

## Appendix: Parameters of 611 $\gamma$ Dor stars

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### ABSTRACT

We list the observed and TAR fitting parameters of 611  $\gamma$  Dor stars in this paper. The parameters are: the *Kepler* magnitudes, the effective temperatures, the luminosities, the mode identifications ( $k \equiv l - |m|$ ,  $l$  is the angular degree and  $m$  is the azimuthal order), mean pulsation periods  $\langle P \rangle$ , mean period spacings  $\langle \Delta P \rangle$ , slopes  $\langle \Sigma \rangle$ , asymptotic spacings  $\Pi_0$ , near-core rotation rates  $f_{\text{rot}}$ , the ranges of radial orders  $n$ , and ranges of spin parameters  $s$ . We also mark the stars which have short-cadence data or have p modes oscillations.

**Key words:** stars: oscillations – stars: rotation – stars: variables

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**Table 1.** KIC numbers, Kepler magnitudes  $K_p$ , effective temperatures  $T_{\text{eff}}$ , luminosities  $L$ , mode identifications (for g modes, we give the angular degrees  $l$  and the azimuthal orders  $m$ , While for r modes, we list the value  $k$  and  $m$ ), mean pulsation periods  $\langle P \rangle$ , mean period spacings  $\langle \Delta P \rangle$ , slopes  $\Sigma$ , asymptotic spacings  $\Pi_0$ , near-core rotation rates  $f_{\text{rot}}$ , the ranges of radial orders  $n$ , and ranges of spin parameters  $s$  of 611 stars in this paper. For the last two columns, ‘1’ marks the stars which have short-cadence data (SC) or are  $\gamma$  Dor– $\delta$  Sct hybrids (H).

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$ min max	$s$ min max	SC	H
1026861	11.00	$7060 \pm 80$	$8.5 \pm 0.5$	2		2	0.8	530	$-0.0123 \pm 0.0002$	$4310 \pm 50$	$0.311 \pm 0.002$	57 92	0.7 1.3	1	
				1		1	1.5	1240	$-0.0167 \pm 0.0007$			45 79	1.1 2.1		
1160891	13.21	$6840 \pm 80$		1		1	0.6	200	$-0.022 \pm 0.002$	$2800 \pm 400$	$1.14 \pm 0.03$	66 88	4.5 6.2		
1162345	11.68	$6500 \pm 200$	$38 \pm 3$	2		2	0.3	70	$-0.0275 \pm 0.0002$	$4400 \pm 400$	$1.46 \pm 0.02$	55 71	3.9 5.1		
				1		1	0.5	290	$-0.0372 \pm 0.0003$			35 47	4.8 6.6		
1295531	11.94	$6760 \pm 80$		1		1	0.8	1280	$-0.0266 \pm 0.0002$	$4200 \pm 20$	$0.572 \pm 0.002$	18 50	0.8 2.5		
1431379	12.62	$6670 \pm 80$	$8.5 \pm 0.7$	2		2	0.3	200	$-0.0384 \pm 0.0006$	$4360 \pm 10$	$1.2526 \pm 0.0006$	21 59	1.2 3.6		
				1		1	0.6	330	$-0.0349 \pm 0.0005$			25 66	2.9 8.1		
					-2	-1	1.0	390	$0.0504 \pm 0.0004$			12 60	7.1 23.1		
1432149	11.22	$7500 \pm 300$	$11.6 \pm 0.8$	2		2	0.3	80	$-0.0269 \pm 0.0003$	$4200 \pm 400$	$1.38 \pm 0.02$	54 75	3.4 4.8	1	
				1		1	0.5	260	$-0.0320 \pm 0.0004$			44 52	5.5 6.5		
1575977	13.61	$7300 \pm 300$	$8.8 \pm 0.7$	1		1	0.4	710	$-0.0543 \pm 0.0007$	$3800 \pm 100$	$1.50 \pm 0.02$	18 28	2.0 3.3		1
1872262	13.74	$7100 \pm 200$	$7.6 \pm 0.6$	2		2	0.5	260	$-0.028 \pm 0.002$	$5000 \pm 2000$	$0.70 \pm 0.05$	50 58	2.0 2.4		
1996456	11.44	$7100 \pm 200$	$10.1 \pm 0.8$	2		2	0.4	160	$-0.0294 \pm 0.0002$	$4450 \pm 80$	$1.038 \pm 0.004$	30 84	1.4 4.3	1	
				1		1	0.7	420	$-0.0338 \pm 0.0002$			30 63	2.8 6.3		
2018685	14.05	$6700 \pm 200$	$8.4 \pm 0.7$	2		2	0.3	160	$-0.0315 \pm 0.0004$	$4200 \pm 200$	$1.27 \pm 0.01$	32 57	1.8 3.4		
				1		1	0.6	350	$-0.0343 \pm 0.0005$			35 50	4.1 5.9		
2020444	13.00	$6890 \pm 80$	$8.9 \pm 0.7$	1		1	1.0	1040	$-0.0211 \pm 0.0004$	$4360 \pm 30$	$0.499 \pm 0.002$	30 66	1.2 3.1		
2141387	12.15	$7200 \pm 300$	$7.0 \pm 0.6$	1		1	1.0	1010	$-0.035 \pm 0.001$	$6090 \pm 90$	$0.592 \pm 0.003$	29 51	2.1 4.0		
2163896	13.12	$6900 \pm 200$	$4.8 \pm 0.3$	1		1	0.8	460	$-0.0249 \pm 0.0002$	$3400 \pm 100$	$0.834 \pm 0.008$	44 74	2.5 4.5		
2168333	10.08	$8400 \pm 300$	$34 \pm 3$	1		1	0.5	220	$-0.0358 \pm 0.0004$	$4200 \pm 200$	$1.66 \pm 0.01$	31 62	4.5 9.5	1	1
2300165	11.05	$7400 \pm 300$	$7.2 \pm 0.6$	2		2	0.3	170	$-0.0300 \pm 0.0002$	$4140 \pm 70$	$1.136 \pm 0.004$	29 75	1.4 3.9	1	
				1		1	0.6	380	$-0.0323 \pm 0.0003$			26 71	2.4 7.4		
2309579	13.35	$7200 \pm 300$	$10.0 \pm 0.7$	2		2	0.4	110	$-0.0211 \pm 0.0002$	$4000 \pm 200$	$1.001 \pm 0.007$	58 95	2.5 4.2		
				1		1	0.8	210	$-0.0230 \pm 0.0001$			50 107	4.3 9.4		
2449383	13.92	$7200 \pm 300$	$7.6 \pm 0.6$	2		2	0.2	90	$-0.0310 \pm 0.0003$	$3910 \pm 90$	$1.588 \pm 0.007$	35 76	2.3 5.2		
				1		1	0.4	320	$-0.0419 \pm 0.0004$			20 59	2.5 8.0		
2450944	15.74	$6800 \pm 200$		1		1	1.0	2500	$-0.0084 \pm 0.0004$	$4136 \pm 5$	$0.141 \pm 0.001$	24 37	0.2 0.3		1
				1		-1	1.2	3350	$0.003 \pm 0.001$			30 37	0.2 0.3		
2575161	10.88	$6900 \pm 100$		1		1	0.4	250	$-0.0466 \pm 0.0008$	$4470 \pm 20$	$1.833 \pm 0.001$	20 54	3.6 10.0		
					-2	-1	0.7	580	$0.0753 \pm 0.0004$			8 27	7.3 16.2		
2578582	13.93	$7300 \pm 300$	$5.2 \pm 0.4$	1		1	0.8	1140	$-0.0233 \pm 0.0003$	$3960 \pm 30$	$0.570 \pm 0.003$	24 53	1.0 2.5		
2579147	13.83	$7300 \pm 300$	$14 \pm 1$	2		2	0.7	620	$-0.0096 \pm 0.0004$	$3600 \pm 30$	$0.286 \pm 0.003$	54 72	0.5 0.7		1
				1		1	1.1	1560	$-0.0154 \pm 0.0006$			43 51	0.8 0.9		
2696217	13.45	$7400 \pm 300$	$7.0 \pm 0.5$	1		1	1.3	1310	$-0.0130 \pm 0.0002$	$3460 \pm 20$	$0.290 \pm 0.001$	39 84	0.7 1.7		
2710406	13.27	$6960 \pm 80$	$12.6 \pm 0.9$	1		1	1.5	2270	$-0.0054 \pm 0.0003$	$4270 \pm 70$	$0.138 \pm 0.006$	45 57	0.4 0.6		
2710594	11.79	$7200 \pm 200$	$8.0 \pm 0.5$	1		1	0.7	360	$-0.0290 \pm 0.0003$	$4000 \pm 10$	$0.9920 \pm 0.0006$	27 86	2.3 7.9		
					-2	-1	1.2	470	$0.0381 \pm 0.0005$			20 64	7.4 18.0		
2719928	12.66	$7200 \pm 200$	$9.6 \pm 0.7$	2		2	0.3	70	$-0.0275 \pm 0.0004$	$3700 \pm 700$	$1.47 \pm 0.04$	55 82	3.3 5.0		
				1		1	0.5	150	$-0.006 \pm 0.004$			59 69	7.1 8.4		
2846358	11.02	$6800 \pm 200$		2		2	0.4	360	$-0.0279 \pm 0.0004$	$4020 \pm 50$	$0.755 \pm 0.004$	25 61	0.7 2.0	1	
				1		1	0.8	650	$-0.0336 \pm 0.0004$			32 63	1.9 4.0		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
2859701	13.45	$6840 \pm 80$		1		1	1.0	680	$-0.063 \pm 0.002$	$16400 \pm 200$	$0.803 \pm 0.001$	16	44	4.3	12.8		
2975832	12.60	$6800 \pm 200$	$7.4 \pm 0.5$	1		1	0.5	270	$-0.0496 \pm 0.0006$	$7800 \pm 400$	$1.573 \pm 0.009$	22	48	5.8	14.2		1
2988145	13.25	$7000 \pm 200$	$19 \pm 2$	2		2	0.4	590	$-0.0258 \pm 0.0002$	$4200 \pm 300$	$0.55 \pm 0.03$	31	39	0.7	0.9		1
2998070	11.86	$6900 \pm 200$	$7.4 \pm 0.5$	2		2	0.4	120	$-0.0180 \pm 0.0003$	$3300 \pm 700$	$0.83 \pm 0.04$	77	101	2.3	3.0		
3096317	11.56	$6800 \pm 200$	$13 \pm 1$	2		2	0.3	70	$-0.0236 \pm 0.0005$	$4100 \pm 200$	$1.50 \pm 0.02$	61	72	4.1	4.9		
				1		1	0.5	290	$-0.0372 \pm 0.0003$			33	50	4.3	6.7		
3103576	12.15	$7300 \pm 300$	$4.7 \pm 0.3$	1		1	1.1	880	$-0.0196 \pm 0.0001$	$3870 \pm 20$	$0.476 \pm 0.001$	33	87	1.1	3.5		
3127996	11.55	$7700 \pm 300$	$9.4 \pm 0.8$	2		1	0.7	1540	$-0.0000 \pm 0.0003$	$4007 \pm 2$	$0.0518 \pm 0.0007$	35	42	0.0	0.0		
				2		-2	0.7	1850	$0.0068 \pm 0.0003$			32	39	0.0	0.0		
				2		-1	0.7	1750	$0.0007 \pm 0.0002$			36	41	0.0	0.0		
				1		1	0.9	2690	$-0.0043 \pm 0.0004$			25	33	0.0	0.1		
				1		0	0.9	2830	$-0.0007 \pm 0.0005$			24	35	0.0	0.1		
				1		-1	1.0	2980	$0.0024 \pm 0.0004$			26	36	0.0	0.1		
3216518	12.66	$6800 \pm 200$	$6.9 \pm 0.5$	1		1	1.0	400	$-0.030 \pm 0.001$	$4100 \pm 300$	$0.67 \pm 0.01$	57	92	3.3	5.7		
3221077	13.21	$7000 \pm 200$	$9.6 \pm 0.7$	1		1	0.9	650	$-0.067 \pm 0.002$	$14600 \pm 700$	$0.885 \pm 0.005$	20	35	5.4	10.1		
3222364	11.08	$6800 \pm 100$	$8.9 \pm 0.6$	2		2	0.4	140	$-0.0236 \pm 0.0002$	$5000 \pm 100$	$0.953 \pm 0.004$	49	73	2.5	3.9		
				1		1	0.8	350	$-0.0313 \pm 0.0008$			37	74	3.8	8.1		
3222854	12.50	$6800 \pm 200$	$9.4 \pm 0.7$	2		1	0.6	1620	$-0.0004 \pm 0.0003$	$3955 \pm 9$	$0.005 \pm 0.009$	25	40	0.0	0.0		
				2		-1	0.6	1640	$0.0003 \pm 0.0003$			25	40	0.0	0.0		
				1		0	0.9	2830	$-0.001 \pm 0.001$			24	31	0.0	0.0		
3238245	13.57	$7300 \pm 300$	$7.6 \pm 0.6$	1		1	0.5	440	$-0.038 \pm 0.001$	$3630 \pm 70$	$1.240 \pm 0.009$	21	61	1.8	6.0		
3240316	12.69	$7000 \pm 200$	$9.2 \pm 0.8$	1		1	1.1	680	$-0.0196 \pm 0.0007$	$4300 \pm 100$	$0.561 \pm 0.005$	47	74	2.3	3.9		
3240967	13.77	$7050 \pm 80$	$8.1 \pm 0.6$	1		1	0.6	320	$-0.0344 \pm 0.0002$	$4180 \pm 20$	$1.2857 \pm 0.0008$	30	58	3.5	7.0		
					-2	-1	0.9	450	$0.0507 \pm 0.0004$			13	51	7.2	19.4		
3241199	10.47	$8100 \pm 300$	$21 \pm 1$	1		1	0.5	820	$-0.045 \pm 0.001$	$4190 \pm 60$	$1.125 \pm 0.007$	17	37	1.5	3.7		1
3331147	10.05	$7200 \pm 300$	$5.5 \pm 0.5$	1		1	0.7	500	$-0.0299 \pm 0.0002$	$4290 \pm 60$	$0.900 \pm 0.003$	26	74	2.0	6.3	1	
3341457	13.87	$7800 \pm 300$	$5.1 \pm 0.4$	1		1	0.4	120	$-0.0292 \pm 0.0007$	$3840 \pm 40$	$1.859 \pm 0.001$	41	79	6.5	12.7		
					-2	-1	0.6	100	$0.0526 \pm 0.0008$			34	60	17.2	30.2		
3343854	12.33	$7700 \pm 300$	$5.6 \pm 0.3$	1		1	0.7	440	$-0.0340 \pm 0.0001$	$4600 \pm 100$	$1.031 \pm 0.006$	29	61	2.9	6.4		
3345665	13.50	$7100 \pm 200$	$11 \pm 3$	2		2	0.3	160	$-0.0287 \pm 0.0001$	$3900 \pm 70$	$1.088 \pm 0.005$	38	72	1.7	3.3		
				1		1	0.6	510	$-0.0351 \pm 0.0003$			29	52	2.5	4.7		
3348714	13.91	$7400 \pm 300$	$8.1 \pm 0.7$	1		1	0.6	1140	$-0.0345 \pm 0.0004$	$4000 \pm 30$	$0.768 \pm 0.004$	18	39	1.0	2.4		
				1		0	1.0	1440	$-0.0152 \pm 0.0005$			33	47	1.3	1.7		
3440074	13.15	$6700 \pm 200$	$6.3 \pm 0.4$	2		2	0.3	160	$-0.0292 \pm 0.0003$	$3880 \pm 70$	$1.138 \pm 0.005$	29	82	1.3	4.0		
				1		1	0.6	350	$-0.0306 \pm 0.0002$			32	71	2.9	6.9		
3440840	13.25	$6900 \pm 200$	$9.2 \pm 0.7$	2		2	0.4	100	$-0.0207 \pm 0.0005$	$4000 \pm 2000$	$0.93 \pm 0.07$	74	92	2.9	3.7		
3445468	13.91	$7030 \pm 80$	$7.1 \pm 0.5$	1		1	0.6	200	$-0.0266 \pm 0.0003$	$3860 \pm 10$	$1.2037 \pm 0.0007$	35	101	3.5	10.9		
					-2	-1	1.0	560	$0.0377 \pm 0.0007$			16	42	7.4	14.3		
3446996	13.55	$7300 \pm 300$	$8.6 \pm 0.8$	2		2	0.2	50	$-0.0317 \pm 0.0003$	$3800 \pm 200$	$2.06 \pm 0.01$	39	77	3.3	6.8		
				1		1	0.4	180	$-0.0393 \pm 0.0003$			31	55	5.2	9.6		

Table 1. continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
3448365	9.91	$6700 \pm 200$	$5.6 \pm 0.3$	1		1	0.7	330	$-0.0301 \pm 0.0008$	$4190 \pm 10$	$1.0736 \pm 0.0005$	28	80	2.7	8.0		
					-2	-1	1.1	380	$0.0440 \pm 0.0003$			17	69	7.6	21.9		
3449625	13.40	$7500 \pm 300$	$3.6 \pm 0.2$	2		2	0.3	300	$-0.0317 \pm 0.0008$	$3970 \pm 10$	$1.0514 \pm 0.0005$	24	47	1.0	2.2		
				1		1	0.7	380	$-0.0304 \pm 0.0002$			27	75	2.4	7.1		
					-2	-1	1.1	310	$0.049 \pm 0.001$			28	65	9.6	19.2		
3453272	13.32	$7100 \pm 200$	$7.0 \pm 0.6$	1		1	0.5	250	$-0.0352 \pm 0.0006$	$3500 \pm 100$	$1.38 \pm 0.01$	36	72	3.7	7.8		
3454731	9.63	$7100 \pm 200$	$6.9 \pm 0.6$	1		1	0.5	1670	$-0.022 \pm 0.002$	$3140 \pm 20$	$0.539 \pm 0.006$	14	31	0.3	1.0		1
3456780	12.69	$7800 \pm 300$	$8.6 \pm 0.7$	1		1	0.4	560	$-0.070 \pm 0.001$	$6600 \pm 300$	$1.77 \pm 0.02$	14	26	3.3	6.6		1
3539153	11.39	$6800 \pm 100$	$10 \pm 1$	1		1	0.5	520	$-0.0455 \pm 0.0008$	$4500 \pm 200$	$1.29 \pm 0.02$	23	42	2.7	5.2	1	
3540952	12.96	$7000 \pm 200$	$8.3 \pm 0.6$	1		1	0.7	490	$-0.0329 \pm 0.0002$	$3920 \pm 60$	$0.946 \pm 0.004$	29	68	2.1	5.5		
3559933	13.45	$6900 \pm 200$	$9.3 \pm 0.7$	1		1	0.6	640	$-0.024 \pm 0.003$	$2810 \pm 90$	$0.85 \pm 0.01$	34	55	1.6	2.8		
3626325	10.86	$7100 \pm 200$	$6.5 \pm 0.4$	1		1	0.9	440	$-0.0248 \pm 0.0006$	$3910 \pm 10$	$0.7820 \pm 0.0005$	45	81	2.9	5.8	1	
					-2	-1	1.6	690	$0.0203 \pm 0.0006$			22	53	7.0	12.0		
3627370	12.46	$7100 \pm 200$	$8.1 \pm 0.6$	2		2	0.5	280	$-0.0224 \pm 0.0002$	$4220 \pm 80$	$0.678 \pm 0.004$	33	86	0.9	2.7		
				1		1	0.9	650	$-0.041 \pm 0.001$			44	58	2.5	3.4		
3648936	9.50	$6960 \pm 80$	$13.3 \pm 0.9$	1		1	0.8	490	$-0.0235 \pm 0.0004$	$3400 \pm 100$	$0.749 \pm 0.008$	44	75	2.3	4.1	1	
3655115	13.07	$6800 \pm 200$	$8.5 \pm 0.8$	2		2	0.3	460	$-0.0352 \pm 0.0002$	$4180 \pm 40$	$0.902 \pm 0.005$	16	42	0.5	1.6		1
				1		1	0.5	1190	$-0.0417 \pm 0.0008$			16	30	1.1	2.3		
3734682	13.20	$7200 \pm 200$	$6.6 \pm 0.4$	2		2	0.4	360	$-0.0257 \pm 0.0002$	$3840 \pm 40$	$0.711 \pm 0.004$	32	60	0.8	1.7		
				1		1	0.7	870	$-0.0284 \pm 0.0001$			27	54	1.4	3.1		
3744571	12.03	$7100 \pm 200$	$8.5 \pm 0.6$	1		1	1.0	480	$-0.0279 \pm 0.0008$	$8000 \pm 300$	$0.757 \pm 0.004$	36	61	4.6	8.2		
3748748	12.09	$7600 \pm 300$	$7.0 \pm 0.5$	1		1	0.7	670	$-0.0325 \pm 0.0004$	$4600 \pm 100$	$0.865 \pm 0.008$	30	50	2.3	4.2		
3848351	13.72	$7100 \pm 200$	$8.2 \pm 0.6$	1		1	0.6	250	$-0.0287 \pm 0.0004$	$4890 \pm 30$	$1.344 \pm 0.001$	38	57	5.5	8.4		
					-2	-1	0.9	770	$0.031 \pm 0.009$			14	22	8.4	11.3		
3852595	12.68	$6600 \pm 200$	$15 \pm 1$	1		1	0.8	250	$-0.042 \pm 0.002$	$11000 \pm 1000$	$1.10 \pm 0.01$	35	50	9.4	13.7		
3866714	13.33	$6900 \pm 200$	$9.5 \pm 0.6$	1		1	1.4	2000	$-0.0132 \pm 0.0005$	$4730 \pm 20$	$0.242 \pm 0.001$	27	68	0.5	1.6		
3867256	12.94	$7400 \pm 300$	$18 \pm 2$	1		1	0.4	150	$-0.0480 \pm 0.0006$	$5800 \pm 400$	$2.09 \pm 0.01$	26	55	6.8	14.7		1
3868382	11.05	$6800 \pm 200$	$8.6 \pm 0.6$	2		2	0.4	360	$-0.0325 \pm 0.0002$	$4450 \pm 10$	$0.8441 \pm 0.0004$	14	65	0.5	2.7	1	
				1		1	0.7	630	$-0.0320 \pm 0.0003$			20	68	1.5	5.7		
					-2	-1	1.5	530	$0.0358 \pm 0.0002$			18	62	7.3	16.8		
3942392	9.86	$7000 \pm 200$	$5.4 \pm 0.4$	2		2	0.2	120	$-0.0402 \pm 0.0005$	$4270 \pm 30$	$1.627 \pm 0.001$	24	62	1.8	4.8	1	
				1		1	0.5	230	$-0.0383 \pm 0.0003$			26	63	3.9	9.8		
					-2	-1	0.7	120	$0.0511 \pm 0.0005$			33	62	16.5	30.5		
3964128	12.36	$7000 \pm 200$	$9.7 \pm 0.8$	1		1	0.4	230	$-0.0430 \pm 0.0007$	$4700 \pm 200$	$1.76 \pm 0.01$	18	69	3.0	12.7		
3966357	11.21	$7700 \pm 300$	$11 \pm 1$	1		1	0.6	540	$-0.0351 \pm 0.0005$	$4560 \pm 80$	$1.008 \pm 0.005$	22	59	2.0	6.0	1	
3966950	13.48	$6800 \pm 200$	$11.2 \pm 0.8$	1		1	0.9	1950	$-0.0105 \pm 0.0001$	$3720 \pm 10$	$0.241 \pm 0.002$	19	49	0.2	0.8		1
3967085	12.66	$6800 \pm 200$	$5.7 \pm 0.4$	1		1	0.7	900	$-0.034 \pm 0.001$	$4000 \pm 200$	$0.76 \pm 0.02$	27	47	1.6	3.0		
3967333	11.58	$6900 \pm 200$	$16 \pm 1$	1		1	0.5	830	$-0.035 \pm 0.002$	$3900 \pm 300$	$1.03 \pm 0.03$	25	32	2.0	2.6	1	1
3971170	13.55	$6900 \pm 200$	$7.1 \pm 0.5$	1		1	0.7	190	$-0.0264 \pm 0.0007$	$3920 \pm 30$	$1.198 \pm 0.001$	46	90	4.7	9.8		
					-2	-1	1.0	240	$0.066 \pm 0.001$			37	57	12.8	18.9		

