

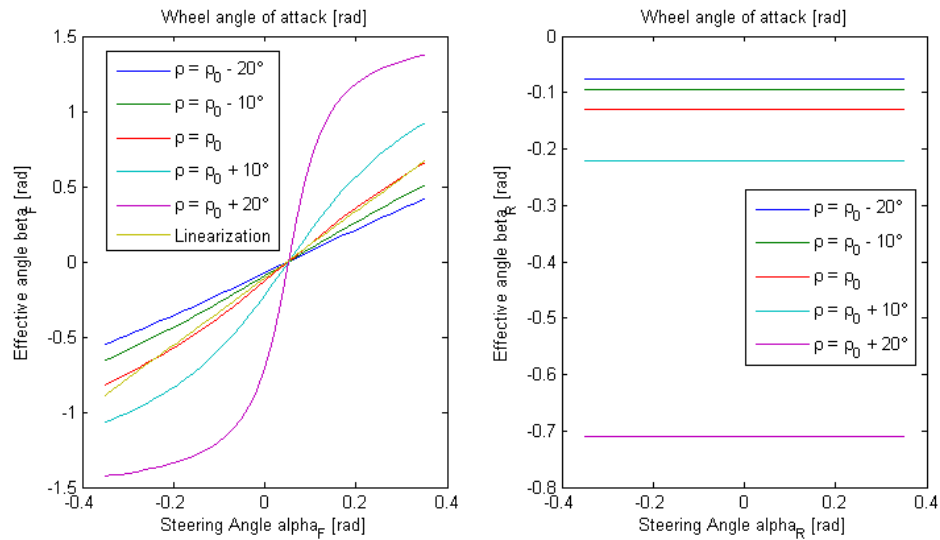
## ATIC Ex. 9

As a difference to the proposal, I do not consider velocity control anymore. The dynamics of the motor are too slow to be interesting. However, introducing a position state and implement line following would be interesting. This would be very similar to an inverted pendulum.

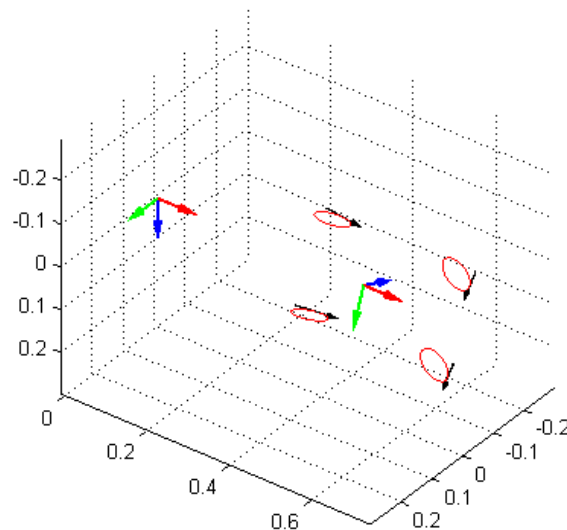
a)

i) Assumptions:

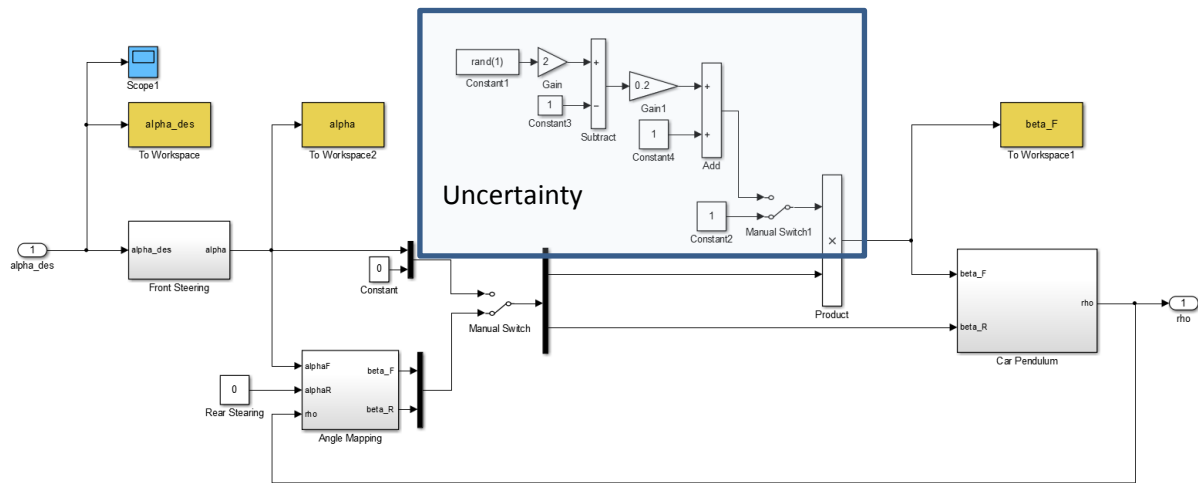
- Operating point was calculated and the system linearized around this point (see iv))
- Constant velocity. Dynamics of motor are slower.
- Coriolis force is neglected, since it small for small steering angles.
- Tires have infinite grip and follow exactly the steering direction.
- Linearization of angle mapping (highly optimistic). Linearization around the operating point.



