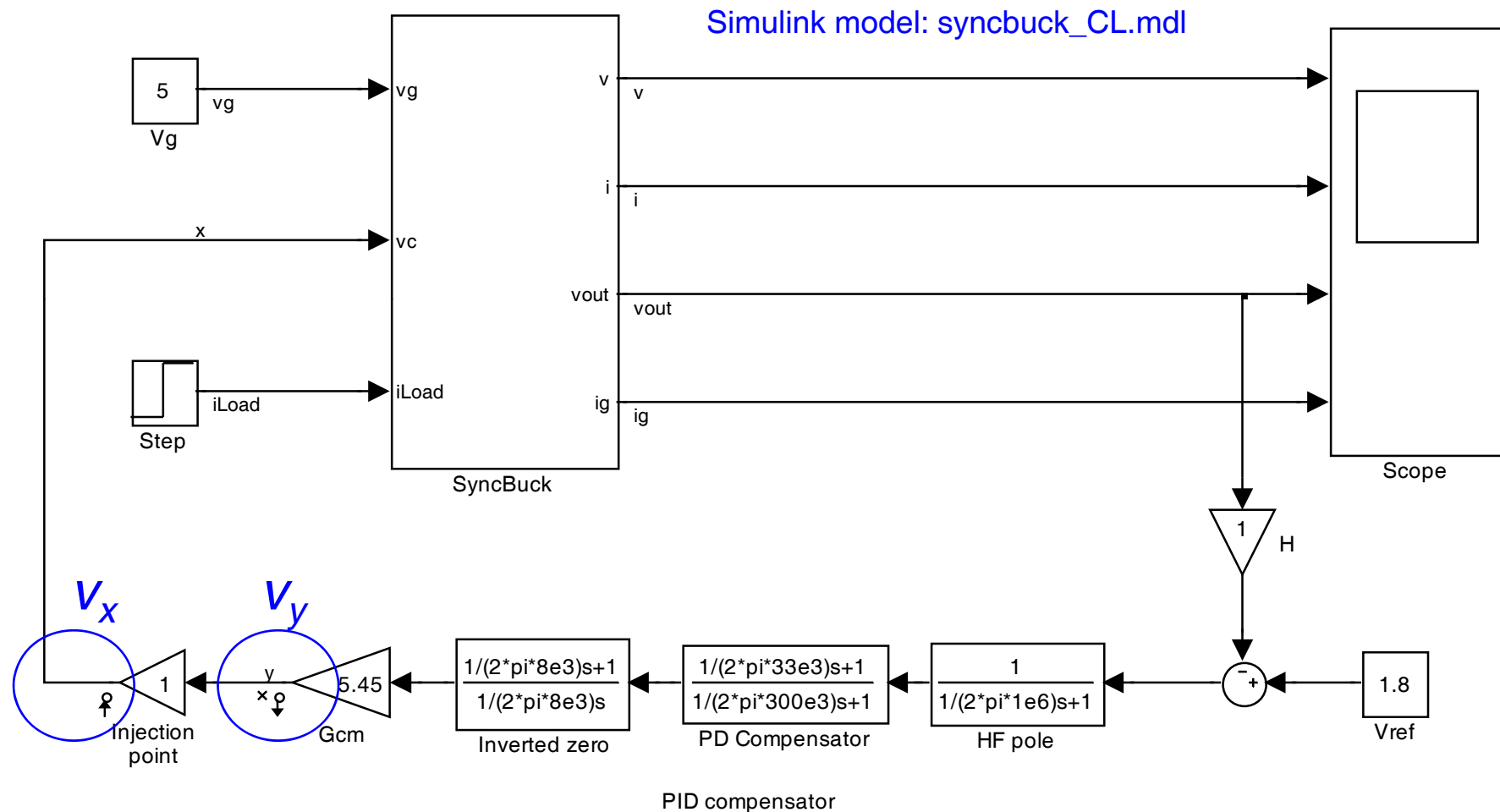
Crossover frequency: $f_c = 100 \text{ kHz}$ ($=1/10$ of f_s)

