

GENERAL DESCRIPTION

The RM4136 and RC4136 include four independent high gain operational amplifiers internally compensated and constructed on a single silicon chip using the planar epitaxial processes.

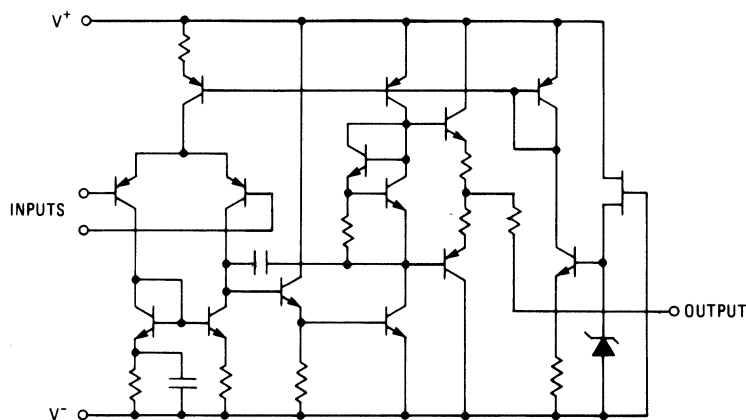
These amplifiers meet or exceed all specifications for 741 type amplifiers. Excellent channel separation allows the use of the 4136 quad amplifier in all 741 operational amplifier applications providing the highest possible packaging density.

The specially designed low noise input transistors allow the 4136 to be used in low noise signal processing applications such as audio preamplifiers and signal conditioners.

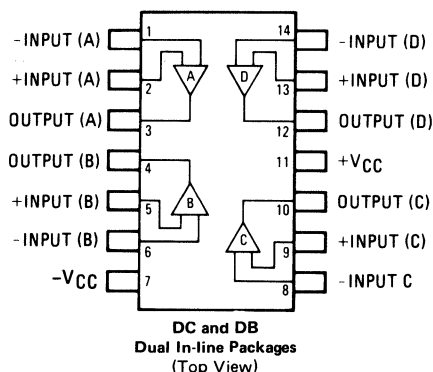
DESIGN FEATURES

- Unity Gain Bandwidth, 3MHz
- Continuous Short Circuit Protection
- No Frequency Compensation Required
- No Latch-up
- Large Common Mode and Differential Voltage Ranges
- Low Power Consumption
- Parameter Tracking Over Temperature Range
- Gain and Phase Match Between Amplifiers

SCHEMATIC DIAGRAM



CONNECTION INFORMATION



Order Part Nos.:
RM4136DC, RV4136 DB,
RC4136DC, RC4136DC

ABSOLUTE MAXIMUM RATINGS

| | | | |
|-------------------------------------|--|--|---|
| Supply Voltage | RM4136: $\pm 22\text{V}$ RV4136, RC4136: $\pm 18\text{V}$ | Storage Temperature Range | -65°C to $+150^{\circ}\text{C}$ |
| Internal Power Dissipation (Note 1) | 800mW | Operating Temperature Range | RM4136: -55°C to $+125^{\circ}\text{C}$ RC4136: 0°C to $+70^{\circ}\text{C}$ RV4136: -40°C to $+85^{\circ}\text{C}$ |
| Differential Input Voltage | $\pm 30\text{V}$ | Lead Temperature (Soldering, 60s) | 300°C |
| Input Voltage (Note 2) | $\pm 15\text{V}$ | Output Short-Circuit Duration (Note 3) | Indefinite |