This graph depicts the resulting angle as a function of roll angle and steering input. The graphic below illustrates the geometry.

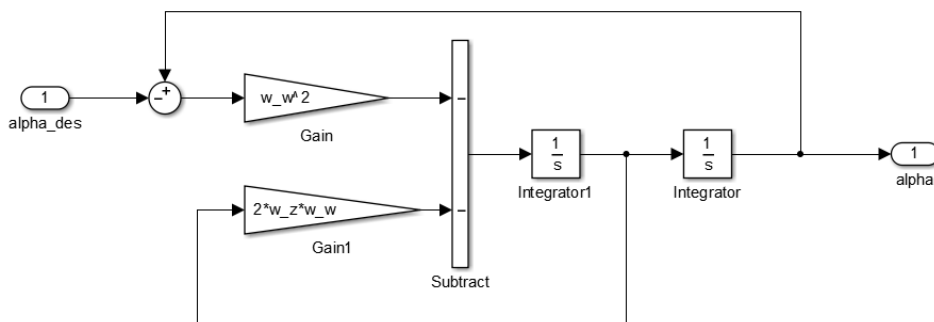


ii / iii)

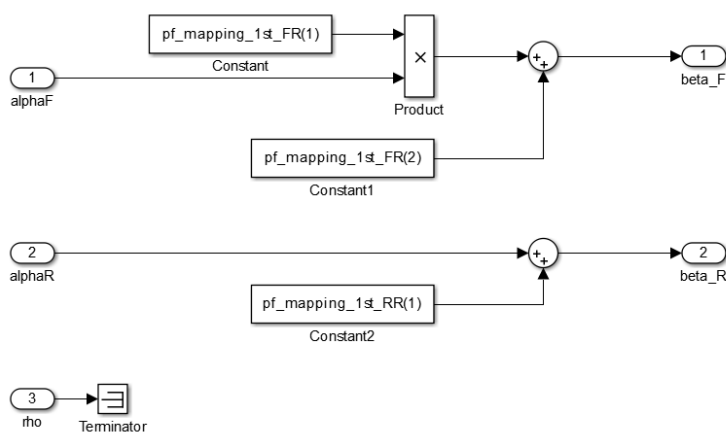


The perturbation is still included in the plant. I did not have the time yet to formulate it in the standard form since the modelling and integration took way more time than expected.

## Steering

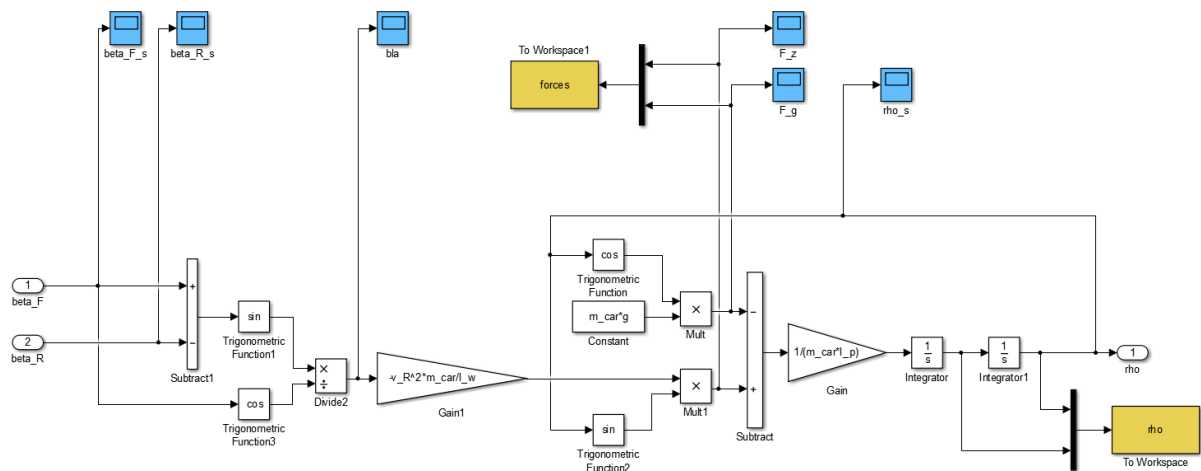


### 1<sup>st</sup> order mapping of steering angle vs. effective angle



I'm thinking of implementing a 3D polyfit which also considers rho

## Car / Pendulum



iv)

