

```
cd matlab
pwd
clear all
imatlab_export_fig('print-svg') % Static svg figures.
format compact

ans =
'/Users/eechris/code/src/github.com/cpjobling/eglm03-textbook/03/3/matlab'
```

### 3.3. Proportional Plus Derivative Compensation

#### 3.3.1. Introduction

First design example (Satellite Attitude Control).

Plant:  $G(s) = \frac{1}{s^2}$

Feedback:

$$H(s) = 1$$

With velocity feedback the system is as shown in Figure 1.

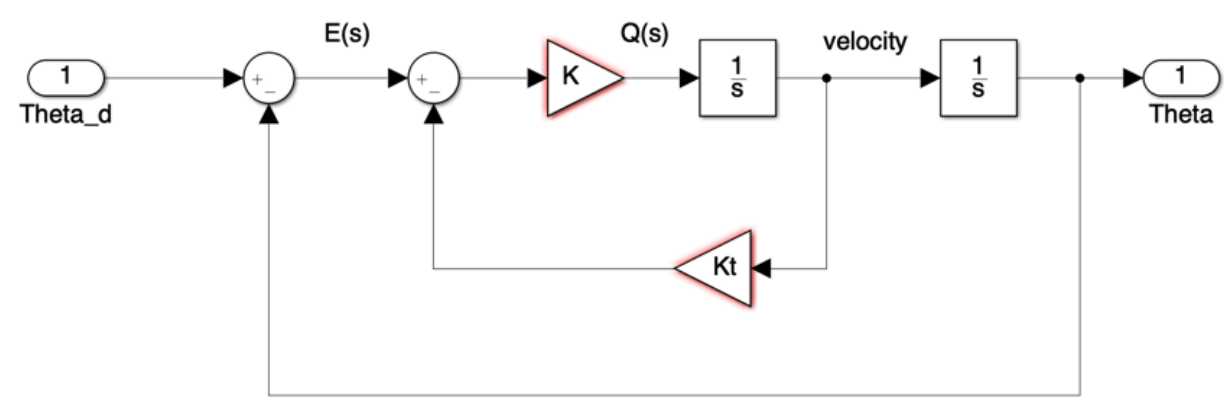


Figure 1 Satellite Attitude

#### Control with Velocity Feedback

For this system, the root locus equation is

$$1 + \frac{KK_T \left(s + \frac{1}{K_T}\right)}{s^2}$$

and the design parameters where calculated to be

```
Kt = 0.5; K = 8;
```

The closed-loop characteristic equation is

```
clce1 = [1, K*Kt, K];
```

The closed-loop transfer function is then:

```
Gc1 = tf(K,clce1)

Gc1 =

      8
-----
s^2 + 4 s + 8

Continuous-time transfer function.
```

In this document we illustrate how we may implement a silimilar control law using cascade compensation.

#### 3.3.2. Cascade compensator

An alternative compensation architecture is the cascade compensator illustrated in Figure 2.

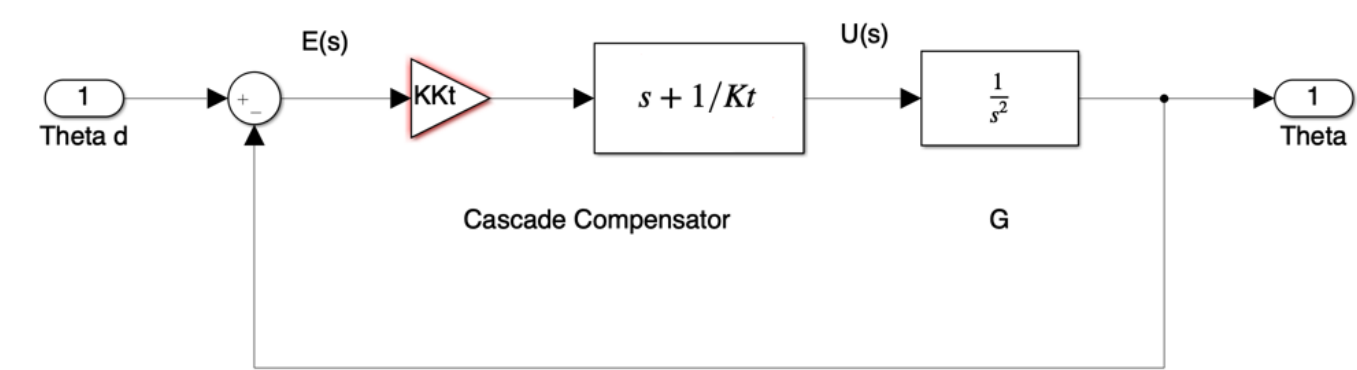


Figure 2 The cascade compensator

The compensator is in series with the plant so that, in general, if the compensator transfer function is

$$D(s) = \frac{K_c(s + z_1) \dots (s + z_r)}{(s + p_1) \dots (s + p_q)}$$

and the compensator poles and zeros are simply added to the poles and zeros of the plant.