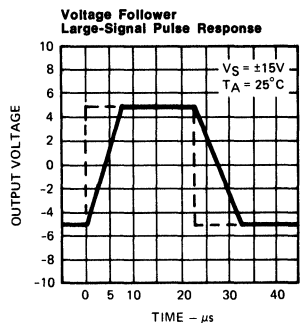
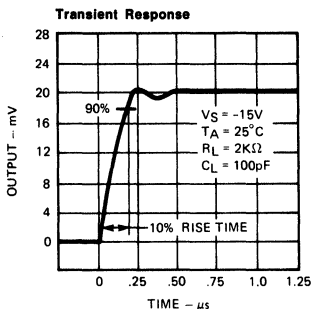
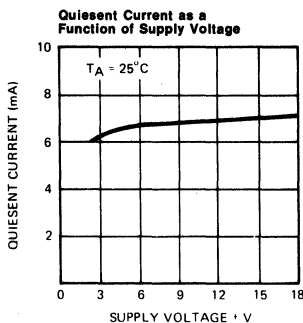
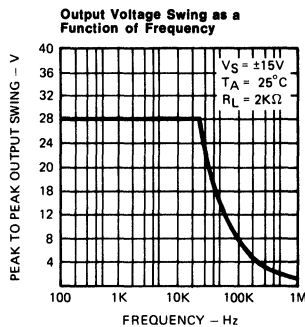
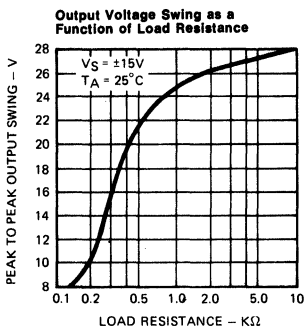
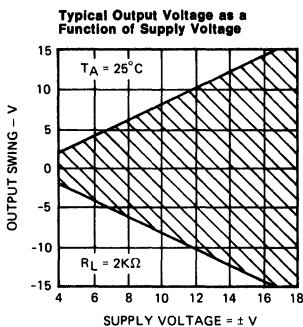
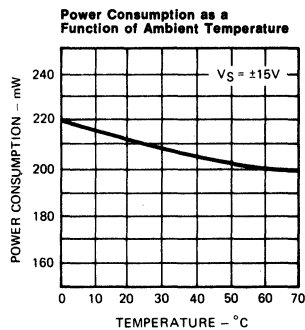
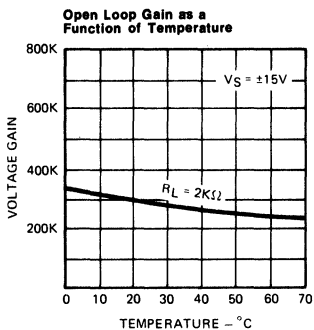
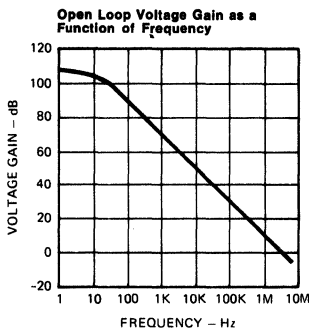
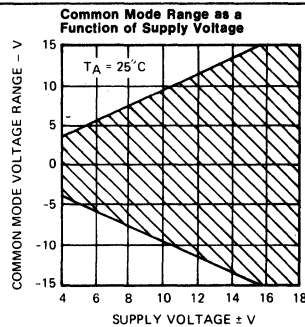
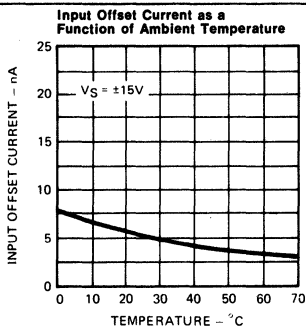
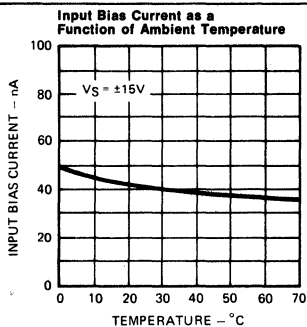
ELECTRICAL CHARACTERISTICS ($V_{CC} = \pm 15\text{V}$, $T_A = +25^{\circ}\text{C}$ unless otherwise noted.)

