

## Lecturer

### Set up MATLAB

In [1]:

```
cd matlab  
pwd  
clear all  
format compact
```

ans =

```
'/Users/eechris/dev/eglm03-textbook/content/03/3/matlab'
```

# Proportional Plus Derivative Compensation

## Introduction

First design example (Satellite Attitude Control).

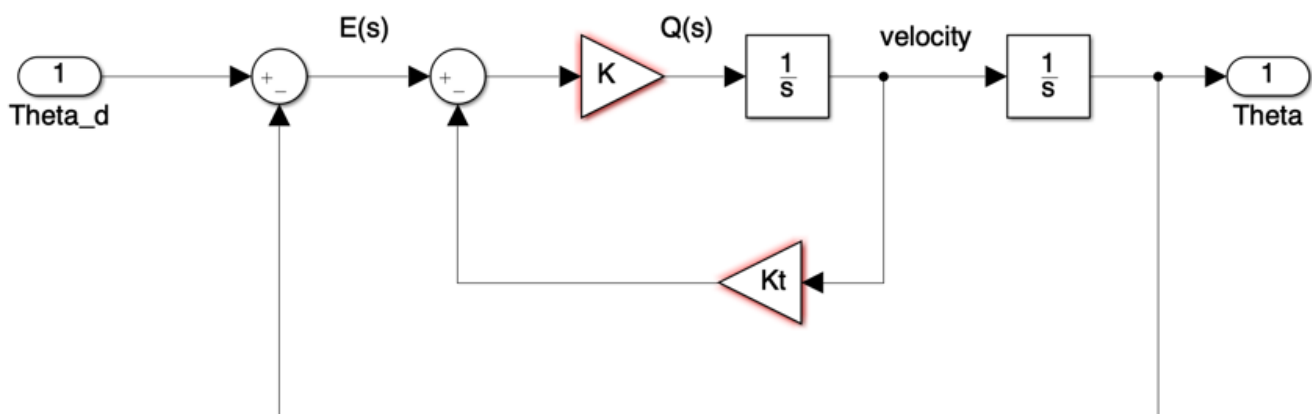
Plant:

$$G(s) = \frac{1}{s^2}$$

Feedback:

$$H(s) = 1$$

With velocity feedback the system is as shown in Figure 1.



**Figure 1 Satellite Attitude Control with Velocity Feedback**

For this system, the root locus equation is

$$1 + \frac{KK_T \left( s + \frac{1}{K_T} \right)}{s^2}$$

and the design parameters where calculated to be

In [2]:

```
Kt = 0.5; K = 8;
```

The closed-loop characteristic equation is

In [3]:

```
clce1 = [1, K*Kt, K];
```

The closed-loop transfer function is then:

In [4]:

```
Gc1 = tf(K,clce1)
```

Gc1 =

$$\frac{8}{s^2 + 4s + 8}$$

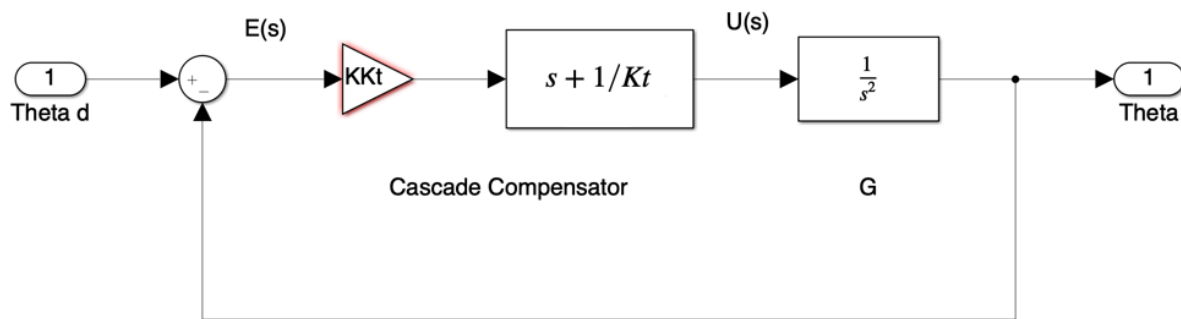
Continuous-time transfer function.