Table 1. continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
3972467	12.55	$7200 \pm 200$	$11.7 \pm 0.8$	2		2	0.3	150	$-0.0304 \pm 0.0003$	$4340 \pm 70$	$1.175 \pm 0.004$	35	70	1.9	4.0		
				1		1	0.6	330	$-0.0318 \pm 0.0004$			21	84	2.2	9.8		
4058206	13.60	$6900 \pm 200$	$8.2 \pm 0.6$	1		1	0.6	1130	$-0.086 \pm 0.003$	$11300 \pm 200$	$1.170 \pm 0.006$	12	21	3.1	6.0		
4067389	10.75	$7700 \pm 300$	$9.2 \pm 0.8$	1		1	0.7	970	$-0.0340 \pm 0.0002$	$4300 \pm 20$	$0.756 \pm 0.002$	18	49	1.1	3.4	1	
4069477	11.21	$7400 \pm 300$	$8.0 \pm 0.9$	1		1	0.5	170	$-0.0328 \pm 0.0004$	$4020 \pm 30$	$1.531 \pm 0.002$	39	73	5.3	10.3	1	
					-2	-1	0.8	640	$0.0532 \pm 0.0006$			12	25	7.6	11.7		
4074388	12.58	$7200 \pm 200$	$8.1 \pm 0.6$	1		1	0.4	410	$-0.0324 \pm 0.0004$	$2800 \pm 90$	$1.50 \pm 0.02$	23	57	1.9	5.4		
4076350	12.42	$7600 \pm 300$	$8.5 \pm 0.7$	2		2	0.3	160	$-0.0583 \pm 0.0008$	$3470 \pm 20$	$1.248 \pm 0.001$	38	56	1.8	2.6		
				1		1	0.6	230	$-0.0454 \pm 0.0008$			46	77	4.3	7.7		
					-2	-1	1.0	430	$0.0412 \pm 0.0007$			19	53	7.6	16.5		
4077558	11.40	$7000 \pm 200$		1		1	0.6	260	$-0.0340 \pm 0.0002$	$3960 \pm 10$	$1.2063 \pm 0.0008$	29	86	3.0	9.4	1	
					-2	-1	1.1	620	$0.0409 \pm 0.0006$			12	39	7.0	13.7		
4078743	10.86	$9280 \pm 80$	$67 \pm 6$	1		1	0.3	240	$-0.0776 \pm 0.0007$	$5300 \pm 200$	$2.96 \pm 0.02$	12	33	4.0	11.5		1
4079482	13.35	$8000 \pm 300$	$14 \pm 1$	1		1	0.3	570	$-0.087 \pm 0.004$	$4200 \pm 300$	$2.45 \pm 0.05$	12	21	2.4	4.5		1
4164363	11.37	$6500 \pm 100$		1		0	0.7	2860	$0.005 \pm 0.001$	$3940 \pm 6$	$0.009 \pm 0.009$	17	28	0.0	0.0	1	
4171102	12.80	$6840 \pm 80$	$6.1 \pm 0.5$	1		1	0.8	650	$-0.0303 \pm 0.0004$	$4500 \pm 10$	$0.7579 \pm 0.0006$	32	61	2.2	4.4		1
					-2	-1	1.7	860	$0.0290 \pm 0.0009$			23	36	7.5	9.7		
4177905	11.68	$7400 \pm 300$	$14 \pm 1$	1		1	0.6	1200	$-0.0378 \pm 0.0003$	$4220 \pm 60$	$0.820 \pm 0.008$	19	30	1.2	2.1		1
4253413	13.41	$7500 \pm 300$	$14 \pm 1$	1		1	0.6	930	$-0.0358 \pm 0.0006$	$4160 \pm 70$	$0.845 \pm 0.007$	22	40	1.5	2.9		1
4255166	10.69	$7700 \pm 300$	$5.0 \pm 0.3$	1		1	0.9	350	$-0.0216 \pm 0.0003$	$4600 \pm 300$	$0.79 \pm 0.01$	55	81	4.3	6.5		
4261149	13.59	$6900 \pm 200$	$4.0 \pm 0.3$	1		1	0.7	220	$-0.0209 \pm 0.0009$	$4820 \pm 40$	$1.1251 \pm 0.0009$	44	82	5.3	10.4		
					-2	-1	1.1	440	$0.024 \pm 0.005$			26	37	11.0	14.6		
4264365	12.59	$7000 \pm 200$	$16 \pm 2$	1		1	0.7	2490	$-0.016 \pm 0.002$	$4900 \pm 100$	$0.34 \pm 0.02$	16	23	0.5	0.7		1
4278083	12.47	$7300 \pm 200$	$6.8 \pm 0.6$	1		1	0.8	350	$-0.0249 \pm 0.0003$	$4590 \pm 80$	$0.915 \pm 0.003$	35	88	3.0	8.4		
4285040	13.57	$7700 \pm 300$	$8.9 \pm 0.7$	1		1	0.6	680	$-0.0250 \pm 0.0006$	$4080 \pm 20$	$0.942 \pm 0.004$	31	42	2.4	3.3		
				1		0	1.1	1070	$-0.0146 \pm 0.0006$			37	65	1.6	2.3		
4386091	12.45	$7700 \pm 300$	$8.7 \pm 0.7$	2		2	0.2	220	$-0.0361 \pm 0.0009$	$3370 \pm 70$	$1.38 \pm 0.01$	28	46	1.3	2.3		1
				1		1	0.4	790	$-0.071 \pm 0.001$			18	27	1.6	2.6		
4390625	13.78	$7000 \pm 200$	$14 \pm 2$	2		2	0.4	80	$-0.0202 \pm 0.0003$	$3800 \pm 200$	$1.12 \pm 0.01$	64	98	3.0	4.7		1
				1		1	0.7	240	$-0.0252 \pm 0.0002$			51	76	4.7	7.2		
4446135	9.43	$6800 \pm 200$	$9.0 \pm 0.6$	1		1	0.8	660	$-0.079 \pm 0.002$	$16400 \pm 300$	$1.021 \pm 0.003$	14	32	5.0	12.6	1	
4448157	13.85	$6800 \pm 200$	$6.4 \pm 0.5$	1		1	0.6	260	$-0.0303 \pm 0.0003$	$4000 \pm 20$	$1.1698 \pm 0.0008$	32	84	3.2	8.8		
					-2	-1	1.0	200	$0.0461 \pm 0.0007$			36	68	12.7	22.5		
4464876	11.99	$6800 \pm 200$	$5.5 \pm 0.4$	2		2	0.3	230	$-0.0311 \pm 0.0003$	$4080 \pm 40$	$1.031 \pm 0.003$	27	65	1.1	3.0		
				1		1	0.6	590	$-0.0359 \pm 0.0003$			22	55	1.8	5.0		
4471379	12.34	$8200 \pm 300$	$33 \pm 3$	1		1	0.6	870	$-0.0237 \pm 0.0004$	$2820 \pm 30$	$0.793 \pm 0.005$	24	48	1.0	2.2		1
4477170	11.65	$6980 \pm 80$	$13 \pm 1$	2		2	0.5	110	$-0.01563 \pm 0.00007$	$3500 \pm 100$	$0.762 \pm 0.005$	75	137	2.2	4.1		
				1		1	1.0	270	$-0.0174 \pm 0.0001$			67	117	3.8	7.0		
4480321	10.28	$7650 \pm 80$	$37 \pm 3$	1		-1	1.3	3030	$-0.0001 \pm 0.0004$	$4229 \pm 3$	$0.0070 \pm 0.0007$	32	42	0.0	0.0	1	1
				1		0	1.3	3010	$-0.002 \pm 0.002$			36	42	0.0	0.0		
				1		1	1.3	2960	$0.0006 \pm 0.0003$			34	44	0.0	0.0		

Table 1. continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
4481004	12.57	$7000 \pm 200$	$11 \pm 1$	1		1	1.0	980	$-0.0307 \pm 0.0007$	$5900 \pm 90$	$0.576 \pm 0.003$	29	56	2.0	4.2		
4481700	13.82	$7100 \pm 300$	$11 \pm 1$	1		1	0.5	720	$-0.046 \pm 0.002$	$6400 \pm 200$	$1.24 \pm 0.01$	18	31	2.9	5.4		1
4482231	12.44	$8330 \pm 80$	$23 \pm 3$	1		1	0.3	200	$-0.0560 \pm 0.0003$	$4300 \pm 400$	$2.45 \pm 0.03$	23	42	5.0	9.5		1
4483943	13.70	$7100 \pm 200$	$10.4 \pm 0.9$	1		1	0.8	430	$-0.0418 \pm 0.0004$	$7400 \pm 500$	$1.02 \pm 0.01$	24	62	3.8	11.3		
4552374	13.09	$7000 \pm 200$	$7.3 \pm 0.6$	2		2	0.3	330	$-0.042 \pm 0.001$	$4600 \pm 100$	$1.059 \pm 0.008$	21	40	1.1	2.1		
				1		1	0.6	700	$-0.0425 \pm 0.0007$			19	41	1.9	4.3		
4566474	11.30	$7300 \pm 200$	$6.5 \pm 0.5$	1		1	0.6	280	$-0.0312 \pm 0.0006$	$4130 \pm 10$	$1.2345 \pm 0.0007$	29	76	3.2	9.0	1	
					-2	-1	1.0	570	$0.0435 \pm 0.0004$			14	41	7.3	15.1		
4566498	13.51	$7000 \pm 200$		2		2	0.3	130	$-0.0292 \pm 0.0002$	$4100 \pm 200$	$1.17 \pm 0.01$	41	74	2.0	3.8		
				1		1	0.6	270	$-0.0285 \pm 0.0002$			43	71	4.3	7.4		
4567531	10.77	$6700 \pm 200$	$6.1 \pm 0.4$	2		2	0.3	190	$-0.0195 \pm 0.0008$	$3490 \pm 60$	$1.018 \pm 0.005$	42	68	1.5	2.7		
				1		1	0.7	330	$-0.0259 \pm 0.0003$			36	89	2.6	7.2		
4577969	15.28	$6700 \pm 200$	$8 \pm 2$	1		1	0.6	220	$-0.0255 \pm 0.0003$	$3720 \pm 30$	$1.225 \pm 0.001$	45	84	4.4	8.8		
					-2	-1	0.9	230	$0.026 \pm 0.004$			45	57	14.4	18.5		
4585982	13.64	$7200 \pm 300$	$6 \pm 1$	1		1	0.6	180	$-0.0249 \pm 0.0003$	$3370 \pm 20$	$1.3924 \pm 0.0009$	39	96	3.9	10.1		1
					-2	-1	0.8	130	$0.030 \pm 0.001$			40	87	13.5	28.7		
4650137	12.93	$7100 \pm 200$	$12 \pm 1$	1		1	0.8	840	$-0.062 \pm 0.001$	$8900 \pm 300$	$0.867 \pm 0.006$	20	37	3.1	6.2		
4650563	13.59	$6770 \pm 80$	$8.1 \pm 0.6$	1		1	1.2	910	$-0.0180 \pm 0.0005$	$4440 \pm 80$	$0.457 \pm 0.003$	45	73	1.8	3.2		
4658336	13.58	$7300 \pm 300$	$9.8 \pm 0.7$	1		1	0.6	1090	$-0.0344 \pm 0.0003$	$4000 \pm 30$	$0.819 \pm 0.004$	14	46	0.8	3.2		1
4659837	10.73	$6900 \pm 200$	$6.5 \pm 0.4$	1		1	0.7	700	$-0.0203 \pm 0.0006$	$3090 \pm 30$	$0.743 \pm 0.004$	24	77	1.0	4.0	1	
4661223	11.65	$7300 \pm 300$	$5.7 \pm 0.4$	1		1	0.9	470	$-0.036 \pm 0.001$	$13100 \pm 400$	$0.890 \pm 0.004$	21	49	5.1	12.4		
4672176	13.62	$6800 \pm 200$	$8.0 \pm 0.6$	1		1	0.4	200	$-0.0398 \pm 0.0005$	$4280 \pm 20$	$1.748 \pm 0.001$	24	67	3.9	11.2		
					-2	-1	0.7	290	$0.0723 \pm 0.0004$			10	46	8.0	24.6		
4727286	13.06	$7000 \pm 200$	$8.1 \pm 0.5$	1		1	1.2	1370	$-0.0140 \pm 0.0002$	$3940 \pm 50$	$0.343 \pm 0.003$	36	69	0.8	1.9		
4743189	13.32	$7000 \pm 200$		2		2	0.3	200	$-0.0296 \pm 0.0006$	$3200 \pm 300$	$1.13 \pm 0.02$	41	54	1.5	2.1		
				1		1	0.6	390	$-0.0284 \pm 0.0005$			42	54	3.2	4.2		
				-	-	-	0.7	590	$-0.022 \pm 0.007$			-	-	-	-		
4757184	11.69	$7900 \pm 300$	$8.8 \pm 0.7$	1		1	0.8	710	$-0.015 \pm 0.001$	$3100 \pm 400$	$0.72 \pm 0.03$	43	61	1.9	2.9		
4758316	11.13	$7300 \pm 200$	$5.9 \pm 0.4$	1		1	0.6	380	$-0.0395 \pm 0.0003$	$4470 \pm 20$	$1.2445 \pm 0.0009$	23	61	2.7	7.5	1	
					-2	-1	1.0	820	$0.042 \pm 0.001$			12	23	7.3	10.2		
4774194	11.34	$9900 \pm 300$	$60 \pm 7$	2		2	0.2	120	$-0.0437 \pm 0.0004$	$4340 \pm 20$	$1.835 \pm 0.001$	20	57	1.8	5.2		
				1		1	0.4	280	$-0.0483 \pm 0.0005$			21	47	3.7	8.5		
					-2	-1	0.6	330	$0.0758 \pm 0.0004$			11	41	8.2	23.2		
4774208	13.46	$7000 \pm 200$	$6.3 \pm 0.5$	1		1	0.4	190	$-0.0427 \pm 0.0005$	$4340 \pm 20$	$1.834 \pm 0.001$	29	57	5.2	10.1		
					-2	-1	0.6	290	$0.0751 \pm 0.0004$			10	44	8.3	25.0		
4826031	12.51	$7000 \pm 200$	$5.9 \pm 0.5$	2		2	0.3	90	$-0.0269 \pm 0.0002$	$3700 \pm 200$	$1.421 \pm 0.009$	43	81	2.5	4.8		
				1		1	0.5	200	$-0.0287 \pm 0.0001$			41	74	4.7	8.7		
4839508	13.48	$6700 \pm 200$	$5.7 \pm 0.4$	1		1	0.5	230	$-0.0315 \pm 0.0002$	$3100 \pm 100$	$1.44 \pm 0.01$	35	77	3.4	7.8		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
4842057	12.58	$7200 \pm 200$	$5.7 \pm 0.4$	1		1	0.8	650	$-0.0253 \pm 0.0003$	$3850 \pm 40$	$0.718 \pm 0.003$	30	73	1.6	4.5		
4843037	13.26	$6800 \pm 200$	$8.4 \pm 0.7$	1		1	0.5	180	$-0.0320 \pm 0.0003$	$3910 \pm 20$	$1.627 \pm 0.001$	31	74	4.4	11.0		
					-2	-1	0.7	330	$0.0604 \pm 0.0004$			12	51	7.5	23.0		
4846809	12.35	$7500 \pm 300$	$8.6 \pm 0.7$	1		1	0.6	320	$-0.0334 \pm 0.0004$	$3910 \pm 20$	$1.266 \pm 0.002$	31	66	3.2	7.2		
				1		0	1.0	820	$-0.0108 \pm 0.0002$			39	72	2.0	2.8		
4847691	11.17	$6800 \pm 200$	$14 \pm 1$	1		1	0.4	190	$-0.0464 \pm 0.0006$	$4600 \pm 300$	$2.18 \pm 0.02$	24	49	5.2	11.1	1	
4857064	12.36	$7300 \pm 300$	$7.4 \pm 0.6$	1		1	1.1	570	$-0.0206 \pm 0.0002$	$3832 \pm 9$	$0.5738 \pm 0.0004$	39	102	1.7	5.1		1
					-2	-1	2.3	740	$0.010 \pm 0.001$			37	60	7.6	10.2		
4859790	12.60	$6700 \pm 200$	$7 \pm 3$	1		1	0.5	240	$-0.0358 \pm 0.0004$	$4550 \pm 20$	$1.4584 \pm 0.0007$	28	64	4.1	9.5		
					-2	-1	0.8	320	$0.0611 \pm 0.0004$			10	60	7.3	27.9		
4860458	13.43	$7300 \pm 300$	$20 \pm 2$	2		2	0.4	180	$-0.0262 \pm 0.0002$	$4240 \pm 50$	$0.934 \pm 0.003$	44	69	1.8	3.0		
				1		1	0.7	550	$-0.0321 \pm 0.0003$			26	62	2.1	5.4		
4863260	13.11	$6600 \pm 200$	$7.8 \pm 0.8$	1		1	0.9	340	$-0.0205 \pm 0.0002$	$4080 \pm 10$	$0.7980 \pm 0.0005$	49	93	3.4	6.9		
					-2	-1	1.6	760	$0.019 \pm 0.001$			19	40	7.0	10.2		
4904182	12.83	$6900 \pm 200$	$5.9 \pm 0.4$	1		1	0.7	240	$-0.066 \pm 0.001$	$16000 \pm 1000$	$1.283 \pm 0.009$	23	43	9.9	19.3		
4919344	13.28	$7500 \pm 300$	$9.0 \pm 0.6$	1		1	0.6	2510	$-0.0221 \pm 0.0006$	$4107 \pm 4$	$0.196 \pm 0.002$	18	22	0.2	0.3		
				1		0	0.7	2860	$-0.0167 \pm 0.0003$			16	24	0.2	0.3		
				1		-1	0.8	3240	$-0.0108 \pm 0.0004$			20	23	0.2	0.2		
4932276	12.61	$7000 \pm 300$	$8.2 \pm 0.6$	1		1	1.2	1150	$-0.0066 \pm 0.0001$	$2360 \pm 50$	$0.22 \pm 0.01$	59	90	0.5	0.8		
4932417	13.25	$7200 \pm 300$	$5.9 \pm 0.4$	1		1	0.5	710	$-0.0476 \pm 0.0004$	$4670 \pm 80$	$1.285 \pm 0.008$	14	38	1.6	5.1		
4951030	13.35	$7300 \pm 300$	$6.0 \pm 0.5$	1		1	0.3	160	$-0.048 \pm 0.001$	$5100 \pm 500$	$2.53 \pm 0.03$	23	44	6.3	13.0		
4952246	12.30	$7200 \pm 300$	$18 \pm 2$	1		1	1.1	700	$-0.011 \pm 0.003$	$7370 \pm 30$	$0.644 \pm 0.001$	39	50	3.9	5.1		
				1		0	1.8	1610	$-0.0136 \pm 0.0006$			43	64	2.0	2.5		
4952608	11.65	$6800 \pm 300$	$9 \pm 1$	1		1	1.3	780	$-0.0195 \pm 0.0001$	$4670 \pm 40$	$0.472 \pm 0.002$	41	89	1.8	4.3		
4995953	12.15	$6700 \pm 200$	$6.3 \pm 0.5$	2		2	0.5	280	$-0.0164 \pm 0.0006$	$2500 \pm 200$	$0.51 \pm 0.02$	72	99	0.9	1.3		
5018590	9.86	$7000 \pm 200$	$5.9 \pm 0.3$	1		1	0.5	270	$-0.0366 \pm 0.0002$	$4020 \pm 20$	$1.3790 \pm 0.0006$	27	72	3.2	8.9	1	
					-2	-1	0.9	360	$0.0559 \pm 0.0005$			14	52	7.7	20.7		
5021329	12.49	$7300 \pm 300$	$6.7 \pm 0.5$	1		1	0.4	260	$-0.040 \pm 0.002$	$4800 \pm 300$	$2.02 \pm 0.02$	20	43	4.1	9.1		
5021374	11.84	$7100 \pm 200$	$10.3 \pm 0.8$	1		1	1.1	950	$-0.0196 \pm 0.0002$	$4030 \pm 40$	$0.461 \pm 0.002$	37	76	1.3	3.0		
5025464	13.22	$7600 \pm 300$	$5.6 \pm 0.4$	2		2	0.2	130	$-0.0363 \pm 0.0005$	$3900 \pm 400$	$1.57 \pm 0.03$	35	50	2.3	3.4		
				1		1	0.5	320	$-0.0395 \pm 0.0006$			33	41	4.4	5.5		
5031804	12.82	$6900 \pm 200$	$15 \pm 1$	2		2	0.3	70	$-0.0223 \pm 0.0003$	$4100 \pm 200$	$1.30 \pm 0.01$	58	94	3.4	5.7		
				1		1	0.6	250	$-0.0304 \pm 0.0002$			37	67	4.2	7.9		
5033298	13.34	$6800 \pm 200$	$5.4 \pm 0.5$	2		2	0.2	120	$-0.0381 \pm 0.0004$	$4140 \pm 80$	$1.568 \pm 0.007$	22	73	1.5	5.2		
				1		1	0.5	360	$-0.0454 \pm 0.0006$			20	52	2.6	7.5		
5037681	13.62	$7000 \pm 300$	$9.5 \pm 0.7$	1		1	0.7	330	$-0.0281 \pm 0.0004$	$3600 \pm 100$	$1.044 \pm 0.007$	40	77	3.2	6.6		
5038228	11.37	$7000 \pm 200$	$19 \pm 2$	2		2	0.6	1170	$-0.0079 \pm 0.0004$	$4152 \pm 3$	$0.1594 \pm 0.0008$	35	41	0.2	0.2	1	
				1		1	0.9	2470	$-0.0116 \pm 0.0008$			26	32	0.2	0.3		
				1		0	1.0	2840	$-0.0006 \pm 0.0007$			28	33	0.2	0.3		
				1		-1	1.1	3360	$0.0042 \pm 0.0002$			28	35	0.2	0.3		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
5038548	12.65	$7200 \pm 200$	$7.6 \pm 0.7$	1		1	0.9	480	$-0.0235 \pm 0.0002$	$4140 \pm 90$	$0.739 \pm 0.004$	41	82	2.5	5.5		
5040435	13.11	$6800 \pm 200$	$9.6 \pm 0.8$	1		1	0.5	190	$-0.0296 \pm 0.0004$	$4070 \pm 30$	$1.440 \pm 0.001$	34	77	4.4	10.2		
					-2	-1	0.8	280	$0.073 \pm 0.004$			29	40	12.6	16.7		
5042993	11.68	$7100 \pm 200$	$9.5 \pm 0.9$	1		1	1.0	430	$-0.022 \pm 0.001$	$4100 \pm 200$	$0.710 \pm 0.007$	52	85	3.1	5.5		
5089498	11.31	$7060 \pm 80$	$10.8 \pm 0.8$	1		1	0.4	510	$-0.0593 \pm 0.0004$	$4500 \pm 80$	$1.661 \pm 0.009$	13	40	1.9	6.5		
5092684	13.60	$7200 \pm 300$	$7.0 \pm 0.5$	2		1	0.6	240	$-0.0295 \pm 0.0006$	$7700 \pm 100$	$0.938 \pm 0.002$	33	84	1.7	3.1		
				1		1	0.9	250	$-0.027 \pm 0.002$			50	70	8.0	11.9		
5113797	9.15	$8400 \pm 300$	$45 \pm 3$	2		2	0.2	80	$-0.0390 \pm 0.0002$	$4500 \pm 100$	$1.960 \pm 0.008$	30	61	2.8	6.1	1	
				1		1	0.4	250	$-0.0499 \pm 0.0006$			18	54	3.2	10.6		
5114262	13.36	$6900 \pm 200$	$4.6 \pm 0.3$	2		2	0.2	110	$-0.0336 \pm 0.0003$	$3810 \pm 70$	$1.549 \pm 0.006$	27	75	1.7	4.9		
				1		1	0.5	270	$-0.0382 \pm 0.0005$			22	70	2.6	9.2		
5114382	11.55	$6700 \pm 200$	$8.7 \pm 0.7$	1		1	0.7	230	$-0.0234 \pm 0.0002$	$4110 \pm 30$	$1.140 \pm 0.001$	46	81	4.7	8.6		
					-2	-1	1.1	510	$0.057 \pm 0.002$			21	43	8.5	14.6		
5115637	13.60	$7300 \pm 300$	$7.3 \pm 0.6$	2		2	0.4	350	$-0.0246 \pm 0.0002$	$3690 \pm 70$	$0.714 \pm 0.006$	32	63	0.8	1.7		
				1		1	0.8	700	$-0.0249 \pm 0.0004$			31	65	1.6	3.6		
5123889	12.30	$7300 \pm 300$	$13 \pm 1$	1		0	1.0	2840	$0.0003 \pm 0.0002$	$4014 \pm 6$	$0.02 \pm 0.02$	23	39	0.0	0.0		1
5179602	11.63	$7200 \pm 200$	$8.0 \pm 0.5$	2		2	0.4	190	$-0.0276 \pm 0.0001$	$4000 \pm 200$	$0.96 \pm 0.01$	43	66	1.7	2.7		
				1		1	0.7	430	$-0.0293 \pm 0.0002$			39	62	3.1	5.2		
5196787	12.14	$7300 \pm 300$	$10.1 \pm 0.8$	1		1	0.4	600	$-0.048 \pm 0.002$	$3900 \pm 300$	$1.45 \pm 0.03$	21	32	2.4	3.9		1
5210153	13.67	$7300 \pm 300$	$13 \pm 1$	2		2	0.3	180	$-0.0276 \pm 0.0002$	$4040 \pm 70$	$1.051 \pm 0.004$	32	75	1.4	3.5		
				1		1	0.7	380	$-0.0294 \pm 0.0002$			30	72	2.6	6.8		
5213221	13.01	$7000 \pm 200$	$6.2 \pm 0.5$	1		1	0.4	230	$-0.0452 \pm 0.0007$	$4400 \pm 100$	$1.89 \pm 0.01$	18	64	3.0	11.8		
5219533	9.20	$7600 \pm 300$	$50 \pm 5$	1		1	0.6	880	$-0.0149 \pm 0.0005$	$2400 \pm 40$	$0.59 \pm 0.01$	36	55	0.9	1.5	1	1
5220979	13.29	$7200 \pm 300$	$7.3 \pm 0.6$	1		1	0.6	410	$-0.0331 \pm 0.0006$	$3600 \pm 100$	$1.19 \pm 0.01$	33	53	2.9	4.8		1
5253740	12.48	$7200 \pm 300$	$7.9 \pm 0.5$	2		2	0.2	380	$-0.052 \pm 0.003$	$3670 \pm 70$	$1.15 \pm 0.01$	23	32	0.9	1.4		1
				1		1	0.5	670	$-0.039 \pm 0.002$			22	40	1.8	3.6		
5254203	12.92	$6600 \pm 200$	$4.8 \pm 0.3$	1		1	0.8	570	$-0.029 \pm 0.003$	$3000 \pm 100$	$0.65 \pm 0.01$	49	71	1.9	2.8		
5267421	11.80	$7060 \pm 80$	$6.7 \pm 0.4$	1		1	1.1	480	$-0.0204 \pm 0.0005$	$4700 \pm 100$	$0.642 \pm 0.004$	50	84	3.2	5.6		
5271224	13.32	$7560 \pm 80$	$10.3 \pm 0.9$	1		1	0.5	1400	$-0.0389 \pm 0.0003$	$4170 \pm 50$	$0.840 \pm 0.009$	16	25	1.0	1.7		1
5271803	13.68	$7300 \pm 300$	$7.5 \pm 0.6$	1		1	1.0	680	$-0.0241 \pm 0.0005$	$4150 \pm 50$	$0.605 \pm 0.003$	40	80	2.0	4.5		
5272524	13.08	$6800 \pm 200$	$6.4 \pm 0.4$	1		1	1.2	970	$-0.0191 \pm 0.0004$	$4930 \pm 70$	$0.470 \pm 0.003$	40	68	1.8	3.4		
5294571	10.52	$6900 \pm 200$	$5.8 \pm 0.5$	2		2	0.2	100	$-0.0318 \pm 0.0004$	$4150 \pm 20$	$1.6421 \pm 0.0009$	35	62	2.6	4.7	1	1
				1		1	0.5	200	$-0.0383 \pm 0.0005$			31	62	4.7	9.5		
					-2	-1	0.7	250	$0.0620 \pm 0.0004$			16	53	9.2	25.4		
5300094	12.41	$6800 \pm 200$	$6.1 \pm 0.4$	2		2	0.3	190	$-0.0369 \pm 0.0008$	$4400 \pm 100$	$1.188 \pm 0.005$	26	60	1.4	3.4		
				1		1	0.7	230	$-0.0246 \pm 0.0003$			40	82	4.5	9.7		
5301537	12.37	$6900 \pm 200$		2		2	0.3	140	$-0.0208 \pm 0.0006$	$3300 \pm 200$	$1.05 \pm 0.01$	53	85	1.9	3.4		
				1		1	0.7	330	$-0.029 \pm 0.001$			47	71	3.4	5.4		
5302643	15.32	$7000 \pm 200$	$11 \pm 2$	2		2	0.3	60	$-0.0248 \pm 0.0005$	$4000 \pm 3000$	$1.5 \pm 0.1$	61	82	3.8	5.2		
5370431	13.50	$7000 \pm 200$	$7.5 \pm 0.5$	1		1	1.1	440	$-0.0198 \pm 0.0005$	$4000 \pm 100$	$0.618 \pm 0.005$	56	100	2.9	5.5		



Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
5374279	12.85	$6800 \pm 200$	$9.6 \pm 0.8$	2		2	0.4	150	$-0.042 \pm 0.002$	$9000 \pm 2000$	$1.00 \pm 0.03$	38	53	3.7	5.2		
5390694	14.48	$6800 \pm 200$	$9 \pm 1$	1		1	1.1	430	$-0.0161 \pm 0.0009$	$3400 \pm 200$	$0.585 \pm 0.008$	73	103	3.1	4.6		
5391059	13.32	$6800 \pm 200$	$5.8 \pm 0.4$	1		1	0.4	190	$-0.0419 \pm 0.0004$	$4210 \pm 20$	$1.796 \pm 0.001$	28	59	4.7	10.0		
					-2	-1	0.7	340	$0.0710 \pm 0.0002$			11	41	8.1	22.3		
5392089	12.88	$7100 \pm 200$	$6.6 \pm 0.5$	1		1	0.5	370	$-0.0411 \pm 0.0004$	$4320 \pm 80$	$1.445 \pm 0.006$	21	56	2.6	7.7		
5395139	13.79	$7000 \pm 200$	$7.3 \pm 0.6$	1		1	0.6	340	$-0.0342 \pm 0.0003$	$4800 \pm 100$	$1.275 \pm 0.006$	25	63	3.1	8.7		
5450503	10.00	$7100 \pm 200$	$6.3 \pm 0.5$	1		1	0.6	360	$-0.0342 \pm 0.0005$	$4150 \pm 80$	$1.277 \pm 0.005$	24	63	2.6	7.4	1	
5459805	13.48	$7000 \pm 200$	$22 \pm 2$	2		-2	0.9	2740	$-0.008 \pm 0.005$	$4649 \pm 4$	$0.1265 \pm 0.0007$	34	38	0.1	0.2		1
				1		1	1.0	2860	$-0.000 \pm 0.002$			26	32	0.2	0.3		
				1		-1	1.2	3730	$0.011 \pm 0.001$			26	33	0.2	0.2		
5475187	14.75	$6900 \pm 200$	$11 \pm 2$	1		1	0.6	780	$-0.0293 \pm 0.0003$	$3770 \pm 70$	$0.847 \pm 0.008$	27	46	1.7	3.1		1
5476299	13.56	$7200 \pm 300$	$9.5 \pm 0.7$	2		2	0.3	100	$-0.0281 \pm 0.0003$	$3800 \pm 100$	$1.39 \pm 0.01$	42	76	2.4	4.5		
				1		1	0.5	290	$-0.0340 \pm 0.0004$			30	64	3.3	7.5		
5476473	13.74	$6600 \pm 200$	$13 \pm 1$	1		1	0.4	280	$-0.0519 \pm 0.0004$	$4130 \pm 20$	$1.917 \pm 0.004$	23	46	3.8	8.0		
				1		0	0.7	810	$-0.0152 \pm 0.0001$			29	50	2.2	2.9		
5476854	12.79	$7000 \pm 200$	$5.9 \pm 0.5$	1		1	1.0	410	$-0.0183 \pm 0.0004$	$4060 \pm 10$	$0.6647 \pm 0.0004$	54	92	3.1	5.4		1
					-2	-1	1.9	630	$0.0281 \pm 0.0007$			30	65	7.6	13.0		
5476864	11.46	$6600 \pm 100$	$16 \pm 1$	1		1	0.7	1120	$-0.034 \pm 0.002$	$4280 \pm 30$	$0.697 \pm 0.004$	19	44	1.0	2.7	1	1
5478788	13.36	$6600 \pm 200$	$11.2 \pm 0.8$	2		2	0.4	120	$-0.0223 \pm 0.0002$	$3900 \pm 100$	$0.987 \pm 0.006$	48	94	2.0	4.1		
				1		1	0.7	330	$-0.0265 \pm 0.0005$			43	73	3.6	6.3		
5481390	13.26	$9800 \pm 300$	$60 \pm 10$	2		2	0.3	120	$-0.045 \pm 0.002$	$9000 \pm 3000$	$1.49 \pm 0.05$	29	38	4.6	6.0		
5481482	14.31	$6500 \pm 200$	$5.6 \pm 0.6$	2		2	0.5	400	$-0.012 \pm 0.001$	$4670 \pm 60$	$0.594 \pm 0.003$	40	59	1.1	1.7		
				1		1	1.0	700	$-0.0233 \pm 0.0002$			38	72	2.1	4.3		
5522154	10.43	$6900 \pm 200$	$4.3 \pm 0.3$	1		1	0.3	350	$-0.0626 \pm 0.0007$	$4300 \pm 100$	$2.13 \pm 0.01$	15	39	2.8	8.0		
5530816	12.76	$6910 \pm 80$	$23 \pm 2$	2		2	0.3	60	$-0.0287 \pm 0.0004$	$4500 \pm 300$	$1.61 \pm 0.02$	55	69	4.4	5.6		
				1		1	0.5	280	$-0.0425 \pm 0.0003$			33	44	5.1	7.0		
				-	-	-	0.5	310	$0.002 \pm 0.004$			-	-	-	-		
5544996	13.96	$7200 \pm 300$	$6.9 \pm 0.6$	2		1	0.8	1270	$-0.0101 \pm 0.0002$	$4649 \pm 8$	$0.2333 \pm 0.0006$	24	65	0.2	0.6		
				1		1	1.2	2140	$-0.0114 \pm 0.0001$			16	65	0.3	1.4		
5557072	12.88	$7000 \pm 200$	$34 \pm 4$	1		-1	1.7	2580	$0.0020 \pm 0.0003$	$3465 \pm 3$	$0.0001 \pm 0.0002$	47	75	0.0	0.0		1
				1		0	1.7	2560	$0.0020 \pm 0.0003$			46	74	0.0	0.0		
				1		1	1.7	2540	$0.0012 \pm 0.0003$			46	75	0.0	0.0		
5565100	15.07	$6700 \pm 200$	$10 \pm 2$	2		2	0.3	70	$-0.028 \pm 0.003$	$3650 \pm 60$	$1.091 \pm 0.005$	39	56	1.6	1.9		
				1		1	0.6	430	$-0.0365 \pm 0.0005$			29	65	2.4	6.1		
5608334	9.91	$6900 \pm 200$	$7.4 \pm 0.4$	1		1	0.4	140	$-0.0418 \pm 0.0009$	$4400 \pm 200$	$2.25 \pm 0.01$	23	64	4.8	14.1	1	
5617102	13.57	$7600 \pm 300$	$7.7 \pm 0.5$	1		1	0.5	940	$-0.0534 \pm 0.0004$	$4670 \pm 90$	$1.18 \pm 0.01$	16	26	1.8	3.1		1
5640438	13.68	$6900 \pm 200$	$8.0 \pm 0.6$	1		1	0.7	370	$-0.0276 \pm 0.0003$	$4230 \pm 20$	$0.9788 \pm 0.0005$	35	73	3.1	6.8		
					-2	-1	1.2	390	$0.0376 \pm 0.0003$			14	81	6.9	23.7		
5646058	10.89	$6900 \pm 200$	$8.3 \pm 0.5$	1		1	0.4	130	$-0.0341 \pm 0.0007$	$4700 \pm 200$	$1.93 \pm 0.01$	29	74	5.6	14.9		
5648562	13.99	$6800 \pm 300$	$11 \pm 1$	1		1	0.8	950	$-0.0291 \pm 0.0002$	$4410 \pm 70$	$0.677 \pm 0.005$	26	49	1.5	3.1		1