| PARAMETER | CONDITIONS | RM4136 | | | RV4136, RC4136 | | | UNITS |
|---|---|----------|----------|------|----------------|----------|-----|------------------|
| | | MIN | TYP | MAX | MIN | TYP | MAX | |
| Input Offset Voltage | $R_S \leq 10\text{ k}\Omega$ | | 0.5 | 5.0 | | 0.5 | 6.0 | mV |
| Input Offset Current | | | 5.0 | 200 | | 5.0 | 200 | nA |
| Input Bias Current | | | 40 | 500 | | 40 | 500 | nA |
| Input Resistance | | 0.3 | 5.0 | | 0.3 | 5.0 | | M Ω |
| Large-Signal Voltage Gain | $R_L \geq 2\text{ k}\Omega$ $V_{out} = \pm 10\text{V}$ | 50,000 | 300,000 | | 20,000 | 300,000 | | V/V |
| Output Voltage Swing | $R_L \geq 10\text{ k}\Omega$ | ± 12 | ± 14 | | ± 12 | ± 14 | | V |
| | $R_L \geq 2\text{ k}\Omega$ | ± 10 | ± 13 | | ± 10 | ± 13 | | V |
| Input Voltage Range | | ± 12 | ± 14 | | ± 12 | ± 14 | | V |
| Common Mode Rejection Ratio | $R_S \leq 10\text{ k}\Omega$ | 70 | 100 | | 70 | 100 | | dB |
| Supply Voltage Rejection Ratio | $R_S \leq 10\text{ k}\Omega$ | | 10 | 150 | | 10 | 150 | $\mu\text{V/V}$ |
| Power Consumption | $R_L = \infty$, All Outputs | | 210 | 340 | | 210 | 340 | mW |
| Transient Response (unity gain) | $V_{in} = 20\text{ mV}$ $R_L = 2\text{ k}\Omega$ $C_L \leq 100\text{ pF}$ | | | | | | | |
| Risetime | | | 0.13 | | | 0.13 | | μs |
| Overshoot | | | 5.0 | | | 5.0 | | % |
| Unity Gain Bandwidth | | | 3.0 | | | 3.0 | | MHz |
| Slew Rate (unity gain) | $R_L \geq 2\text{ k}\Omega$ | | 1.5 | | | 1.0 | | V/ μs |
| Channel Separation (open loop) (Gain = 100) | $f = 10\text{ kHz}$ $R_S = 1\text{ k}\Omega$ | | 105 | | | 105 | | dB |
| | $f = 10\text{ kHz}$ $R_S = 1\text{ k}\Omega$ | | 105 | | | 105 | | dB |
| The following specifications apply for $-55^{\circ}\text{C} \leq T_A \leq +125^{\circ}\text{C}$ for RM4136; $0^{\circ}\text{C} \leq T_A \leq +70^{\circ}\text{C}$ for RC4136. | | | | | | | | |
| Input Offset Voltage | $R_S \leq 10\text{ k}\Omega$ | | | 6.0 | | | 7.5 | mV |
| Input Offset Current | | | | 500 | | | 300 | nA |
| Input Bias Current | | | | 1500 | | | 800 | nA |
| Large-Signal Voltage Gain | $R_L \geq 2\text{ k}\Omega$ $V_{out} = \pm 10\text{V}$ | 25,000 | | | 15,000 | | | V/V |
| Output Voltage Swing | $R_L \geq 2\text{ k}\Omega$ | ± 10 | | | ± 10 | | | V |
| Power Consumption | $T_A = \text{High}$ | | 180 | 300 | | 180 | 300 | mW |
| | $T_A = \text{Low}$ | | 240 | 400 | | 240 | 400 | mW |