### States

Name	Description	Unit	Initial condition / Operating point
Phi	Angle of the pendulum	rad	Pi/2
Phi_dot	Rate of above described	rad/s	0
Alpha	Angle of the steering mechanism (not equal to the effective angle on the ground)	rad	0
Alpha_dot	Rate of above described	rad/s	0

### Inputs

Name	Description	Unit	
Alpha_des	Desired steering angle	rad	

### Outputs

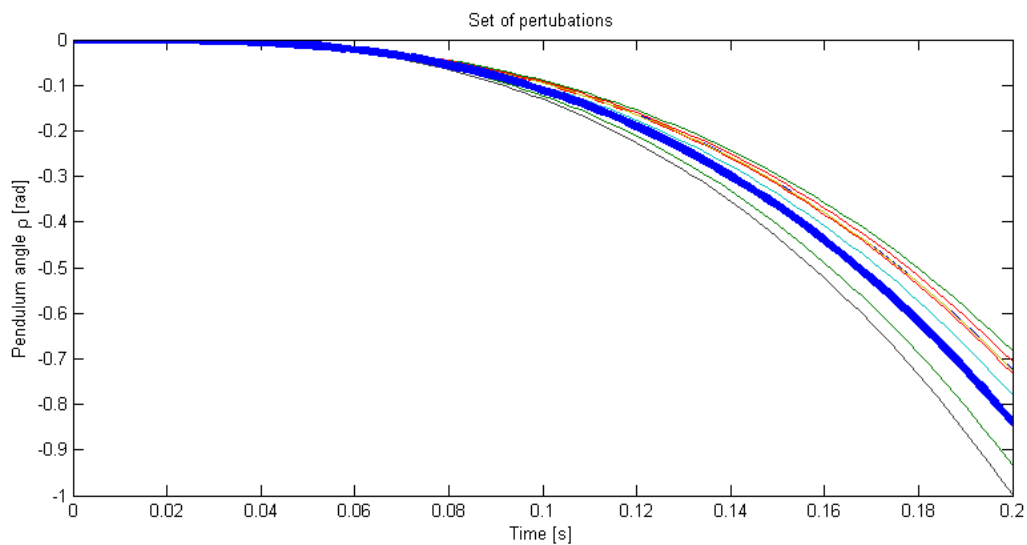
Name	Description	Unit	
rho	Balancing angle of the car (inverted pendulum)	rad	

v)

#### Sources of uncertainty:

- Effective steering angle  
Why: No tire model for slip, nonlinear  
Could be up to  $\pm 100\%$
- Pendulum angle  $\rho$   
Why: Noise, no accurate estimation  
 $\pm 1$  degree (should be conservative)
- Vehicle velocity  
Why: Has an impact on centrifugal force (to the power of 2).  
 $\pm 10\%$

b & c)