In this document we illustrate how we may implement a silimilar control law using cascade compensation.

## Cascade compensator

An alternative compensation architecture is the cascade compensator illustrated in Figure 2.

## Satellite Attitude Control

**Figure 2 The cascade compensator**

The compensator is in series with the plant so that, in general, if the compensator transfer function is

$$D(s) = \frac{K_c(s + z_1) \dots (s + z_r)}{(s + p_1) \dots (s + p_q)}$$

and the compensator poles and zeros are simply added to the poles and zeros of the plant.

If we wish to achieve the same root-locus equation as the previous design (1) then the compensator must have transfer function

$$D(s) = K_c(s + z_1)$$

where

$$K_c = KK_t = 4$$

$$z_1 = 1/K_t = 2$$

Let us verify that this gives the same results as the previous example:

In [5]:

```
z1 = -1/Kt;
Go = zpk(z1,[0, 0],1) % root locus gain initially set to unity
```

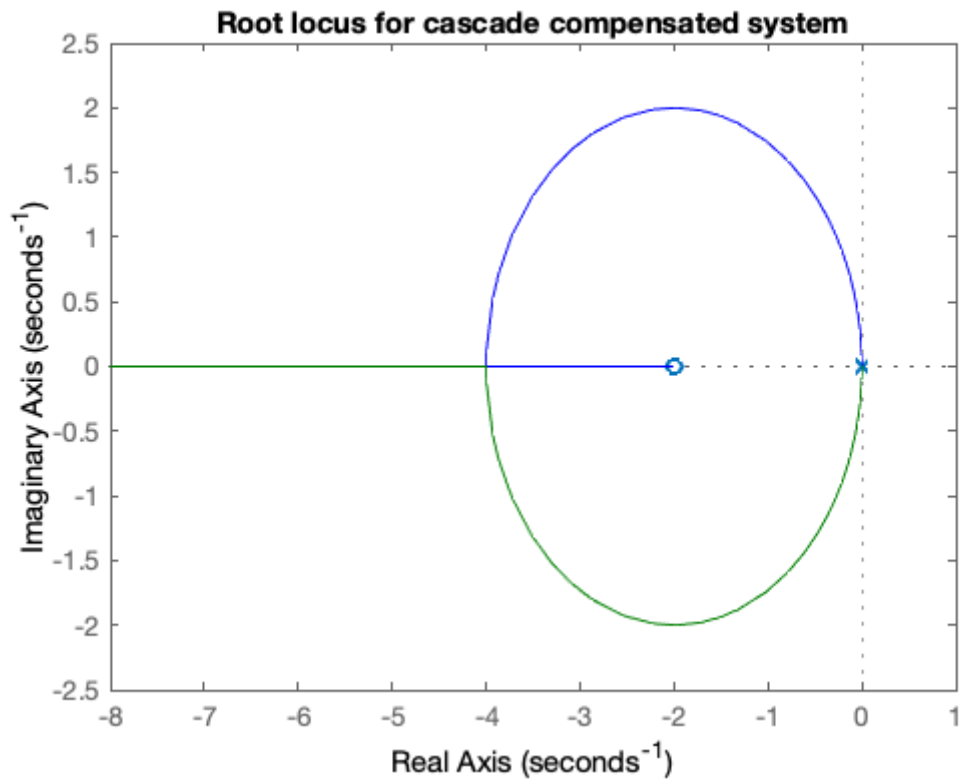
Go =

$$\frac{(s+2)}{s^2}$$

Continuous-time zero/pole/gain model.

In [6]:

```
rlocus(Go),title('Root locus for cascade compensated system')
```



Find the root locus gain at the point on the root locus where the poles are located at  $s = -2 + j2$ .