If we wish to achieve the same root-locus equation as the previous design (1) then the compensator must have transfer function

$$D(s) = K_c(s + z_1)$$

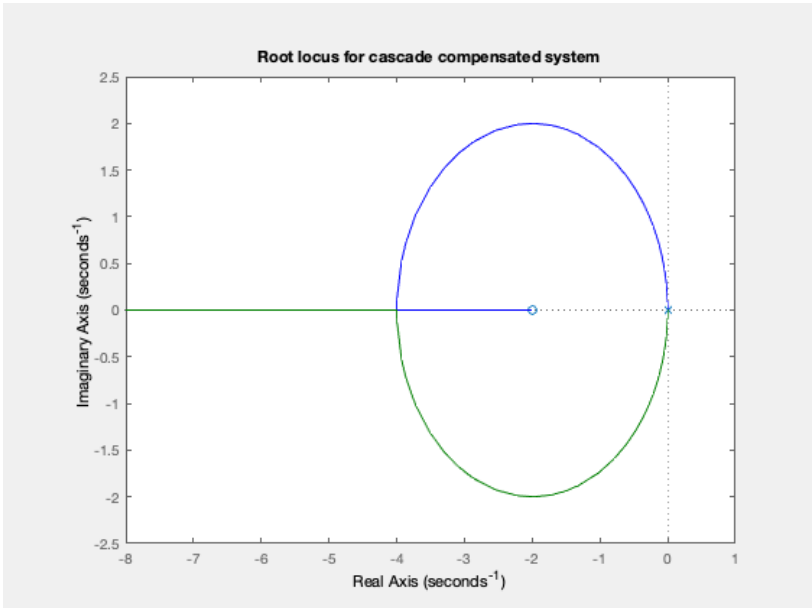
where

$$K_c = KK_t = 4$$

$$z_1 = 1/K_t = 2$$

Let us verify that this gives the same results as the previous example:

```
Kt = 1/2;  
z1 = -1/Kt;  
Go = zpk(z1,[0, 0],1) % root locus gain initially set to unity  
  
Go =  
  
  
(s+2)  
  
-----  
  
s^2  
  
  
Continuous-time zero/pole/gain model.  
  
rlocus(Go),title('Root locus for cascade compensated system')
```



Find the root locus gain at the point on the root locus where the poles are located at  $s = -2 + j2$ .

```
Kc = rlocfind(Go,-2+2j)  
  
Kc =  
4
```

Now add this to the compensator

D = tf(Kc\*[1 -z1],1)

D =

4 s + 8

Continuous-time transfer function.

$D(s) = 4s + 8$

Analysis of this compensator reveals that it is of a type known as “*proportional plus derivative*” (P+D). The output of the compensator is of the form

$U(s) = K_D sE(s) + K_{\text{prop}}E(s)$

$u(t) = K_d \frac{de(t)}{dt} + K_{\text{prop}}e(t)$

and is made up of a “proportion” of the error plus a proportion of the rate-of-change (or derivative) of the error. It is the derivative term that gives the dampening effect required to allow the frictionless system to come to rest.

### 3.3.3. Closed-loop response

The closed-loop tranfer function is given by

$G_c(s) = \frac{D(s)G(s)}{1 + D(s)G(s)}$

G=tf(1,[1,0,0])

G =

1

---

s^2

Continuous-time transfer function.

Gc2 = feedback(D\*G,1)

Gc2 =

4 s + 8

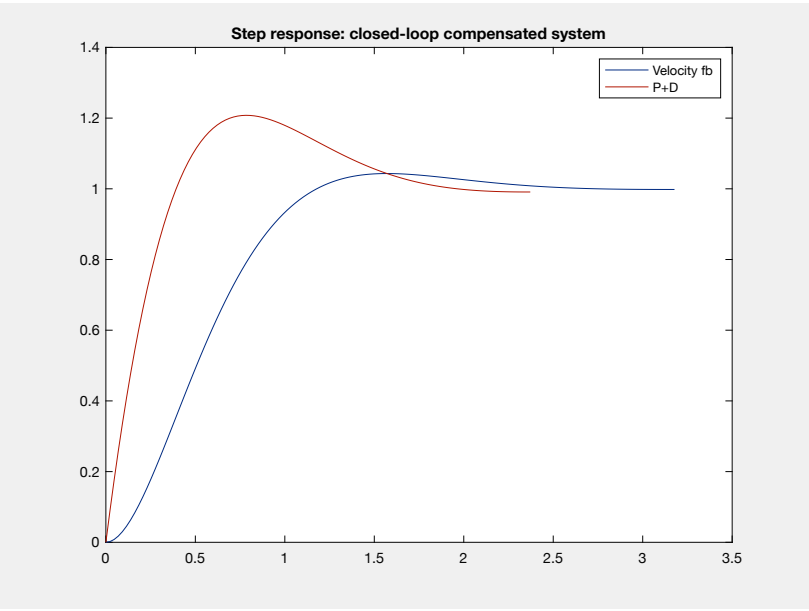
-----

s^2 + 4 s + 8

Continuous-time transfer function.

Let us plot and compare the step responses of the P+D and velocity feedback results.

```
[y1,t1]=step(Gc1);
[y2,t2]=step(Gc2);
plot(t1,y1,t2,y2),...
    legend('Velocity fb','P+D'),...
    title('Step response: closed-loop compensated system')
```



### 3.3.4. Notes

Notice that, although the settling time is about the same in both designs, the overshoot is considerably larger in the P+D compensated system. This is because the zero added by the P+D compensator appears in the numerator of the closed-loop transfer function. (refer back to Contact Hour 2 for an explanation).

### 3.3.5. Resources

An executable version of this document is available to download as a MATLAB Live Script file `pplustd.mlx`.

The Simulink model of the satellite attitude control system with P+D compensation is `satellite.slx`.