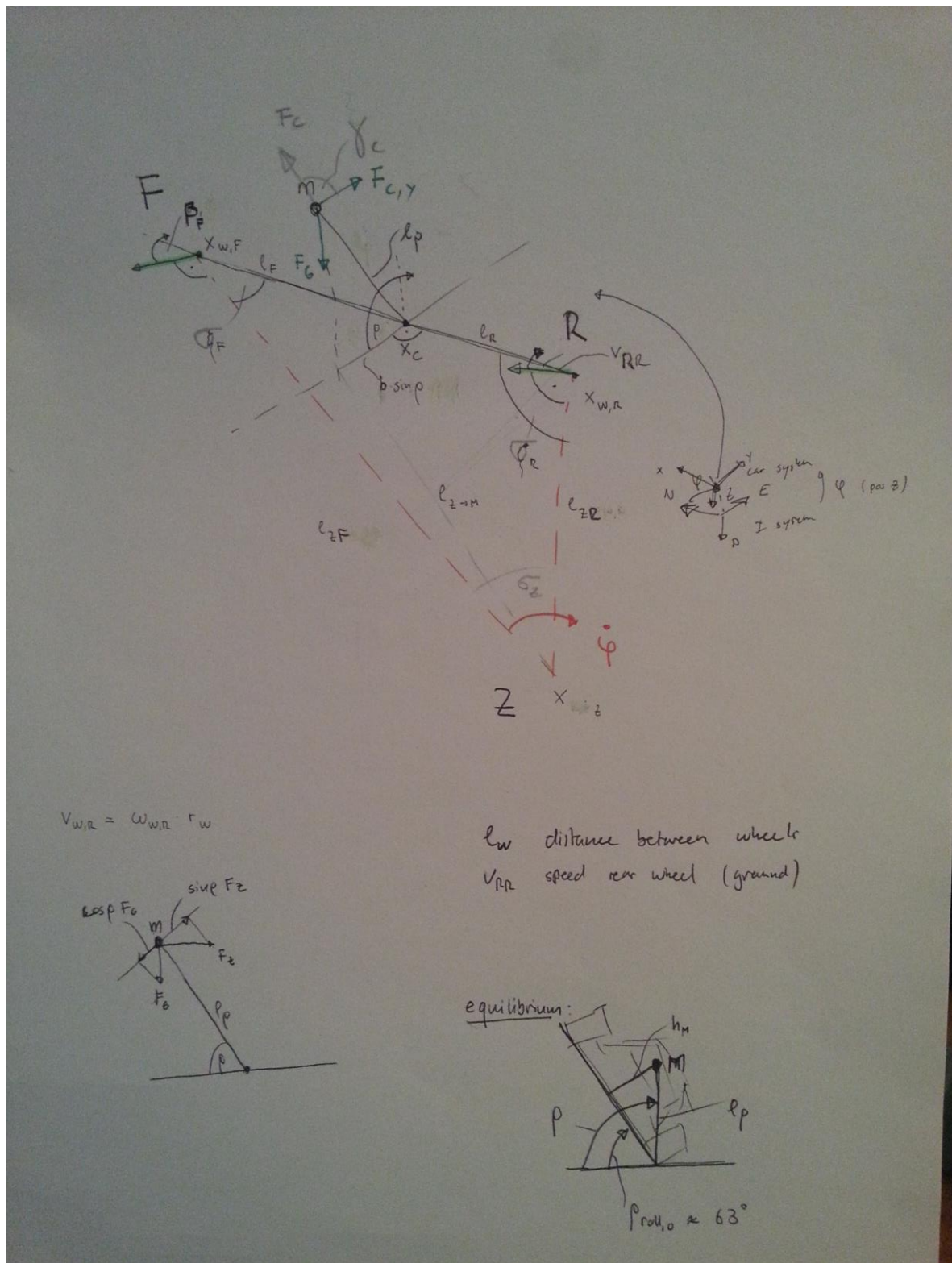
This plot shows step inputs on the system. The blue line is the nominal plant whereas the other lines are perturbed systems. Since the system is open-loop unstable, just 0.2 seconds are shown.

The car is expected to drive on the right wheels. A positive input to the steering ( $\alpha$ ) is equivalent to turning the car to the right side. This leads to a centrifugal force which pushes the car to the ground and hence decreases the pendulum angle  $\rho$ .

The uncertainty is chosen to be  $\pm 20\%$  on the effective steering angle of the front wheel. This is motivated through the delay of the steering actuation as well as unmodelled influence of the tires.

The system response makes sense so far.

Equations and drawings:



$$\frac{d\dot{\rho}}{dt} = \ddot{\rho}$$

$$\frac{d\dot{\rho}}{dt} = \frac{1}{m_{car} l_p} \left( \overset{\substack{\text{centrifugal} \\ \text{force}}}{\sin \rho F_{c,y}} - \overset{\substack{\text{gravitation}}}{\cos \rho F_G} \right)$$

$$F_G = m \cdot g$$

$$F_{c,y} = \cos \gamma_c m \dot{\psi}^2 l_{zM}$$

$$\text{with } \dot{\psi} = \frac{v_{Rn}}{l_{zn}}$$

speed at rear wheel  
(const.)

$$\approx m v_{Rn}^2 \frac{1}{l_{zn}} = m \frac{v_{Rn}^2}{l_w} \frac{\sin(\beta_F - \beta_n)}{\cos(\beta_F)}$$

$$\frac{d\dot{\alpha}}{dt} = \ddot{\alpha}$$

$$\frac{d\dot{\alpha}}{dt} = -\omega^2 (\alpha - \alpha_{des}) - 2\zeta\omega\ddot{\alpha}$$