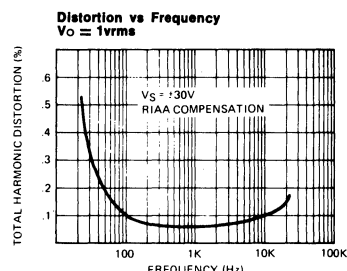
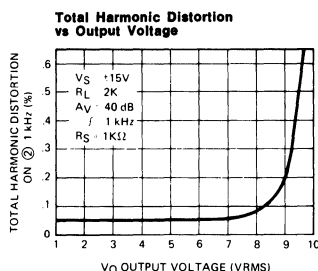
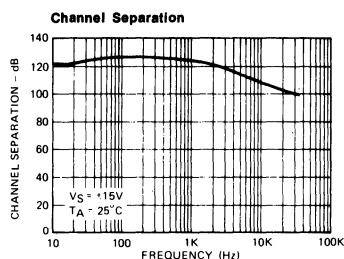
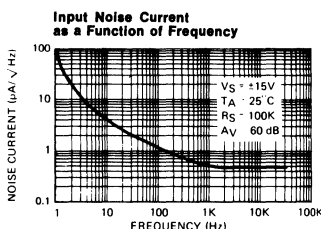
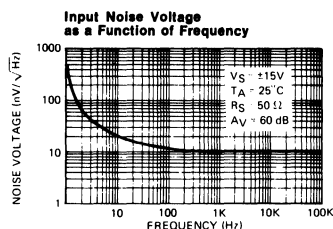
NOTES:

- Rating applies for case temperature to $+25^{\circ}\text{C}$; derate linearly at 6.4 mW/ $^{\circ}\text{C}$ for ambient temperatures above $+25^{\circ}\text{C}$.
- For supply voltages less than $\pm 15\text{V}$ the absolute maximum input voltage is equal to the supply voltage.
- Short-circuit may be to ground or one amplifier only. $I_{CC} = 45\text{mA}$ (typical).

TYPICAL ELECTRICAL DATA



TYPICAL ELECTRICAL DATA

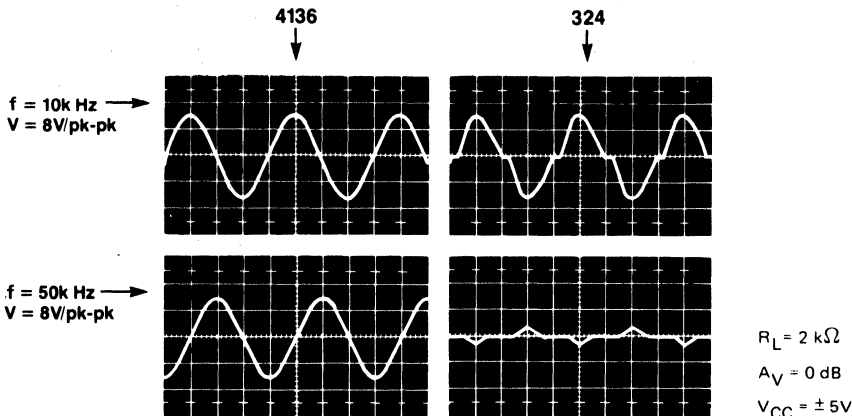
ELECTRICAL CHARACTERISTICS COMPARISON ($V_{CC} = \pm 15V$, $T_A = +25^\circ C$)

| PARAMETER | RC4136 (typ) | RC741 (typ) | LM324 (typ) | UNIT |
|--|--------------|-------------|------------------------------------|-----------------|
| Input Offset Voltage | 0.5 | 2.0 | 2 | mV |
| Input Offset Current | 5 | 10 | 5 | nA |
| Input Bias Current | 40 | 80 | 55 | nA |
| Input Resistance | 5 | 2 | | M Ω |
| Large-Signal Voltage Gain ($R_L = 2 k\Omega$) | 300,000 | 200,000 | 100,000 | V/V |
| Output Voltage Swing ($R_L = 2 k\Omega$) | $\pm 13V$ | $\pm 13V$ | $ +V_{CC} - 1.2V $ to $-V_{CC}$ | \bar{V} |
| Input Voltage Range | $\pm 14V$ | $\pm 13V$ | $ +V_{CC} - 1.5V $ to $-V_{CC}$ | \bar{V} |
| Common-Mode Rejection Ratio | 100 | 90 | 85 | dB |
| Supply Voltage Rejection Ratio | 10 | 30 | 10 | $\mu V/V$ |
| Transient Response (gain = 1) | | | | |
| | Risetime | 0.13 | 0.3 | μs |
| | Overshoot | 5 | 5 | % |
| Unity-Gain Bandwidth | 3 | 0.8 | 0.8 | MHz |
| Unity-Gain Slew Rate | 1.0 | 0.5 | 0.5 | V/ μs |
| Input Noise Voltage ($f_0 = 1 kHz$) | 10 | 22.5 | | nV/ \sqrt{Hz} |
| Output Short-Circuit Current | ± 45 | ± 25 | | mA |