Phase margin: $\varphi_m = 53^\circ$

Magnitude and phase Bode plots of T



Closed-loop voltage regulator in Simulink



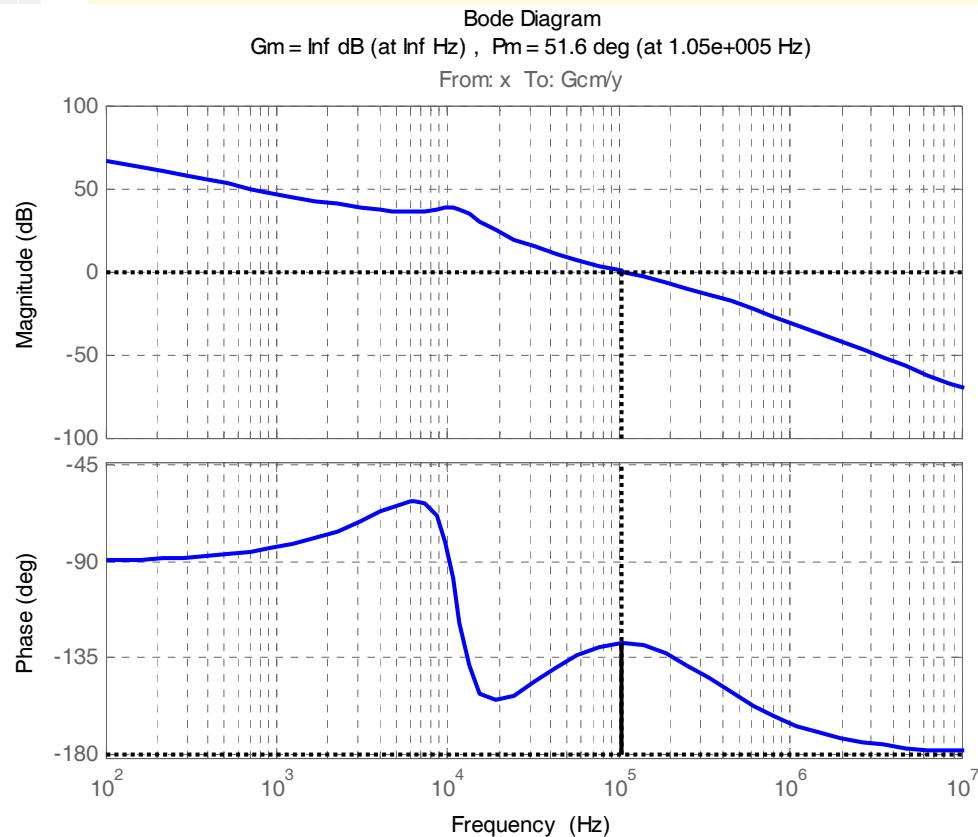
Input and output linearization points for finding the loop-gain, $T = -v_y/v_x$
 The output point (y) should be “Open Loop” , as shown by an x symbol next to the output arrow

Loop gain and stability margins

MATLAB script
BodePlotter_scriptT.m
(computes dc op,
linearizes, calculates
and plots frequency
response and stability
margins)

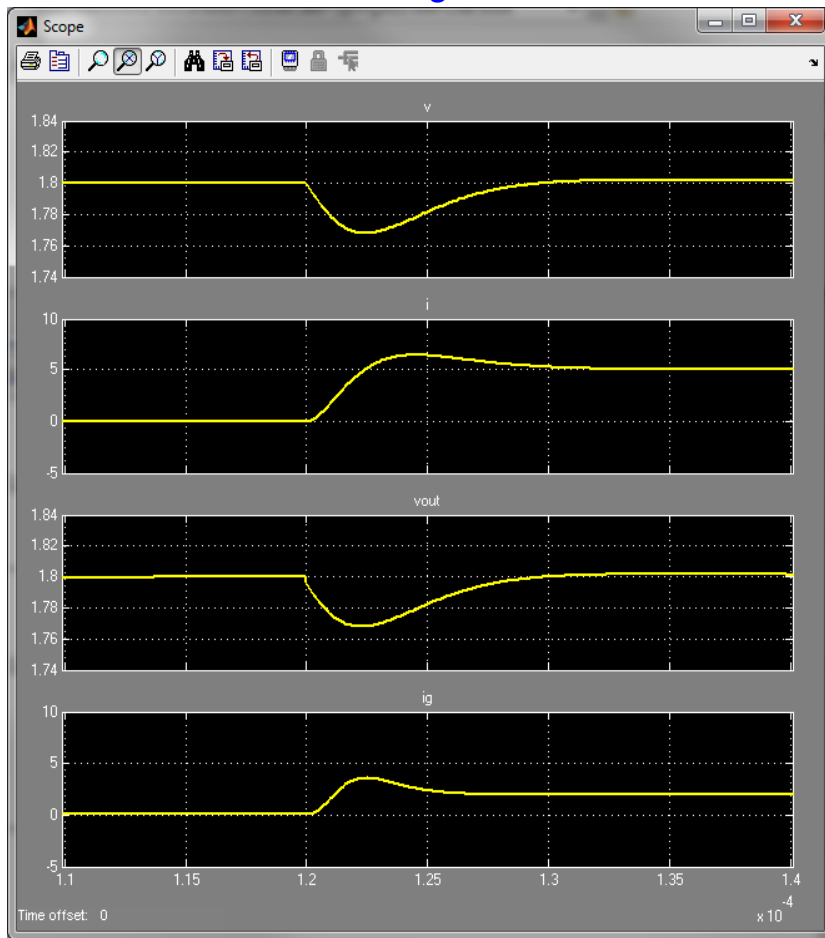
```

1  %% Loop gain bode plotter using linearization tool
2  % requires Simulink Control Design toolbox
3  %
4  %
5  model = 'syncbuck_CL'; % set to file name of simulink model. Must have i/o points set within this model
6  io = getlinio(model) % get i/o signals of model
7  op = operspec(model)
8  op = findop(model,op) % calculate model operating point
9  ssm = linearize(model,op,io) % compute state space model of linearized system
10 %
11 %
12 %ltiview('bode',-ssm) % send linearized model to LTI Viewer tool
13 margin(-ssm) % show loop-gain magnitude and phase responses and calculate fc, PM and GM
14 %
    
```