**Table 1.** continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
5652678	11.91	$6800 \pm 200$	$8.0 \pm 0.8$	1		1	0.6	280	$-0.0280 \pm 0.0002$	$3660 \pm 80$	$1.140 \pm 0.005$	35	89	3.0	8.3		
5702637	12.11	$7100 \pm 200$	$10 \pm 3$	1		1	0.4	340	$-0.0511 \pm 0.0005$	$4440 \pm 90$	$1.796 \pm 0.008$	18	44	3.0	7.8		1
5706866	12.55	$7100 \pm 200$		1		1	0.6	180	$-0.027 \pm 0.001$	$3610 \pm 20$	$1.218 \pm 0.001$	60	90	5.8	9.3		
					-2	-1	1.1	610	$0.0342 \pm 0.0004$			15	37	7.2	12.1		
5708550	11.92	$7400 \pm 300$	$7.3 \pm 0.7$	1		1	0.9	360	$-0.0233 \pm 0.0004$	$3840 \pm 10$	$0.7911 \pm 0.0006$	40	99	2.5	6.7		
					-2	-1	1.7	800	$0.010 \pm 0.001$			16	40	6.6	9.7		
5721632	13.41	$7300 \pm 300$	$6.8 \pm 0.4$	1		1	0.4	320	$-0.0479 \pm 0.0006$	$4371 \pm 8$	$1.6969 \pm 0.0009$	17	53	2.7	9.0		
					-2	-1	0.7	220	$0.0696 \pm 0.0004$			24	43	12.9	22.5		
					-1	-1	1.9	4270	$0.094 \pm 0.001$			24	42	2.6	3.2		
5781077	11.78	$7300 \pm 300$	$7.0 \pm 0.4$	1		1	0.6	340	$-0.0334 \pm 0.0002$	$4800 \pm 100$	$1.205 \pm 0.007$	28	62	3.4	8.0		
5788623	12.07	$7070 \pm 80$	$6.1 \pm 0.4$	1		1	1.3	980	$-0.0163 \pm 0.0001$	$3890 \pm 30$	$0.397 \pm 0.002$	41	86	1.2	2.8		
5801556	13.65	$6900 \pm 200$	$8.4 \pm 0.9$	2		2	0.3	230	$-0.0401 \pm 0.0007$	$4240 \pm 20$	$1.2186 \pm 0.0008$	19	55	1.0	3.2		
				1		1	0.6	230	$-0.042 \pm 0.001$			43	69	4.9	7.8		
					-2	-1	1.1	740	$0.0335 \pm 0.0007$			12	29	7.1	11.3		
5810197	12.61	$7550 \pm 80$	$19 \pm 3$	1		1	1.6	1930	$-0.0066 \pm 0.0003$	$3193 \pm 4$	$0.0825 \pm 0.0006$	59	72	0.2	0.3		
				1		-1	1.7	2590	$-0.006 \pm 0.002$			58	67	0.2	0.2		
5811454	11.62	$7810 \pm 80$	$14 \pm 2$	1		1	0.3	300	$-0.0793 \pm 0.0009$	$5200 \pm 400$	$2.80 \pm 0.04$	15	26	4.5	8.2		1
5821056	15.51	$6600 \pm 200$	$10 \pm 3$	1		1	0.5	210	$-0.0319 \pm 0.0003$	$3940 \pm 20$	$1.5344 \pm 0.0009$	33	70	4.3	9.6		
					-2	-1	0.8	280	$0.0562 \pm 0.0004$			14	61	7.8	25.9		
5872733	13.46	$7100 \pm 80$	$6.5 \pm 0.5$	1		1	1.8	1470	$-0.002 \pm 0.001$	$2440 \pm 70$	$0.10 \pm 0.01$	86	111	0.3	0.4		
5876187	11.99	$6850 \pm 80$	$9.2 \pm 0.6$	3		3	0.4	140	$-0.0175 \pm 0.0003$	$4100 \pm 100$	$0.596 \pm 0.005$	66	90	1.1	1.6		
				2		2	0.6	230	$-0.0174 \pm 0.0002$			57	96	1.4	2.5		
				1		1	1.2	380	$-0.0180 \pm 0.0001$			58	119	2.9	6.4		
5879641	13.93	$7200 \pm 200$	$7.1 \pm 0.6$	1		1	0.8	220	$-0.0175 \pm 0.0007$	$3000 \pm 400$	$0.88 \pm 0.02$	83	110	4.7	6.4		
5887983	10.81	$7120 \pm 80$	$11 \pm 1$	1		1	0.6	420	$-0.0351 \pm 0.0004$	$4150 \pm 70$	$1.145 \pm 0.005$	26	61	2.6	6.4	1	
5891975	15.27	$7100 \pm 200$	$10 \pm 2$	1		1	0.4	650	$-0.0497 \pm 0.0004$	$3400 \pm 20$	$1.444 \pm 0.004$	8	47	0.7	5.0		1
5894044	12.05	$6700 \pm 200$		1		1	0.5	270	$-0.0405 \pm 0.0002$	$4300 \pm 200$	$1.62 \pm 0.02$	28	52	4.2	8.0		
5954264	8.16	$6900 \pm 100$	$11.1 \pm 0.6$	2		2	0.3	90	$-0.0305 \pm 0.0003$	$4700 \pm 100$	$1.330 \pm 0.008$	44	74	3.0	5.1	1	
				1		1	0.5	470	$-0.0454 \pm 0.0004$			25	39	3.3	5.3		
5978913	13.84	$6600 \pm 200$	$13 \pm 2$	2		2	0.4	180	$-0.0192 \pm 0.0006$	$4000 \pm 100$	$0.955 \pm 0.005$	40	78	1.6	3.4		
				1		1	0.8	200	$-0.0132 \pm 0.0005$			68	98	5.8	8.6		
5984615	13.86	$7500 \pm 300$	$12 \pm 2$	1		1	0.8	240	$-0.0235 \pm 0.0002$	$3820 \pm 20$	$0.9892 \pm 0.0007$	47	101	3.8	8.5		
					-2	-1	1.3	530	$0.0368 \pm 0.0008$			20	61	7.0	16.4		
5985441	15.83	$7000 \pm 300$	$5 \pm 1$	2		2	0.2	160	$-0.0382 \pm 0.0002$	$4320 \pm 90$	$1.473 \pm 0.008$	27	53	1.8	3.7		
				1		1	0.5	380	$-0.0486 \pm 0.0005$			23	48	3.0	6.5		
6019416	11.05	$7300 \pm 300$	$7.0 \pm 0.4$	1		1	0.5	1000	$-0.0349 \pm 0.0008$	$3600 \pm 100$	$0.92 \pm 0.02$	23	31	1.4	2.0		1
6035335	11.86	$7300 \pm 200$	$5.2 \pm 0.3$	2		2	0.2	120	$-0.0341 \pm 0.0005$	$4200 \pm 100$	$1.580 \pm 0.008$	27	63	1.9	4.7		
				1		1	0.5	250	$-0.0347 \pm 0.0005$			26	63	3.6	9.3		
6041803	12.90	$7220 \pm 80$	$8.0 \pm 0.6$	2		2	0.2	120	$-0.0348 \pm 0.0002$	$4100 \pm 200$	$1.53 \pm 0.02$	35	61	2.3	4.1		
				1		1	0.5	320	$-0.0408 \pm 0.0007$			30	47	3.9	6.4		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
6044597	12.07	$7300 \pm 200$	$6.2 \pm 0.4$	1		1	0.9	410	$-0.0271 \pm 0.0003$	$4400 \pm 100$	$0.781 \pm 0.004$	41	85	2.9	6.4		
6048255	13.86	$7300 \pm 300$	$6.6 \pm 0.5$	1		1	0.6	170	$-0.0252 \pm 0.0002$	$3750 \pm 30$	$1.3748 \pm 0.0009$	43	94	4.9	11.1		
					−2	−1	0.8	130	$0.0374 \pm 0.0005$			40	76	14.9	27.6		
6058830	11.46	$6600 \pm 200$		2		2	0.3	150	$-0.0294 \pm 0.0005$	$5000 \pm 100$	$1.213 \pm 0.005$	28	66	1.8	4.6	1	
				1		1	0.6	260	$-0.0305 \pm 0.0002$			32	71	4.2	9.8		
6062766	12.21	$7300 \pm 300$	$11 \pm 2$	2		2	0.3	90	$-0.0267 \pm 0.0001$	$4000 \pm 200$	$1.458 \pm 0.009$	35	94	2.1	6.0		
				1		1	0.5	160	$-0.0290 \pm 0.0002$			47	80	5.9	10.3		
6064932	10.47	$7000 \pm 200$	$6.4 \pm 0.6$	1		1	0.9	700	$-0.026 \pm 0.001$	$4790 \pm 70$	$0.668 \pm 0.003$	31	64	2.0	4.3		
6067707	11.17	$8800 \pm 300$	$130 \pm 20$	1		1	0.4	380	$-0.0552 \pm 0.0007$	$4800 \pm 200$	$1.94 \pm 0.02$	18	35	3.5	7.2		
6126012	11.62	$6800 \pm 200$	$11.7 \pm 0.8$	1		1	0.7	370	$-0.034 \pm 0.001$	$4800 \pm 200$	$1.016 \pm 0.008$	36	66	3.7	7.1		
6131093	9.25	$6600 \pm 200$	$8 \pm 1$	2		2	0.3	240	$-0.0351 \pm 0.0004$	$4160 \pm 70$	$1.136 \pm 0.005$	22	56	1.1	2.9	1	
				1		1	0.6	440	$-0.0353 \pm 0.0003$			23	61	2.3	6.4		
6207355	13.45	$7400 \pm 300$	$6.6 \pm 0.4$	1		1	0.7	480	$-0.0261 \pm 0.0006$	$2420 \pm 90$	$0.82 \pm 0.01$	51	81	2.0	3.6		
6229502	12.08	$7400 \pm 300$	$15 \pm 1$	1		1	0.8	980	$-0.0274 \pm 0.0003$	$4130 \pm 50$	$0.644 \pm 0.004$	28	49	1.4	2.7		1
6229965	13.02	$7400 \pm 300$	$7.5 \pm 0.6$	1		1	0.7	470	$-0.0337 \pm 0.0004$	$4530 \pm 80$	$0.991 \pm 0.004$	23	66	2.1	6.6		
6230921	13.25	$7300 \pm 300$	$9.8 \pm 0.9$	2		2	0.6	1830	$-0.0100 \pm 0.0009$	$4890 \pm 10$	$0.047 \pm 0.002$	25	30	0.0	0.0		1
				1		1	0.9	3300	$-0.004 \pm 0.001$			18	28	0.0	0.1		
6284209	13.56	$7300 \pm 300$	$6.3 \pm 0.4$	1		1	0.5	330	$-0.0390 \pm 0.0002$	$4000 \pm 300$	$1.48 \pm 0.02$	31	45	4.0	5.9		
6286468	13.25	$7200 \pm 200$	$5.9 \pm 0.4$	1		1	0.7	250	$-0.0215 \pm 0.0002$	$2500 \pm 200$	$0.99 \pm 0.02$	63	105	3.3	5.9		
6290382	13.18	$7200 \pm 300$		1		1	0.5	1040	$-0.0432 \pm 0.0006$	$4050 \pm 50$	$0.998 \pm 0.007$	16	29	1.3	2.5		1
6291473	13.64	$7300 \pm 300$	$6.3 \pm 0.5$	2		2	0.2	110	$-0.0329 \pm 0.0004$	$5770 \pm 40$	$1.671 \pm 0.001$	20	63	2.1	7.3		
				1		1	0.5	210	$-0.0342 \pm 0.0004$			26	57	5.6	13.0		
					−2	−1	0.7	310	$0.11 \pm 0.02$			22	29	15.1	19.9		
6292398	9.83	$7700 \pm 300$		2		2	0.3	150	$-0.0332 \pm 0.0002$	$4000 \pm 100$	$1.338 \pm 0.007$	27	68	1.5	4.0	1	
				1		1	0.6	230	$-0.0308 \pm 0.0001$			36	76	4.1	9.1		
6293045	12.23	$7200 \pm 200$	$7.9 \pm 0.5$	1		1	0.7	250	$-0.032 \pm 0.001$	$4100 \pm 400$	$1.05 \pm 0.02$	51	77	4.8	7.4		
6301745	10.85	$6700 \pm 100$	$5.8 \pm 0.4$	1		1	0.3	210	$-0.0495 \pm 0.0008$	$4210 \pm 40$	$2.297 \pm 0.002$	22	42	4.8	9.3	1	
					−2	−1	0.5	110	$0.0672 \pm 0.0009$			22	47	15.7	32.1		
6302589	12.68	$7700 \pm 300$	$12 \pm 1$	1		0	0.7	3110	$-0.011 \pm 0.003$	$4335 \pm 5$	$0.111 \pm 0.002$	18	21	0.1	0.1		1
				1		1	0.7	2810	$-0.005 \pm 0.001$			18	27	0.1	0.2		
				1		−1	0.8	3330	$-0.000 \pm 0.002$			18	25	0.1	0.1		
6366512	11.56	$6980 \pm 80$	$6.1 \pm 0.3$	2		2	0.3	120	$-0.036 \pm 0.001$	$3900 \pm 200$	$1.17 \pm 0.01$	49	72	2.4	3.7	1	
				1		1	0.6	320	$-0.040 \pm 0.002$			41	57	4.1	5.7		
6383932	12.59	$7100 \pm 200$		1		1	0.4	330	$-0.0508 \pm 0.0004$	$4400 \pm 200$	$1.84 \pm 0.01$	21	38	3.7	6.9		
6387770	12.52	$7500 \pm 300$	$9.7 \pm 0.9$	1		1	0.6	380	$-0.0364 \pm 0.0003$	$4240 \pm 10$	$1.2517 \pm 0.0008$	28	53	3.2	6.3		
					−2	−1	1.0	610	$0.0493 \pm 0.0006$			12	36	7.2	14.0		
6387895	11.97	$7400 \pm 300$	$5.5 \pm 0.4$	1		1	0.4	150	$-0.0478 \pm 0.0009$	$4800 \pm 200$	$2.34 \pm 0.01$	16	67	3.7	17.1		
6389098	13.46	$7000 \pm 200$	$15 \pm 1$	1		1	0.3	470	$-0.078 \pm 0.002$	$4800 \pm 200$	$2.32 \pm 0.02$	12	26	2.7	6.4		1
6445969	12.88	$7300 \pm 300$	$10.7 \pm 0.9$	2		2	0.3	90	$-0.0264 \pm 0.0002$	$4500 \pm 200$	$1.263 \pm 0.007$	42	86	2.6	5.5		
				1		1	0.6	200	$-0.0275 \pm 0.0004$			41	80	5.1	10.2		

Table 1. continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
6448666	11.00	$7200 \pm 300$	$5.9 \pm 0.4$	1		1	0.4	210	$-0.0413 \pm 0.0009$	$3800 \pm 600$	$2.06 \pm 0.05$	31	45	5.3	7.9	1	
6449081	10.65	$6930 \pm 80$	$2.4 \pm 0.6$	1		1	1.0	520	$-0.0218 \pm 0.0003$	$3900 \pm 100$	$0.651 \pm 0.005$	50	82	2.6	4.6	1	
6467639	12.01	$7100 \pm 200$	$18 \pm 2$	1		1	0.6	2380	$-0.0228 \pm 0.0004$	$3889 \pm 3$	$0.217 \pm 0.002$	17	23	0.2	0.3		1
				1		0	0.7	2610	$-0.001 \pm 0.001$			22	25	0.2	0.3		
				1		-1	0.9	3180	$0.0081 \pm 0.0002$			22	30	0.2	0.3		
6468146	9.96	$6600 \pm 200$	$8.2 \pm 0.5$	1		1	0.6	570	$-0.0351 \pm 0.0002$	$4270 \pm 50$	$0.981 \pm 0.004$	24	58	2.0	5.3		1
6468987	12.66	$7300 \pm 300$	$9.6 \pm 0.7$	1		1	0.5	230	$-0.035 \pm 0.001$	$4020 \pm 50$	$1.551 \pm 0.002$	29	64	4.0	9.1		
					-2	-1	0.7	190	$0.07 \pm 0.01$			37	45	16.6	20.2		
6469599	13.26	$7600 \pm 300$	$2.6 \pm 0.2$	2		2	0.2	190	$-0.0410 \pm 0.0004$	$3880 \pm 80$	$1.502 \pm 0.008$	20	54	1.2	3.4		
				1		1	0.4	380	$-0.0426 \pm 0.0005$			24	50	2.8	6.3		
6469690	13.91	$7700 \pm 300$	$8.2 \pm 0.9$	2		2	0.5	270	$-0.0170 \pm 0.0002$	$3710 \pm 80$	$0.566 \pm 0.005$	57	92	1.2	2.1		
				1		1	1.0	700	$-0.0197 \pm 0.0003$			44	77	1.8	3.5		
6470973	13.14	$8600 \pm 300$	$22 \pm 2$	1		1	0.6	770	$-0.0205 \pm 0.0002$	$2550 \pm 30$	$0.704 \pm 0.007$	30	61	1.0	2.2		1
6519869	10.47	$7400 \pm 300$	$6.3 \pm 0.3$	1		1	0.8	490	$-0.014 \pm 0.002$	$3000 \pm 200$	$0.78 \pm 0.02$	51	69	2.5	3.5	1	
6522144	13.56	$7600 \pm 300$	$12 \pm 1$	1		1	0.5	920	$-0.057 \pm 0.002$	$5400 \pm 300$	$1.09 \pm 0.02$	21	27	2.4	3.2		1
6531801	13.59	$7300 \pm 300$	$6.2 \pm 0.5$	2		2	0.3	130	$-0.0242 \pm 0.0009$	$3540 \pm 90$	$1.408 \pm 0.008$	31	68	1.6	3.7		
				1		1	0.5	270	$-0.0336 \pm 0.0003$			32	65	3.4	7.2		
6595406	13.33	$7300 \pm 300$	$7.0 \pm 0.5$	2		2	0.3	60	$-0.0137 \pm 0.0008$	$3300 \pm 500$	$1.57 \pm 0.04$	61	79	3.4	4.5		
				1		1	0.5	200	$-0.020 \pm 0.003$			51	59	5.7	6.7		
6604303	13.30	$7500 \pm 300$	$9.7 \pm 0.6$	1		1	0.6	800	$-0.0376 \pm 0.0003$	$3950 \pm 50$	$0.960 \pm 0.005$	19	46	1.3	3.7		1
6614168	11.44	$7500 \pm 300$	$8.8 \pm 0.6$	1		1	0.6	1080	$-0.037 \pm 0.001$	$4800 \pm 200$	$0.93 \pm 0.02$	20	30	1.7	2.8	1	1
6678174	11.73	$6800 \pm 200$	$8.5 \pm 0.5$	1		1	1.0	990	$-0.034 \pm 0.002$	$8600 \pm 200$	$0.697 \pm 0.005$	26	39	3.2	5.1		
6681516	13.50	$7400 \pm 300$	$7.0 \pm 0.5$	1		1	1.1	1030	$-0.0194 \pm 0.0007$	$4100 \pm 100$	$0.444 \pm 0.009$	46	59	1.6	2.1		
6696689	13.25	$7400 \pm 300$	$9.2 \pm 0.7$	1		1	0.7	180	$-0.0239 \pm 0.0002$	$3830 \pm 20$	$1.1057 \pm 0.0006$	51	104	4.7	9.9		
					-2	-1	1.0	190	$0.0347 \pm 0.0004$			44	79	13.2	23.6		
6701459	11.59	$7000 \pm 200$	$9.3 \pm 0.7$	1		1	1.3	410	$-0.0196 \pm 0.0005$	$3600 \pm 300$	$0.53 \pm 0.01$	85	110	3.4	4.6	1	
6706038	13.60	$7200 \pm 300$	$6.6 \pm 0.5$	2		2	0.3	80	$-0.0315 \pm 0.0001$	$3800 \pm 300$	$1.56 \pm 0.02$	47	70	3.1	4.7		
				1		1	0.5	120	$-0.0232 \pm 0.0002$			51	98	6.7	13.4		
6720889	13.17	$6800 \pm 200$	$13 \pm 1$	1		1	0.7	720	$-0.0318 \pm 0.0002$	$4240 \pm 90$	$0.816 \pm 0.007$	30	49	2.1	3.6		1
6757160	13.00	$7000 \pm 200$	$9.3 \pm 0.7$	1		1	0.5	1060	$-0.037 \pm 0.001$	$3400 \pm 100$	$0.87 \pm 0.02$	23	30	1.3	1.7		1
6762992	12.63	$7700 \pm 300$	$12 \pm 1$	1		1	0.7	880	$-0.0277 \pm 0.0002$	$3500 \pm 30$	$0.721 \pm 0.004$	26	51	1.2	2.7		1
6764812	10.93	$6800 \pm 200$	$14.6 \pm 0.9$	2		2	0.3	150	$-0.0215 \pm 0.0009$	$3000 \pm 200$	$1.05 \pm 0.01$	47	78	1.5	2.7	1	
				1		1	0.7	220	$-0.025 \pm 0.005$			66	83	4.6	5.8		
6777669	13.30	$7300 \pm 300$	$6.0 \pm 0.4$	1		1	1.1	860	$-0.0180 \pm 0.0001$	$3590 \pm 30$	$0.468 \pm 0.002$	41	81	1.3	2.8		
6778063	12.17	$7400 \pm 300$	$12 \pm 1$	1		1	0.5	1310	$-0.0365 \pm 0.0004$	$3890 \pm 90$	$0.89 \pm 0.02$	15	25	0.9	1.7		1
6778113	13.34	$7300 \pm 200$	$11 \pm 1$	1		1	1.0	400	$-0.052 \pm 0.002$	$21000 \pm 1000$	$0.863 \pm 0.004$	25	38	10.0	15.7		
6780397	10.05	$11400 \pm 400$		1		1	1.6	2150	$-0.060 \pm 0.001$	$18100 \pm 500$	$0.415 \pm 0.003$	16	34	2.3	5.5		
6782360	12.63	$7300 \pm 200$	$7.0 \pm 0.5$	1		1	0.8	380	$-0.0257 \pm 0.0003$	$4510 \pm 80$	$0.873 \pm 0.003$	29	93	2.3	8.5		
6784155	11.99	$7500 \pm 300$	$17 \pm 1$	1		1	0.4	780	$-0.0550 \pm 0.0002$	$4370 \pm 50$	$1.310 \pm 0.006$	15	32	1.6	3.9		1
6784170	13.61	$7300 \pm 300$	$6.9 \pm 0.5$	2		2	0.3	220	$-0.0305 \pm 0.0007$	$2400 \pm 100$	$0.87 \pm 0.01$	45	75	0.9	1.6		
				1		1	0.7	370	$-0.0071 \pm 0.0009$			60	86	2.5	3.9		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
6790408	12.64	$7400 \pm 300$	$3.5 \pm 0.3$	1		1	0.5	320	$-0.0422 \pm 0.0004$	$4500 \pm 100$	$1.525 \pm 0.008$	22	55	3.2	8.5		
6806005	13.17	$6800 \pm 200$	$7.8 \pm 0.6$	1		1	0.6	240	$-0.0307 \pm 0.0006$	$4000 \pm 20$	$1.3235 \pm 0.0008$	34	71	4.0	8.5		
					-2	-1	0.9	380	$0.0501 \pm 0.0004$			13	60	7.2	22.3		
6862920B	12.31	$7400 \pm 300$	$22 \pm 2$	1		1	0.5	1160	$-0.0383 \pm 0.0006$	$4200 \pm 100$	$0.85 \pm 0.01$	20	29	1.4	2.1		1
6862920A	12.31	$7400 \pm 300$	$22 \pm 2$	2		2	0.3	410	$-0.0309 \pm 0.0003$	$3970 \pm 40$	$0.837 \pm 0.005$	29	39	1.0	1.3		1
				1		1	0.5	1130	$-0.0369 \pm 0.0003$			19	33	1.1	2.2		
6864276	13.14	$7300 \pm 300$	$6.0 \pm 0.5$	1		1	0.5	350	$-0.0319 \pm 0.0003$	$3000 \pm 200$	$1.29 \pm 0.02$	34	60	2.7	5.1		
6877258	13.84	$7500 \pm 300$	$8.4 \pm 0.7$	1		1	0.6	980	$-0.0350 \pm 0.0006$	$3720 \pm 60$	$0.791 \pm 0.007$	24	40	1.3	2.4		
6891998	13.65	$6900 \pm 200$	$18 \pm 2$	1		1	0.3	750	$-0.062 \pm 0.001$	$4290 \pm 60$	$1.677 \pm 0.009$	12	26	1.7	4.0		1
6923424	11.28	$7300 \pm 300$	$5.8 \pm 0.3$	2		2	0.2	80	$-0.0398 \pm 0.0005$	$4230 \pm 30$	$2.023 \pm 0.002$	22	74	2.0	7.0	1	
				1		1	0.4	240	$-0.0496 \pm 0.0006$			16	55	3.0	10.7		
					-2	-1	0.5	80	$0.0494 \pm 0.0007$			31	59	19.1	35.5		
6935014	10.90	$7100 \pm 200$	$4.7 \pm 0.3$	1		1	0.9	430	$-0.0263 \pm 0.0002$	$4390 \pm 70$	$0.789 \pm 0.003$	38	85	2.7	6.5		
6937123	11.37	$7000 \pm 200$	$12.0 \pm 0.8$	2		2	0.7	1010	$-0.0061 \pm 0.0003$	$3486 \pm 3$	$0.1292 \pm 0.0004$	47	60	0.2	0.2		1
				2		1	0.8	1160	$-0.0023 \pm 0.0006$			51	58	0.2	0.2		
				1		1	1.2	2050	$-0.0039 \pm 0.0002$			38	52	0.2	0.4		
				2		-2	1.2	2210	$0.011 \pm 0.001$			54	62	0.2	0.2		
				1		0	1.2	2390	$-0.0007 \pm 0.0009$			39	49	0.2	0.3		
				1		-1	1.5	2850	$0.0004 \pm 0.0005$			46	54	0.3	0.3		
6940150	12.46	$7700 \pm 300$	$13 \pm 1$	1		1	0.8	700	$-0.003 \pm 0.005$	$3700 \pm 500$	$0.72 \pm 0.04$	45	53	2.4	2.9		
6945362	11.31	$6690 \pm 80$	$9 \pm 2$	1		1	0.6	270	$-0.026 \pm 0.001$	$5000 \pm 400$	$1.28 \pm 0.01$	36	58	5.0	8.3	1	
6947195	12.91	$7300 \pm 300$	$14 \pm 1$	1		1	1.0	430	$-0.0197 \pm 0.0004$	$3700 \pm 100$	$0.684 \pm 0.005$	53	98	2.8	5.7		
6952259	12.42	$7000 \pm 200$	$6.3 \pm 0.4$	2		2	0.2	120	$-0.0386 \pm 0.0005$	$3900 \pm 100$	$1.589 \pm 0.007$	27	67	1.8	4.6		
				1		1	0.5	260	$-0.0387 \pm 0.0003$			25	64	3.2	8.9		
6953103	12.56	$7400 \pm 300$	$6.0 \pm 0.4$	1		1	0.9	630	$-0.0304 \pm 0.0004$	$4080 \pm 80$	$0.704 \pm 0.005$	37	69	2.1	4.4		
6974111	12.80	$8200 \pm 300$	$11 \pm 1$	1		1	0.3	630	$-0.099 \pm 0.002$	$4890 \pm 80$	$2.51 \pm 0.01$	8	22	1.8	5.7		1
7007103	11.23	$7200 \pm 200$	$6.6 \pm 0.4$	2		2	0.3	130	$-0.0280 \pm 0.0004$	$4400 \pm 200$	$1.177 \pm 0.009$	40	73	2.2	4.1	1	
				1		1	0.6	310	$-0.0317 \pm 0.0005$			35	65	3.8	7.4		
7023122	10.83	$6900 \pm 200$	$5.3 \pm 0.3$	1		1	0.5	1070	$-0.0438 \pm 0.0003$	$4390 \pm 60$	$0.942 \pm 0.008$	17	32	1.3	2.7		
7035394	13.38	$7200 \pm 300$	$6.9 \pm 0.4$	1		1	1.0	570	$-0.0246 \pm 0.0004$	$4800 \pm 100$	$0.649 \pm 0.004$	40	81	2.5	5.7		
7039007	13.65	$6900 \pm 200$	$6.9 \pm 0.6$	1		1	0.7	290	$-0.0300 \pm 0.0005$	$3970 \pm 20$	$1.039 \pm 0.001$	45	74	4.1	6.9		
					-2	-1	1.2	650	$0.0257 \pm 0.0007$			20	35	7.9	11.1		
7050378	13.82	$7100 \pm 200$	$5.6 \pm 0.4$	1		1	0.8	500	$-0.0256 \pm 0.0002$	$4320 \pm 80$	$0.786 \pm 0.004$	32	78	2.2	5.9		
7059699	13.66	$7500 \pm 300$	$8.2 \pm 0.7$	1		1	0.3	240	$-0.0608 \pm 0.0003$	$5100 \pm 200$	$2.30 \pm 0.02$	17	44	4.1	11.3		
7106648	10.49	$7300 \pm 200$	$8.5 \pm 0.4$	1		1	0.3	490	$-0.0581 \pm 0.0001$	$3800 \pm 300$	$1.88 \pm 0.04$	20	28	2.9	4.3	1	1
7137351	12.47	$7100 \pm 200$	$9.0 \pm 0.8$	1		1	0.6	230	$-0.0329 \pm 0.0003$	$3820 \pm 10$	$1.2129 \pm 0.0009$	35	88	3.5	9.0		
					-2	-1	1.0	550	$0.0353 \pm 0.0003$			15	47	7.0	15.5		
7175943	12.86	$7000 \pm 200$	$8.1 \pm 0.6$	1		1	0.7	350	$-0.022 \pm 0.001$	$3100 \pm 300$	$1.00 \pm 0.03$	52	66	3.4	4.4		
7202395	11.81	$7350 \pm 80$	$8.0 \pm 0.5$	1		1	0.3	300	$-0.0624 \pm 0.0008$	$4900 \pm 300$	$2.25 \pm 0.02$	16	38	3.6	9.2		1