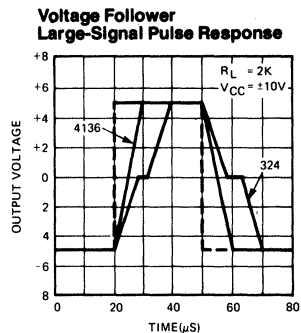
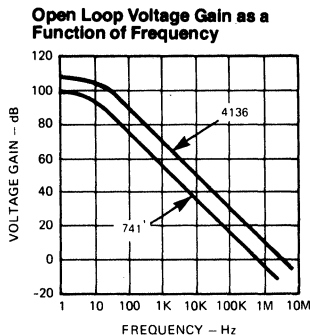
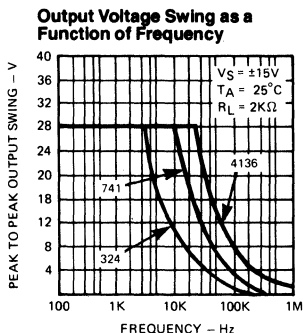
4136 vs. 741

Although the 324 is an excellent device for single-supply applications where ground-sensing is important, it is a poor substitute for four 741's in split-supply circuits.

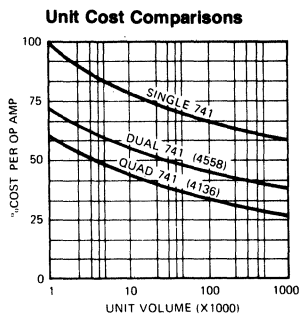
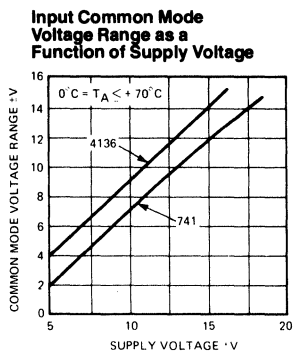
The simplified input circuit of the 4136 exhibits much lower noise than that of the 324 and exhibits no crossover distortion as compared with the 324 (see illustration). The 324 shows serious crossover distortion and pulse delay in attempting to handle a large-signal input pulse.