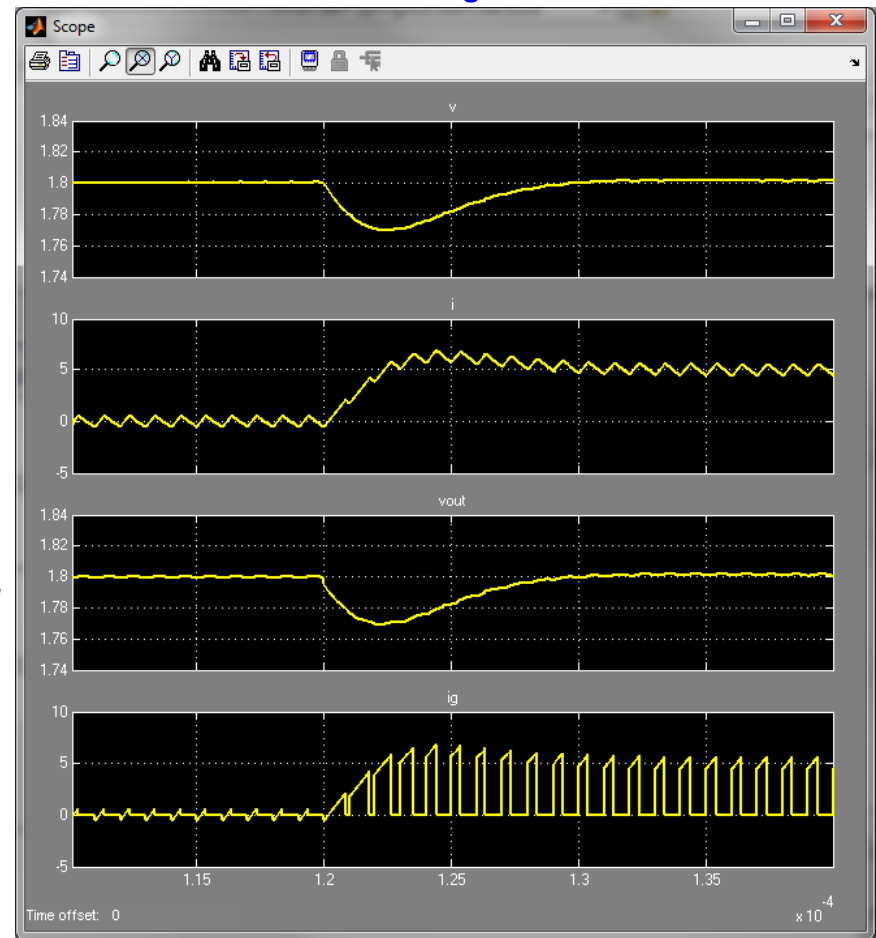
Closed-loop 0-5 A step-load transient responses

Averaged model



5 μ s/div

Switching model



5 μ s/div

See MATLAB/Simulink page on the course website (“Materials” page) for complete step-by-step details, and to download the example files