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
7205868	13.88	$7000 \pm 200$	$12 \pm 1$	1		1	1.3	1790	$-0.006 \pm 0.001$	$2920 \pm 50$	$0.106 \pm 0.008$	52	71	0.2	0.3		
7211991	12.24	$6800 \pm 200$	$15 \pm 1$	2		2	0.4	160	$-0.024 \pm 0.001$	$3100 \pm 200$	$0.93 \pm 0.01$	64	81	1.9	2.6		
				1		1	0.7	360	$-0.0278 \pm 0.0004$			48	78	2.9	4.9		
7215607	10.48	$6800 \pm 200$	$10.6 \pm 0.9$	2		2	0.2	130	$-0.0369 \pm 0.0005$	$4200 \pm 200$	$1.66 \pm 0.01$	28	51	2.1	3.9	1	
				1		1	0.5	240	$-0.0387 \pm 0.0004$			25	63	3.7	9.8		
7285845	12.29	$7100 \pm 200$	$7.7 \pm 0.6$	1		1	1.1	540	$-0.031 \pm 0.002$	$6600 \pm 300$	$0.626 \pm 0.006$	45	69	3.9	6.2		
7286276	13.25	$6900 \pm 200$	$1.7 \pm 0.4$	1		1	1.0	1600	$-0.0167 \pm 0.0001$	$4200 \pm 30$	$0.357 \pm 0.003$	28	51	0.7	1.5		
7287165	11.53	$7300 \pm 300$	$8.9 \pm 0.6$	1		1	0.8	240	$-0.0156 \pm 0.0003$	$3300 \pm 200$	$0.95 \pm 0.01$	58	104	3.8	7.0		
7344999	13.50	$7200 \pm 200$	$6.1 \pm 0.4$	1		1	0.5	480	$-0.0451 \pm 0.0004$	$4300 \pm 100$	$1.40 \pm 0.01$	23	41	2.8	5.3		
7365537	9.18	$6700 \pm 200$	$5.7 \pm 0.3$	1		1	0.3	320	$-0.0627 \pm 0.0006$	$4600 \pm 400$	$2.24 \pm 0.03$	20	30	4.4	6.8		
7380501	11.97	$6700 \pm 200$	$8.0 \pm 0.8$	1		1	1.0	520	$-0.0226 \pm 0.0008$	$4270 \pm 90$	$0.669 \pm 0.004$	47	85	2.7	5.5		
7385783	10.77	$6800 \pm 200$	$10.5 \pm 0.8$	1		1	0.4	210	$-0.0394 \pm 0.0005$	$4400 \pm 200$	$1.790 \pm 0.009$	22	68	3.5	11.9	1	
7386431	13.90	$6800 \pm 200$	$8.8 \pm 0.7$	1		1	0.5	780	$-0.0459 \pm 0.0005$	$4300 \pm 100$	$1.15 \pm 0.01$	19	35	1.8	3.6		
7421324	12.95	$6700 \pm 200$	$4.2 \pm 0.3$	2		2	0.3	230	$-0.0345 \pm 0.0009$	$3840 \pm 80$	$1.128 \pm 0.005$	30	50	1.4	2.4		
				1		1	0.6	300	$-0.0267 \pm 0.0004$			36	76	3.4	7.7		
7434470	12.02	$7200 \pm 200$	$5.1 \pm 0.3$	2		2	0.2	130	$-0.0424 \pm 0.0005$	$4300 \pm 100$	$1.77 \pm 0.01$	23	53	1.8	4.5		
				1		1	0.4	270	$-0.0441 \pm 0.0005$			21	55	3.3	9.3		
7436266	11.39	$6990 \pm 80$	$7.8 \pm 0.4$	1		1	0.6	220	$-0.0298 \pm 0.0004$	$4070 \pm 10$	$1.2897 \pm 0.0007$	31	90	3.5	10.4	1	
					-2	-1	0.9	370	$0.0487 \pm 0.0005$			9	67	6.8	24.7		
7448050	11.77	$7400 \pm 300$	$6.6 \pm 0.4$	1		1	0.8	1300	$-0.0276 \pm 0.0003$	$4410 \pm 30$	$0.578 \pm 0.003$	20	47	0.9	2.5	1	
7455752	13.78	$7300 \pm 300$	$6.9 \pm 0.5$	2		2	0.3	170	$-0.043 \pm 0.003$	$4100 \pm 100$	$1.13 \pm 0.01$	45	54	2.2	2.7		
				1		1	0.5	650	$-0.043 \pm 0.001$			21	44	1.9	4.5		
7456441	12.94	$7300 \pm 300$	$16 \pm 1$	1		1	0.5	1250	$-0.014 \pm 0.001$	$2530 \pm 30$	$0.46 \pm 0.01$	25	39	0.5	0.8		1
7461607	12.68	$7200 \pm 300$	$7.9 \pm 0.6$	1		1	0.5	920	$-0.0435 \pm 0.0002$	$3980 \pm 60$	$1.075 \pm 0.009$	18	32	1.4	2.8		1
7463623	13.39	$6600 \pm 200$	$12.9 \pm 0.9$	2		2	0.3	90	$-0.0297 \pm 0.0003$	$4400 \pm 100$	$1.397 \pm 0.005$	35	84	2.3	5.8		
				1		1	0.5	260	$-0.0349 \pm 0.0004$			29	69	3.7	9.4		
7467518	12.75	$7700 \pm 300$	$7.5 \pm 0.6$	1		1	0.4	840	$-0.0448 \pm 0.0006$	$3100 \pm 20$	$1.267 \pm 0.006$	12	37	0.8	3.1		1
7499407	13.59	$7300 \pm 200$	$7.8 \pm 0.6$	2		2	0.3	120	$-0.0300 \pm 0.0002$	$4300 \pm 200$	$1.256 \pm 0.009$	35	77	2.0	4.6		
				1		1	0.6	330	$-0.0326 \pm 0.0005$			36	55	4.1	6.4		
7511994	11.59	$6900 \pm 200$	$8.9 \pm 0.6$	1		1	0.7	290	$-0.0239 \pm 0.0001$	$3700 \pm 100$	$1.019 \pm 0.008$	44	84	3.5	7.0		
7513405	11.85	$6800 \pm 200$	$9.6 \pm 0.7$	1		1	1.3	1150	$-0.017 \pm 0.002$	$5780 \pm 70$	$0.419 \pm 0.003$	33	63	1.5	3.2		
7538181	11.92	$7400 \pm 300$	$7.3 \pm 0.5$	1		1	0.6	260	$-0.0335 \pm 0.0008$	$3840 \pm 20$	$1.1939 \pm 0.0009$	40	72	4.0	7.4		
					-2	-1	1.1	580	$0.0405 \pm 0.0009$			13	40	7.1	13.5		
7549852	12.40	$7100 \pm 200$	$21 \pm 2$	1		1	0.7	700	$-0.0362 \pm 0.0007$	$4010 \pm 70$	$0.841 \pm 0.006$	26	53	1.7	3.7		1
7551589	13.98	$7400 \pm 300$	$10 \pm 1$	1		1	0.6	180	$-0.0292 \pm 0.0003$	$3820 \pm 20$	$1.3182 \pm 0.0009$	42	90	4.6	10.2		
					-2	-1	0.9	490	$0.0460 \pm 0.0009$			14	45	7.3	16.2		
7583663	12.69	$7400 \pm 300$	$7.4 \pm 0.5$	1		1	0.6	280	$-0.0307 \pm 0.0005$	$4220 \pm 20$	$1.1608 \pm 0.0007$	37	70	4.0	7.7		
					-2	-1	1.0	180	$0.0385 \pm 0.0005$			38	69	13.8	24.0		
7596250	11.30	$6740 \pm 80$	$8.4 \pm 0.4$	1		1	0.6	350	$-0.0346 \pm 0.0005$	$4290 \pm 20$	$1.1876 \pm 0.0007$	27	66	2.9	7.5	1	
					-2	-1	1.0	590	$0.0502 \pm 0.0006$			16	37	7.9	13.7		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
7597150	12.30	$7300 \pm 300$	$11.1 \pm 0.9$	2		2	0.4	310	$-0.0264 \pm 0.0002$	$4000 \pm 40$	$0.775 \pm 0.003$	32	63	1.0	2.1		
				1		1	0.7	730	$-0.0290 \pm 0.0002$			24	62	1.4	4.1		
7597269	13.78	$7500 \pm 300$	$7.9 \pm 0.7$	1		1	0.9	420	$-0.0242 \pm 0.0002$	$4700 \pm 100$	$0.799 \pm 0.005$	42	77	3.3	6.3		
7617709	12.68	$7000 \pm 200$	$6.5 \pm 0.5$	1		1	0.6	350	$-0.0321 \pm 0.0005$	$4080 \pm 70$	$1.162 \pm 0.004$	27	74	2.6	7.8		
7620654	11.77	$7100 \pm 200$	$6.9 \pm 0.6$	1		1	0.4	270	$-0.0456 \pm 0.0005$	$4400 \pm 200$	$1.88 \pm 0.02$	24	47	4.2	8.7		
7621649	12.84	$7000 \pm 200$	$11 \pm 1$	1		1	0.8	510	$-0.0270 \pm 0.0002$	$3990 \pm 10$	$0.7745 \pm 0.0004$	30	80	1.9	5.5		
					-2	-1	1.6	530	$0.0307 \pm 0.0004$			28	62	8.0	13.9		
7621793	13.79	$6800 \pm 200$	$7.1 \pm 0.6$	1		1	0.5	510	$-0.0462 \pm 0.0002$	$3890 \pm 90$	$1.416 \pm 0.009$	20	41	2.2	4.9		1
7661054	9.88	$7000 \pm 200$	$5.3 \pm 0.8$	1		1	1.2	2780	$-0.0000 \pm 0.0005$	$4078 \pm 4$	$0.0391 \pm 0.0008$	29	43	0.0	0.1	1	
				1		-1	1.2	3040	$0.0013 \pm 0.0005$			28	45	0.0	0.1		
7672492	13.64	$7500 \pm 300$	$5.1 \pm 0.3$	1		1	1.5	1560	$-0.0112 \pm 0.0001$	$3860 \pm 20$	$0.245 \pm 0.001$	37	83	0.6	1.5		
7694191	10.78	$8100 \pm 300$	$150 \pm 10$	2		2	0.2	60	$-0.0370 \pm 0.0003$	$4400 \pm 200$	$2.08 \pm 0.01$	28	78	2.7	8.1	1	
				1		1	0.4	150	$-0.0404 \pm 0.0007$			24	68	4.6	14.0		
7695445	13.14	$6600 \pm 200$	$10.0 \pm 0.7$	2		2	0.7	490	$-0.0166 \pm 0.0004$	$4950 \pm 20$	$0.397 \pm 0.001$	45	78	0.9	1.7		
				1		1	1.2	1340	$-0.0206 \pm 0.0003$			29	63	1.1	2.6		
7697861	12.10	$7300 \pm 300$	$9.6 \pm 0.9$	1		1	1.1	3010	$-0.0079 \pm 0.0006$	$4506 \pm 4$	$0.0459 \pm 0.0007$	27	37	0.0	0.1		
				1		-1	1.3	3400	$-0.0018 \pm 0.0008$			28	40	0.0	0.1		
7698937	12.08	$6900 \pm 200$	$11.4 \pm 0.8$	2		2	0.3	150	$-0.0284 \pm 0.0002$	$4200 \pm 100$	$1.126 \pm 0.007$	36	74	1.7	3.8		
				1		1	0.6	510	$-0.0384 \pm 0.0007$			25	52	2.3	5.2		
7699478	13.32	$7000 \pm 200$	$7.7 \pm 0.5$	2		2	0.3	140	$-0.0200 \pm 0.0006$	$2500 \pm 200$	$1.06 \pm 0.03$	60	82	1.7	2.3		
				1		1	0.6	240	$-0.0273 \pm 0.0004$			62	90	3.5	5.2		
7701947	13.47	$7200 \pm 300$	$7.0 \pm 0.6$	1		1	0.8	840	$-0.0275 \pm 0.0002$	$4080 \pm 20$	$0.666 \pm 0.002$	28	60	1.4	3.4		
				1		0	1.2	1430	$-0.0157 \pm 0.0003$			36	60	1.3	1.8		
7746984	12.46	$5600 \pm 200$		2		2	0.3	120	$-0.033 \pm 0.001$	$3900 \pm 200$	$1.46 \pm 0.02$	39	61	2.4	3.9		
				1		1	0.5	280	$-0.035 \pm 0.001$			34	56	4.1	7.0		
7748238	9.52	$7300 \pm 100$	$7.2 \pm 0.4$	1		1	0.4	390	$-0.0528 \pm 0.0006$	$4400 \pm 100$	$1.75 \pm 0.01$	20	40	3.1	6.6	1	1
7757478	13.41	$7300 \pm 300$	$14 \pm 1$	1		1	0.9	590	$-0.0152 \pm 0.0008$	$3200 \pm 200$	$0.65 \pm 0.01$	54	74	2.3	3.3		
7761855	11.66	$7400 \pm 300$	$21 \pm 2$	1		1	0.6	2330	$-0.0283 \pm 0.0007$	$5070 \pm 60$	$0.462 \pm 0.008$	14	21	0.6	0.9		1
7770282	9.73	$7700 \pm 300$	$28 \pm 4$	1		1	1.1	910	$-0.0194 \pm 0.0002$	$4040 \pm 50$	$0.475 \pm 0.003$	41	73	1.5	2.9	1	1
7778114	11.97	$9000 \pm 300$	$57 \pm 6$	1		1	0.6	520	$-0.0355 \pm 0.0002$	$4280 \pm 20$	$1.015 \pm 0.002$	30	52	2.6	4.8		
				1		0	0.9	1170	$-0.0200 \pm 0.0002$			33	50	1.6	2.1		
7778826	13.61	$7200 \pm 300$	$7.2 \pm 0.7$	1		1	0.4	270	$-0.0510 \pm 0.0004$	$4020 \pm 30$	$2.060 \pm 0.002$	20	47	3.6	9.0		
					-2	-1	0.6	330	$0.0792 \pm 0.0007$			8	40	7.1	23.4		
7840642	13.84	$6800 \pm 200$	$10 \pm 1$	1		1	0.6	330	$-0.0297 \pm 0.0003$	$3700 \pm 90$	$1.158 \pm 0.006$	33	75	2.9	7.2		
7900126	11.47	$6700 \pm 200$	$6.7 \pm 0.5$	1		1	0.6	740	$-0.025 \pm 0.003$	$3360 \pm 60$	$0.752 \pm 0.008$	28	49	1.4	2.4		
7902286	15.93	$7000 \pm 300$		1		1	0.7	2860	$-0.003 \pm 0.002$	$4568 \pm 5$	$0.152 \pm 0.001$	17	22	0.2	0.2		1
				1		-1	0.8	3600	$0.0106 \pm 0.0009$			18	23	0.1	0.2		
7939065	12.14	$7500 \pm 300$	$5.9 \pm 0.4$	1		1	0.6	570	$-0.0388 \pm 0.0004$	$4250 \pm 50$	$1.114 \pm 0.005$	19	54	1.7	5.6		
7956547	11.93	$7100 \pm 200$	$10.8 \pm 0.8$	1		1	0.6	220	$-0.064 \pm 0.005$	$7000 \pm 2000$	$1.31 \pm 0.04$	39	51	7.8	10.1		
7968803	11.82	$7400 \pm 300$	$6.8 \pm 0.5$	2		2	0.2	50	$-0.0303 \pm 0.0003$	$4100 \pm 300$	$1.94 \pm 0.01$	47	70	4.1	6.3		
				1		1	0.4	110	$-0.0282 \pm 0.0006$			37	82	6.4	14.6		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
7977996	11.52	$7300 \pm 300$	$12 \pm 1$	1		1	0.4	540	$-0.066 \pm 0.003$	$5000 \pm 300$	$1.87 \pm 0.03$	16	25	3.1	5.1	1	1
7984890	12.84	$6700 \pm 200$	$13 \pm 1$	1		1	0.4	240	$-0.043 \pm 0.001$	$4700 \pm 200$	$1.76 \pm 0.01$	27	50	4.7	9.1		
8029546	11.04	$7350 \pm 80$	$21 \pm 1$	1		1	0.6	1840	$-0.041 \pm 0.002$	$5630 \pm 90$	$0.748 \pm 0.009$	14	22	1.0	1.8	1	
8053078	13.21	$6800 \pm 200$		1		1	0.9	1920	$-0.0129 \pm 0.0002$	$4050 \pm 10$	$0.297 \pm 0.001$	17	52	0.3	1.2		
8086490	12.09	$7700 \pm 300$	$10.1 \pm 0.7$	1		1	0.5	1110	$-0.0486 \pm 0.0004$	$4800 \pm 200$	$0.99 \pm 0.02$	20	25	1.8	2.3		1
8087018	12.01	$7360 \pm 80$	$9.8 \pm 0.6$	1		1	0.5	1600	$-0.0402 \pm 0.0008$	$4410 \pm 40$	$0.819 \pm 0.008$	13	24	0.8	1.6		1
8087269	12.12	$11700 \pm 400$		2		2	0.3	90	$-0.009 \pm 0.003$	$9000 \pm 1000$	$1.38 \pm 0.02$	41	53	5.3	7.1	1	
				1		1	0.6	130	$-0.0369 \pm 0.0007$			44	63	11.8	17.0		
8104065	13.61	$7300 \pm 300$	$8.0 \pm 0.7$	2		2	0.4	230	$-0.028 \pm 0.001$	$4500 \pm 200$	$0.761 \pm 0.007$	51	61	1.8	2.2		
				1		1	0.9	370	$-0.0233 \pm 0.0002$			42	93	3.0	7.0		
8110123	13.63	$7100 \pm 200$	$6.4 \pm 0.4$	1		1	0.9	370	$-0.0215 \pm 0.0002$	$4000 \pm 100$	$0.793 \pm 0.005$	48	89	3.1	6.2		
8122232	12.77	$7000 \pm 200$	$12 \pm 1$	1		1	0.4	1460	$-0.041 \pm 0.001$	$4230 \pm 60$	$0.91 \pm 0.01$	13	22	0.9	1.7		1
8123127	10.95	$7400 \pm 300$	$8.2 \pm 0.8$	1		1	0.5	990	$-0.0425 \pm 0.0005$	$4130 \pm 50$	$0.955 \pm 0.007$	16	37	1.1	3.0	1	
8123645	13.75	$7100 \pm 200$	$9.4 \pm 0.9$	1		1	0.4	680	$-0.0563 \pm 0.0006$	$4390 \pm 90$	$1.54 \pm 0.01$	15	30	2.0	4.3		1
8125339	12.87	$6900 \pm 200$	$6.7 \pm 0.6$	1		1	0.6	280	$-0.0271 \pm 0.0004$	$3620 \pm 90$	$1.131 \pm 0.006$	36	83	3.1	7.6		
8126271	13.93	$6600 \pm 200$	$12 \pm 2$	2		2	0.4	260	$-0.0241 \pm 0.0004$	$4220 \pm 50$	$0.737 \pm 0.003$	41	73	1.3	2.5		
				1		1	0.8	710	$-0.0305 \pm 0.0004$			29	60	1.9	4.1		
8127448	13.72	$7400 \pm 300$	$8.1 \pm 0.7$	1		1	0.5	900	$-0.045 \pm 0.002$	$4300 \pm 100$	$1.14 \pm 0.01$	19	28	1.8	2.9		1
8127778	11.96	$9000 \pm 300$	$70 \pm 40$	1		1	0.7	350	$-0.0302 \pm 0.0002$	$4700 \pm 100$	$1.029 \pm 0.005$	32	74	3.2	8.1		
8173017	12.77	$6800 \pm 200$	$25 \pm 3$	1		1	0.9	1120	$-0.001 \pm 0.002$	$4900 \pm 500$	$0.54 \pm 0.03$	33	44	1.6	2.2		1
8175399	12.47	$7300 \pm 300$	$38 \pm 6$	1		1	0.4	380	$-0.0453 \pm 0.0007$	$3900 \pm 300$	$1.60 \pm 0.02$	26	41	3.4	5.5		
8178778	12.19	$7000 \pm 200$	$5.5 \pm 0.4$	2		2	0.2	130	$-0.0342 \pm 0.0003$	$3900 \pm 100$	$1.497 \pm 0.007$	28	67	1.7	4.3		
				1		1	0.5	300	$-0.0372 \pm 0.0004$			27	60	3.2	7.7		
8180062	13.88	$6800 \pm 200$	$15 \pm 4$	2		2	0.4	200	$-0.0252 \pm 0.0006$	$4100 \pm 100$	$0.907 \pm 0.005$	40	71	1.5	2.9		
				1		1	0.8	360	$-0.0251 \pm 0.0003$			41	81	3.2	6.7		
8196181	11.78	$7400 \pm 300$	$6.5 \pm 0.7$	1		1	0.7	1490	$-0.0295 \pm 0.0004$	$4520 \pm 30$	$0.613 \pm 0.003$	17	37	0.8	2.0	1	
8197019	13.96	$7300 \pm 300$	$8 \pm 3$	1		1	0.4	270	$-0.0441 \pm 0.0006$	$3900 \pm 600$	$1.89 \pm 0.05$	28	42	4.4	6.8		
8197406	12.57	$7000 \pm 200$		1		1	0.8	350	$-0.0177 \pm 0.0005$	$2390 \pm 60$	$0.777 \pm 0.007$	60	109	2.3	4.4		
8197761	10.65	$7300 \pm 300$		1		-1	1.0	2780	$-0.005 \pm 0.002$	$3873 \pm 3$	$0.0007 \pm 0.0005$	28	37	0.0	0.0	1	
				1		1	1.1	2770	$0.0004 \pm 0.0009$			28	40	0.0	0.0		
				1		0	1.1	2780	$0.0019 \pm 0.0009$			28	42	0.0	0.0		
8198031	13.82	$7600 \pm 300$	$11 \pm 1$	1		1	0.4	170	$-0.0375 \pm 0.0005$	$4140 \pm 20$	$1.855 \pm 0.001$	25	74	4.3	12.9		
					-2	-1	0.6	370	$0.0767 \pm 0.0005$			12	38	8.2	20.6		
8231370	12.44	$7000 \pm 80$	$6.0 \pm 0.4$	2		2	0.2	110	$-0.0358 \pm 0.0003$	$4000 \pm 100$	$1.75 \pm 0.01$	29	61	2.1	4.7		
				1		1	0.4	230	$-0.0401 \pm 0.0003$			26	59	3.9	9.2		
8231525	13.02	$7600 \pm 300$	$7.5 \pm 0.6$	1		1	0.4	270	$-0.0464 \pm 0.0003$	$4800 \pm 100$	$1.772 \pm 0.007$	19	56	3.4	10.8		
8240902	13.51	$7300 \pm 300$	$8.5 \pm 0.6$	1		1	0.6	880	$-0.0374 \pm 0.0004$	$4440 \pm 50$	$0.896 \pm 0.004$	21	41	1.6	3.4		
8243158	12.14	$7100 \pm 200$	$8.5 \pm 0.6$	1		1	0.8	1160	$-0.0106 \pm 0.0003$	$2330 \pm 40$	$0.325 \pm 0.009$	38	61	0.5	0.8		
8259061	13.68	$7100 \pm 200$	$14 \pm 3$	1		1	0.5	810	$-0.0431 \pm 0.0002$	$4300 \pm 100$	$1.05 \pm 0.01$	23	32	2.1	3.0		1



Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
8260818	13.50	$7000 \pm 200$	$12 \pm 1$	2		2	0.5	180	$-0.028 \pm 0.004$	$5100 \pm 200$	$0.796 \pm 0.007$	51	75	2.2	3.3		
				1		1	0.9	450	$-0.033 \pm 0.002$			43	69	3.7	6.2		
8263970	13.78	$7600 \pm 300$	$7.8 \pm 0.7$	1		1	0.4	170	$-0.0393 \pm 0.0005$	$4180 \pm 20$	$1.946 \pm 0.001$	21	76	3.7	14.3		
					-2	-1	0.6	470	$0.0786 \pm 0.0001$			10	29	8.0	17.2		
8264304	13.99	$7300 \pm 300$	$8 \pm 2$	2		2	0.2	160	$-0.01 \pm 0.01$	$2300 \pm 600$	$1.4 \pm 0.1$	46	51	1.5	1.7		
				1		1	0.5	350	$-0.0422 \pm 0.0005$			44	52	2.9	3.5		
8264550	11.92	$8400 \pm 300$	$36 \pm 4$	1		1	0.5	420	$-0.0458 \pm 0.0006$	$4500 \pm 200$	$1.54 \pm 0.01$	20	41	3.1	6.4		1
8264667	12.49	$7400 \pm 300$	$40 \pm 20$	1		1	1.0	430	$-0.0203 \pm 0.0002$	$4200 \pm 100$	$0.684 \pm 0.005$	54	85	3.3	5.4		
8264708	13.46	$7700 \pm 300$	$13 \pm 4$	2		2	0.2	100	$-0.0366 \pm 0.0003$	$4240 \pm 40$	$1.636 \pm 0.001$	28	65	2.1	5.0		
					-3	-2	0.3	40	$0.0376 \pm 0.0007$			16	33	11.9	15.7		
				1		1	0.5	140	$-0.0262 \pm 0.0007$			42	72	6.5	11.1		
					-2	-1	0.7	110	$0.0479 \pm 0.0005$			32	62	16.7	30.1		
8264720	13.79	$6900 \pm 200$	$7 \pm 1$	1		1	0.5	410	$-0.0430 \pm 0.0006$	$4200 \pm 200$	$1.45 \pm 0.01$	23	47	2.9	6.3		
8265068	11.88	$7500 \pm 300$		1		1	0.7	630	$-0.030 \pm 0.003$	$5000 \pm 100$	$0.971 \pm 0.006$	25	45	2.4	4.6		1
8265126	13.79	$7600 \pm 300$	$10 \pm 1$	2		2	0.3	390	$-0.0345 \pm 0.0002$	$4200 \pm 40$	$0.891 \pm 0.004$	30	36	1.1	1.4		
				1		1	0.6	840	$-0.0368 \pm 0.0003$			17	49	1.2	3.9		
8293692	13.90	$7500 \pm 300$	$6.8 \pm 0.5$	2		2	0.4	90	$-0.0191 \pm 0.0002$	$2400 \pm 200$	$1.00 \pm 0.02$	84	129	2.1	3.4		
				1		1	0.7	190	$-0.020 \pm 0.001$			85	118	4.3	6.2		
8316105	13.76	$7300 \pm 300$	$8.6 \pm 0.9$	1		1	0.6	300	$-0.0354 \pm 0.0005$	$4240 \pm 20$	$1.3352 \pm 0.0008$	24	70	2.9	9.0		
					-2	-1	0.9	420	$0.0539 \pm 0.0004$			15	50	7.9	20.2		
8321903	12.45	$7000 \pm 200$	$9.9 \pm 0.8$	1		1	0.8	1770	$-0.0154 \pm 0.0002$	$3950 \pm 20$	$0.365 \pm 0.002$	18	46	0.4	1.3		
8324305	12.60	$6700 \pm 200$	$4.5 \pm 0.5$	2		2	0.3	240	$-0.0358 \pm 0.0004$	$3790 \pm 60$	$1.215 \pm 0.006$	22	51	1.1	2.6		
				1		1	0.5	460	$-0.0363 \pm 0.0004$			22	55	2.1	5.7		
8326356	12.95	$7300 \pm 300$	$10 \pm 1$	1		1	0.3	160	$-0.049 \pm 0.001$	$4500 \pm 300$	$2.38 \pm 0.02$	21	54	4.7	12.7		1
8328005	12.59	$7100 \pm 200$		1		1	0.6	420	$-0.0379 \pm 0.0006$	$4120 \pm 10$	$1.2125 \pm 0.0008$	22	59	2.3	6.7		
					-2	-1	1.1	720	$0.037 \pm 0.001$			15	29	7.5	11.0		
8329014	13.48	$6700 \pm 200$	$12 \pm 1$	1		1	0.6	750	$-0.0386 \pm 0.0004$	$4050 \pm 80$	$0.993 \pm 0.008$	20	46	1.5	3.9		1
8330056	13.81	$7500 \pm 300$	$17 \pm 2$	1		1	0.4	170	$-0.0393 \pm 0.0005$	$4100 \pm 20$	$1.913 \pm 0.001$	26	68	4.4	11.9	1	
					-2	-1	0.6	390	$0.0731 \pm 0.0005$			9	42	7.3	23.4		
8330222	13.79	$7100 \pm 200$	$6.7 \pm 0.7$	1		1	0.9	1680	$-0.0193 \pm 0.0001$	$4270 \pm 20$	$0.398 \pm 0.002$	23	45	0.7	1.5		
8330312	13.96	$7100 \pm 200$	$6.3 \pm 0.7$	2		2	0.3	210	$-0.0390 \pm 0.0005$	$4240 \pm 90$	$1.338 \pm 0.005$	21	54	1.2	3.4		
				1		1	0.6	180	$-0.0292 \pm 0.0002$			41	89	5.0	11.4		
8351778	13.13	$7500 \pm 300$	$5.5 \pm 0.3$	2		2	0.3	260	$-0.0361 \pm 0.0008$	$3760 \pm 20$	$0.9645 \pm 0.0009$	29	57	1.1	2.3		1
				1		1	0.7	320	$-0.0262 \pm 0.0002$			40	84	3.1	6.9		
					-2	-1	1.2	130	$0.026 \pm 0.002$			71	85	18.4	21.8		
8352439	12.66	$7700 \pm 300$	$8.5 \pm 0.7$	1		1	0.5	780	$-0.0407 \pm 0.0006$	$4100 \pm 100$	$1.02 \pm 0.01$	22	36	1.9	3.2		
8355130	10.33	$7300 \pm 200$	$6.9 \pm 0.4$	1		1	0.7	1270	$-0.0347 \pm 0.0008$	$4720 \pm 50$	$0.706 \pm 0.005$	18	37	1.1	2.5	1	
8364249	11.94	$7300 \pm 300$	$11.1 \pm 0.7$	1		1	0.5	200	$-0.0332 \pm 0.0002$	$4400 \pm 300$	$1.52 \pm 0.01$	36	68	5.3	10.3		
8375138	11.02	$6800 \pm 200$	$6.1 \pm 0.5$	1		1	0.5	200	$-0.0376 \pm 0.0004$	$4150 \pm 20$	$1.6421 \pm 0.0009$	29	65	4.3	9.9		
					-2	-1	0.7	400	$0.0659 \pm 0.0002$			8	42	7.0	20.6		

**Table 1.** continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
8382539	12.00	$7400 \pm 300$	$7.6 \pm 0.5$	1		1	0.6	980	$-0.046 \pm 0.003$	$5100 \pm 100$	$1.01 \pm 0.01$	20	29	2.1	3.2		
8389518	12.80	$6900 \pm 200$	$12 \pm 1$	2		2	0.2	50	$-0.0290 \pm 0.0002$	$4000 \pm 1000$	$1.87 \pm 0.05$	46	81	3.7	6.6		
8390631	13.78	$6900 \pm 200$	$10 \pm 1$	2		2	0.2	160	$-0.0373 \pm 0.0007$	$4200 \pm 100$	$1.48 \pm 0.01$	33	44	2.1	2.9		
				1		1	0.5	410	$-0.0444 \pm 0.0005$			25	43	3.2	5.7		
8411693	12.73	$7400 \pm 300$	$6.1 \pm 0.4$	2		2	0.2	110	$-0.0324 \pm 0.0009$	$3600 \pm 200$	$1.65 \pm 0.02$	43	49	2.8	3.2		
				1		1	0.4	340	$-0.0409 \pm 0.0007$			29	44	3.6	5.7		
8443132	12.35	$7100 \pm 200$	$8.0 \pm 0.7$	2		2	0.4	140	$-0.0258 \pm 0.0002$	$4400 \pm 300$	$1.07 \pm 0.01$	45	72	2.2	3.7		
				1		1	0.7	300	$-0.0270 \pm 0.0003$			40	70	4.0	7.2		
8458690A	12.71	$7900 \pm 300$	$25 \pm 4$	1		1	0.3	290	$-0.0813 \pm 0.0005$	$5000 \pm 500$	$3.01 \pm 0.05$	16	23	5.0	7.5		1
8458690B	12.71	$7900 \pm 300$	$25 \pm 4$	1		1	0.3	300	$-0.0806 \pm 0.0005$	$4900 \pm 500$	$2.99 \pm 0.05$	16	23	4.9	7.3		1
8459899	8.73	$9500 \pm 300$	$240 \pm 50$	1		1	1.0	1080	$-0.0197 \pm 0.0005$	$3640 \pm 60$	$0.469 \pm 0.005$	39	64	1.3	2.3	1	
8495755	11.26	$7300 \pm 300$	$8.5 \pm 0.6$	2		2	0.4	220	$-0.0291 \pm 0.0002$	$4700 \pm 100$	$0.958 \pm 0.004$	34	61	1.6	3.0	1	
				1		1	0.7	420	$-0.0302 \pm 0.0002$			29	73	2.7	7.3		
8496367	13.50	$7000 \pm 200$	$9.2 \pm 0.7$	1		1	1.4	1230	$-0.01270 \pm 0.00006$	$3800 \pm 40$	$0.282 \pm 0.002$	49	91	0.9	1.9		
8523871	12.36	$8500 \pm 300$	$600 \pm 100$	1		1	0.8	3010	$-0.065 \pm 0.003$	$12160 \pm 30$	$0.644 \pm 0.001$	9	17	1.3	2.7		
				1		0	1.2	4610	$-0.070 \pm 0.003$			11	19	1.1	1.7		
8525691	11.93	$7500 \pm 300$	$6.7 \pm 0.6$	1		1	0.4	560	$-0.0494 \pm 0.0006$	$4200 \pm 100$	$1.43 \pm 0.01$	17	39	2.0	5.1		
8542993	13.31	$7300 \pm 300$	$18 \pm 2$	1		1	1.2	450	$-0.0327 \pm 0.0007$	$12500 \pm 800$	$0.673 \pm 0.005$	34	64	6.2	12.5		
8559796	13.15	$7100 \pm 200$	$9.8 \pm 0.7$	2		2	0.6	300	$-0.0170 \pm 0.0002$	$6800 \pm 200$	$0.612 \pm 0.004$	33	80	1.4	3.8		
				1		1	1.2	610	$-0.036 \pm 0.002$			46	66	4.1	6.3		
8591404	13.55	$6600 \pm 200$	$9.4 \pm 0.9$	2		2	0.2	60	$-0.0376 \pm 0.0002$	$4700 \pm 200$	$2.07 \pm 0.01$	29	75	3.0	8.3		
				1		1	0.4	200	$-0.0489 \pm 0.0007$			25	49	5.2	10.6		
8605096	12.16	$6900 \pm 200$	$6.8 \pm 0.4$	1		1	0.5	440	$-0.0454 \pm 0.0004$	$4000 \pm 100$	$1.49 \pm 0.01$	22	41	2.7	5.4		
8630712	13.49	$7100 \pm 200$	$7.1 \pm 0.5$	1		1	0.6	290	$-0.0333 \pm 0.0002$	$4000 \pm 100$	$1.315 \pm 0.007$	29	69	3.2	8.2		
8645874	9.92	$6700 \pm 200$	$7 \pm 1$	1		1	0.6	2180	$-0.018 \pm 0.002$	$5040 \pm 30$	$0.540 \pm 0.003$	11	30	0.5	1.7		1
8651452	10.80	$7200 \pm 200$	$6.6 \pm 0.7$	1		1	0.4	330	$-0.058 \pm 0.002$	$4800 \pm 300$	$1.87 \pm 0.02$	19	40	3.5	7.6	1	
8655082	12.87	$6500 \pm 200$	$20 \pm 3$	2		2	0.4	110	$-0.0237 \pm 0.0001$	$4220 \pm 90$	$1.070 \pm 0.004$	45	93	2.2	4.7		
				1		1	0.7	340	$-0.0292 \pm 0.0004$			34	71	3.2	7.2		
8686975	12.59	$7500 \pm 300$	$8.1 \pm 0.6$	1		1	0.4	290	$-0.054 \pm 0.001$	$6000 \pm 2000$	$1.82 \pm 0.08$	25	36	5.5	8.2		
8712174	11.57	$6800 \pm 200$	$7 \pm 1$	1		1	1.1	800	$-0.0200 \pm 0.0003$	$3670 \pm 30$	$0.487 \pm 0.002$	40	86	1.4	3.3	1	
8714886	10.94	$19000 \pm 400$		1		1	1.1	1490	$-0.0290 \pm 0.0003$	$6190 \pm 50$	$0.487 \pm 0.003$	21	53	1.2	3.6		
8718678	12.73	$7200 \pm 300$	$100 \pm 20$	1		1	0.4	230	$-0.0465 \pm 0.0008$	$4600 \pm 300$	$2.00 \pm 0.02$	21	52	4.0	10.6		
8752359	12.65	$8100 \pm 300$	$8.0 \pm 0.6$	1		1	0.5	1310	$-0.043 \pm 0.001$	$4200 \pm 100$	$0.94 \pm 0.02$	16	23	1.2	1.8		1
8759258	12.41	$11400 \pm 400$		1		1	1.0	830	$-0.046 \pm 0.002$	$7700 \pm 300$	$0.706 \pm 0.007$	29	43	3.2	5.1		
8775173	12.65	$6600 \pm 200$	$4.9 \pm 0.6$	1		1	1.1	1470	$-0.0401 \pm 0.0005$	$7630 \pm 60$	$0.513 \pm 0.002$	20	45	1.6	4.0		
8782821	13.22	$6700 \pm 200$	$9 \pm 1$	1		1	0.7	1130	$-0.027 \pm 0.002$	$4000 \pm 100$	$0.69 \pm 0.02$	27	36	1.4	2.0		
8816310	13.27	$7300 \pm 300$	$5.5 \pm 0.4$	2		2	0.3	140	$-0.0227 \pm 0.0004$	$3400 \pm 200$	$1.25 \pm 0.01$	39	68	1.8	3.3		
				1		1	0.6	310	$-0.0307 \pm 0.0008$			37	64	3.4	6.1		
8816903	8.52	$7100 \pm 100$	$7.1 \pm 0.4$	1		1	0.8	330	$-0.0280 \pm 0.0006$	$7300 \pm 200$	$0.943 \pm 0.004$	35	67	5.2	10.4	1	
8836473	12.77	$6400 \pm 200$		1		1	0.6	520	$-0.0416 \pm 0.0003$	$4440 \pm 80$	$1.164 \pm 0.006$	24	48	2.5	5.4		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
8869302	14.07	$7500 \pm 300$	$7.9 \pm 0.6$	1		1	1.7	2630	$-0.0024 \pm 0.0008$	$3660 \pm 20$	$0.004 \pm 0.003$	47	68	0.0	0.0		
8871304	10.79	$7400 \pm 300$	$6.1 \pm 0.3$	2		2	0.3	190	$-0.019 \pm 0.001$	$3920 \pm 30$	$1.090 \pm 0.001$	35	55	1.6	2.5	1	
				1		1	0.7	290	$-0.0237 \pm 0.0004$			41	75	3.8	7.1		
					-2	-1	1.1	300	$0.119 \pm 0.004$			30	44	11.0	13.9		
8879964	11.35	$7300 \pm 200$	$7.2 \pm 0.4$	1		1	0.5	430	$-0.0434 \pm 0.0003$	$4800 \pm 100$	$1.343 \pm 0.008$	23	44	3.2	6.3	1	
8973529	12.99	$6900 \pm 200$	$5.9 \pm 0.5$	2		2	0.3	140	$-0.0308 \pm 0.0003$	$4000 \pm 20$	$1.204 \pm 0.001$	22	90	1.1	4.8		
				1		1	0.6	320	$-0.0325 \pm 0.0004$			22	83	2.2	9.0		
					-2	-1	0.9	220	$0.066 \pm 0.002$			38	59	13.2	20.0		
8975515	9.52	$7400 \pm 300$	$27 \pm 2$	1		1	0.4	170	$-0.0388 \pm 0.0008$	$4600 \pm 200$	$1.854 \pm 0.009$	26	67	4.7	12.8	1	1
8978113	11.96	$10000 \pm 300$		1		1	1.1	1450	$-0.054 \pm 0.001$	$11420 \pm 80$	$0.605 \pm 0.001$	16	37	2.2	5.8		
9016344	12.50	$7200 \pm 300$	$11 \pm 1$	1		1	0.4	120	$-0.0472 \pm 0.0003$	$4400 \pm 300$	$2.35 \pm 0.02$	25	68	5.6	15.0		
9028134	12.77	$6600 \pm 200$	$10.6 \pm 0.9$	1		1	0.5	2260	$0.002 \pm 0.002$	$3448 \pm 4$	$0.168 \pm 0.003$	16	21	0.1	0.2		
				1		0	0.5	2430	$-0.001 \pm 0.003$			17	23	0.1	0.2		
				1		-1	0.6	2670	$-0.002 \pm 0.003$			16	27	0.1	0.2		
9092496	14.84	$7000 \pm 200$	$12 \pm 2$	2		2	0.3	100	$-0.0389 \pm 0.0006$	$4200 \pm 400$	$1.16 \pm 0.01$	56	79	3.0	4.4		
				1		1	0.7	200	$-0.0250 \pm 0.0006$			51	74	5.5	8.7		
9182854	13.23	$6800 \pm 200$	$9.6 \pm 0.8$	1		1	0.8	340	$-0.0166 \pm 0.0004$	$2670 \pm 80$	$0.825 \pm 0.007$	57	102	2.6	5.0		
9210943	11.80	$6900 \pm 200$	$9.6 \pm 0.7$	1		1	0.4	300	$-0.043 \pm 0.001$	$4310 \pm 20$	$1.703 \pm 0.001$	24	45	3.9	7.4		
					-2	-1	0.7	410	$0.0693 \pm 0.0005$			9	40	7.3	20.8		
9238121	12.19	$6900 \pm 200$	$8.8 \pm 0.8$	2		2	0.4	220	$-0.0291 \pm 0.0002$	$4070 \pm 60$	$0.842 \pm 0.004$	42	66	1.5	2.5		
				1		1	0.7	680	$-0.0313 \pm 0.0004$			27	53	1.9	4.0		
9242383	11.93	$6800 \pm 200$		1		1	0.3	210	$-0.065 \pm 0.001$	$6200 \pm 400$	$2.49 \pm 0.02$	19	35	6.4	12.2		1
9244992	13.99	$6900 \pm 300$	$13 \pm 1$	1		1	0.8	2260	$-0.0022 \pm 0.0002$	$3232 \pm 2$	$0.0148 \pm 0.0009$	22	43	0.0	0.0		1
				1		0	0.8	2290	$-0.0022 \pm 0.0002$			23	41	0.0	0.0		
				1		-1	0.9	2330	$0.0002 \pm 0.0002$			22	52	0.0	0.0		
9292463	12.82	$6800 \pm 200$	$7 \pm 2$	1		1	0.9	780	$-0.0274 \pm 0.0006$	$4610 \pm 60$	$0.638 \pm 0.003$	32	64	1.9	4.1		1
9344493	13.01	$7400 \pm 300$	$13 \pm 1$	4		4	0.2	40	$-0.0184 \pm 0.0001$	$4700 \pm 400$	$0.95 \pm 0.01$	68	105	1.7	2.6		
				3		3	0.3	70	$-0.0204 \pm 0.0001$			58	95	1.9	3.1		
				2		2	0.4	110	$-0.02191 \pm 0.00006$			51	99	2.5	4.9		
9347494	12.97	$7400 \pm 300$	$26 \pm 3$	2		2	0.2	130	$-0.0350 \pm 0.0004$	$3750 \pm 90$	$1.574 \pm 0.007$	25	65	1.6	4.4		1
				1		1	0.5	210	$-0.0347 \pm 0.0003$			27	74	3.5	10.0		
9348946	12.76	$6700 \pm 200$	$7.5 \pm 0.6$	2		2	0.5	310	$-0.0228 \pm 0.0001$	$4370 \pm 30$	$0.610 \pm 0.002$	30	89	0.8	2.6		
				1		1	1.0	710	$-0.0243 \pm 0.0001$			28	79	1.5	4.7		
9349426	12.42	$6800 \pm 400$	$12 \pm 1$	2		2	0.6	300	$-0.01857 \pm 0.00009$	$4300 \pm 40$	$0.507 \pm 0.002$	47	98	1.0	2.3		
				1		1	1.1	830	$-0.0205 \pm 0.0002$			40	74	1.7	3.4		
9366994	13.26	$6600 \pm 200$	$11 \pm 1$	1		1	0.4	2120	$-0.062 \pm 0.004$	$5400 \pm 100$	$0.93 \pm 0.02$	8	14	0.7	1.4		1
9396399	12.64	$7700 \pm 300$	$10.2 \pm 0.8$	1		1	0.3	500	$-0.0625 \pm 0.0003$	$4300 \pm 200$	$1.90 \pm 0.02$	17	29	2.7	5.0		1
9409239	12.35	$7400 \pm 300$	$7.9 \pm 0.6$	2		2	0.3	130	$-0.0322 \pm 0.0007$	$4120 \pm 10$	$1.3598 \pm 0.0006$	33	65	2.0	4.1		
				1		1	0.6	220	$-0.0319 \pm 0.0002$			35	75	4.3	9.5		
					-2	-1	0.9	340	$0.0526 \pm 0.0003$			12	62	7.2	24.7		