Comparative Cross-over Distortion

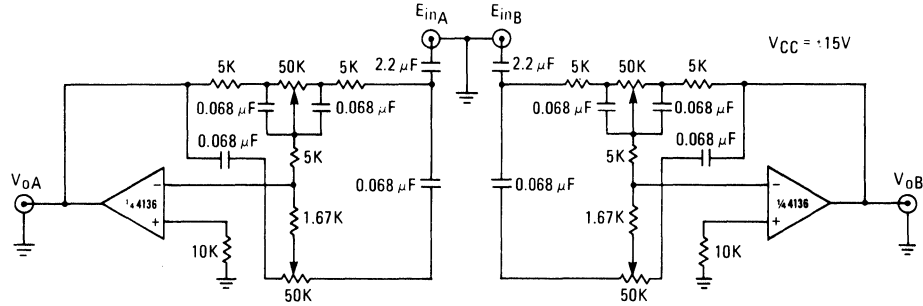


Typical Characteristics Curves Comparison

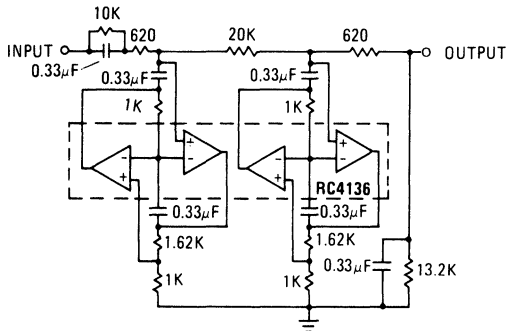


4136 TYPICAL APPLICATIONS

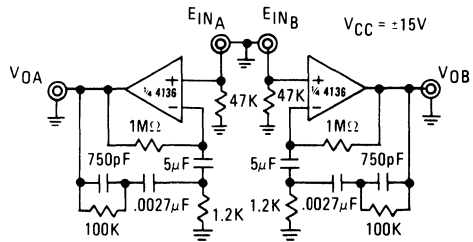
Stereo Tone Control



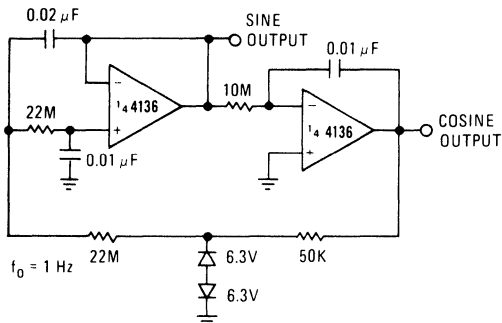
400 Hz Lowpass Butterworth Active Filter