In [7]:

```
Kc = rlocfind(Go,-2+2j)
```

Kc =  
4

Now add this to the compensator

In [8]:

```
D = tf(Kc*[1 -z1],1)
```

D =

4 s + 8

Continuous-time transfer function.

$$D(s) = 4s + 8$$

Analysis of this compensator reveals that it is of a type known as "*proportional plus derivative*" (P+D). The output of the compensator is of the form

$$U(s) = K_D s E(s) + K_{\text{prop}} E(s)$$

$$u(t) = K_d \frac{de(t)}{dt} + K_{\text{prop}} e(t)$$

and is made up of a "proportion" of the error plus a proportion of the rate-of-change (or derivative) of the error. It is the derivative term that gives the dampening effect required to allow the frictionless system to come to rest.

## Closed-loop response

The closed-loop transfer function is given by

$$G_c(s) = \frac{D(s)G(s)}{1 + D(s)G(s)}$$

In [9]:

```
G=tf(1,[1,0,0])
```

G =

$$\frac{1}{s^2}$$

Continuous-time transfer function.

In [10]:

```
Gc2 = feedback(D*G,1)
```

Gc2 =

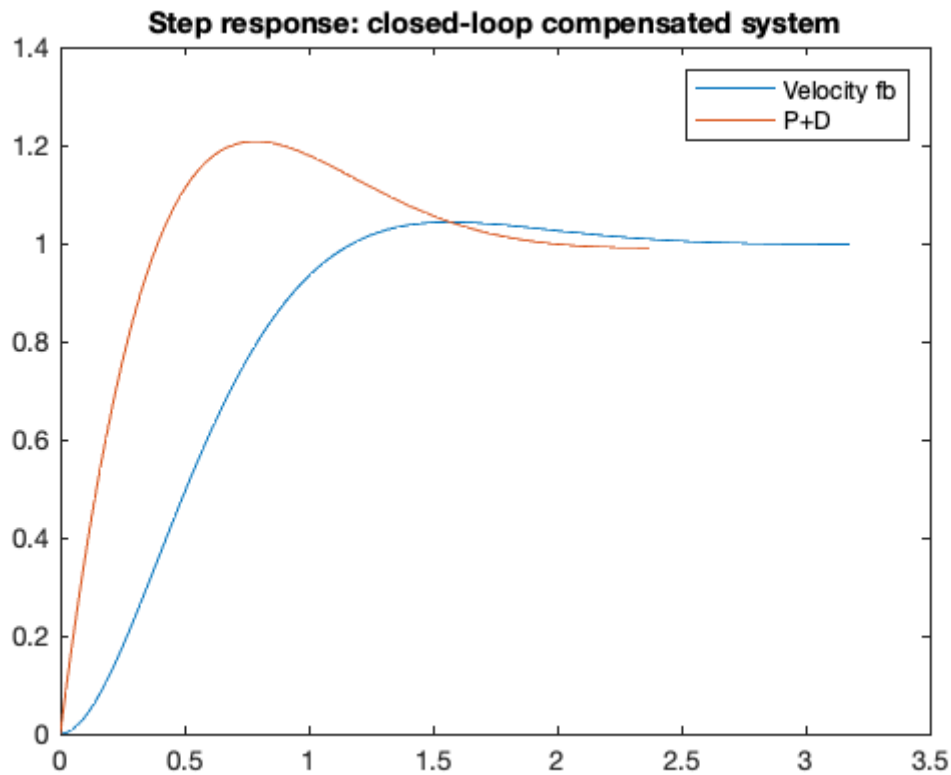
$$\frac{4s + 8}{s^2 + 4s + 8}$$

Continuous-time transfer function.

Let us plot and compare the step responses of the P+D and velocity feedback results.

In [11]:

```
[y1,t1]=step(Gc1);  
[y2,t2]=step(Gc2);  
plot(t1,y1,t2,y2),...  
    legend('Velocity fb','P+D'),...  
    title('Step response: closed-loop compensated system')
```



## Notes

Notice that, although the settling time is about the same in both designs, the overshoot is considerably larger in the P+D compensated system. This is because the zero added by the P+D compensator appears in the numerator of the closed-loop transfer function. (refer back to Contact Hour 2 for an explanation).

## Resources

An executable version of this document is available to download as a MATLAB Live Script file [pplusrd.mlx](#) ([matlab/pplusrd.mlx](#)).

The Simulink model of the satellite attitude control system with P+D compensation is [satellite.slx](#) ([matlab/pd.slx](#)).