Table 1. continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
9413296	13.32	$7500 \pm 300$	$6.4 \pm 0.5$	2		2	0.3	120	$-0.0329 \pm 0.0002$	$3990 \pm 80$	$1.444 \pm 0.006$	34	65	2.1	4.2		
				1		1	0.5	340	$-0.0392 \pm 0.0004$			22	58	2.7	7.5		
9419182	9.20	$6800 \pm 200$	$7.8 \pm 0.5$	2		2	0.3	180	$-0.0385 \pm 0.0007$	$4190 \pm 10$	$1.1510 \pm 0.0006$	27	62	1.4	3.3	1	
				1		1	0.7	250	$-0.0282 \pm 0.0003$			37	82	3.9	8.9		
					-2	-1	1.1	470	$0.0434 \pm 0.0006$			15	61	7.0	20.9		
9425193	10.11	$6800 \pm 200$	$10 \pm 2$	1		1	0.7	550	$-0.0402 \pm 0.0008$	$5500 \pm 100$	$1.019 \pm 0.005$	25	47	3.1	6.1		
9480469	12.77	$6900 \pm 200$	$7.2 \pm 0.5$	1		1	0.5	160	$-0.032 \pm 0.001$	$4330 \pm 20$	$1.554 \pm 0.001$	40	72	6.1	11.2		
					-2	-1	0.8	400	$0.0647 \pm 0.0002$			11	44	7.7	21.1		
9490067	10.62	$7100 \pm 200$	$6.3 \pm 0.7$	2		2	0.3	120	$-0.0339 \pm 0.0003$	$4480 \pm 80$	$1.489 \pm 0.005$	22	75	1.6	5.6	1	
				1		1	0.5	260	$-0.0362 \pm 0.0003$			22	69	3.2	10.2		
9533489	12.96	$7200 \pm 300$		2		2	0.3	590	$-0.0419 \pm 0.0006$	$4300 \pm 300$	$0.85 \pm 0.05$	16	28	0.6	1.0	1	1
9552574	13.04	$6700 \pm 200$	$33 \pm 4$	1		1	0.4	340	$-0.052 \pm 0.001$	$4300 \pm 500$	$1.84 \pm 0.04$	23	39	3.7	6.7		
9573582	12.45	$7400 \pm 300$	$6.5 \pm 0.4$	2		2	0.4	210	$-0.0291 \pm 0.0009$	$3880 \pm 10$	$0.9495 \pm 0.0005$	33	68	1.3	2.8		
				1		1	0.8	230	$-0.0201 \pm 0.0006$			57	98	4.6	8.2		
					-2	-1	1.3	560	$0.0344 \pm 0.0007$			15	61	6.7	16.1		
9579818	12.77	$8800 \pm 300$	$12 \pm 1$	1		1	0.2	320	$-0.086 \pm 0.001$	$4800 \pm 100$	$3.08 \pm 0.02$	10	27	3.2	9.0		1
9594007	13.04	$6800 \pm 200$		2		2	0.2	130	$-0.0428 \pm 0.0005$	$3980 \pm 20$	$1.671 \pm 0.001$	27	53	1.9	3.9		1
				1		1	0.5	200	$-0.0366 \pm 0.0008$			22	80	3.2	12.2		
					-2	-1	0.7	160	$0.0550 \pm 0.0007$			25	61	12.4	28.6		
9594100	13.01	$6700 \pm 200$	$6.8 \pm 0.7$	2		2	0.3	240	$-0.0370 \pm 0.0005$	$4110 \pm 20$	$1.2159 \pm 0.0009$	23	47	1.2	2.6	1	
				1		1	0.6	260	$-0.0313 \pm 0.0003$			31	77	3.3	8.5		
					-2	-1	1.0	320	$0.03 \pm 0.01$			31	46	11.6	16.5		
9595743	12.08	$7100 \pm 200$	$6.4 \pm 0.4$	—	—	—	0.5	2010	$0.006 \pm 0.005$	$4140 \pm 20$	$0.881 \pm 0.003$	—	—	—	—		
				1		1	0.7	590	$-0.043 \pm 0.001$			36	48	2.8	3.8		
				1		0	0.9	1340	$-0.021 \pm 0.002$			29	45	1.4	1.8		
9598448	11.57	$7510 \pm 80$	$27 \pm 2$	1		1	0.4	1220	$-0.0522 \pm 0.0006$	$4270 \pm 60$	$1.08 \pm 0.01$	14	23	1.2	2.1		1
9651065	11.06	$7000 \pm 100$	$8.7 \pm 0.6$	1		1	0.4	730	$-0.0545 \pm 0.0003$	$3600 \pm 200$	$1.53 \pm 0.03$	18	26	1.9	2.9	1	1
9652302	12.86	$7300 \pm 300$	$16 \pm 1$	1		1	0.8	330	$-0.021 \pm 0.001$	$3710 \pm 20$	$0.9147 \pm 0.0006$	48	88	3.5	6.9		
					-2	-1	1.3	270	$0.061 \pm 0.003$			47	66	11.9	16.0		
9655151	13.23	$7300 \pm 300$	$6.1 \pm 0.5$	1		1	0.5	260	$-0.0362 \pm 0.0002$	$3820 \pm 10$	$1.5523 \pm 0.0008$	24	66	3.1	9.0	1	
					-2	-1	0.8	330	$0.0555 \pm 0.0003$			11	57	7.1	23.7		
9673483	13.90	$6500 \pm 200$	$9 \pm 1$	1		1	0.6	200	$-0.0301 \pm 0.0005$	$4500 \pm 200$	$1.227 \pm 0.009$	43	85	5.2	10.6		
9713610	13.09	$6800 \pm 200$	$5.8 \pm 0.4$	1		1	0.7	420	$-0.029 \pm 0.001$	$2900 \pm 100$	$0.95 \pm 0.01$	42	68	2.4	4.1		
9716107	13.07	$7700 \pm 300$	$6.8 \pm 0.5$	1		1	0.4	220	$-0.0418 \pm 0.0005$	$4000 \pm 20$	$1.802 \pm 0.001$	20	65	3.2	10.6	1	
					-2	-1	0.7	350	$0.0708 \pm 0.0008$			15	38	8.9	19.4		
9716350	12.49	$6800 \pm 200$	$11.8 \pm 0.9$	1		1	0.8	310	$-0.0227 \pm 0.0002$	$4080 \pm 60$	$0.863 \pm 0.003$	35	111	2.5	8.7	1	
9716358	13.25	$6700 \pm 200$	$5.5 \pm 0.4$	1		1	1.5	1090	$-0.01306 \pm 0.00006$	$3830 \pm 30$	$0.306 \pm 0.001$	44	106	0.9	2.6	1	
9716563	13.63	$7000 \pm 200$	$4.3 \pm 0.3$	2		2	0.4	210	$-0.0258 \pm 0.0002$	$3860 \pm 10$	$0.9081 \pm 0.0008$	29	83	1.0	3.2		
				1		1	0.7	570	$-0.0307 \pm 0.0004$			23	67	1.6	5.2		
					-2	-1	1.5	820	$0.0119 \pm 0.0008$			17	26	7.0	8.3		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
9730397	13.57	$7400 \pm 300$	$9.9 \pm 0.7$	1		1	0.4	320	$-0.0525 \pm 0.0006$	$4700 \pm 100$	$1.807 \pm 0.009$	15	53	2.5	9.9		1
9751996	10.96	$6800 \pm 200$	$11.1 \pm 0.6$	1		1	0.9	2910	$-0.0042 \pm 0.0002$	$4371 \pm 3$	$0.0703 \pm 0.0009$	20	31	0.0	0.1		
				1		0	1.0	3070	$0.001 \pm 0.001$			26	31	0.1	0.1		
				1		-1	1.0	3320	$0.0037 \pm 0.0005$			20	38	0.0	0.1		
9766218	13.61	$6800 \pm 200$	$7.2 \pm 0.5$	2		2	0.2	60	$-0.0324 \pm 0.0005$	$4000 \pm 1000$	$1.84 \pm 0.04$	42	71	3.8	6.5		
9776816	13.03	$7000 \pm 200$	$8.1 \pm 0.7$	2		2	0.2	290	$-0.049 \pm 0.002$	$4090 \pm 60$	$1.392 \pm 0.006$	22	34	1.2	2.0		1
				1		1	0.5	460	$-0.0435 \pm 0.0004$			18	50	2.1	6.3		
9777807	12.68	$7700 \pm 300$	$9.0 \pm 0.7$	1		1	0.8	820	$-0.0381 \pm 0.0006$	$5900 \pm 100$	$0.836 \pm 0.005$	24	40	2.5	4.4		
9847243	13.83	$7000 \pm 200$	$6.7 \pm 0.5$	2		2	0.3	360	$-0.0335 \pm 0.0002$	$4170 \pm 50$	$0.933 \pm 0.004$	19	50	0.7	2.1		
				1		1	0.6	690	$-0.0334 \pm 0.0004$			23	48	1.9	4.1		
9875566	11.65	$7200 \pm 300$	$30 \pm 3$	1		1	1.0	2740	$-0.008 \pm 0.002$	$5000 \pm 200$	$0.19 \pm 0.02$	25	29	0.4	0.5		
9896606	13.93	$7200 \pm 200$	$8.7 \pm 0.8$	2		2	0.3	110	$-0.0234 \pm 0.0001$	$4000 \pm 2000$	$1.14 \pm 0.07$	57	74	2.9	3.7		
9897089	12.90	$7440 \pm 80$	$9.7 \pm 0.7$	1		1	0.4	540	$-0.0521 \pm 0.0004$	$4200 \pm 100$	$1.55 \pm 0.01$	17	36	2.2	5.2		1
9936518	13.83	$7200 \pm 300$	$3.5 \pm 0.3$	1		1	0.4	650	$-0.028 \pm 0.002$	$2300 \pm 100$	$1.07 \pm 0.03$	31	42	1.5	2.1		1
9962653	10.11	$7300 \pm 200$	$6.1 \pm 0.3$	1		1	0.4	200	$-0.0410 \pm 0.0004$	$4150 \pm 20$	$1.763 \pm 0.001$	27	61	4.3	10.0	1	
					-2	-1	0.7	290	$0.0686 \pm 0.0002$			10	49	8.0	25.6		
10056297	13.40	$7400 \pm 300$	$26 \pm 3$	1		1	0.8	1210	$-0.0194 \pm 0.0001$	$3530 \pm 30$	$0.475 \pm 0.003$	29	53	0.9	1.7	1	1
10080943A	11.81	$7220 \pm 80$	$23 \pm 2$	1		1	1.0	2640	$-0.0028 \pm 0.0003$	$4090 \pm 3$	$0.0884 \pm 0.0007$	24	38	0.1	0.2		1
				1		-1	1.2	3210	$0.0019 \pm 0.0005$			30	43	0.1	0.2		
10080943B	11.81	$7220 \pm 80$	$23 \pm 2$	1		1	0.8	2570	$-0.0172 \pm 0.0008$	$4072 \pm 3$	$0.136 \pm 0.001$	21	28	0.1	0.2		1
				1		0	0.8	2820	$-0.008 \pm 0.001$			24	28	0.2	0.2		
				1		-1	1.0	3220	$0.0025 \pm 0.0007$			22	33	0.1	0.2		
10091792	13.23	$7200 \pm 300$	$11 \pm 2$	3		3	0.2	50	$-0.0365 \pm 0.0004$	$3900 \pm 100$	$1.230 \pm 0.008$	48	92	1.6	3.0		
				2		2	0.3	140	$-0.0282 \pm 0.0001$			39	67	2.0	3.6		
				1		1	0.6	250	$-0.0285 \pm 0.0002$			37	83	3.8	8.9		
10154094	12.23	$7400 \pm 80$	$11 \pm 1$	1		1	0.4	1040	$-0.0537 \pm 0.0003$	$4050 \pm 40$	$1.249 \pm 0.006$	12	27	1.1	2.8		1
10224094	11.89	$7300 \pm 300$		1		1	0.9	1570	$-0.0161 \pm 0.0006$	$3600 \pm 80$	$0.33 \pm 0.01$	31	53	0.6	1.2		
10224550	12.86	$6800 \pm 200$	$10.0 \pm 0.8$	2		2	0.2	150	$-0.0387 \pm 0.0005$	$4000 \pm 200$	$1.60 \pm 0.02$	27	53	1.8	3.7		
				1		1	0.5	330	$-0.0417 \pm 0.0005$			25	51	3.3	7.2		
10256787	12.25	$7300 \pm 200$		1		1	1.0	550	$-0.0195 \pm 0.0003$	$3220 \pm 90$	$0.569 \pm 0.006$	59	92	2.2	3.7		
10317467	9.24	$7400 \pm 300$	$23 \pm 2$	2		2	0.2	100	$-0.0333 \pm 0.0002$	$4300 \pm 200$	$1.68 \pm 0.01$	35	59	2.7	4.8		
				1		1	0.5	190	$-0.0362 \pm 0.0002$			33	64	5.1	10.3		
10347481	13.42	$7300 \pm 300$	$5.5 \pm 0.5$	2		2	0.3	210	$-0.0392 \pm 0.0004$	$4230 \pm 60$	$1.303 \pm 0.006$	17	61	1.0	3.8		
				1		1	0.5	520	$-0.0434 \pm 0.0005$			18	47	2.1	5.8		
10360294	12.74	$7300 \pm 300$	$4.1 \pm 0.5$	2		2	0.2	70	$-0.0374 \pm 0.0002$	$4400 \pm 200$	$2.04 \pm 0.01$	29	67	2.8	6.8		
				1		1	0.4	150	$-0.0385 \pm 0.0007$			24	69	4.6	13.9		
10405019	12.73	$7500 \pm 300$	$5.4 \pm 0.4$	1		1	0.6	580	$-0.037 \pm 0.002$	$4160 \pm 10$	$0.9709 \pm 0.0007$	26	50	2.2	4.4		
					-2	-1	1.3	660	$0.059 \pm 0.001$			26	31	9.0	10.1		
10416175	12.48	$7600 \pm 300$	$9.3 \pm 0.6$	2		2	0.3	100	$-0.0301 \pm 0.0004$	$5000 \pm 2000$	$1.23 \pm 0.05$	48	70	3.1	4.5		
10423501	13.31	$6800 \pm 200$	$5.0 \pm 0.5$	1		1	0.8	480	$-0.0271 \pm 0.0002$	$4240 \pm 20$	$0.8420 \pm 0.0006$	29	76	2.1	6.0		
					-2	-1	1.4	480	$0.0339 \pm 0.0009$			36	50	10.2	13.2		

**Table 1.** continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
10424977	13.29	$7000 \pm 200$	$5.3 \pm 0.4$	2		2	0.3	150	$-0.0279 \pm 0.0002$	$4150 \pm 90$	$1.081 \pm 0.005$	37	80	1.7	3.9		
				1		1	0.6	400	$-0.0319 \pm 0.0003$			33	62	3.0	6.1		
10467146	12.65	$7300 \pm 300$	$11 \pm 1$	1		1	0.5	250	$-0.035 \pm 0.002$	$4100 \pm 500$	$1.41 \pm 0.03$	43	59	5.3	7.7		
10468883	13.82	$7200 \pm 300$	$8.2 \pm 0.7$	1		0	0.5	2720	$0.011 \pm 0.001$	$3931 \pm 4$	$0.134 \pm 0.002$	14	19	0.1	0.1		1
				1		-1	0.6	3020	$0.024 \pm 0.001$			15	20	0.1	0.1		
				1		1	0.6	2610	$0.003 \pm 0.002$			17	22	0.1	0.1		
10470294	10.98	$7200 \pm 300$	$6.0 \pm 0.3$	1		1	0.4	330	$-0.0548 \pm 0.0008$	$4300 \pm 200$	$2.00 \pm 0.02$	17	40	3.1	7.7	1	
10481462	13.00	$6900 \pm 200$	$4.9 \pm 0.4$	1		1	0.4	210	$-0.052 \pm 0.001$	$4410 \pm 30$	$2.208 \pm 0.002$	17	52	3.7	11.6		
					-2	-1	0.5	440	$0.0973 \pm 0.0005$			10	25	8.7	17.6		
10483230	12.91	$7700 \pm 300$	$4.6 \pm 0.7$	2		2	0.3	270	$-0.0308 \pm 0.0002$	$4190 \pm 10$	$0.9126 \pm 0.0004$	24	65	0.9	2.7		
				1		1	0.8	390	$-0.0284 \pm 0.0003$			33	78	2.7	6.7		
					-2	-1	1.3	500	$0.0371 \pm 0.0003$			24	57	8.2	15.6		
10548240	11.60	$6820 \pm 80$	$4.7 \pm 0.8$	1		1	0.7	930	$-0.0340 \pm 0.0003$	$4390 \pm 40$	$0.785 \pm 0.004$	20	48	1.3	3.5		
10551271	13.06	$7400 \pm 300$	$6.7 \pm 0.4$	1		1	0.4	310	$-0.0581 \pm 0.0007$	$4700 \pm 200$	$2.12 \pm 0.01$	18	37	3.7	8.2		
10586837	12.43	$7300 \pm 200$	$9.2 \pm 0.6$	2		2	0.3	100	$-0.0298 \pm 0.0004$	$4600 \pm 300$	$1.19 \pm 0.01$	47	81	2.8	4.9	1	
				1		1	0.6	290	$-0.0317 \pm 0.0007$			40	59	4.7	7.2		
10645230	12.66	$6800 \pm 200$	$14 \pm 1$	1		1	0.8	330	$-0.0226 \pm 0.0006$	$2800 \pm 200$	$0.78 \pm 0.01$	64	98	3.0	4.8		
10647493	11.72	$7100 \pm 200$	$7.9 \pm 0.5$	1		1	0.5	830	$-0.0438 \pm 0.0002$	$3800 \pm 200$	$1.15 \pm 0.03$	22	28	1.9	2.5	1	1
10652134	11.92	$7100 \pm 200$	$6.4 \pm 0.4$	1		1	0.8	290	$-0.0238 \pm 0.0004$	$3930 \pm 20$	$0.9149 \pm 0.0007$	48	89	3.7	7.1		
					-2	-1	1.4	580	$0.047 \pm 0.001$			28	48	8.4	12.6		
10669515	12.82	$7300 \pm 300$	$5.4 \pm 0.4$	2		2	0.2	120	$-0.0335 \pm 0.0004$	$4100 \pm 100$	$1.596 \pm 0.007$	24	73	1.6	5.5		
				1		1	0.5	210	$-0.0361 \pm 0.0005$			31	69	4.3	10.0		
10669516	13.02	$7200 \pm 200$	$4.4 \pm 0.9$	1		1	1.2	1410	$-0.021 \pm 0.003$	$4140 \pm 50$	$0.294 \pm 0.004$	35	58	0.8	1.3		
10679607	13.65	$7900 \pm 300$	$5.9 \pm 0.4$	1		1	0.5	780	$-0.0492 \pm 0.0003$	$4570 \pm 50$	$1.181 \pm 0.005$	16	37	1.6	4.2		
10681464	11.47	$9000 \pm 300$	$38 \pm 4$	1		1	0.8	1720	$-0.055 \pm 0.002$	$6370 \pm 50$	$0.618 \pm 0.002$	16	34	1.2	3.0		
10744342	13.65	$7200 \pm 200$	$24 \pm 5$	–	–	–	0.5	170	$-0.009 \pm 0.003$	$3110 \pm 90$	$0.676 \pm 0.009$	–	–	–	–		
				1		1	0.8	770	$-0.0190 \pm 0.0007$			36	60	1.4	2.6		
10750903	13.22	$6840 \pm 80$	$10.0 \pm 0.6$	2		2	0.3	180	$-0.0272 \pm 0.0003$	$3800 \pm 100$	$1.052 \pm 0.006$	33	74	1.4	3.4		
				1		1	0.7	310	$-0.0262 \pm 0.0005$			42	74	3.6	6.8		
10803371	13.09	$7500 \pm 300$	$6.8 \pm 0.5$	3		3	0.2	90	$-0.018 \pm 0.002$	$3700 \pm 300$	$0.98 \pm 0.02$	63	72	1.6	1.8		
				2		2	0.4	120	$-0.0232 \pm 0.0002$			58	87	2.2	3.4		
				1		1	0.7	270	$-0.0241 \pm 0.0003$			55	82	4.2	6.4		
10818266	12.93	$7500 \pm 300$	$6.3 \pm 0.5$	1		1	0.4	250	$-0.0468 \pm 0.0005$	$4290 \pm 20$	$1.849 \pm 0.001$	18	56	3.1	10.0		
					-2	-1	0.7	460	$0.0772 \pm 0.0003$			10	33	7.9	18.7		
10859386	11.78	$7200 \pm 200$	$6.7 \pm 0.4$	1		1	0.4	290	$-0.045 \pm 0.001$	$4420 \pm 30$	$1.813 \pm 0.001$	23	44	4.1	8.2		
					-2	-1	0.6	120	$0.062 \pm 0.002$			34	51	19.1	28.7		
10875239	13.82	$7600 \pm 300$	$7.9 \pm 0.6$	1		1	0.5	180	$-0.0297 \pm 0.0004$	$3900 \pm 100$	$1.537 \pm 0.008$	30	87	3.8	11.8		
10923648	13.27	$7050 \pm 80$	$8.6 \pm 0.5$	1		1	0.5	320	$-0.0390 \pm 0.0004$	$4200 \pm 200$	$1.46 \pm 0.01$	28	51	3.7	7.0		
10961011	11.47	$7400 \pm 300$	$7.4 \pm 0.4$	1		1	1.0	730	$-0.0201 \pm 0.0007$	$3480 \pm 70$	$0.541 \pm 0.004$	47	81	1.8	3.4		

Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
10979359	13.14	$7300 \pm 200$	$9.4 \pm 0.6$	1		1	0.9	470	$-0.016 \pm 0.003$	$2400 \pm 300$	$0.63 \pm 0.04$	73	87	2.3	2.8		
11017637	10.10	$7300 \pm 200$	$5.9 \pm 0.3$	1		1	0.5	250	$-0.0419 \pm 0.0003$	$4240 \pm 20$	$1.6153 \pm 0.0008$	27	58	4.0	8.9	1	
					-2	-1	0.7	400	$0.0637 \pm 0.0003$			9	44	7.2	21.5		
11032600	12.99	$7700 \pm 300$	$7.3 \pm 0.6$	1		1	0.9	620	$-0.0253 \pm 0.0004$	$4230 \pm 70$	$0.685 \pm 0.004$	36	73	2.1	4.7		
11044372	12.45	$8300 \pm 300$	$26 \pm 2$	1		1	0.3	840	$-0.132 \pm 0.002$	$7390 \pm 80$	$2.268 \pm 0.007$	7	18	2.1	6.5		1
11080103	12.93	$7600 \pm 300$	$6.7 \pm 0.5$	1		1	1.0	740	$-0.020 \pm 0.002$	$2890 \pm 50$	$0.502 \pm 0.005$	48	80	1.3	2.3		
11081053	13.28	$7600 \pm 300$	$8.5 \pm 0.5$	2		2	0.2	60	$-0.0255 \pm 0.0002$	$4600 \pm 300$	$1.69 \pm 0.01$	45	75	3.8	6.5		
				1		1	0.5	130	$-0.0261 \pm 0.0005$			36	82	6.1	14.1		
11091071	12.95	$7200 \pm 200$	$7.1 \pm 0.5$	2		2	0.8	480	$-0.01257 \pm 0.00008$	$3900 \pm 30$	$0.316 \pm 0.002$	53	104	0.6	1.4		
				1		1	1.5	1130	$-0.0136 \pm 0.0002$			52	84	1.2	2.1		
11092638	12.66	$7700 \pm 300$	$6.3 \pm 0.4$	1		1	0.5	1250	$-0.0372 \pm 0.0002$	$4130 \pm 40$	$0.833 \pm 0.006$	16	31	1.0	2.1		
11099031	10.02	$6600 \pm 200$	$6.7 \pm 0.4$	1		1	0.7	320	$-0.0281 \pm 0.0005$	$4900 \pm 100$	$1.029 \pm 0.005$	28	85	2.9	9.6		
11137377	12.75	$7400 \pm 300$	$5.8 \pm 0.4$	1		1	0.7	300	$-0.0264 \pm 0.0003$	$4030 \pm 20$	$1.0261 \pm 0.0006$	39	82	3.4	7.7		
					-2	-1	1.1	290	$0.039 \pm 0.001$			37	56	11.7	16.6		
11145123	13.12	$8000 \pm 300$	$7.6 \pm 0.6$	1		-1	0.7	2100	$0.0031 \pm 0.0005$	$2912 \pm 3$	$0.009 \pm 0.002$	21	35	0.0	0.0		1
				1		1	0.7	2080	$0.0026 \pm 0.0005$			21	37	0.0	0.0		
				1		0	0.7	2100	$0.001 \pm 0.001$			24	35	0.0	0.0		
11147994	13.59	$7700 \pm 300$	$6.9 \pm 0.5$	2		2	0.4	390	$-0.0278 \pm 0.0004$	$4250 \pm 70$	$0.749 \pm 0.006$	31	49	1.0	1.6		
				1		1	0.7	950	$-0.0353 \pm 0.0005$			26	41	1.6	2.7		
11152649	13.03	$7400 \pm 300$	$16 \pm 1$	1		1	0.6	720	$-0.03357 \pm 0.00008$	$3900 \pm 100$	$0.91 \pm 0.01$	30	41	2.1	3.0		1
11183399	12.83	$7500 \pm 300$	$8.7 \pm 0.9$	1		1	0.4	170	$-0.0395 \pm 0.0006$	$4600 \pm 500$	$1.89 \pm 0.02$	29	60	5.5	11.8		
11201483	12.29	$7200 \pm 300$	$5.5 \pm 0.4$	1		1	0.4	170	$-0.0484 \pm 0.0005$	$5000 \pm 300$	$2.28 \pm 0.02$	22	50	5.3	12.7		
11242284	13.82	$6900 \pm 200$	$4.4 \pm 0.3$	1		1	1.4	860	$-0.0069 \pm 0.0003$	$2640 \pm 30$	$0.323 \pm 0.003$	70	112	1.1	2.0		
11256244	12.91	$6800 \pm 200$	$12.8 \pm 0.9$	1		1	0.8	300	$-0.0242 \pm 0.0002$	$3930 \pm 10$	$0.9622 \pm 0.0006$	45	84	3.7	7.1		
					-2	-1	1.3	640	$0.026 \pm 0.001$			22	44	7.7	12.3		
11294808	11.72	$7200 \pm 200$	$8.4 \pm 0.5$	2		2	0.4	170	$-0.0216 \pm 0.0002$	$4300 \pm 100$	$0.802 \pm 0.005$	45	95	1.6	3.7		
				1		1	0.9	390	$-0.016 \pm 0.001$			47	77	3.4	5.7		
11349012	11.46	$6700 \pm 200$	$8.2 \pm 0.5$	1		1	0.5	250	$-0.0362 \pm 0.0005$	$4190 \pm 30$	$1.479 \pm 0.001$	33	57	4.5	7.8		
					-2	-1	0.8	510	$0.0547 \pm 0.0003$			14	35	7.9	15.5		
11395936	12.12	$7600 \pm 300$	$6.8 \pm 0.4$	2		2	0.4	190	$-0.0257 \pm 0.0008$	$3800 \pm 100$	$0.944 \pm 0.007$	46	63	1.8	2.5		
				1		1	0.7	370	$-0.0272 \pm 0.0002$			41	74	3.1	5.9		
11409748	13.37	$6980 \pm 80$	$5.7 \pm 0.4$	2		2	0.4	130	$-0.048 \pm 0.001$	$4400 \pm 20$	$0.8812 \pm 0.0006$	62	79	2.6	3.4		
				1		1	0.8	520	$-0.0486 \pm 0.0005$			32	61	2.6	5.2		
					-2	-1	1.3	400	$0.078 \pm 0.004$			40	51	11.5	14.2		
11410261	13.35	$7300 \pm 300$	$8.5 \pm 0.6$	2		2	0.3	120	$-0.0272 \pm 0.0003$	$3930 \pm 20$	$1.2025 \pm 0.0007$	37	83	1.9	4.4		
				1		1	0.6	270	$-0.0285 \pm 0.0003$			33	80	3.3	8.4		
					-2	-1	0.9	150	$0.0361 \pm 0.0004$			44	76	15.0	25.4		
11456474	12.49	$6940 \pm 80$	$7.1 \pm 0.5$	2		2	0.3	160	$-0.0259 \pm 0.0002$	$4200 \pm 100$	$1.063 \pm 0.005$	36	74	1.6	3.6		
				1		1	0.7	250	$-0.0249 \pm 0.0002$			41	90	3.8	9.0		
11456933	11.48	$6960 \pm 80$	$8.1 \pm 0.5$	2		2	0.5	230	$-0.0214 \pm 0.0002$	$4200 \pm 70$	$0.680 \pm 0.003$	51	81	1.5	2.5		
				1		1	0.9	600	$-0.0237 \pm 0.0002$			41	68	2.4	4.2		

Table 1. continued.

KIC	$K_P$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
11462151	12.08	$7500 \pm 300$	$5.3 \pm 0.3$	1		1	0.4	320	$-0.0533 \pm 0.0008$	$4500 \pm 200$	$2.00 \pm 0.02$	21	37	3.9	7.3		
11466960	13.49	$6700 \pm 200$	$7.6 \pm 0.5$	1		1	0.6	210	$-0.0324 \pm 0.0004$	$4240 \pm 10$	$1.3874 \pm 0.0007$	29	82	3.7	10.9		
					-2	-1	0.9	400	$0.0560 \pm 0.0004$			12	52	7.3	21.7		
11519475	11.64	$6800 \pm 200$	$11.1 \pm 0.8$	1		1	0.5	190	$-0.0333 \pm 0.0003$	$4070 \pm 30$	$1.576 \pm 0.001$	29	75	4.1	10.8		
					-2	-1	0.7	200	$0.0550 \pm 0.0009$			30	49	13.8	22.2		
11520274	13.82	$6800 \pm 200$	$5.8 \pm 0.4$	2		2	0.4	140	$-0.0231 \pm 0.0002$	$3500 \pm 400$	$1.03 \pm 0.02$	51	80	2.0	3.2		
				1		1	0.7	260	$-0.0200 \pm 0.0009$			59	78	4.6	6.2		
11520310	12.60	$7000 \pm 200$	$6.0 \pm 0.4$	1		1	0.6	300	$-0.0311 \pm 0.0003$	$4490 \pm 90$	$1.170 \pm 0.004$	23	84	2.5	10.0		
11550154	11.50	$7500 \pm 300$	$6.0 \pm 0.3$	2		2	0.2	90	$-0.0409 \pm 0.0003$	$4140 \pm 20$	$2.017 \pm 0.001$	24	58	2.2	5.5		
				1		1	0.4	140	$-0.0367 \pm 0.0006$			23	79	4.3	14.9		
					-2	-1	0.6	320	$0.0794 \pm 0.0006$			10	39	8.1	23.2		
11564882	13.70	$7000 \pm 200$	$5.2 \pm 0.4$	1		1	0.6	1210	$-0.0374 \pm 0.0003$	$4400 \pm 200$	$0.83 \pm 0.02$	19	31	1.3	2.3		1
11571757	12.77	$6700 \pm 200$	$9.4 \pm 0.8$	2		2	0.4	220	$-0.048 \pm 0.002$	$6130 \pm 30$	$1.0291 \pm 0.0005$	28	51	1.9	3.6		
				1		1	0.8	240	$-0.0223 \pm 0.0005$			31	104	4.2	17.7		
					-2	-1	1.1	380	$0.064 \pm 0.002$			25	45	11.8	20.2		
11607017	10.90	$7200 \pm 200$	$15.0 \pm 0.8$	1		1	0.4	240	$-0.0533 \pm 0.0009$	$4900 \pm 100$	$2.119 \pm 0.009$	14	54	3.0	13.0		
11612274	10.58	$7700 \pm 300$	$8.0 \pm 0.5$	1		1	0.4	270	$-0.0470 \pm 0.0004$	$3900 \pm 300$	$1.89 \pm 0.02$	27	44	4.2	7.2		1
11619868	13.04	$7600 \pm 300$	$6.0 \pm 0.4$	2		2	0.3	250	$-0.0407 \pm 0.0004$	$4190 \pm 40$	$1.290 \pm 0.005$	24	44	1.3	2.5		
				1		1	0.4	810	$-0.0518 \pm 0.0003$			16	32	1.6	3.6		
11649699	10.14	$7200 \pm 200$	$5.5 \pm 0.3$	2		2	0.2	110	$-0.0403 \pm 0.0003$	$4090 \pm 20$	$1.729 \pm 0.002$	22	66	1.6	5.2		1
				1		1	0.4	250	$-0.0437 \pm 0.0004$			22	59	3.3	9.3		
					-2	-1	0.6	140	$0.055 \pm 0.002$			35	48	17.7	24.1		
11657371	12.66	$7300 \pm 300$	$6.3 \pm 0.4$	1		1	0.4	250	$-0.0436 \pm 0.0007$	$3900 \pm 40$	$1.848 \pm 0.002$	26	51	4.1	8.4		
					-2	-1	0.6	60	$0.077 \pm 0.002$			49	70	25.0	35.5		
11662513	12.57	$7500 \pm 300$	$18 \pm 2$	2		2	0.2	50	$-0.0316 \pm 0.0005$	$3800 \pm 300$	$1.92 \pm 0.01$	50	82	4.0	6.8		
				1		1	0.4	120	$-0.0292 \pm 0.0008$			39	76	6.3	12.7		
11721304	11.70	$7070 \pm 80$	$6.2 \pm 0.3$	1		1	1.1	970	$-0.0189 \pm 0.0001$	$4180 \pm 30$	$0.452 \pm 0.002$	36	77	1.3	3.1		
11754232	12.24	$6600 \pm 200$	$9.1 \pm 0.7$	1		1	0.8	2720	$0.000 \pm 0.002$	$4110 \pm 50$	$0.13 \pm 0.01$	20	30	0.1	0.2		
11772971	11.56	$7430 \pm 80$	$9.8 \pm 0.7$	1		1	0.4	1060	$-0.045 \pm 0.001$	$3500 \pm 200$	$1.00 \pm 0.03$	18	28	1.2	2.0		1
11775251	12.68	$7400 \pm 300$	$8.7 \pm 0.7$	1		1	0.6	190	$-0.0327 \pm 0.0002$	$4040 \pm 20$	$1.4115 \pm 0.0007$	31	88	3.9	11.0		
					-2	-1	0.8	350	$0.0572 \pm 0.0006$			14	48	8.2	19.6		
11809145	10.23	$7100 \pm 200$		1		1	0.7	490	$-0.035 \pm 0.001$	$3900 \pm 200$	$0.96 \pm 0.01$	35	53	2.8	4.4		1
11826272	10.21	$6800 \pm 200$	$7.6 \pm 0.7$	1		1	1.3	1220	$-0.0175 \pm 0.0002$	$4130 \pm 40$	$0.353 \pm 0.002$	41	73	1.1	2.1		
11907454	11.37	$7200 \pm 200$	$5.5 \pm 0.3$	1		1	0.6	240	$-0.0368 \pm 0.0006$	$4200 \pm 20$	$1.3387 \pm 0.0006$	30	74	3.7	9.1		
					-2	-1	0.9	270	$0.0543 \pm 0.0001$			10	66	7.8	26.0		
11917550	11.11	$6800 \pm 200$	$4.9 \pm 0.3$	1		1	0.7	470	$-0.0288 \pm 0.0002$	$4200 \pm 100$	$0.906 \pm 0.006$	32	68	2.5	5.7		
11920505	9.88	$6600 \pm 200$	$5.5 \pm 0.3$	1		1	0.8	720	$-0.0291 \pm 0.0002$	$4260 \pm 50$	$0.755 \pm 0.003$	27	61	1.7	4.2		
11922283	12.63	$7100 \pm 200$	$12 \pm 1$	2		2	0.4	100	$-0.0236 \pm 0.0001$	$4500 \pm 300$	$1.088 \pm 0.008$	52	87	2.9	4.9		
				1		1	0.7	210	$-0.0244 \pm 0.0003$			44	88	4.8	9.9		



Table 1. continued.

KIC	$K_p$	$T_{\text{eff}}$ K	$L$ $L_{\odot}$	$l$	$k$	$m$	$\langle P \rangle$ days	$\langle \Delta P \rangle$ Seconds	$\Sigma$ days/days	$\Pi_0$ Seconds	$f_{\text{rot}}$ $\text{d}^{-1}$	$n$		$s$		SC	H
												min	max	min	max		
11923562	13.32	$7050 \pm 80$	$7.5 \pm 0.5$	1		1	0.5	200	$-0.0260 \pm 0.0005$	$3790 \pm 20$	$1.645 \pm 0.001$	36	64	4.9	9.0		
					−2	−1	0.7	360	$0.0593 \pm 0.0004$			9	50	7.0	22.1		
12011851	10.73	$8000 \pm 300$	$43 \pm 3$	2		2	0.2	120	$-0.046 \pm 0.002$	$3800 \pm 400$	$1.50 \pm 0.03$	34	54	2.1	3.3	1	
				1		1	0.5	220	$-0.0320 \pm 0.0005$			39	62	4.9	8.0		
12058428	11.14	$7300 \pm 300$	$7.0 \pm 0.5$	1		1	0.6	330	$-0.0296 \pm 0.0002$	$4410 \pm 20$	$1.1895 \pm 0.0007$	34	60	3.8	7.1	1	
					−2	−1	1.1	710	$0.0412 \pm 0.0005$			12	32	7.2	12.6		
12066947	10.22	$6900 \pm 200$	$6.0 \pm 0.3$	1		1	0.4	140	$-0.0399 \pm 0.0008$	$4170 \pm 30$	$2.159 \pm 0.002$	25	64	5.1	13.1		
					−2	−1	0.5	270	$0.0804 \pm 0.0005$			11	44	8.4	28.0		
12102187	11.10	$7300 \pm 200$	$7.2 \pm 0.4$	1		1	1.1	450	$-0.0180 \pm 0.0002$	$4020 \pm 10$	$0.595 \pm 0.001$	60	97	3.0	5.2	1	
				1		0	1.4	1310	$-0.0175 \pm 0.0005$			47	70	1.4	1.8		
12104142	13.05	$7400 \pm 300$	$10.3 \pm 0.7$	1		1	0.8	410	$-0.0374 \pm 0.0008$	$5400 \pm 200$	$0.964 \pm 0.008$	36	60	4.0	7.0		
12111004	13.68	$7700 \pm 300$	$8.2 \pm 0.6$	1		1	0.5	620	$-0.0485 \pm 0.0008$	$4700 \pm 100$	$1.36 \pm 0.01$	18	36	2.2	4.9		
12117689	10.82	$7200 \pm 200$	$5.7 \pm 0.3$	1		1	0.3	280	$-0.0677 \pm 0.0004$	$4400 \pm 100$	$2.29 \pm 0.01$	16	43	3.2	9.3	1	
12170722	12.90	$7300 \pm 300$	$9.4 \pm 0.8$	2		2	0.2	100	$-0.0362 \pm 0.0003$	$4270 \pm 20$	$1.702 \pm 0.001$	22	77	1.8	6.4		
				1		1	0.5	150	$-0.0334 \pm 0.0002$			33	79	5.4	13.0		
					−2	−1	0.7	390	$0.0715 \pm 0.0005$			10	38	7.9	19.9		
12202137	12.05	$7300 \pm 300$	$14.3 \pm 0.9$	2		2	0.2	60	$-0.0325 \pm 0.0001$	$4000 \pm 200$	$1.96 \pm 0.01$	35	73	3.0	6.5		
				1		1	0.4	130	$-0.0328 \pm 0.0003$			35	71	6.0	12.6		
12303838	13.68	$7300 \pm 300$	$7.4 \pm 0.5$	1		1	0.6	250	$-0.0329 \pm 0.0004$	$4160 \pm 20$	$1.3301 \pm 0.0007$	33	70	4.0	8.8		
					−2	−1	0.8	190	$0.0483 \pm 0.0006$			27	68	11.2	26.3		
12365420	11.85	$7800 \pm 300$	$19 \pm 1$	1		1	0.7	400	$-0.0297 \pm 0.0004$	$3800 \pm 200$	$0.97 \pm 0.01$	42	66	3.2	5.2		1
12401800	11.15	$7200 \pm 200$	$5.5 \pm 0.3$	1		1	0.7	480	$-0.0294 \pm 0.0002$	$4220 \pm 20$	$0.889 \pm 0.002$	31	70	2.4	5.9	1	
				1		0	1.1	1170	$-0.024 \pm 0.002$			41	51	1.7	2.0		
12407395	11.92	$6800 \pm 200$	$10.9 \pm 0.8$	3		3	0.2	60	$-0.0224 \pm 0.0002$	$4800 \pm 300$	$1.109 \pm 0.008$	62	85	2.4	3.4		
				2		2	0.4	100	$-0.0236 \pm 0.0001$			54	82	3.1	4.9		
				1		1	0.7	210	$-0.0254 \pm 0.0003$			44	86	5.1	10.2		
12458189	11.45	$6700 \pm 200$	$4.2 \pm 0.2$	1		1	0.9	520	$-0.0389 \pm 0.0004$	$7700 \pm 100$	$0.859 \pm 0.002$	20	65	2.7	9.5		
12505154	13.55	$7000 \pm 200$	$7.2 \pm 0.4$	1		1	0.6	260	$-0.0326 \pm 0.0004$	$4060 \pm 20$	$1.2971 \pm 0.0009$	38	65	4.4	7.9		
					−2	−1	1.0	660	$0.0392 \pm 0.0008$			10	34	6.8	13.1		
12508604	12.40	$6500 \pm 200$	$9.7 \pm 0.6$	2		2	0.3	190	$-0.0383 \pm 0.0004$	$4240 \pm 90$	$1.290 \pm 0.005$	22	57	1.3	3.5		
				1		1	0.6	290	$-0.0328 \pm 0.0005$			26	74	3.0	9.2		
12520187	11.07	$6700 \pm 200$	$13 \pm 2$	1		1	0.4	310	$-0.0568 \pm 0.0006$	$4650 \pm 50$	$1.872 \pm 0.002$	18	44	3.4	8.4		
					−2	−1	0.6	90	$0.062 \pm 0.002$			29	51	20.2	31.4		
12643786	11.52	$7600 \pm 300$	$7.3 \pm 0.4$	1		1	0.7	1470	$-0.065 \pm 0.001$	$8200 \pm 100$	$0.877 \pm 0.005$	13	24	1.8	3.7		
12691831	13.95	$7400 \pm 300$	$9.2 \pm 0.9$	2		2	0.4	740	$-0.0314 \pm 0.0006$	$4700 \pm 100$	$0.61 \pm 0.01$	20	32	0.5	0.9		
12783511	13.20	$6800 \pm 200$	$6.3 \pm 0.5$	1		1	1.0	600	$-0.0226 \pm 0.0001$	$4030 \pm 60$	$0.637 \pm 0.003$	41	80	2.1	4.5		

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