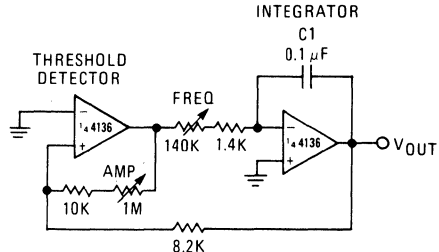
RIAA Preamplifier



Low Frequency Sine Wave Generator with Quadrature Output

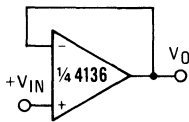


Triangular-Wave Generator

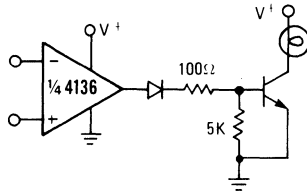


4136 TYPICAL APPLICATIONS

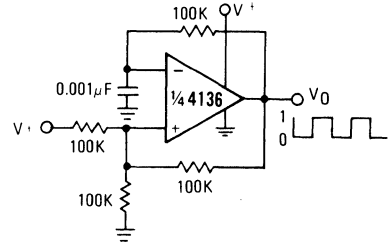
Voltage Follower



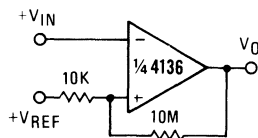
Lamp Driver



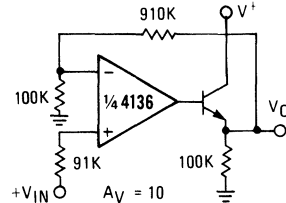
Squarewave Oscillator



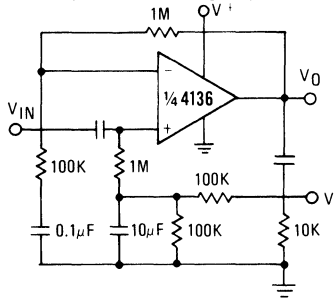
Comparator With Hysteresis



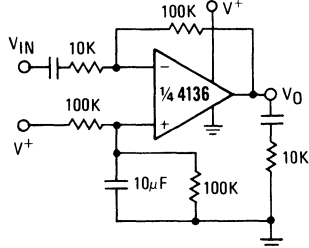
Power Amplifier



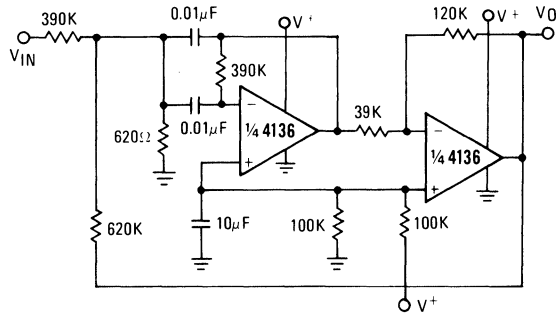
AC Coupled Non-Inverting Amplifier



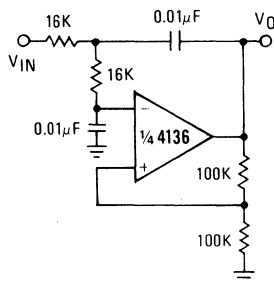
AC Coupled Inverting Amplifier



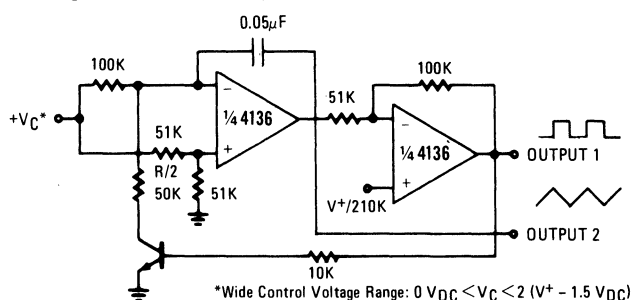
1 kHz Bandpass Active Filter



DC Coupled 1 kHz Low-Pass Active Filter



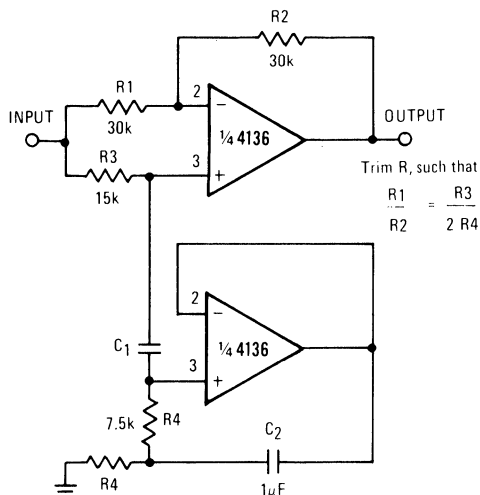
Voltage Controlled Oscillator (VCO)



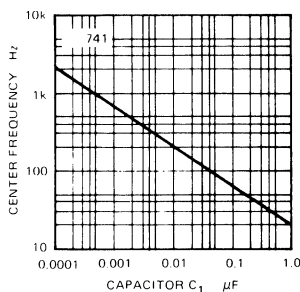
*Wide Control Voltage Range: $0 V_{DC} < V_C < 2 (V^+ - 1.5 V_{DC})$

4136 TYPICAL APPLICATIONS

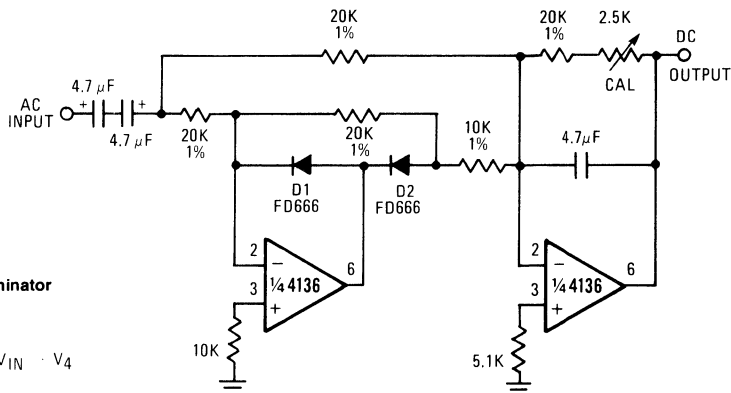
Notch Filter Using the 4136 as a Gyrator



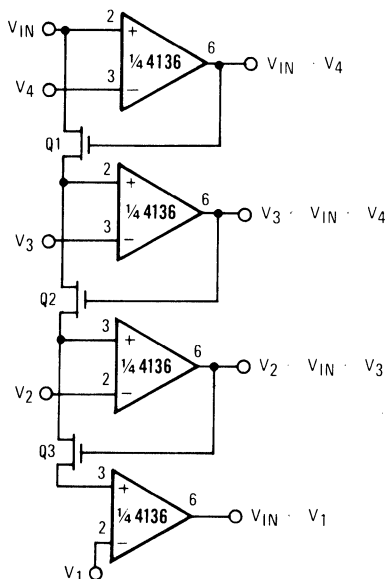
Notch Frequency as a Function of C_1



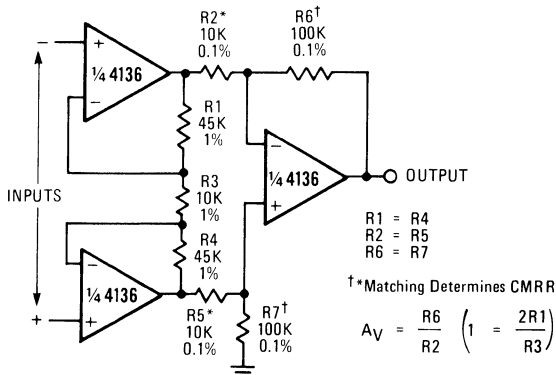
Full-Wave Rectifier and Averaging Filter



Multiple Aperture Window Discriminator

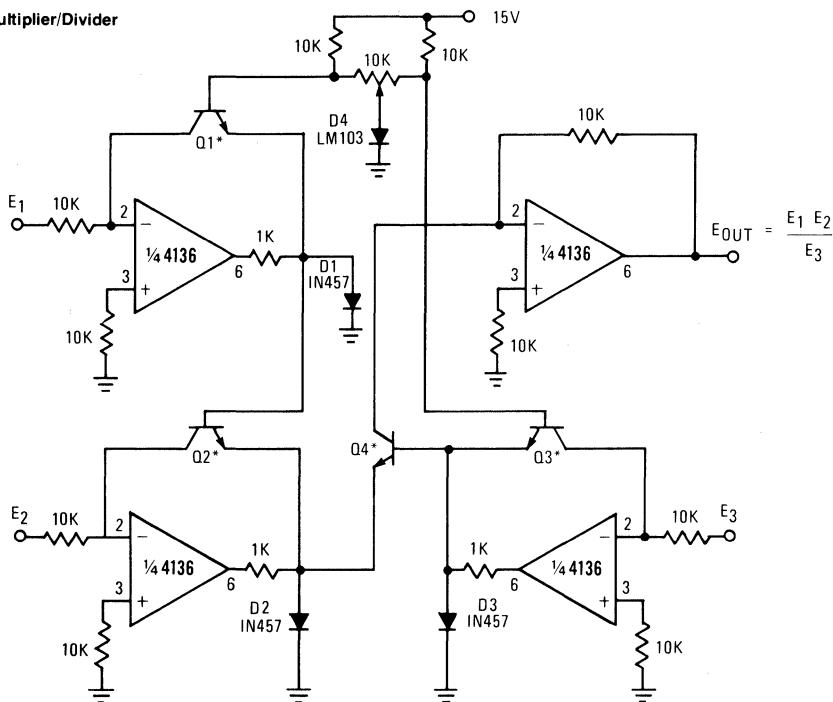


Differential Input Instrumentation Amplifier with High Common Mode Rejection



4136 TYPICAL APPLICATIONS

Analog Multiplier/Divider



Noise Measurement Test Circuit

